

ANALYSIS AND DESIGN OF SUPERSONIC WING-BODY COMBINATIONS,
INCLUDING FLOW PROPERTIES IN THE NEAR FIELD

PART II—DIGITAL COMPUTER PROGRAM DESCRIPTION

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1. INTRODUCTION

This part of the document describes the digital computer program developed to analyze and design wing-body combinations at supersonic speeds. The program is an extension of an earlier program that is presented in references 1 and 2. The theoretical considerations underlying the method used in the program are discussed in reference 3.

The complete program consists of five sections: Geometry Definition, Geometry Transformation, Geometry Paneling, Aerodynamics, and Flow Visualization. The first three sections present, in a form acceptable to the Aerodynamics section, a geometric description of the configuration under study. A wing-alone, body-alone, or wing-body combination configuration may be defined. The Geometry sections redefine the body as an equivalent body of circular cross section. The wing and that part of the body in the region aft of the wing leading-edge intersection are subdivided into a large number of panels. The wing may be defined to have thickness or may consist of a camber surface only. The Aerodynamics section then solves the problem by first computing the velocity components induced by the various singularities that represent the configuration. The body thickness and camber effects are represented by line sources and doublets along the body axis, and wing thickness effects are represented by a distribution of sources located in the wing reference plane. The effects of camber and incidence of the wing and the effects of any residual interferences are simulated by a surface distribution of vortices on the wing and body. When the velocity components are computed, the program determines the strengths of the singularities required to satisfy the given boundary conditions. In addition to solving the problem of optimizing wing camber shape, the program will also solve the direct analysis problem of calculating pressures, forces, and moments on a given configuration, and the indirect design problem of determining the wing shape for a given lift distribution. The program selects the boundary conditions appropriate to the particular optimization, direct or indirect problem being considered, and solves the problem. The last section of the program, Flow Visualization, computes velocities at selected field points and integrates streamlines about the configuration.

This part of the document is a guide for program maintenance. An outline of the program structure is followed by a detailed description of each section of the program. The section on program usage contains the input format, timing and output estimates, and the required machine components. Input and output

formats of a sample case are also included. The section on program records contains flow charts, overlay diagrams, and descriptions of each subroutine. A program listing and other appendixes complete this part of the document.

2. DESCRIPTION

2.1 Geometry Definition

This part of the program defines geometrically a wing, a body, or a wing-body combination. The definition, in the form of body meridian lines and wing percent chord lines, is written on a tape that is read by the Geometry Transformation section of the program

Meridian lines may be visualized as stringers running lengthwise along the surface of the body. Each meridian line consists of a series of straight-line segments connecting points on the body surface; adjacent points are connected by straight lines. Constant percent chord lines, much like meridian lines, run along the wing surface in a spanwise direction.

A body surface is specified by a set of defining sections normal to the X-axis. Points on defining sections are given in polar coordinate form (ρ, θ) or in rectangular coordinates (Y, Z) . The number of points in each section must be the same as the number of meridian lines. Since the X-coordinate of each defining section is known, the X, Y, Z-coordinates of each point in a section can be computed. The first meridian line is constructed by joining the first point in each section; succeeding meridian lines are similarly constructed. As an option, the meridian lines may be "enriched"; additional meridian line points are inserted by three-dimensional interpolation from a space curve through the original points.

Both upper and lower wing surfaces may be defined. Only the construction of upper wing percent chord lines will be discussed, because later sections of the program are presently limited to this case. Although more complicated, the procedure is similar to that used to define the body. Percent chord lines (enriched if desired) on the surface of the wing are computed from a given set of control chords. These control chords must be parallel to the X-Y plane but are not necessarily parallel to the X-Z plane. In order to locate each control chord in space, sufficient data are given to find the intersections of the chord with the leading and trailing edges of the given planform. The distance between these intersections is called (in this discussion only) the "oblique chord length," because control chords need not be streamwise.

The projection of wing planform in the X-Y plane is specified by a set of points on the leading and trailing edges; the number of points in each set need not be the same. The planform may extend past the control chord region, but

the program will reject any chord which does not intersect both the leading and trailing edges. The planform may be open or closed at the wing tip. A planform is closed if the leading edge and trailing edge intersect at the wing tip; the generated percent chord lines will then converge to that point. If the leading and trailing edges do not intersect the planform is open.

A control chord is given as a set of points in a two-dimensional coordinate system. These points are scaled (except for zero-length chords) so that the difference in abscissa of the first and last points is equal to the oblique chord length. This scaled chord is then placed on the planform. Wing percent chord lines are constructed between scaled control chords.

The wing-body intersection option calculates the intersection of each wing percent chord line with the body surface. The wing percent lines are then truncated at the body surface.

All variable-length arrays are stored in a single buffer of 10,000 cells. As such there are no individual limits on the number of body stations, number of meridian or percent lines, number of chords or number of points defining the leading and trailing edges of the wing. (However, the data are scanned and excessively large arrays are rejected.) Maximum sizes for data arrays are usually set by later program segments.

2.2 Geometry Transformation

This section of the program reads the body and wing definitions from a tape written by the previous section. It then transforms the body and wing to a new coordinate system, orients the wing planform parallel to the x-y plane in this transformed system, and finds the intersections of wing percent chord lines with the body surface. Results are written on tapes for use by later program sections.

Three types of configurations may be handled: body alone, wing alone, or wing-body combination. If a body surface is involved only half of it is given; it is assumed to be symmetrical about the X-Z plane. Then a new x, y, z coordinate system is set up with the origin at the centroid of the forward end of the body and the x-axis passing through the aft end centroid; the z-axis lies in the X-Z plane. In the new coordinate system the body ends (unless of zero radius) are not necessarily parallel to the y-z plane; this is corrected by a

linear adjustment of all x-coordinates of the body points. Also, the new body length (distance between body end centroids) may differ from the original length. The original set of body defining stations is converted to the new coordinate system by a transformation of the form $x = \alpha X + \beta$ where α and β are constants. The body radius and centroid are computed at each of these stations. In a body alone case, the radius and centroid are then found by interpolation at a given number of equally spaced stations.

In a wing-body combination case, the wing is also transformed to the x, y, z coordinate system. Then the intersections of the wing leading and trailing edges with the body surface are computed; let z_A be the average of the z-coordinates of these two points. The wing is effectively flattened by changing each z-coordinate of the wing to z_A . The body is then intersected by the wing percent chord lines of the flattened wing.

The calculation of body radius and centroid is now resumed. A set of equally spaced stations is chosen between the forward end of the body and the station at which the wing leading edge intersects the body; a similar set is selected from there on aft. The calculation of the interval between stations in each region is subject to the constraints that the total number of stations must agree with a given number and that the two intervals must be approximately the same in each region.

In a wing alone case, the transformation is omitted. However, the wing is flattened; z_A is taken as the average of the z-coordinates of the inboard point on the leading and trailing edge percent chord lines. Bodies defined by a maximum of 16 meridian lines of 90 points each and wings of 16 percent chord lines of 90 points each can be processed.

2.3 Geometry Paneling

This program section panels the body and/or wing and provides additional data required by the following section (Aerodynamics). Two cases can be given as input to the Geometry Paneling section under the present program Overlay setup: the wing-body case and the wing alone case. The body alone case does not use the paneling section.

For a wing-body case, the body definition that is written on a scratch tape by the previous section (Geometry Transformation) is read into storage by an

input subroutine, INPUTB. The paneling is accomplished by combining this definition with data for the body cutting planes, read from input cards. A body cutting plane is oriented normal to the X-axis. The body panel areas are computed, and the panel centroid and control point coordinates are calculated. Streamwise chords are constructed through the panel control points, and the chord lengths are calculated. Finally the panel θ -inclination and α -incidence angles are computed. The paneling description and the additional geometric data are written on an output tape for printout purposes and on a scratch tape for use in the Aerodynamics section.

The wing paneling that is required for either the wing-body or the wing alone case is obtained similarly. The wing definition written by the Geometry Transformation section is read into storage arrays by an input subroutine, INPUTW, and used with card input data to provide a wing paneling scheme. Again the wing panel areas, chord lengths, and centroid and control point coordinates are calculated. The inclination and incidence angles are defined to be zero for wing panels since the wing is assumed to be a flat plate with no dihedral at zero incidence. As an option, camber and thickness ordinates and slopes are computed from airfoil ordinate tables. The wing paneling data are written on output and scratch tapes.

Certain program restrictions are present. Though a body that closes to a point can be defined in the definition section, such a body can not be paneled. For this case the leading row of panels would consist of triangular, not quadrilateral panels. This difficulty is avoided by excluding body cutting planes that intersect the body at the nose.

A second restriction requires a flat wing for all program cases. Under the current Overlay scheme, however, the Geometry Transformation section always provides such a definition. Hence this restriction results in no difficulty to the user.

When errors occur, an error message appears, execution of the present case is terminated, a partial data printout is given, and the next case is processed.

2.4 Aerodynamics

The aerodynamics problem is solved in three stages: (1) geometry input and calculation of the velocity components, and (2) a preprocessing stage, which is preparation for (3) the calculation of the aerodynamic cases. Control of the flow through the main links of this section of the program is provided by the subroutine AERO and is dependent on the configuration (wing alone, body alone, or wing-body combination) used.

The wing is defined by a number of panels. For an isolated body, the definition is given as an equivalent body of circular cross-section. In order to compute the interference effects on the body, for wing-body combinations, the body surface aft of the wing leading-edge intersection is also represented by panels. The geometric definition of the configuration is read from tapes generated by the geometry sections; this information also includes the areas, centroids, and control points of each panel.

Velocity components due to the various singularities representing the configuration are computed and stored on tape. For a wing defined to have thickness, the program computes velocity components induced by sources located in the reference plane of the wing. The effects of body thickness, camber, and incidence are simulated by placing line sources and doublets along the axis of the body. The effects of camber and incidence of the wing, and any residual interference effects, are represented by a surface distribution of vorticity on the wing and body panels. An option is provided to print out velocity components due to the individual singularities.

The preprocessing stage consists of the following computations. The velocity components are reordered and rewritten on tape. Several matrix operations are performed on the matrix of the aerodynamic influence coefficients (the normal components of velocity due to the vortex distributions), and the results of these are also written on tape. In particular, if the matrix is represented by the following sub-matrices:

$$\begin{bmatrix} [A_{BB}] & [A_{BW}] \\ [A_{WB}] & [A_{WW}] \end{bmatrix}$$

where $[A_{BB}]$ is the influence on the body due to the body
 $[A_{WB}]$ is the influence on the wing due to the body
 $[A_{BW}]$ is the influence on the body due to the wing
 $[A_{WW}]$ is the influence on the wing due to the wing

Then the following matrices are formed:

$$[D] = [A_{WB}] \cdot [A_{BB}]^{-1}$$

$$[E] = [A_{BB}]^{-1} \cdot [A_{BW}]$$

$$[A_R] = [A_{WW}] - [A_{WB}] \cdot [A_{BB}]^{-1} \cdot [A_{BW}]$$

A_R is referred to as the "reduced" matrix of the aerodynamic influence coefficients.

For optimization of the wing camber surface shape, the Lagrange multiplier technique is applied, and the coefficients of the resulting system of equations are computed (see equation (153), Part I):

$$\begin{bmatrix} -2A_1 a_{11} & -(A_1 a_{12} + A_2 a_{21}) & \dots & -A_1 & -x_1 A_1 \\ -(A_2 a_{21} + A_1 a_{12}) & & & -A_2 & \cdot \\ \cdot & & & \cdot & \cdot \\ \cdot & & & \cdot & \cdot \\ \cdot & & & \cdot & \cdot \\ -A_1 & \cdot & -A_N & 0 & 0 \\ -x_1 A_1 & \cdot & -x_1 A_N & 0 & 0 \end{bmatrix} \cdot \begin{Bmatrix} p_{W1} \\ p_{W2} \\ \cdot \\ \cdot \\ p_{WN} \\ \lambda_1 \\ \lambda_2 \end{Bmatrix} = \begin{Bmatrix} A_1(\bar{n}_1 + \bar{n}_{B1}) \\ A_2(\bar{n}_2 + \bar{n}_{B2}) \\ \cdot \\ \cdot \\ A_N(\bar{n}_N + \bar{n}_{BN}) \\ \bar{L} \\ \bar{M} \end{Bmatrix}$$

This operation results in the formation of two matrices. The first matrix includes wing lift and pitching moment constraints, and the second only the wing lift constraint. For the latter case, the row and column of the matrix corresponding to λ_2 is omitted. Both matrices are inverted and stored on tape.

The aerodynamic cases can now be computed. Additional input cards are used to request the following cases:

- 1) To compute the wing camber and twist, given the pressure distribution of the wing
- 2) To compute the pressure distribution, given the geometry of the configuration
- 3) To optimize the wing shape for minimum drag, given the wing lift or wing lift and pitching moment constraints

In each case a drag polar may be computed by inputting a series of incremental angles of attack. If a wing with thickness is specified in the input geometry, the program provides an option to compute the pressures due to thickness and to add them to the pressures due to camber. Another option selects either the linear, nonlinear, or exact isentropic equation for computing pressure coefficients. For a given configuration and Mach number, any number of aerodynamic cases may be computed.

Upon completion, the Aerodynamics section either transfers control to the Flow Visualization section if this additional analysis is requested or returns control to the main link.

2.5 Flow Visualization

This section of the program provides a method of analyzing the flow about a wing, body, or wing-body combination. The configuration is first processed by the Geometric and Aerodynamic sections of the program. The necessary information is transmitted to subroutine FLOVIZ via an intermediate tape (see Appendix D, Tape Formats). This tape may be saved for future runs, thereby eliminating the necessity of rerunning through the Geometric and Aerodynamic sections.

The method of aerodynamic influence coefficients is also applied to the calculation of field velocity components. The perturbation velocities in the field are determined by summing the product of the elementary influence components and their appropriate singularity strengths. From the perturbation velocities, the local flow vectors and pressure coefficients in the field are computed.

Three methods are available for presenting the flow-field data. First, streamlines may be generated by computing the velocity at discrete points and

integrating by a variable-step Adams-Moulton predictor-corrector method. Second, the flow may be examined at points of a two-dimensional or three-dimensional rectangular grid by specifying the increments of spacing along each axis and an origin for the grid. The two-dimensional grid may be skewed by specifying an implicit axis and a vector formed by the grid origin and another point. Finally, the flow may be analyzed at individual field points.

A special printing option provides the capability of examining the velocity and pressure contributions of the various singularities individually. The results of this option, if requested, immediately follow the total velocity components and pressure coefficient, and are labelled as to type of singularity.

The flow through the Flow Visualization section of the program is controlled by subroutine FLOVIZ. Upon completion of all requested options, control is returned to the subroutine AERO.

3. USE OF THE PROGRAM

3.1 Machine Components

The program is coded in FORTRAN IV and MAP for the IBM 7090/7094 (32K) digital computer under the control of the Systems Monitor, IBSYS Version 13. As the program is organized to utilize the Overlay feature of the Loader, IBLDR, one of the system units must be used as the input-output tape on which the links are written. This unit is specified on the \$ORIGIN control card according to the procedure outlined in reference 2.

In addition to the input and output tapes, the program uses seven tape units for scratch purposes. The choice of tape units to be used will depend on the particular computer installation, and tapes must be changed as required. Subroutine OPCAMI (see section 4.2) initializes all the tape units by assigning a logical number to each. To make the necessary changes, it will be sufficient to change only the logical designations in this subroutine.

3.2 Program Timing and Output Estimates

The computer time and number of lines of printout for a single configuration can be estimated from the following equations based on experience on the IBM 7094/M2.

$$\text{Time (minutes)} = 2.5 + .5G (4. \times 10^{-4} \times P^2) \times A + C + .1F$$

where G indicates type of paneling:

= 0., no paneling

= 1., wing paneling only

= 2., wing and body paneling

P is number of panels. If no paneling is required, use P = 10.

A indicates aerodynamic calculations:

= 0., no aerodynamic calculations

= 1., aerodynamic calculations requested

C is number of aerodynamic cases. Each of the following is considered a case:

Wing optimization case;

Direct aerodynamic case;

Indirect aerodynamic case;

Each angle of a polar series.

F is total number of field points, grid points, and streamline points required for flow visualization calculations.

$$\text{Output (lines)} = 100 + \left[500 + (10 \times P^{1/2}) \times V \times C \right] \times T + F$$

where T indicates type of case:

= 1., wing-alone case

= 2., body-alone case

= 3., wing-body case

V indicates velocity component printout:

= 1., no velocity component printout:

= 2., velocity components requested

3.3 Input Data Format

SUMMARY

The following chart summarizes the input data cards required to analyze each of the three basic configurations.

Geometry Definition Card Set	Wing-Alone	Body-Alone	Wing-Body
Card 1D	Yes	Yes	Yes
Cards 2D-9D	No	Yes	Yes
Cards 10D-18D	Yes	No	Yes
Cards 19D-20D	No	No	Yes
Card 21D	Opt	Opt	Opt
Card 22D	Yes	Yes	Yes

Geometry Paneling Card Set	Wing-Alone	Body-Alone	Wing-Body
Cards 1P-2P	Yes	Yes	Yes
Card 3P	Yes	No	Yes
Cards 4P-7P	No	No	Yes
Cards 8P-13P	Yes	No	Yes
Card 14P	Yes	No	Yes

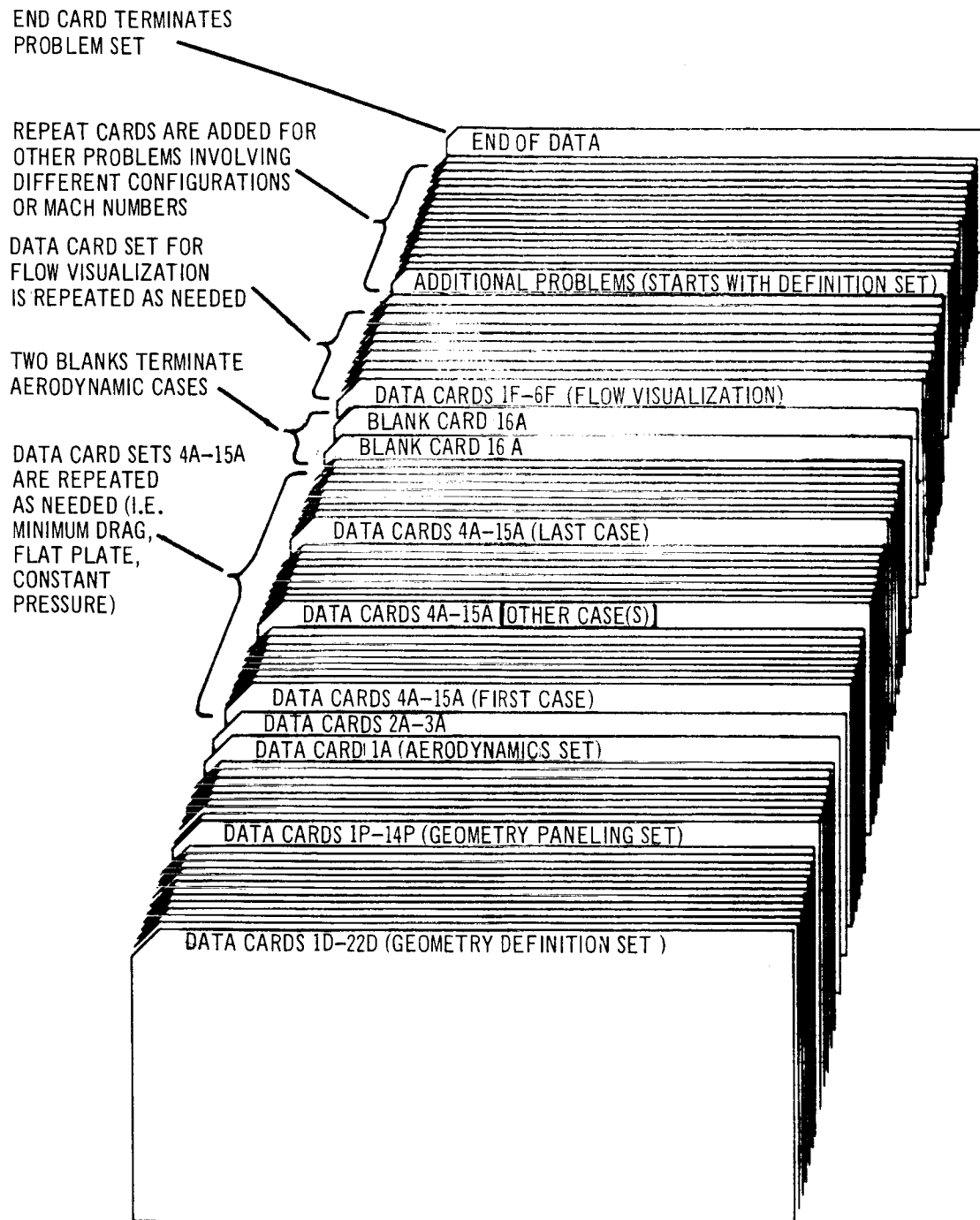
Aerodynamic Card Set	Wing-Alone	Body-Alone	Wing-Body
Cards 1A-6A	Yes	Yes	Yes
Cards 7A, 8A-8AA, 9A-9AA	No	Yes	Yes
Cards 10A-10AA (or -10AB)	Opt (if CASE = 1.)	No	Opt
Cards 11A-11AA, 12A-12AA (or -12AC)	Opt (if CASE = 2.)	No	Opt
Card 13A	Opt (if CASE = 3.)	No	Opt
Cards 14A-14AA (or -14AB)	Opt (if THICK = 1.)	No	Opt
Cards 15A	Opt (if POLAR > 0.)	No	Opt
Card 16A	Yes	Yes	Yes

Flow Visualization Card Set	Wing-Alone	Body-Alone	Wing-Body
Cards 1F-2F	Yes	Yes	Yes
Cards 3F, 3FA, 3FB, 3FC	Opt (GRIDS option)	Opt	Opt
Cards 4F, 4FA, 4FB, 4FC	Opt (STREAMLINES option)	Opt	Opt
Cards 5F, 5FA	Opt (POINTS option)	Opt	Opt
Card 6F	Yes	Yes	Yes
Terminal Card	Yes	Yes	Yes

Note: For Aerodynamic section input data, only one of the following three card sets can be used per case:

1. Cards 10A-10AA (or -10AB). For CASE = 1. (design case), defines ΔC_p distribution.
2. Cards 11A-11AA, 12A-12AA (or -12AC). For CASE = 2. (analysis case), gives wing angle of attack, twist, and $\Delta z / \Delta x$ camber distribution.
3. Card 13A. For CASE = 3. (optimization case), gives constraints.

A typical stacking sequence of input data cards is illustrated in the following figure.



GEOMETRY DEFINITION CARD SET

All geometry definition data, except title cards and literal statements, are punched in six-field, ten-digit format. A decimal point is required in each data field.

For a body-alone problem definition, Cards 10D through 20D are omitted. For a wing-alone problem definition, Cards 2D through 9D, 19D and 20D are omitted.

	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card 1D</u>	1-6	DE FINE	Columns 1-6 contain the word DEFINE.
<u>Card 2D</u>	1-4	BODY	Columns 1-4 contain the work BODY. Card 2D is used only when a body or wing-body combination is defined.
<u>Card 3D</u>	1-72	TITLE	Any desired title.
<u>Card 4D</u>	1-10	BNS	Number of defining body stations. 2. \leq BNS \leq 50..
	11-20	BTHETA	There is a defining-body cross section at each body station. This column gives number of points on each cross section. 3. \leq BTHETA \leq 10..
	21-30	AXIS (1)	Y-coordinate of body definition axis.
	31-40	AXIS (2)	Z-coordinate of body definition axis.
	41-50	CHDB	Dimensional tolerance to be used in generating additional body-meridian line points between given stations. If CHDB \leq 0. or if BNS $<$ 4., no additional points will be generated. If 0. $<$ CHDB \leq 0.001, then a value of 0.001 will be used.
<u>Card(s) 5D</u>	1-10	θ_1	Array of angles (θ), in degrees at each defining station. There must be exactly BTHETA angles \leq 10, six per card.
	\vdots	\vdots	
(2 cards maximum)	51-60	θ_6	
	etc.		

	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card(s) 6D*</u> (50 maximum)	1-10	STA	X-coordinate of body station.
	11-20	YZ(1)	Δ Y-increment added to body definition axis to establish a local origin from which all ρ , θ for this station are measured.
	21-30	YZ(2)	Δ Z-increment added to body definition axis to establish a local origin from which all ρ , θ for this station are measured.
	31-40	SCODE	<ul style="list-style-type: none"> = 0. this cross section is identical to previous section. = 1. this cross section is specified by BTHETA values of ρ (on cards 7D). The θ-array of card(s) 5D will be used. = 2. this cross section is a circle. (Radius given in columns 41-50.) = 3. this cross section is an ellipse. (Horizontal semi-axis is given in columns 41-50, the vertical in columns 51-60.) = 4. this cross section is circular (radius given in columns 41-50) with an angle array (on card(s) 8D) different from the θ-array on card(s) 5D. This option allows local deviations in the meridian lines. = 5. this cross section is specified by a set of ρ (on card(s) 7D) and by a nonstandard set of θ (on card(s) 8D). = 6. this cross section is given by a set of Y, Z pairs (on cards 9D).

Note — If options 1, 4, 5, or 6 are designated, the added information card(s) 7D, 8D, or 9D must be inserted behind that station card 6D and before the next station card 6D.

*One card is needed for each defining station.

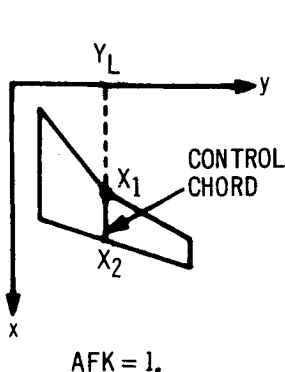
	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
	41-50	RAD(1)	Radius of section if SCODE = 2. or 4.. Horizontal semi-axis if SCODE = 3.. Not used otherwise.
	51-60	RAD(2)	Vertical semi-axis, if SCODE = 3.. Not used otherwise.
<u>Card(s) 7D</u>	1-10 : : 51-60 etc.	ρ_1 : : ρ_6	A set of body radii ρ if SCODE = 1. or 5.. There must be BTHETA \leq 10 values of ρ .
<u>Card(s) 8D</u> (2 maximum per station)	1-10 : : 51-60 etc.	θ_1 : : θ_6	A set of θ if SCODE = 4. or 5.. There must be BTHETA \leq 10 values of θ .
<u>Card 9D</u> (3 maximum per station)	1-10 11-20 21-30 31-40 41-50 51-60 etc.	Y_1 Z_1 Y_2 Z_2 Y_3 Z_3	Array of Y, Z coordinate pairs if SCODE = 6..

- Notes -
1. There is a maximum of three Card(s) 7D and/or Card(s) 8D per station.
 2. For inputting a body meridian exactly coincident with a wing's intersection, it is recommended that the cross-section option SCODE = 6. be used and that CHDB = 0.. The Z-height of the intersection's meridian [Card(s) 9D] is held constant and at exactly the same height as the wing [Card(s) 17D]. The aft-most body-defining station must be a zero-radius circle.

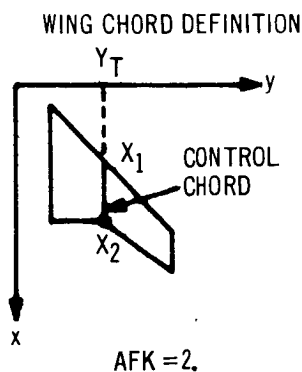
	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card 10D</u>	1-4	WING	Columns 1-4 contain the word WING. This card is used whenever a wing is defined. For the case of a body alone, omit cards 10D through 19D. After reading a WING card, the program expects wing definition data.
<u>Card 11D</u>	1-72	TITLE	Any desired title.
<u>Card 12D</u>	1-10	PNLE	Number of corner or break points defining the planform leading edge.
	11-20	PNTE	Number of corner or break points defining the planform trailing edge.
	21-30	AFN	Number of planform control chords. $AFN \geq 2$, including the wing-tip control chord. AFN must equal the larger of PNLE and PNTE; that is, each control chord must begin or end at a planform defining point.
	31-40	PLN	Number of constant percent chord lines used to form spanwise panel edges. Wing leading and trailing edges are counted in this number.
	41-50	WUL	= 1.
	51-60	CHD	Must be left blank.
<u>Card 13D</u>	1-10	PCODE	= 1.
	11-20	ACODE	= 1.
	21-30	EPS	Must be left blank.
<u>Card(s) 14D</u>	1-10	X_1	Notes - 1. For wing-body combinations, X_1 and Y_1 must lie inside the body so that an intersection can be calculated.
	11-20	Y_1	
	21-30	X_2	
	31-40	Y_2	
	41-50	X_3	

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
51-60 etc.	Y_3	2. The X-axis defining these points originates at the nose of the configuration (for wing-body cases) as defined by the first Card 6D.
<u>Card(s) 15D</u>	1-10 X_1	Array of points defining the planform trailing edge, arranged in order from inboard to outboard. There must be PNTE point pairs; three coordinates per card. Note - For wing-body combinations, X_1 and Y_1 must lie inside the body so that an intersection can be calculated.
	11-20 Y_1	
	21-30 X_2	
	31-40 Y_2	
	41-50 X_3	
51-60 etc.	Y_3	
<u>Cards 16D</u>	Cards 16D and 17D always occur in pairs (unless AFNU = 0. on card 16D) to define each wing control chord. There must be $AFN \geq 2$. pairs of 16D and 17D cards.	

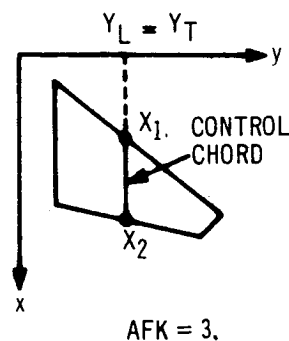
1-10 AFK Code to indicate how the control chord is oriented on the planform. See sketches below.



LEADING-EDGE POINT
DEFINES CONTROL CHORD:
The control chord leading
point X_1 is at a planform
leading-edge defining point.



TRAILING-EDGE POINT
DEFINES CONTROL CHORD:
The control chord trailing
point X_2 is at a planform
trailing-edge defining point.

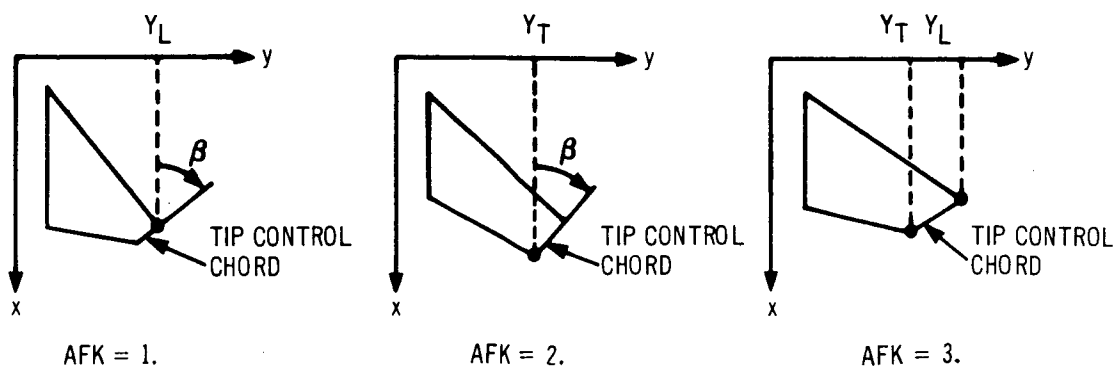


LEADING- AND TRAILING-
EDGE POINTS BOTH DEFINE
CONTROL CHORD: The control
chord leading edge X_1 is at
a planform leading-edge defining
point
or
The control chord trailing point
 X_2 is at a planform trailing-edge
defining point.

Both conditions must be
satisfied at the tip.

Column	Code	Explanation
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WINGTIP CONTROL CHORD DEFINITION (OBLIQUE)



Two of the three quantities Y_L , Y_T or β must be given. AFK indicates the appropriate pair. In summary:

if AFK = 1., input Y_L and β ;
 if AFK = 2., input Y_T and β ;
 if AFK = 3., input Y_T and Y_L .

11-20	BETA	The angle of yaw, β , in the diagram. If AFK = 1. or 2. and BETA = 0., the chord is streamwise. BETA is ignored if AFK = 3..
21-30	Y_L	Y-coordinate of leading edge of control chord. If AFK = 1. or 3., Y_L is equal to the Y-coordinate of the corresponding planform leading-edge defining point. If AFK = 2., Y_L is ignored.
31-40	Y_T	Y-coordinate of trailing edge of control chord. If AFK = 2. or 3., Y_T is equal to the Y-coordinate of the corresponding planform trailing-edge defining point. If AFK = 1., Y_T is ignored.
41-50	AFNU	<p>= 2. The height and control-chord true length are specified on the following card 17D.</p> <p>= 0. The previous 17D card values are used. Card 17D should not follow if AFNU = 0..</p>

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card(s) 17D</u> 1-10	X_O	$= 0.$
11-20	Z_O	Z-coordinate at the leading edge of control chord.
21-30	X_C	The control-chord true length. If $Z_O = Z_C = 0$, X_C may be given an arbitrary length, which is then scaled by the program to make X_C equal to the true chord length.
31-40	Z_C	Z-coordinate of control chord at the trailing edge.

Notes -

1. Z_O and Z_C specify the height of the wing. $Z_O = Z_C$, always; furthermore, the height of each control chord, including the tip, must be the same.
2. For wing-body configurations, $Z_O = Z_C$ must equal the height of the body meridian intended as the intersection meridian [Z-values, Card(s) 9D for SCODE = 6.] .
3. The control-chord true length X_C may be determined for AFK = 3. streamwise chords by subtracting the X-coordinates of the corresponding leading- and trailing-edge points (or by applying the right-triangle rule at an oblique chord).

For AFK = 1. or 2., interpolation must be done along the planform edge to locate a point corresponding to the chord's associated planform defining point.

<u>Card(s) 18D</u> 1-10	P_1	Array of constant percent chord values corresponding to the panel spanwise edges. The leading-edge value $P_1 = 0..$ There are PLN values required with the last value (for the trailing edge) = 100.
⋮	⋮	
51-60	P_6	
etc.		

	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card 19D</u>	1-3	WBX	Columns 1-3 contain the letters WBX. This card indicates that a wing-body intersection is desired. For wing only or body alone cases, this card is omitted.
<u>Card 20D</u>	1-10		= 1. linear interpolation used on body station perimeters to compute additional points between meridian lines in the wing intersection region.
			= 2. biquadratic interpolation used on body station perimeters to compute additional points between meridian lines in the wing intersection region.
	11-20		Dimensional intersection tolerance. Specifies the accuracy desired in locating wing-body intersection points. A value of 0.001 is suggested.
<u>Card 21D</u>	1-5	TDUMP	Columns 1-5 contain the letters TDUMP. This card is included if a dump of geometry definition and geometry transformation tapes is desired. See Appendix C for a detailed description of these tapes.
<u>Card 22D</u>	1-6	DEFEND	Columns 1-6 contain the word DEFEND. This card ends the definition set and must not be omitted.

GEOMETRY PANELING CARD SET

All paneling data, except title cards and literal statements, are punched in six-field, ten-digit format. A decimal point is required in each data field.

For body-alone case, cards 3P-14P are omitted.

For wing-alone case, cards 4P-7P are omitted.

	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card 1P</u>	1-5	PANEL	Columns 1-5 contain the word PANEL. This is the first card in the paneling link and must always follow the DEFEND card.
<u>Card 2P</u>	1-10		The number of source control stations at which the radius for an equivalent body of circular cross section and the actual body station centroid height are computed. A maximum of 50 stations may be requested. It is recommended that 50 stations be used. The radius at each control station is used to determine the source strength necessary to simulate the body thickness. The camber height at each control station and the body angle of attack (Card 7A) are used to determine the doublet strength necessary to simulate body camber and angle of attack.
Note -	In a wing-alone problem, Card 2P is blank.		
	11-20		Dimensional tolerance applied to the additional points generated between meridian lines on the perimeter of body defining stations. This controls the area and centroid location calculations. A value of 0.001 is suggested.
	21-30		This field contains an interpolation code. The program first determines an equivalent radius, R , at each body defining section, X , and then establishes an R vs. X array. Interpolation for additional radii at other stations is

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
		performed on this array. The same technique is used to determine centroid locations.
		= 1. linear interpolation for equivalent radii and centroid locations of the source control stations that are between body defining stations.
		= 2. biquadratic interpolation for equivalent radii and centroid locations at the source control stations that are between body defining stations.
31-40		= 1. linear interpolation between meridian line points on the body definition sections.
		= 2. if biquadratic interpolation is desired.
41-50		A dimensional tolerance value, E, such that if any equivalent radius length or centroid height, (z centroid), is less than E, its value will be set equal to zero. A value of 0.001 is suggested.
<u>Card 3P</u>	1-10	XPER
		Fraction of local streamwise panel chord at which panel control point is located. $0. < XPER < 1..$
		Note - XPER = .95 for all cases discussed in this report.
	11-20	YPER
		Fraction of local panel width at which panel control point is located. $0. < YPER < 1..$
		Note - YPER = 0. is a code used to locate the panel control point on the chord through the panel centroid. YPER = 0., for all cases discussed in this report.

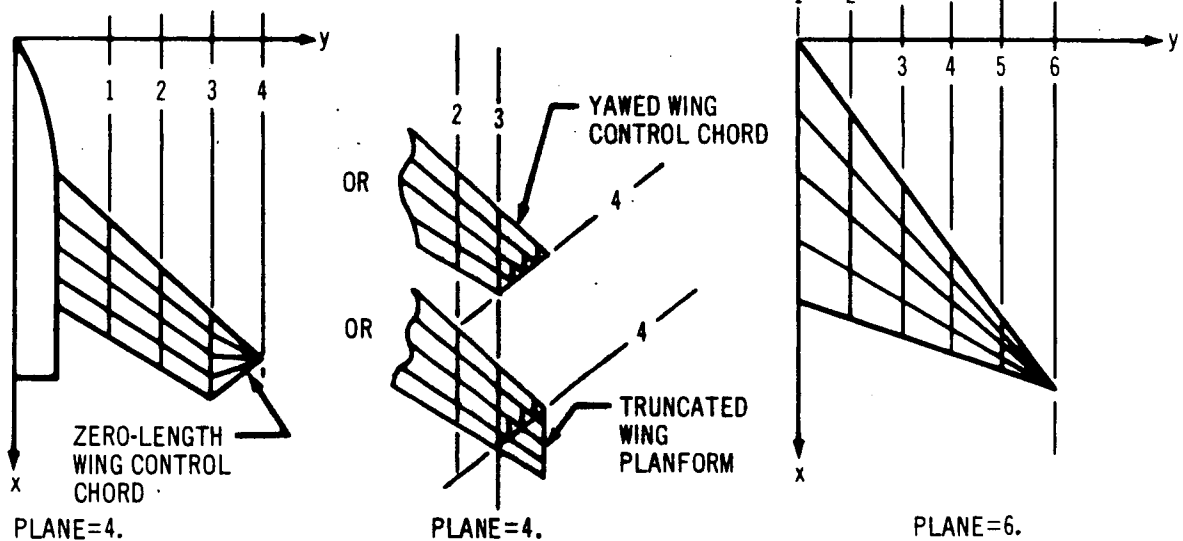
	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card 4P</u>	1-10	BODY PANEL	Columns 1-10 contain the words BODY PANEL.
<u>Card 5P</u>	1-10	PLNB*	Number of transverse body panel edges aft of wing trailing edge-body intersection ≤ 21 . If PLNB = 0., omit card 6P.
	11-20	PLNW*	Number of transverse body panel edges within the wing body intersection region ≤ 16 .
	21-30	TOLB	Slope tolerance on body secondary panel part leading edges. Panel parts with slopes $\left \frac{\Delta Y}{\Delta X} \right = \text{TOLB}$ in the local panel coordinate system) are eliminated. TOLB = 0.02 is suggested.
<u>Card(s) 6P</u>	1-10 : 51-60 etc.	XCEPTB ₁ : XCEPTB ₆	x-values of transverse body panel edges aft of the wing trailing edge - body intersection. There are PLNB values. Omit this card(s) if PLNB = 0.
<u>Card(s) 7P</u>	1-10 : 51-60 etc.	CODEBW ₁ : CODEBW ₆	Each field contains a number identifying those spanwise wing panel edges which continue around the body to form transverse body panel edges at the body intersection. The table must always start with the number 1. and terminate with the wing trailing-edge number. There are PLNW values.
<u>Card 8P</u>	1-10	WING PANEL	Columns 1-10 contain the words WING PANEL.
<u>Card 9P</u>	1-10	PLANE	Number of buttock lines which locate the streamwise wing panel edges specified by cards 10P and 11P. <u>Wing-alone problem:</u> PLANE is the number of buttock lines locating the streamwise panel edges including both

*(PLNB + PLNW) \leq 21

Column	Code	Explanation
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the wing tip and centerline.

Wing-body problem: PLANE is the number of buttock lines locating the streamwise panel edges, but does not include the inboard edge located by the program at the wing-body intersection. $PLANE \geq 2$. See sketches below.



11-20	OPTF	<p>= 1. upper and lower airfoil ordinates are read in (cards 12P and 13P) at each wing buttock line passing through the <u>panel centroids</u>. If the wing is untwisted and has the same airfoil section from root to tip, only one airfoil table is necessary. The program will scale this table to fit the appropriate chord.</p> <p>= 0. no tables are read in and the wing is a flat plate at zero incidence.</p>
21-30	SNUM	<p>Number of given airfoil ordinate tables.</p> <p>= 0., only if OPTF = 0.</p>

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
		= 1., same airfoil section from wing root to tip.
		= (PLANE - 1), wing alone case airfoils specified.
		= PLANE, wing-body case airfoils specified.
31-40	TOLW	Slope tolerance on wing secondary panel part leading edges. Panel parts with slopes $\left \frac{\Delta Y}{\Delta X} \right = \text{TOLW}$ are eliminated. TOLW = 0.01 is suggested.
<u>Card(s) 10P</u>	1-10 : : 51-60 etc.	YCEPT ₁ : : YCEPT ₆
		Wing buttock line values at which streamwise panel edges are specified. There are (PLANE -1) values. The tip edge is specified on card 11P.
<u>Card 11P</u>	1-10	CPNT
		Code indicating how the most outboard panel edge or wing tip is specified.

Note - This card controls the outboard panel edge and in no way influences the spanwise edges which are established by the geometry definition. The outboard panel edge is usually made coincident with the definition wing tip, but it may be used to truncate the defined wing tip and the spanwise panel edges anywhere between the two outboard wing buttock lines specified by card 9P. If truncation is specified, the wing span and area are reduced.

= 0. X and Y coordinates of the wing tip leading and trailing edge are given. Use VALUE(1) through (4).

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
		= 1. X and Y coordinates of the leading edge and the slope ($\Delta X/\Delta Y$) of the wing tip are given. Use VALUE(1), (2) and (5).
		= 2. X and Y coordinates of the trailing edge and the slope ($\Delta X/\Delta Y$) of the wing tip are given. Use VALUE(3), (4) and (5).
11-20	VALUE(1)	X-coordinate of wing tip leading edge if CPNT = 0. or 1..
21-30	VALUE(2)	Y-coordinate of wing tip leading edge if CPNT = 0. or 1..
31-40	VALUE(3)	X-coordinate of wing tip trailing edge if CPNT = 0. or 2..
41-50	VALUE(4)	Y-coordinate of wing tip trailing edge if CPNT = 0. or 2..
51-60	VALUE(5)	wing tip slope, $\frac{\Delta X}{\Delta Y}$, if CPNT = 1. or 2..

Card(s) 12P Card(s) 12P and Card(s) 13P give the SNUM set of airfoil coordinates. These card sets (12P and 13P) are always used in pairs to define each airfoil; the coordinates apply at the centroid buttock line of each chordwise row of wing panels. The inboard row is read in first, then the next row outboard, then the next, etc. out to and including the tip row.

Chordwise biquadratic interpolation is used between input points. Thus it is recommended that XNUM (1) be 25., or nearly 25.; input points should be concentrated around regions of rapidly varying thickness and/or camber, such as the airfoil leading edge.

The card sets (12P and 13P) are omitted if OPTF = 0.

First Card	1-10	XNUM(1)	Number of points (X, Z coordinate pairs) in upper surface airfoil ordinate table. $4. \leq XNUM(1) \leq 25..$
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	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
Second Cards	1-10	XFOIL ₁	Upper surface airfoil ordinate table. <u>Local</u> X and Z coordinates are given from leading edge to trailing edge. That is, the first values of ZFOIL and XFOIL entered are always zero. If the wing has no twist, an unscaled set of ordinates may be given and the program will scale the airfoil to the local chord. The section has no twist, if and only if, $ZFOIL_{upper, trailing\ edge} = - (ZFOIL_{lower, T.E})$
	11-20	ZFOIL ₁	
	.	.	
	.	.	
	41-50	XFOIL ₃	
	51-60	ZFOIL ₃	
	etc.		

Cards 13P

First Card	1-10	XNUM(2)	Number of points (X, Z coordinate pairs) in lower surface airfoil ordinate table. $4. \leq XNUM(2) \leq 25..$
Second Cards	1-10	XFOIL ₁	Lower surface airfoil ordinate table. To input a completely uncambered section, it is recommended that $XNUM(1) = XNUM(2)$ and that for I such that $1. \leq I \leq XNUM$, $XFOIL(I), upper = XFOIL(I), lower$ and that $ZFOIL(I), upper = - (ZFOIL(I), lower)$
	11-20	ZFOIL ₁	
	.	.	
	.	.	
	41-50	XFOIL ₃	
	51-60	ZFOIL ₃	
	etc.		

<u>Card 14P</u>	1-6	PANEND	Columns 1-6 contain the word PANEND. This card ends the paneling set and must be used whenever any paneling is performed. It is not needed for a body-alone problem.
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AERODYNAMIC CARD SET

All aerodynamic data, except title cards and literal statements, are punched in seven-field, ten-digit format. A decimal point is required in each data field. Data Cards 1A and 2A are input only once for a given configuration and Mach number. The remaining aerodynamic data cards may be repeated as necessary to solve the selected aerodynamic cases.

	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card 1A</u>	1-11	AERO-DYNAMIC	Columns 1-11 contain the word AERO-DYNAMIC.
<u>Card 2A</u>	Select and input one of the following data control cards.		
	1-7	COMPUTE	The aerodynamic matrices and geometry data are not saved on tape; this card is used when a defined and paneled configuration is input.
	1-9	SAVE TAPE	The aerodynamic matrices and geometry data are saved on tape for repeated analysis. The body and wing thickness and camber from the geometry section are also saved for optional use. This card is used when a defined and paneled configuration is input.
	1-8	USE TAPE	A previously saved tape is to be used; no definition nor paneling data are input when this option is selected.
<u>Card 3A</u>	1-10	XMACH	Mach number.
	11-20	SYM	= 0. the aerodynamic problem solved is asymmetric about the vertical X-Z plane (image panels not included). = 1. the aerodynamic problem solved is symmetric about the vertical X-Z plane (image panels included).

	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card 4A</u>	1-72	TITLE	Any desired title.
<u>Card 5A</u>	1-10	CASE	<p>= 1. calculates wing twist and camber for a given ΔC_p distribution on wing where</p> $\Delta C_p = C_{p \text{ lower}} - C_{p \text{ upper}}$ <p>= 2. calculates pressure distribution over the configuration. Wing and body camber can be changed within this option.</p> <p>= 3. optimizes wing twist and camber for minimum drag.</p> <p>Note - For body-alone problems, only case = 2. option is available.</p>
	11-20	CPCALC	<p>= 0. C_p calculations use linear equation,</p> $C_p = -2u.$ <p>= 1. C_p calculations use nonlinear equation,</p> $C_p = -2u + \beta^2 u^2 - v^2 - w^2$ <p>= 2. C_p calculations use the "exact" isentropic equation on the isolated body and the linear equation on the wing and body panels. The "exact" isentropic equation is</p> $C_p = \frac{2}{\gamma M^2} \left\{ \left[1 + \frac{\gamma - 1}{2} M^2 \left(1 - (1 + u)^2 + v^2 + w^2 \right) \right]^{\frac{\gamma}{\gamma - 1} - 1} - 1 \right\}$ <p>where M is the mainstream Mach number, U is the mainstream velocity and γ (1.4) is the coefficient of specific heats.</p>
	21-30	POLAR	<p>= 0. drag polar not requested.</p> <p>= N. drag polar requested. A series of N incremental angles of attack is specified on Card(s) 15A.</p>
	31-40	THICK	<p>= 0. wing thickness pressures are not calculated.</p> <p>= 1. wing thickness pressures are calculated.</p>

	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
	41-50	VOUT	= 0. the velocity components are not printed. = 1. the velocity components are printed.
<u>Card 6A</u>	1-10	RFAREA	<u>Half-wing</u> reference area. If this field is left blank, the program sums the wing panel areas to obtain the reference area which is the half-wing exposed area. For the body-alone problem, a value <u>must</u> be input, or a unit area is used.
	11-20	XP	x-coordinate about which the pitching moments are computed.
	21-30	ZP	z-coordinate about which the pitching moments are computed.
	31-40	CBAR	= 0. Unit (1.) reference chord length to be used in pitching-moment calculations. = CBAR, Reference chord length of CBAR to be used.
	41-50	SEMIS	= 0. Unit (1.) wing semispan to be used in spanwise C_L , C_D calculations. = SEMIS, Wing semispan of SEMIS to be used.
<u>Card 7A</u>	For configurations that include a body, the body angle of attack is specified on this card.		
	1-10	ARB	Body angle of attack in degrees.
<u>Card 8A</u>	For configurations that include a body, two options are available for specifying the body radii. The first word on the first card indicates the type of input. Omit this card set for wing-alone problems.		
	1-5	<u>Option A</u> = "GIVEN" The body radii to be used are those calculated in the geometry definition section. No additional cards are needed.	
	1-72	<u>Option B</u> = Identifying title. Any title calls the option of inputting body radii directly. The radii from the geometry section are superseded.	

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card(s) 8AA</u> (used only with Option B)		
1-10	R_1	The body radii are input on these cards.
11-20	R_2	They are input from nose to tail and
.	.	apply at the source control stations
.	.	generated by the paneling section. There
61-70	R_7	are XNRX radii required (Card 2P,
etc.		columns 1-10).

Card 9A For configurations that include a body, two options are available for specifying body camber. The first word on the first card is the key to the type of input the program expects. Omit this card set for wing-alone problems.

1-5	GIVEN	<u>Option A</u>
7-80	Any additional identifying symbols	Columns 1-5 contain the word GIVEN. The program takes the body camber as that calculated in the geometry definition section. No additional cards are necessary for this option.
1-80	Any identifying symbols	<u>Option B</u>
		The first card contains any arbitrary identifying symbols (other than GIVEN or CONSTANT as the first word) to describe the body camber. The program expects more cards immediately to specify the body camber.

Card(s) 9AA (used only with Option B)

1-10	Z_1	The body camber is input on these cards
11-21	Z_2	as Z-heights of body cross sections at
.	.	the source control stations. The values
.	.	are input from nose to tail; there are
.	.	XNRX values required (Card 2P, columns
61-70	Z_7	1-10).
etc.		

Card 10A Calculates wing twist and camber for a given wing ΔC_p distribution (CASE = 1., field 1 of Card 5A). Two options are available for specifying the ΔC_p distribution. These options are selected by the first word on the first card of this set. Omit this set for body-alone problems or CASE = 2. or 3.

1-8	CONSTANT	<u>Option A</u>
9-80	Any additional identifying symbols	Columns 1-8 contain the word CONSTANT. This option restricts the wing to have a constant ΔC_p distribution. This constant value is specified on the following card. Recall that $\Delta C_p = C_{p \text{ lower}} - C_{p \text{ upper}}$

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
1-80	Any identifying symbols	<u>Option B</u> The first card contains appropriate identifying symbols (other than GIVEN or CONSTANT as the first word) to select Option B. ΔC_p for each panel is specified on the following card set.

Card 10AA (used only with Option A)

1-10	ΔC_p	ΔC_p for Option A.
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Card(s) 10AB (used only with Option B)

1-10	ΔC_{p1}	ΔC_p 's for Option B. This array must be ordered starting with the inboard panel at the leading edge and running aft to the trailing edge, then proceeding outboard to the tip in the same manner.
.	.	
.	.	
.	.	
61-70 etc.	ΔC_{p7}	There must be the same number of values as there are wing panels. Values apply at panel centroids.

Card 11A For configurations that include a wing and for which CASE (Card 5A) = 2, the wing angle of attack and an optional twist distribution are indicated on these cards.

1-10	ARW	Wing angle of attack in degrees (relative to body axis if wing-body configuration)
11-20	TWIST	= 0. No twist distribution to be given. = 1. Twist distribution to be specified on following cards.

Card(s) 11AA (used only if TWIST = 1.)

1-10	ARWT ₁	Twist angle for successive wing panel columns; ARWT ₁ applies to the inboard-most column.
11-20	ARWT ₂	
.	.	
.	.	
61-70 etc.	ARWT ₇	

Note - Card 11AA is repeated until angle for each column of wing panels is given. Do not use Card 11AA if TWIST (Card 11A) = 0.

Card 12A Calculates the pressure distribution over the configuration (CASE = 2., field 1 of Card 5A). Three options are available for specifying the camber shape of the wing. The options are selected by the first word on the first card of this set. Omit this set for body-alone problems or CASE = 1. or 3.

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Option A</u>		
1-8	CONSTANT	Columns 1-8 contain the word CONSTANT.
9-80	Any other identifying symbols	This option restricts the wing camber shape to have a constant slope for each wing panel. This constant value is specified on the following card.
<u>Option B</u>		
1-5	GIVEN	The wing camber shape is specified by the input geometry. The panel slopes used are those generated in the paneling section of the program. In this case, no more cards are needed.
7-80	Any other identifying symbols	
<u>Option C</u>		
1-80	Any identifying symbols	Appropriate identifying symbols (other than GIVEN or CONSTANT as the first word) on the first card of this set are used to select this option. The wing camber shape is specified by a slope for each panel. Other cards must be input which contain the slope values.

Card 12AA (used only with Option A)

1-10	ALPHAC	The constant wing panel $\Delta z/\Delta x$ slope for Option A.
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There is no auxiliary card for Option B.

Card(s) 12AC (used only with Option C)

1-10	ALPHAC ₁	Wing panel $\Delta z/\Delta x$ slopes for Option C.
.	.	The array must be ordered starting with the inboard panel at the leading edge and running aft to the trailing edge, then proceeding outboard to the tip in the same manner. There must be the same number of values as there are wing panels. Values apply to panel control points.
.	.	
.	.	
61-70 etc.	ALPHAC ₇	

Card 13A

Optimizes wing twist and camber for minimum drag (CASE = 3., field 1 of Card 5A). Two options are available. The first option optimizes the wing for a given wing-lift constraint, and the second option optimizes the wing for both the wing-lift and center-of-pressure constraints. Only one data card is required. Omit this card for a body-alone problem or CASE = 1. or 2.

1-10	CONSNT	= 0. the wing is optimized for minimum drag with a wing-lift constraint.
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<u>Column</u>	<u>Code</u>	<u>Explanation</u>
		= 1. the wing is optimized for minimum drag with both wing-lift constraint and x-coordinate of the center-of-pressure constraint.
11-20	CLBAR	Wing-lift-coefficient constraint.
21-30	XCPBAR	The x-coordinate of the wing center-of-pressure constraint. If the center of pressure is not constrained, omit this field.

Card 14A For configurations that include a wing and for which THICK (Card 5A) = 1., two options are available for specifying the wing thickness distribution. The first word on the first card indicates the type of input. Omit this card and card(s) 14AB if thickness effects are not requested (THICK = 0).

1-5	<u>Option A</u> = "GIVEN." The wing thickness distribution to be used is that computed in the geometry paneling section. No more cards are needed.
1-72	<u>Option B</u> = Identifying title. The wing thickness distribution is input on the following cards.

Card(s) 14AB (use only with Option B)

1-10	ALPHAT ₁	Wing thickness $\Delta z/\Delta x$ slopes. For the purpose of these cards, wing thickness is the distance from the airfoil camber line to either airfoil surface. A leading-edge thickness slope (less than the tangent of the Mach angle) is given for the inboard wing-panel column and followed by thickness slopes for each panel in that column of the wing panels. This is repeated for each wing-panel column. The total number of input wing-thickness slopes equals the number of wing panels plus the number of panel columns.
11-20	ALPHAT ₂	
21-30	ALPHAT ₃	
.	.	
.	.	
61-70	ALPHAT ₇	

Card(s) 15A 1-10 DADEG If drag polar is requested (POLAR = N. on Card 5A), incremental angles of attack (in degrees) are specified on Card(s) 15A. A terminating blank card is used. Omit this card set if Polar option is not selected (POLAR = 0.).

FLOW VISUALIZATION CARD SET

All flow visualization data, except title cards and literal statements, are punched in seven-field, ten-digit format. A decimal point is required in each data field. This card set instruction applies to any type of configuration and any type of aerodynamic analysis. Only the last angle of attack of the last aerodynamic analysis is visualized.

	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card 1F</u>	1-8	FLOW VIZ	Columns 1-8 contain the word FLOW VIZ. This card calls the Flow Visualization section of the program.
<u>Card 2F</u>	1-10	CPCALC	= 0. The linear C_p equation is used to calculate field pressure points. = 1. The nonlinear C_p equation is used. = 2. The "exact" isentropic equation is used. The C_p equations are defined for Card 5A of the aerodynamic set.
	11-20	CAMN	= 1. Visualization calculation of only the thickness effects of the wing and/or body. No camber, twist, angle-of-attack, or interference effects are computed. If lifting effects are not of interest, selecting this option will save computer time. = 0. Visualization calculation takes account of all effects included in the analysis.
	11-21	POP	= 0. No special print option. ≠ 0. Prints velocity components due to various singularities.
NOTE: The three modes of flow visualization (grids, streamlines, and points) may be called in any order and any number of times by inputting the appropriate literal card.			
<u>Card 3F</u>	1-5	GRIDS	Columns 1-5 contain the word GRIDS. This card calls the grid mode of flow visualization.
<u>Card 3FA</u>	1-10	XNG	The number of two-dimensional or three-dimensional grid structures; any number may be requested.

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card(s) 16A</u> 1-72	(blank)	(This is a blank card.) To conduct an additional aerodynamic analysis, begin the new set of aerodynamic data with Card 4A. To terminate the data of the last analysis or to call the flow visualization section, place two Card(s) 16A after the terminating polar card.

	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card 3FB</u>	1-10	XO	The rectangular coordinates of the origin of the grid structure.
	11-20	YO	
	21-30	ZO	
	31-40	XA	The rectangular coordinates of a point which, together with the origin (above), defines an axis of a skew grid; the positive direction is from the origin to point A.
	41-50	YA	
	51-60	ZA	
			Enter values only if a skew grid is called; AMD (Card 3FC) = 4.
	61	LIT	= X Select and input the letter of the = Y coordinate axis which is used to- = Z gether with the skew axis defined above to define the two-dimensional skew grid. Enter a letter only if AMD = 4.
<u>Card 3FC</u>	1-10	DX	Values of increments which position points on the grid. If a two-dimensional grid is desired, set one of the increments to zero and the corresponding increment count (next three fields) to 1.
	11-20	DY	
	21-30	DZ	
	31-40	XN	The respective number of increments which position points on the grid. If AMD = 1., $YN \times ZN \leq 500$. If AMD = 2., $XN \times ZN \leq 500$. If AMD = 3., $XN \times ZN \leq 500$.
	41-50	YN	
	51-60	ZN	
	61-70	AMD	This code controls the format in which the data is output. = 1. Data is output for all the (Y, Z) points at a given X-value; then the data for the next X-value, etc. Always select this code value when DX = 0. = 2. Data is output for all the (X, Z) points at a given Y-value; then the data for the next Y-value, etc. Always select this code value when DY = 0.

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
		= 3. Data is output for all the (X, Y) points at a given Z-value; then the data for the next Z-value, etc. Always select this code value when $DZ = 0$.
		= 4. A skew grid has been specified for the plane defined by LIT-axis and the line from the origin through point A. The following notes apply.

- Notes— 1. Increments and the number of increments determining points on a skew grid are input in the following way: The axis specified by LIT is input as if for a rectangular array. One of the other two axes is input with zero (0.) increment size and number. The remaining axis is input as if for a rectangular array also, but its graduations apply to the skew axis; planes are established normal to the remaining axis through each of its graduations. Where these planes intersect the skew axis, a skew-axis graduation is established.
2. Repeat Card 3FB and Card 3FC for each grid called. That is, there must be KNG sets of Cards 3FB-3FC.

<u>Card 4F</u>	1-11	STREAMLINES	This word appears in columns 1-11 and calls the streamlines option.
<u>Card 4FA</u>	1-10	DXMAX	The maximum permissible step size for the streamline's integrator. A value of $10. \times XDEL T$ is recommended.
	11-20	DXMIN	The minimum permissible step size for the streamline's integrator. $DXMIN > 0.$, always. A value of $0.1 \times XDEL T$ is recommended.
	21-30	PRINT	The result is a series of points in rectangular coordinates (X, Y, Z) from XMIN through point S to XMAX. The values of X are determined by this code. (See Card 4FC.)
			= 0. Points are printed out in even increments of $XDEL T$.
			= 1. Points are generated by the integrator and are printed out directly.

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
Note— If printout with PRINT = 1. shows that DXMIN is reached as an actual interval in printing out the results, the streamline may not be accurate. To ensure accuracy, reduce DXMIN and XDELT and repeat the calculation.		
<u>Card 4FB</u>	1-10 XNS	The number of streamlines to be specified; any number may be requested.
<u>Card(s) 4FC</u>	1-10 XS	The streamlines' starting point. The streamline begins on the XMIN plane, proceeds downstream, passes through point S, and continues to the XMAX plane.
	11-20 YS	
	21-30 ZS	
	31-40 XMIN	The farthest point upstream and downstream to which the streamline will be calculated. The relationship $XMIN \leq XS \leq XMAX$ must be observed.
	41-50 XMAX	
	51-60 XDELT	The initial step size for the streamline's integration. For configurations that include a wing, a value of $0.1 \times$ (mean chord length) is recommended. For body-alone analyses, a value of $0.1 \times$ (body length) is recommended. For streamlines passing very near the configuration, a smaller value should be used. $DXMAX > XDELT > DXMIN$, always. There must be exactly XNS number of Card(s) 4FC.
<u>Card 5F</u>	1-6 POINTS	Columns 1-6 contain the word POINTS. This card calls the points mode of the flow visualization.
<u>Card 5FA</u>	1-10 XP	The number of points requested; any number may be requested.
<u>Card(s) 5FB</u>	1-10 XF	Rectangular coordinates of point; there must be XP number of Card(s) 5FB.
	11-20 YF	
	21-30 ZF	

	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card 6F</u>	1-8	VIZEND	Columns 1-6 contain the word VIZEND. This card terminates the Flow Visualization section. The flow visualization calculations may be continued after the above data has been calculated and this card has been entered, by inputting Card 1F again and continuing the data.
<u>Terminal Card</u>	1-11	END OF DATA	If no further analysis is required, the run is terminated by an END OF DATA card.

3.4 Sample Input and Output Data

SEVEN FIELD, TEN DIGIT CRD FORMAT

1	10	11	20	21	30	31	40	41	50	51	60	61	69	70	71	72	DENT	80
DEFINE																		1D
BODY																		2D
TR-805/EQUIVALENT/BODY																		3D
24.	8.																	4D
0.	25.	50.	75.	102.19	130.													5D
155.	180.																	5D
0.	0.	0.	2.	0.														6D
1.5	0.	0.	2.	.270														6D
3.	0.	0.	2.	.4464														6D
4.5	0.	0.	2.	.5943														6D
6.	0.	0.	2.	.7234														6D
7.5	0.	0.	2.	.837														6D
9.	0.	0.	2.	.9364														6D
10.5	0.	0.	2.	1.0223														6D
12.	0.	0.	2.	1.0936														6D
13.5	0.	0.	2.	1.1479														6D
15.	0.	0.	2.	1.184														6D
15.1	0.	0.	0.															6D
17.5	0.	0.	0.															6D
20.	0.	0.	0.															6D
22.5	0.	0.	0.															6D
25.	0.	0.	0.															6D
27.5	0.	0.	0.															6D
29.9	0.	0.	0.															6D
31.	0.	0.	2.	1.174														6D
32.	0.	0.	2.	1.154														6D
33.	0.	0.	2.	1.124														6D
34.	0.	0.	2.	1.084														6D
35.	0.	0.	2.	1.034														6D
36.	0.	0.	2.	1.														6D
WING																		10D
TR-805 WING (TWP = -.25)																		11D
2.	3.	4.	11.	1.	0.													12D
1.	1.	0.																13D
10.67	0.	40.27	10.774															14D
19.88	0.	43.518	8.603	40.27	10.774													15D
3.	0.	0.	0.	2.														16D
0.	-.25	9.21	-.25															17D
1.	0.	5.	0.	0.														16D
3.	0.	8.603	8.603	2.														16D
0.	-.25	9.21	-.25															17D
3.	0.	10.774	10.774	2.														16D
0.	-.25	0.	-.25															17D
0.	10.	20.	30.	40.	50.													18D
60.	70.	80.	90.	100.														18D
WBX																		19D
2.	.0001																	20D
DEFEND																		22D
PANEL																		1P
50.	0.	1.	1.	.001														2P
.95	0.																	3P
BODY PANEL																		4P
4.	11.	.02	.01															5P
25.	27.	29.5	32.415															6P
TITLE BOEING WING-BODY MODEL										NAME	DATE	PAGE	OF					

SEVEN FIELD, TEN DIGIT CRD FORMAT

10	11	20	21	30	31	40	41	50	51	60	61	69	70	71	72	DFNT	80																
1.	2.	3.	4.	5.	6.											7P																	
7.	8.	9.	10.	11.												7P																	
WING PANEL																	8P																
10.	1.	1.	.05													9P																	
1.9846	2.8119	3.6392	4.4665	5.2938	6.1211											10P																	
6.9484	7.7757	8.603														10P																	
0.	40.27	10.774	40.27	10.774												11P																	
15.																12P																	
0.	0.	.025	.0108	.05	.01556											12P																	
.1	.02155	.15	.02548	.2	.02832											12P																	
.3	.03215	.4	.0342	.5	.03385											12P																	
.6	.03112	.7	.02599	.8	.01915											12P																	
.9	.01084	.95	.00616	1.	0.											12P																	
15.																13P																	
0.	0.	.025	-.00257	.05	-.00325											13P																	
.1	-.00428	.15	-.0051	.2	-.00581											13P																	
.3	-.00701	.4	-.00735	.5	-.0065											13P																	
.6	-.00469	.7	-.00239	.8	-.00068											13P																	
.9	.0.	.95	0.	1.	0.											13P																	
PANEND																	14P																
AERODYNAMIC																	1A																
SAVE TAPE																	2A																
1.8																	3A																
TR 805/EQUIVALENT/BODY																	4A																
2.	0.	0.	1.	1.												5A																	
89.375	0.	0.														6A																	
6.																7A																	
GIVEN BODY RADII																	8A																
GIVEN BODY CAMBER																	9A																
0.	0.															11A																	
CONSTANT WING CAMBER																	12A																
0.																12AA																	
GIVEN WING THICKNESS																	14A																
																16A																	
																16A																	
FLOW VIZ																	1F																
0.	0.															2F																	
POINTS																	5F																
9.																5FA																	
24.	4.	-1.														5FB																	
24.	4.	-.5														5FB																	
24.	4.3535	-.6465														5FB																	
24.	4.5	-1.														5FB																	
24.	4.3535	-1.3535														5FB																	
24.	4.	-1.5														5FB																	
24.	3.6465	-1.3535														5FB																	
24.	3.5	-1.														5FB																	
24.	3.6465	-.6465														5FB																	
GRIDS																	3F																
2.																3FA																	
30.	1.2	-1.2														3FB																	
.5	1.	.5	10.	3.	2.	2.										3FC																	
14.90	0.	-1000.														3FB																	
1.	200.	0.	70.	1.	0.	2.										3FC																	
TITLE																	BOEING WING-BODY MODEL																
																	NAME																
																	DATE																
																	PAGE																
																	OF																

SEVEN FIELD, TEN DIGIT CRD FORMAT

[illegible]

Sample Data Printout

The computer output for a sample case is given on the following pages:

Data card listing	48
Geometry Definition	50
Body definition	50
Wing definition	61
Intersection	66
Geometry Transformation	68
Transformed body description	69
Transformed wing description	73
Transformed intersection	75
Body section radius and centroid coordinate vs x-array	76
Geometry Paneling	77
Body paneling data	77
Additional body geometry data	80
Wing paneling data	82
Additional wing geometry data	85
Aerodynamics	87
Flow Visualization	105

DATA CARDS ARE LISTED BELOW

DEFINE

body

TP-A05/EQUIVALENT/ANDY

	6.	50.	75.	102.19	130.
24.	25.				
25.	180.				
30.	0.	0.	2.	0.	
35.	0.	0.	2.	.270	
40.	0.	0.	2.	.4464	
45.	0.	0.	2.	.5943	
50.	0.	0.	2.	.7234	
55.	0.	0.	2.	.837	
60.	0.	0.	2.	.9364	
65.	0.	0.	2.	1.0223	
70.	0.	0.	2.	1.0936	
75.	0.	0.	2.	1.1479	
80.	0.	0.	2.	1.184	
85.	0.	0.	0.		
90.	0.	0.	0.		
95.	0.	0.	0.		
100.	0.	0.	0.		
105.	0.	0.	0.		
110.	0.	0.	0.		
115.	0.	0.	0.		
120.	0.	0.	0.		
125.	0.	0.	0.		
130.	0.	0.	0.		
135.	0.	0.	0.		
140.	0.	0.	0.		
145.	0.	0.	0.		
150.	0.	0.	0.		
155.	0.	0.	0.		
160.	0.	0.	0.		
165.	0.	0.	0.		
170.	0.	0.	0.		
175.	0.	0.	0.		
180.	0.	0.	0.		
185.	0.	0.	0.		
190.	0.	0.	0.		
195.	0.	0.	0.		
200.	0.	0.	0.		
205.	0.	0.	0.		
210.	0.	0.	0.		
215.	0.	0.	0.		
220.	0.	0.	0.		
225.	0.	0.	0.		
230.	0.	0.	0.		
235.	0.	0.	0.		
240.	0.	0.	0.		
245.	0.	0.	0.		
250.	0.	0.	0.		
255.	0.	0.	0.		
260.	0.	0.	0.		
265.	0.	0.	0.		
270.	0.	0.	0.		
275.	0.	0.	0.		
280.	0.	0.	0.		
285.	0.	0.	0.		
290.	0.	0.	0.		
295.	0.	0.	0.		
300.	0.	0.	0.		
305.	0.	0.	0.		
310.	0.	0.	0.		
315.	0.	0.	0.		
320.	0.	0.	0.		
325.	0.	0.	0.		
330.	0.	0.	0.		
335.	0.	0.	0.		
340.	0.	0.	0.		
345.	0.	0.	0.		
350.	0.	0.	0.		
355.	0.	0.	0.		
360.	0.	0.	0.		
365.	0.	0.	0.		
370.	0.	0.	0.		
375.	0.	0.	0.		
380.	0.	0.	0.		
385.	0.	0.	0.		
390.	0.	0.	0.		
395.	0.	0.	0.		
400.	0.	0.	0.		
405.	0.	0.	0.		
410.	0.	0.	0.		
415.	0.	0.	0.		
420.	0.	0.	0.		
425.	0.	0.	0.		
430.	0.	0.	0.		
435.	0.	0.	0.		
440.	0.	0.	0.		
445.	0.	0.	0.		
450.	0.	0.	0.		
455.	0.	0.	0.		
460.	0.	0.	0.		
465.	0.	0.	0.		
470.	0.	0.	0.		
475.	0.	0.	0.		
480.	0.	0.	0.		
485.	0.	0.	0.		
490.	0.	0.	0.		
495.	0.	0.	0.		
500.	0.	0.	0.		
505.	0.	0.	0.		
510.	0.	0.	0.		
515.	0.	0.	0.		</

DEFINE

20

BODY

MAY 20, 1967

BODY DEFINITION

TR-805/EQUIVALENT/BODY

THERE ARE 24 STATIONS AND 8 MERIDIAN LINES

THE MAIN BODY AXIS (PARALLEL TO THE X AXIS) IS LOCATED AT

Y = -0.0000 Z = -0.0000

CHORD-WEIGHT TOLERANCE = -0.0000

BODY STATION X = 0.0000 SCODE = 2.
 RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000)

MERIDIAN NO.	RHO	THETA	Y	Z
1	0.0000	0.0000	0.0000	0.0000
2	0.0000	25.0000	0.0000	0.0000
3	0.0000	50.0000	0.0000	0.0000
4	0.0000	75.0000	0.0000	0.0000
5	0.0000	102.1900	0.0000	-0.0000
6	0.0000	130.0000	0.0000	-0.0000
7	0.0000	155.0000	0.0000	-0.0000
8	0.0000	180.0000	0.0000	-0.0000

BODY STATION X = 1.5000 SCODE = 2.
 RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000)

MERIDIAN NO.	RHO	THETA	Y	Z
1	0.2700	0.0000	0.0000	0.2700
2	0.2700	25.0000	0.1141	0.2447
3	0.2700	50.0000	0.2068	0.1736
4	0.2700	75.0000	0.2608	0.0699
5	0.2700	102.1900	0.2639	-0.0570
6	0.2700	130.0000	0.2068	-0.1736
7	0.2700	155.0000	0.1141	-0.2447
8	0.2700	180.0000	0.0000	-0.2700

BODY STATION X = 3.0000 SCODE = 2.
 RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000)

MERIDIAN NO.	RHO	THETA	Y	Z
1	0.4464	0.0000	0.0000	0.4464
2	0.4464	25.0000	0.1887	0.4046
3	0.4464	50.0000	0.3420	0.2869
4	0.4464	75.0000	0.4312	0.1155
5	0.4464	102.1900	0.4363	-0.0943
6	0.4464	130.0000	0.3420	-0.2869
7	0.4464	155.0000	0.1887	-0.4046
8	0.4464	180.0000	0.0000	-0.4464

TR-805/EQUIVALENT/BODY

MAY 20, 1967

BODY STATION X = 4.5000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	0.5943	0.0000	0.0000	0.5943
2	0.5943	25.0000	0.2512	0.5386
3	0.5943	50.0000	0.4553	0.3820
4	0.5943	75.0000	0.5740	0.1538
5	0.5943	102.1900	0.5809	-0.1255
6	0.5943	130.0000	0.4553	-0.3820
7	0.5943	155.0000	0.2512	-0.5386
8	0.5943	180.0000	0.0000	-0.5943

BODY STATION X = 6.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	0.7234	0.0000	0.0000	0.7234
2	0.7234	25.0000	0.3057	0.6556
3	0.7234	50.0000	0.5542	0.4650
4	0.7234	75.0000	0.6988	0.1872
5	0.7234	102.1900	0.7071	-0.1527
6	0.7234	130.0000	0.5542	-0.4650
7	0.7234	155.0000	0.3057	-0.6556
8	0.7234	180.0000	0.0000	-0.7234

BODY STATION X = 7.5000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	0.8370	0.0000	0.0000	0.8370
2	0.8370	25.0000	0.3537	0.7586
3	0.8370	50.0000	0.5412	0.5380
4	0.8370	75.0000	0.8085	0.2166
5	0.8370	102.1900	0.8181	-0.1767
6	0.8370	130.0000	0.6412	-0.5380
7	0.8370	155.0000	0.3537	-0.7586
8	0.8370	180.0000	0.0000	-0.8370

BODY STATION X = 9.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	0.9364	0.0000	0.0000	0.9364
2	0.9364	25.0000	0.3957	0.8487
3	0.9364	50.0000	0.7173	0.6019
4	0.9364	75.0000	0.9045	0.2424
5	0.9364	102.1900	0.9153	-0.1977
6	0.9364	130.0000	0.7173	-0.6019
7	0.9364	155.0000	0.3957	-0.8487
8	0.9364	180.0000	0.0000	-0.9364

MAY 20, 1967

BODY STATION X = 10.5000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.0223	0.0000	0.0000	1.0223
2	1.0223	25.0000	0.4320	0.9265
3	1.0223	50.0000	0.7831	0.6571
4	1.0223	75.0000	0.9875	0.2646
5	1.0223	102.1900	0.9992	-0.2159
6	1.0223	130.0000	0.7831	-0.6571
7	1.0223	155.0000	0.4320	-0.9265
8	1.0223	180.0000	0.0000	-1.0223

BODY STATION X = 12.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.0936	0.0000	0.0000	1.0936
2	1.0936	25.0000	0.4622	0.9911
3	1.0936	50.0000	0.8377	0.7030
4	1.0936	75.0000	1.0563	0.2830
5	1.0936	102.1900	1.0689	-0.2309
6	1.0936	130.0000	0.8377	-0.7030
7	1.0936	155.0000	0.4622	-0.9911
8	1.0936	180.0000	0.0000	-1.0936

BODY STATION X = 13.5000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1479	0.0000	0.0000	1.1479
2	1.1479	25.0000	0.4851	1.0404
3	1.1479	50.0000	0.8793	0.7379
4	1.1479	75.0000	1.1088	0.2971
5	1.1479	102.1900	1.1220	-0.2424
6	1.1479	130.0000	0.8793	-0.7379
7	1.1479	155.0000	0.4851	-1.0404
8	1.1479	180.0000	0.0000	-1.1479

BODY STATION X = 15.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1840	0.0000	0.0000	1.1840
2	1.1840	25.0000	0.5004	1.0731
3	1.1840	50.0000	0.9070	0.7611
4	1.1840	75.0000	1.1437	0.3064
5	1.1840	102.1900	1.1573	-0.2500
6	1.1840	130.0000	0.9070	-0.7611
7	1.1840	155.0000	0.5004	-1.0731
8	1.1840	180.0000	0.0000	-1.1840

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BODY STATION X = 15.1000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 0.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1840	0.0000	0.0000	1.1840
2	1.1840	25.0000	0.5004	1.0731
3	1.1840	50.0000	0.9070	0.7611
4	1.1840	75.0000	1.1437	0.3064
5	1.1840	102.1900	1.1573	-0.2500
6	1.1840	130.0000	0.9070	-0.7611
7	1.1840	155.0000	0.5004	-1.0731
8	1.1840	180.0000	0.0000	-1.1840

BODY STATION X = 17.5000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 0.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1840	0.0000	0.0000	1.1840
2	1.1840	25.0000	0.5004	1.0731
3	1.1840	50.0000	0.9070	0.7611
4	1.1840	75.0000	1.1437	0.3064
5	1.1840	102.1900	1.1573	-0.2500
6	1.1840	130.0000	0.9070	-0.7611
7	1.1840	155.0000	0.5004	-1.0731
8	1.1840	180.0000	0.0000	-1.1840

BODY STATION X = 20.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 0.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1840	0.0000	0.0000	1.1840
2	1.1840	25.0000	0.5004	1.0731
3	1.1840	50.0000	0.9070	0.7611
4	1.1840	75.0000	1.1437	0.3064
5	1.1840	102.1900	1.1573	-0.2500
6	1.1840	130.0000	0.9070	-0.7611
7	1.1840	155.0000	0.5004	-1.0731
8	1.1840	180.0000	0.0000	-1.1840

BODY STATION X = 22.5000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 0.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1840	0.0000	0.0000	1.1840
2	1.1840	25.0000	0.5004	1.0731
3	1.1840	50.0000	0.9070	0.7611
4	1.1840	75.0000	1.1437	0.3064
5	1.1840	102.1900	1.1573	-0.2500
6	1.1840	130.0000	0.9070	-0.7611
7	1.1840	155.0000	0.5004	-1.0731
8	1.1840	180.0000	0.0000	-1.1840

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BODY STATION X = 25.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 0.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1840	0.0000	0.0000	1.1840
2	1.1840	25.0000	0.5004	1.0731
3	1.1840	50.0000	0.9070	0.7611
4	1.1840	75.0000	1.1437	0.3064
5	1.1840	102.1900	1.1573	-0.2500
6	1.1840	130.0000	0.9070	-0.7611
7	1.1840	155.0000	0.5004	-1.0731
8	1.1840	180.0000	0.0000	-1.1840

BODY STATION X = 27.5000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 0.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1840	0.0000	0.0000	1.1840
2	1.1840	25.0000	0.5004	1.0731
3	1.1840	50.0000	0.9070	0.7611
4	1.1840	75.0000	1.1437	0.3064
5	1.1840	102.1900	1.1573	-0.2500
6	1.1840	130.0000	0.9070	-0.7611
7	1.1840	155.0000	0.5004	-1.0731
8	1.1840	180.0000	0.0000	-1.1840

BODY STATION X = 29.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 0.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1840	0.0000	0.0000	1.1840
2	1.1840	25.0000	0.5004	1.0731
3	1.1840	50.0000	0.9070	0.7611
4	1.1840	75.0000	1.1437	0.3064
5	1.1840	102.1900	1.1573	-0.2500
6	1.1840	130.0000	0.9070	-0.7611
7	1.1840	155.0000	0.5004	-1.0731
8	1.1840	180.0000	0.0000	-1.1840

BODY STATION X = 31.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1740	0.0000	0.0000	1.1740
2	1.1740	25.0000	0.4962	1.0640
3	1.1740	50.0000	0.8993	0.7546
4	1.1740	75.0000	1.1340	0.3039
5	1.1740	102.1900	1.1475	-0.2479
6	1.1740	130.0000	0.8993	-0.7546
7	1.1740	155.0000	0.4962	-1.0640
8	1.1740	180.0000	0.0000	-1.1740

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BODY STATION X = 32.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1540	0.0000	0.0000	1.1540
2	1.1540	25.0000	0.4877	1.0459
3	1.1540	50.0000	0.8840	0.7418
4	1.1540	75.0000	1.1147	0.2987
5	1.1540	102.1900	1.1280	-0.2437
6	1.1540	130.0000	0.8840	-0.7418
7	1.1540	155.0000	0.4877	-1.0459
8	1.1540	180.0000	0.0000	-1.1540

BODY STATION X = 33.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.1240	0.0000	0.0000	1.1240
2	1.1240	25.0000	0.4750	1.0187
3	1.1240	50.0000	0.8610	0.7225
4	1.1240	75.0000	1.0857	0.2409
5	1.1240	102.1900	1.0987	-0.2373
6	1.1240	130.0000	0.8610	-0.7225
7	1.1240	155.0000	0.4750	-1.0187
8	1.1240	180.0000	0.0000	-1.1240

BODY STATION X = 34.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.0840	0.0000	0.0000	1.0840
2	1.0840	25.0000	0.4581	0.9824
3	1.0840	50.0000	0.8304	0.6968
4	1.0840	75.0000	1.0471	0.2806
5	1.0840	102.1900	1.0596	-0.2289
6	1.0840	130.0000	0.8304	-0.6968
7	1.0840	155.0000	0.4581	-0.9824
8	1.0840	180.0000	0.0000	-1.0840

BODY STATION X = 35.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.0340	0.0000	0.0000	1.0340
2	1.0340	25.0000	0.4370	0.9371
3	1.0340	50.0000	0.7921	0.6646
4	1.0340	75.0000	0.9986	0.2676
5	1.0340	102.1900	1.0107	-0.2183
6	1.0340	130.0000	0.7921	-0.6646
7	1.0340	155.0000	0.4370	-0.9371
8	1.0340	180.0000	0.0000	-1.0340

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BODY STATION X = 36.0000
RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000) SCODE = 2.

MERIDIAN NO.	RHO	THETA	Y	Z
1	1.0000	0.0000	0.0000	1.0000
2	1.0000	25.0000	0.4226	0.9063
3	1.0000	50.0000	0.7660	0.6428
4	1.0000	75.0000	0.9659	0.2588
5	1.0000	102.1900	0.9775	-0.2112
6	1.0000	130.0000	0.7660	-0.6428
7	1.0000	155.0000	0.4226	-0.9063
8	1.0000	180.0000	0.0000	-1.0000

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BODY MERIDIAN LINE 1							
	X	Y	Z	RHO	THETA		
1	0.0000	0.0000	0.0000	0.0000	0.0000		
2	1.5000	0.0000	0.2700	0.2700	0.0000		
3	3.0000	0.0000	0.4464	0.4464	0.0000		
4	4.5000	0.0000	0.5943	0.5943	0.0000		
5	6.0000	0.0000	0.7234	0.7234	0.0000		
6	7.5000	0.0000	0.8370	0.8370	0.0000		
7	9.0000	0.0000	0.9364	0.9364	0.0000		
8	10.5000	0.0000	1.0223	1.0223	0.0000		
9	12.0000	0.0000	1.0936	1.0936	0.0000		
10	13.5000	0.0000	1.1479	1.1479	0.0000		
11	15.0000	0.0000	1.1840	1.1840	0.0000		
12	15.1000	0.0000	1.1840	1.1840	0.0000		
13	17.5000	0.0000	1.1840	1.1840	0.0000		
14	20.0000	0.0000	1.1840	1.1840	0.0000		
15	22.5000	0.0000	1.1840	1.1840	0.0000		
16	25.0000	0.0000	1.1840	1.1840	0.0000		
17	27.5000	0.0000	1.1840	1.1840	0.0000		
18	29.9000	0.0000	1.1840	1.1840	0.0000		
19	31.0000	0.0000	1.1740	1.1740	0.0000		
20	32.0000	0.0000	1.1540	1.1540	0.0000		
21	33.0000	0.0000	1.1240	1.1240	0.0000		
22	34.0000	0.0000	1.0840	1.0840	0.0000		
23	35.0000	0.0000	1.0340	1.0340	0.0000		
24	36.0000	0.0000	1.0000	1.0000	0.0000		

BODY MERIDIAN LINE 2							
	X	Y	Z	RHO	THETA		
1	0.0000	0.0000	0.0000	0.0000	0.0000		
2	1.5000	0.1141	0.2447	0.2700	25.0000		
3	3.0000	0.1887	0.4046	0.4464	25.0000		
4	4.5000	0.2512	0.5386	0.5943	25.0000		
5	6.0000	0.3057	0.6556	0.7234	25.0000		
6	7.5000	0.3537	0.7586	0.8370	25.0000		
7	9.0000	0.3957	0.8487	0.9364	25.0000		
8	10.5000	0.4320	0.9265	1.0223	25.0000		
9	12.0000	0.4622	0.9911	1.0936	25.0000		
10	13.5000	0.4851	1.0404	1.1479	25.0000		
11	15.0000	0.5004	1.0731	1.1840	25.0000		
12	15.1000	0.5004	1.0731	1.1840	25.0000		
13	17.5000	0.5004	1.0731	1.1840	25.0000		
14	20.0000	0.5004	1.0731	1.1840	25.0000		
15	22.5000	0.5004	1.0731	1.1840	25.0000		
16	25.0000	0.5004	1.0731	1.1840	25.0000		
17	27.5000	0.5004	1.0731	1.1840	25.0000		
18	29.9000	0.5004	1.0731	1.1840	25.0000		
19	31.0000	0.4962	1.0640	1.1740	25.0000		
20	32.0000	0.4877	1.0459	1.1540	25.0000		
21	33.0000	0.4750	1.0187	1.1240	25.0000		
22	34.0000	0.4581	0.9824	1.0840	25.0000		
23	35.0000	0.4370	0.9371	1.0340	25.0000		
24	36.0000	0.4226	0.9063	1.0000	25.0000		

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BODY MERIDIAN LINE 3							
	X	Y	Z	RHO	THETA		
1	0.0000	0.0000	0.0000	0.0000	0.0000		
2	1.5000	0.2068	0.1736	0.2700	50.0000		
3	3.0000	0.3420	0.2869	0.4464	50.0000		
4	4.5000	0.4553	0.3820	0.5943	50.0000		
5	6.0000	0.5542	0.4650	0.7234	50.0000		
6	7.5000	0.6412	0.5380	0.8370	50.0000		
7	9.0000	0.7173	0.6019	0.9364	50.0000		
8	10.5000	0.7831	0.6571	1.0223	50.0000		
9	12.0000	0.8377	0.7020	1.0936	50.0000		
10	13.5000	0.8793	0.7379	1.1479	50.0000		
11	15.0000	0.9070	0.7611	1.1840	50.0000		
12	15.1000	0.9070	0.7611	1.1840	50.0000		
13	17.5000	0.9070	0.7611	1.1840	50.0000		
14	20.0000	0.9070	0.7611	1.1840	50.0000		
15	22.5000	0.9070	0.7611	1.1840	50.0000		
16	25.0000	0.9070	0.7611	1.1840	50.0000		
17	27.5000	0.9070	0.7611	1.1840	50.0000		
18	29.9000	0.9070	0.7611	1.1840	50.0000		
19	31.0000	0.8993	0.7546	1.1740	50.0000		
20	32.0000	0.8840	0.7418	1.1540	50.0000		
21	33.0000	0.8610	0.7225	1.1240	50.0000		
22	34.0000	0.8304	0.6968	1.0840	50.0000		
23	35.0000	0.7921	0.6646	1.0340	50.0000		
24	36.0000	0.7660	0.6428	1.0000	50.0000		

BODY MERIDIAN LINE 4							
	X	Y	Z	RHO	THETA		
1	0.0000	0.0000	0.0000	0.0000	0.0000		
2	1.5000	0.2608	0.0699	0.2700	75.0000		
3	3.0000	0.4312	0.1155	0.4464	75.0000		
4	4.5000	0.5740	0.1538	0.5943	75.0000		
5	6.0000	0.6988	0.1872	0.7234	75.0000		
6	7.5000	0.8085	0.2166	0.8370	75.0000		
7	9.0000	0.9045	0.2424	0.9364	75.0000		
8	10.5000	0.9875	0.2646	1.0223	75.0000		
9	12.0000	1.0563	0.2830	1.0936	75.0000		
10	13.5000	1.1088	0.2971	1.1479	75.0000		
11	15.0000	1.1437	0.3064	1.1840	75.0000		
12	15.1000	1.1437	0.3064	1.1840	75.0000		
13	17.5000	1.1437	0.3064	1.1840	75.0000		
14	20.0000	1.1437	0.3064	1.1840	75.0000		
15	22.5000	1.1437	0.3064	1.1840	75.0000		
16	25.0000	1.1437	0.3064	1.1840	75.0000		
17	27.5000	1.1437	0.3064	1.1840	75.0000		
18	29.9000	1.1437	0.3064	1.1840	75.0000		
19	31.0000	1.1340	0.3039	1.1740	75.0000		
20	32.0000	1.1147	0.2987	1.1540	75.0000		
21	33.0000	1.0857	0.2909	1.1240	75.0000		
22	34.0000	1.0471	0.2806	1.0840	75.0000		
23	35.0000	0.9988	0.2676	1.0340	75.0000		
24	36.0000	0.9659	0.2598	1.0000	75.0000		

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BODY MERIDIAN LINE	5	X	Y	Z	RHO	THETA
1	0.0000	0.0000	-0.0000	*	0.0000	0.0000
2	1.5000	0.2639	-0.0570	*	0.2700	102.1900
3	3.0000	0.4363	-0.0943	*	0.4464	102.1900
4	4.5000	0.5809	-0.1255	*	0.5943	102.1900
5	6.0000	0.7071	-0.1527	*	0.7234	102.1900
6	7.5000	0.8181	-0.1767	*	0.8370	102.1900
7	9.0000	0.9153	-0.1977	*	0.9364	102.1900
8	10.5000	0.9992	-0.2159	*	1.0223	102.1900
9	12.0000	1.0689	-0.2309	*	1.0936	102.1900
10	13.5000	1.1220	-0.2424	*	1.1479	102.1900
11	15.0000	1.1573	-0.2500	*	1.1840	102.1900
12	16.5000	1.1573	-0.2500	*	1.1840	102.1900
13	18.0000	1.1573	-0.2500	*	1.1840	102.1900
14	19.5000	1.1573	-0.2500	*	1.1840	102.1900
15	21.0000	1.1573	-0.2500	*	1.1840	102.1900
16	22.5000	1.1573	-0.2500	*	1.1840	102.1900
17	24.0000	1.1573	-0.2500	*	1.1840	102.1900
18	25.5000	1.1573	-0.2500	*	1.1840	102.1900
19	27.0000	1.1573	-0.2500	*	1.1840	102.1900
20	28.5000	1.1573	-0.2500	*	1.1840	102.1900
21	30.0000	1.1573	-0.2500	*	1.1840	102.1900
22	31.5000	1.1573	-0.2500	*	1.1840	102.1900
23	33.0000	1.1573	-0.2500	*	1.1840	102.1900
24	34.5000	1.1573	-0.2500	*	1.1840	102.1900

BODY MERIDIAN LINE	6	X	Y	Z	RHO	THETA
1	0.0000	0.0000	-0.0000	*	0.0000	0.0000
2	1.5000	0.2068	-0.1734	*	0.2700	130.0000
3	3.0000	0.3420	-0.2869	*	0.4464	130.0000
4	4.5000	0.4553	-0.3820	*	0.5943	130.0000
5	6.0000	0.5542	-0.4650	*	0.7234	130.0000
6	7.5000	0.6412	-0.5390	*	0.8370	130.0000
7	9.0000	0.7173	-0.6019	*	0.9364	130.0000
8	10.5000	0.7831	-0.6571	*	1.0223	130.0000
9	12.0000	0.8377	-0.7030	*	1.0936	130.0000
10	13.5000	0.8793	-0.7379	*	1.1479	130.0000
11	15.0000	0.9070	-0.7611	*	1.1840	130.0000
12	16.5000	0.9070	-0.7611	*	1.1840	130.0000
13	18.0000	0.9070	-0.7611	*	1.1840	130.0000
14	19.5000	0.9070	-0.7611	*	1.1840	130.0000
15	21.0000	0.9070	-0.7611	*	1.1840	130.0000
16	22.5000	0.9070	-0.7611	*	1.1840	130.0000
17	24.0000	0.9070	-0.7611	*	1.1840	130.0000
18	25.5000	0.9070	-0.7611	*	1.1840	130.0000
19	27.0000	0.9070	-0.7611	*	1.1840	130.0000
20	28.5000	0.9070	-0.7611	*	1.1840	130.0000
21	30.0000	0.9070	-0.7611	*	1.1840	130.0000
22	31.5000	0.9070	-0.7611	*	1.1840	130.0000
23	33.0000	0.9070	-0.7611	*	1.1840	130.0000
24	34.5000	0.9070	-0.7611	*	1.1840	130.0000

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BODY MERIDIAN LINE	X	Y	Z	RHO	THETA
1	0.0000	0.0000	-0.0000	0.0000	0.0000
2	1.5000	0.1141	-0.2447	0.2700	155.0000
3	3.0000	0.1887	-0.4066	0.4464	155.0000
4	4.5000	0.2512	-0.5386	0.5943	155.0000
5	6.0000	0.3057	-0.6536	0.7234	155.0000
6	7.5000	0.3537	-0.7596	0.8370	155.0000
7	9.0000	0.3957	-0.8487	0.9364	155.0000
8	10.5000	0.4320	-0.9265	1.0223	155.0000
9	12.0000	0.4622	-0.9911	1.0936	155.0000
10	13.5000	0.4851	-1.0404	1.1479	155.0000
11	15.0000	0.5004	-1.0731	1.1840	155.0000
12	15.1000	0.5004	-1.0731	1.1840	155.0000
13	17.5000	0.5004	-1.0731	1.1840	155.0000
14	20.0000	0.5004	-1.0731	1.1840	155.0000
15	22.5000	0.5004	-1.0731	1.1840	155.0000
16	25.0000	0.5004	-1.0731	1.1840	155.0000
17	27.5000	0.5004	-1.0731	1.1840	155.0000
18	29.9000	0.5004	-1.0731	1.1840	155.0000
19	31.0000	0.4962	-1.0640	1.1740	155.0000
20	33.0000	0.4977	-1.0459	1.1540	155.0000
21	33.0000	0.4750	-1.0187	1.1240	155.0000
22	34.0000	0.4581	-0.9824	1.0840	155.0000
23	35.0000	0.4370	-0.9371	1.0340	155.0000
24	36.0000	0.4226	-0.9063	1.0000	155.0000

BODY MERIDIAN LINE	X	Y	Z	RHO	THETA
1	0.0000	0.0000	-0.0000	0.0000	0.0000
2	1.5000	0.0000	-0.2700	0.2700	180.0000
3	3.0000	0.0000	-0.4464	0.4464	180.0000
4	4.5000	0.0000	-0.5943	0.5943	180.0000
5	6.0000	0.0000	-0.7234	0.7234	180.0000
6	7.5000	0.0000	-0.8370	0.8370	180.0000
7	9.0000	0.0000	-0.9364	0.9364	180.0000
8	10.5000	0.0000	-1.0223	1.0223	180.0000
9	12.0000	0.0000	-1.0936	1.0936	180.0000
10	13.5000	0.0000	-1.1479	1.1479	180.0000
11	15.0000	0.0000	-1.1840	1.1840	180.0000
12	15.1000	0.0000	-1.1840	1.1840	180.0000
13	17.5000	0.0000	-1.1840	1.1840	180.0000
14	20.0000	0.0000	-1.1840	1.1840	180.0000
15	22.5000	0.0000	-1.1840	1.1840	180.0000
16	25.0000	0.0000	-1.1840	1.1840	180.0000
17	27.5000	0.0000	-1.1840	1.1840	180.0000
18	29.9000	0.0000	-1.1840	1.1840	180.0000
19	31.0000	0.0000	-1.1740	1.1740	180.0000
20	33.0000	0.0000	-1.1540	1.1540	180.0000
21	33.0000	0.0000	-1.1240	1.1240	180.0000
22	34.0000	0.0000	-1.0840	1.0840	180.0000
23	35.0000	0.0000	-1.0340	1.0340	180.0000
24	36.0000	0.0000	-1.0000	1.0000	180.0000

100

WING

WING DEFINITION

MAY 20, 1967

TR-805 WING(TWP=-.25)

THE PLANFORM HAS 2 POINTS ON THE LEADING EDGE,
3 POINTS ON THE TRAILING EDGE.

4 AIRFOILS ARE GIVEN. 11 PERCENT LINES ARE TO BE GENERATED.

PCODE = 1., ACODE = 1., EPS = 0.010000, CHD = -0.0000
UPPER WING SURFACE IS DEFINED

PLANFORM LEADING EDGE POINTS (GIVEN) ARE (X,Y) =
10.6700 0.0000 40.2700 10.7740

PLANFORM TRAILING EDGE POINTS (GIVEN) ARE (X,Y) = 40.2700 10.7740
19.8800 0.0000 43.5180 8.6030

AIRFOIL NO. 1 AFANG = 0.0000, YL = 0.0000, YT = 0.0000
AFK = 3., AFNL = -0.
AFNU = 2.,
LEADING AND TRAILING EDGE POINTS (X,Y) ARE
10.6700 0.0000 19.8800 0.0000
CHORD LENGTH = 9.2100

THE GIVEN 2 UPPER AIRFOIL POINTS ARE
XWING YWING
0.0000 -0.2500
9.2100 -0.2500

AIRFOIL POINTS AFTER SCALING TO FIT ON PLANFORM ARE
XWING (SCALED)
0.0000 -0.2500
9.2100 -0.2500

AIRFOIL NO. 2 AFANG = 0.0000, YL = 5.0000, YT = 0.0000
AFK = 1., AFNL = -0.
AFNU = 0.,
LEADING AND TRAILING EDGE POINTS (X,Y) ARE
24.4068 5.0000 33.6182 5.0000
CHORD LENGTH = 9.2115

THE GIVEN UPPER AIRFOIL IS THE SAME AS PRECEDING ONE

AIRFOIL POINTS AFTER SCALING TO FIT ON PLANFORM ARE
XWING (SCALED)
0.0000 -0.2500
9.2115 -0.2500

WING DEFINITION

MAY 20, 1967

TP-R05 WING(TWP=-.25)

AIRFOIL NO. 3
 AFK = 3.0 AFANG = -0.0000, YL = 8.6030, YT = 8.6030
 AFNU = 2.0 AFNL = -0.
 LEADING AND TRAILING EDGE POINTS (X,Y) ARE
 34.3055 8.6030 43.5180 8.6030
 CHORD LENGTH = 0.2125

THE GIVEN 2 UPPER AIRFOIL POINTS ARE
 XWING
 0.0000
 9.2100
 YWING
 -0.2500
 -0.2500

AIRFOIL POINTS AFTER SCALING TO FIT ON PLATFORM ARE
 XWING (SCALED)
 0.0000
 0.2125
 YWING
 -0.2501
 -0.2501

AIRFOIL NO. 4
 AFK = 3.0 AFANG = -0.0000, YL = 10.7740, YT = 10.7740
 AFNU = 2.0 AFNL = -0.
 LEADING AND TRAILING EDGE POINTS (X,Y) ARE
 40.2700 10.7740 40.2700 10.7740
 CHORD LENGTH = 0.0000

THE GIVEN 2 UPPER AIRFOIL POINTS ARE
 XWING
 0.0000
 0.0000
 YWING
 -0.2500
 -0.2500

THE AIRFOIL IS A POINT

PLATFORM LEADING EDGE POINTS (USED) ARE (X,Y) =
 10.5700 0.0000 24.4068 5.0000 34.3055 8.6030
 40.2700 10.7740

PLATFORM TRAILING EDGE POINTS (USED) ARE (X,Y) =
 19.8800 0.0000 33.6182 5.0000 43.5180 8.6030
 40.2700 10.7740

THE FOLLOWING PERCENT CHORD LINES ARE TO BE CONSTRUCTED
 0.0000 10.0000 20.0000 30.0000 40.0000 50.0000
 60.0000 70.0000 80.0000 90.0000 100.0000

TR-POS WING(TWP=-.25)
POINTS ON UPPER WING SURFACE PERCENT CHORD LINES MAY 20, 1967

WING PERCENT CHORD LINE 1, 0.0000 PERCENT
AF NO. X Y Z
1 10.6700 0.0000 -0.2500
2 24.4068 5.0000 -0.2500
3 34.3055 8.6030 -0.2501
4 40.2700 10.7740 -0.2500

WING PERCENT CHORD LINE 2, 10.0000 PERCENT
AF NO. X Y Z
1 11.5510 0.0000 -0.2500
2 25.3279 5.0000 -0.2500
3 35.2267 8.6030 -0.2501
4 40.2700 10.7740 -0.2500

WING PERCENT CHORD LINE 3, 20.0000 PERCENT
AF NO. X Y Z
1 12.5120 0.0000 -0.2500
2 26.2491 5.0000 -0.2500
3 36.1480 8.6030 -0.2501
4 40.2700 10.7740 -0.2500

WING PERCENT CHORD LINE 4, 30.0000 PERCENT
AF NO. X Y Z
1 13.4330 0.0000 -0.2500
2 27.1702 5.0000 -0.2500
3 37.0692 8.6030 -0.2501
4 40.2700 10.7740 -0.2500

WING PERCENT CHORD LINE 5, 40.0000 PERCENT
AF NO. X Y Z
1 14.3540 0.0000 -0.2500
2 28.0914 5.0000 -0.2500
3 37.9905 8.6030 -0.2501
4 40.2700 10.7740 -0.2500

WING PERCENT CHORD LINE 6, 50.0000 PERCENT
AF NO. X Y Z
1 15.2750 0.0000 -0.2500
2 29.0125 5.0000 -0.2500
3 38.9117 8.6030 -0.2501
4 40.2700 10.7740 -0.2500

WING PERCENT CHORD LINE 7, 60.0000 PERCENT
AF NO. X Y Z
1 16.1960 0.0000 -0.2500
2 29.9336 5.0000 -0.2500
3 39.8330 8.6030 -0.2501
4 40.2700 10.7740 -0.2500

TR-AOS WINGTMP--251
 POINTS ON UPPER WING SURFACE PERCENT CHORD LINES MAY 20, 1967

WING PERCENT CHORD LINE 8, 70.0000 PERCENT
 AF NO. X Y Z
 1 17.1170 0.0000 -0.2500
 2 30.8549 5.0000 -0.2500
 3 40.7542 8.6030 -0.2501
 4 40.2700 10.7740 -0.2500

WING PERCENT CHORD LINE 9, 80.0000 PERCENT
 AF NO. X Y Z
 1 18.0380 0.0000 -0.2500
 2 31.7759 5.0000 -0.2500
 3 41.6755 8.6030 -0.2501
 4 40.2700 10.7740 -0.2500

WING PERCENT CHORD LINE 10, 90.0000 PERCENT
 AF NO. X Y Z
 1 18.9590 0.0000 -0.2500
 2 32.6971 5.0000 -0.2500
 3 42.5967 8.6030 -0.2501
 4 40.2700 10.7740 -0.2500

WING PERCENT CHORD LINE 11, 100.0000 PERCENT
 AF NO. X Y Z
 1 19.9800 0.0000 -0.2500
 2 33.6182 5.0000 -0.2500
 3 43.5180 8.6030 -0.2501
 4 40.2700 10.7740 -0.2500

MRX

190

FIND THE INTERSECTION OF EACH WING PERCENT LINE WITH THE BODY SURFACE.

CODE = 2

TOLERANCE = 0.0001

LET P BE A POINT WHICH LIES ON THE BODY SURFACE
AND Q A POINT ON A LINE SEGMENT CONNECTING TWO ADJACENT
WING PERCENT LINE POINTS, SUCH THAT P AND Q HAVE THE SAME X-COORDINATE.

THE PROGRAM ITERATES UNTIL P AND Q HAVE THE SAME
TOP NEARLY THE SAME Y AND Z COORDINATES.
THEN P IS THE INTERSECTION POINT.

IF P AND Q DIFFER BY MORE THAN THE GIVEN TOLERANCE,
A WARNING MESSAGE IS WRITTEN.

THE SHAPE OF THE BODY SURFACE BETWEEN MERIDIAN LINES (IN ANY SECTION
PARALLEL TO THE YZ PLANE) IS DETERMINED BY THE GIVEN CODE.

IF CODE = 1, LINEAR INTERPOLATION IS USED BETWEEN MERIDIAN LINES.
IF CODE = 2, BICUBIC INTERPOLATION IS USED.

TP-805/EQUIVALENT/BODY
 TP-805 WING(TWO=-.25) MAY 20, 1967
 INTERSECTIONS OF UPPER WING PERCENT CHORD LINES WITH BODY SURFACE
 RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (-0.0000, -0.0000)

NO.	PERCENT	X	Y	Z	RHO	THETA
1	0.0000	13.7701	1.1284	-0.2500	1.1558	102.4926
2	10.0000	14.7548	1.1516	-0.2500	1.1784	102.2492
3	20.0000	15.6916	1.1573	-0.2500	1.1840	102.1901
4	30.0000	16.6126	1.1573	-0.2500	1.1840	102.1901
5	40.0000	17.5337	1.1573	-0.2500	1.1840	102.1901
6	50.0000	18.4547	1.1573	-0.2500	1.1840	102.1901
7	60.0000	19.3757	1.1573	-0.2500	1.1840	102.1901
8	70.0000	20.2968	1.1573	-0.2500	1.1840	102.1901
9	80.0000	21.2178	1.1573	-0.2500	1.1840	102.1901
10	90.0000	22.1384	1.1573	-0.2500	1.1840	102.1901
11	100.0000	23.0599	1.1573	-0.2500	1.1840	102.1901

DEFEND

220

PANEL

1P

TIME 01.574 052067

MAY 20, 1967
PROGRAM ENTERED LINK TO TRANSFORM BODY AND/OR WING BEFORE PANELLING

THE ORIGIN OF THE NEW BODY COORDINATE SYSTEM IS AT
(X,Y,Z) = (0.0000, 0.0000, 0.0000)

A UNIT VECTOR ALONG THE X-PRIME AXIS HAS COMPONENTS
(X,Y,Z) = (1.0000, 0.0000, 0.0000)

NO.	ORIGINAL BODY STATION	CIRCULARIZED BODY STATION	BODY RADIUS	Z-BODY CENTROID
1	0.0000	0.0000	0.0000	0.0000
2	1.5000	1.5000	0.2700	0.0000
3	3.0000	3.0000	0.4464	0.0000
4	4.5000	4.5000	0.5943	0.0000
5	6.0000	6.0000	0.7234	0.0000
6	7.5000	7.5000	0.8370	0.0000
7	9.0000	9.0000	0.9364	0.0000
8	10.5000	10.5000	1.0223	0.0000
9	12.0000	12.0000	1.0936	0.0000
10	13.5000	13.5000	1.1479	0.0000
11	15.0000	15.0000	1.1840	0.0000
12	15.1000	15.1000	1.1840	0.0000
13	17.5000	17.5000	1.1840	0.0000
14	20.0000	20.0000	1.1840	0.0000
15	22.5000	22.5000	1.1840	0.0000
16	25.0000	25.0000	1.1840	0.0000
17	27.5000	27.5000	1.1840	0.0000
18	29.9000	29.9000	1.1840	0.0000
19	31.0000	31.0000	1.1740	0.0000
20	32.0000	32.0000	1.1540	0.0000
21	33.0000	33.0000	1.1240	0.0000
22	34.0000	34.0000	1.0840	0.0000
23	35.0000	35.0000	1.0340	0.0000
24	36.0000	36.0000	1.0000	0.0000

TRANSFORMED BODY (PRIMED-AXIS SYSTEM)

MAY 20, 1967

BODY MERIDIAN LINE	1	Y	Z	RHO	THETA
1	0.0000	0.0000	0.0000	0.0000	0.0000
2	1.5000	-0.0000	0.2700	0.2700	0.0000
3	3.0000	-0.0000	0.4464	0.4464	0.0000
4	4.5000	-0.0000	0.5943	0.5943	0.0000
5	6.0000	-0.0000	0.7234	0.7234	0.0000
6	7.5000	-0.0000	0.8370	0.8370	0.0000
7	9.0000	-0.0000	0.9364	0.9364	0.0000
8	10.5000	-0.0000	1.0223	1.0223	0.0000
9	12.0000	-0.0000	1.0936	1.0936	0.0000
10	13.5000	-0.0000	1.1479	1.1479	0.0000
11	15.0000	-0.0000	1.1840	1.1840	0.0000
12	16.5000	-0.0000	1.1840	1.1840	0.0000
13	17.5000	-0.0000	1.1840	1.1840	0.0000
14	20.0000	-0.0000	1.1840	1.1840	0.0000
15	22.5000	-0.0000	1.1840	1.1840	0.0000
16	25.0000	-0.0000	1.1840	1.1840	0.0000
17	27.5000	-0.0000	1.1840	1.1840	0.0000
18	29.9000	-0.0000	1.1840	1.1840	0.0000
19	31.0000	-0.0000	1.1740	1.1740	0.0000
20	32.0000	-0.0000	1.1540	1.1540	0.0000
21	33.0000	-0.0000	1.1240	1.1240	0.0000
22	34.0000	-0.0000	1.0840	1.0840	0.0000
23	35.0000	-0.0000	1.0340	1.0340	0.0000
24	36.0000	-0.0000	1.0000	1.0000	0.0000

BODY MERIDIAN LINE	2	Y	Z	RHO	THETA
1	0.0000	0.0000	0.0000	0.0000	0.0000
2	1.5000	0.1141	0.2467	0.2700	25.0000
3	3.0000	0.1897	0.4046	0.4464	25.0000
4	4.5000	0.2512	0.5386	0.5943	25.0000
5	6.0000	0.3057	0.6556	0.7234	25.0000
6	7.5000	0.3537	0.7586	0.8370	25.0000
7	9.0000	0.3957	0.8487	0.9364	25.0000
8	10.5000	0.4320	0.9285	1.0223	25.0000
9	12.0000	0.4622	0.9911	1.0936	25.0000
10	13.5000	0.4851	1.0404	1.1479	25.0000
11	15.0000	0.5004	1.0731	1.1840	25.0000
12	16.5000	0.5004	1.0731	1.1840	25.0000
13	17.5000	0.5004	1.0731	1.1840	25.0000
14	20.0000	0.5004	1.0731	1.1840	25.0000
15	22.5000	0.5004	1.0731	1.1840	25.0000
16	25.0000	0.5004	1.0731	1.1840	25.0000
17	27.5000	0.5004	1.0731	1.1840	25.0000
18	29.9000	0.5004	1.0731	1.1840	25.0000
19	31.0000	0.4962	1.0640	1.1740	25.0000
20	32.0000	0.4877	1.0459	1.1540	25.0000
21	33.0000	0.4750	1.0187	1.1240	25.0000
22	34.0000	0.4581	0.9824	1.0840	25.0000
23	35.0000	0.4370	0.9371	1.0340	25.0000
24	36.0000	0.4226	0.9063	1.0000	25.0000

TRANSFORMED BODY (PRIMED-AXIS SYSTEM)

MAY 20, 1967

BODY MERIDIAN LINE 3				7		THETA	
X	Y	Z	RHO	THETA	RHO	THETA	RHO
1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	1.5000	0.2068	0.1736	0.1736	0.2700	50.0000	50.0000
3	3.0000	0.3420	0.2869	0.2869	0.4464	50.0000	50.0000
4	4.5000	0.4553	0.3820	0.3820	0.5943	50.0000	50.0000
5	6.0000	0.5442	0.4650	0.4650	0.7234	50.0000	50.0000
6	7.5000	0.6412	0.5380	0.5380	0.8370	50.0000	50.0000
7	9.0000	0.7173	0.6019	0.6019	0.9364	50.0000	50.0000
8	10.5000	0.7831	0.6571	0.6571	1.0223	50.0000	50.0000
9	12.0000	0.8377	0.7030	0.7030	1.0936	50.0000	50.0000
10	13.5000	0.8793	0.7379	0.7379	1.1479	50.0000	50.0000
11	15.0000	0.9070	0.7611	0.7611	1.1840	50.0000	50.0000
12	15.1000	0.9070	0.7611	0.7611	1.1840	50.0000	50.0000
13	17.5000	0.9070	0.7611	0.7611	1.1840	50.0000	50.0000
14	20.0000	0.9070	0.7611	0.7611	1.1840	50.0000	50.0000
15	22.5000	0.9070	0.7611	0.7611	1.1840	50.0000	50.0000
16	25.0000	0.9070	0.7611	0.7611	1.1840	50.0000	50.0000
17	27.5000	0.9070	0.7611	0.7611	1.1840	50.0000	50.0000
18	29.9000	0.8993	0.7546	0.7546	1.1740	50.0000	50.0000
19	31.0000	0.8840	0.7418	0.7418	1.1540	50.0000	50.0000
20	32.0000	0.8610	0.7225	0.7225	1.1240	50.0000	50.0000
21	33.0000	0.8304	0.6968	0.6968	1.0840	50.0000	50.0000
22	34.0000	0.7921	0.6646	0.6646	1.0340	50.0000	50.0000
23	35.0000	0.7492	0.6276	0.6276	0.9840	50.0000	50.0000
24	36.0000	0.7060	0.5888	0.5888	0.9340	50.0000	50.0000

BODY MERIDIAN LINE 4				7		THETA	
X	Y	Z	RHO	THETA	RHO	THETA	RHO
1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	1.5000	0.2608	0.2608	0.2608	0.2700	75.0000	75.0000
3	3.0000	0.4312	0.4312	0.4312	0.4464	75.0000	75.0000
4	4.5000	0.5740	0.5740	0.5740	0.5943	75.0000	75.0000
5	6.0000	0.6988	0.6988	0.6988	0.7234	75.0000	75.0000
6	7.5000	0.8085	0.8085	0.8085	0.8370	75.0000	75.0000
7	9.0000	0.9045	0.9045	0.9045	0.9364	75.0000	75.0000
8	10.5000	0.9875	0.9875	0.9875	1.0223	75.0000	75.0000
9	12.0000	1.0563	1.0563	1.0563	1.0936	75.0000	75.0000
10	13.5000	1.1088	1.1088	1.1088	1.1479	75.0000	75.0000
11	15.0000	1.1437	1.1437	1.1437	1.1840	75.0000	75.0000
12	15.1000	1.1437	1.1437	1.1437	1.1840	75.0000	75.0000
13	17.5000	1.1437	1.1437	1.1437	1.1840	75.0000	75.0000
14	20.0000	1.1437	1.1437	1.1437	1.1840	75.0000	75.0000
15	22.5000	1.1437	1.1437	1.1437	1.1840	75.0000	75.0000
16	25.0000	1.1437	1.1437	1.1437	1.1840	75.0000	75.0000
17	27.5000	1.1437	1.1437	1.1437	1.1840	75.0000	75.0000
18	29.9000	1.1437	1.1437	1.1437	1.1840	75.0000	75.0000
19	31.0000	1.1340	1.1340	1.1340	1.1740	75.0000	75.0000
20	32.0000	1.1147	1.1147	1.1147	1.1540	75.0000	75.0000
21	33.0000	1.0857	1.0857	1.0857	1.1240	75.0000	75.0000
22	34.0000	1.0471	1.0471	1.0471	1.0840	75.0000	75.0000
23	35.0000	0.9988	0.9988	0.9988	1.0340	75.0000	75.0000
24	36.0000	0.9459	0.9459	0.9459	0.9840	75.0000	75.0000

TRANSFORMED BODY (PRIMED-AXIS SYSTEM)

MAY 20, 1967

BODY MERIDIAN LINE 5							
	X	Y	Z		RHO	THETA	
1	-0.0000	-0.0000	-0.0000		0.0000	0.0000	
2	1.5000	0.2639	-0.0570		0.2700	102.1900	
3	3.0000	0.4363	-0.0943		0.4464	102.1900	
4	4.5000	0.5809	-0.1255		0.5943	102.1900	
5	6.0000	0.7071	-0.1527		0.7234	102.1900	
6	7.5000	0.8181	-0.1767		0.8370	102.1900	
7	9.0000	0.9153	-0.1977		0.9364	102.1900	
8	10.5000	0.9992	-0.2159		1.0223	102.1900	
9	12.0000	1.0689	-0.2309		1.0936	102.1900	
10	13.5000	1.1220	-0.2424		1.1479	102.1900	
11	15.0000	1.1573	-0.2500		1.1840	102.1900	
12	16.5000	1.1573	-0.2500		1.1840	102.1900	
13	17.5000	1.1573	-0.2500		1.1840	102.1900	
14	20.0000	1.1573	-0.2500		1.1840	102.1900	
15	22.5000	1.1573	-0.2500		1.1840	102.1900	
16	25.0000	1.1573	-0.2500		1.1840	102.1900	
17	27.5000	1.1573	-0.2500		1.1840	102.1900	
18	29.9000	1.1573	-0.2500		1.1840	102.1900	
19	31.0000	1.1475	-0.2479		1.1740	102.1900	
20	32.0000	1.1280	-0.2437		1.1540	102.1900	
21	33.0000	1.0987	-0.2373		1.1240	102.1900	
22	34.0000	1.0596	-0.2289		1.0840	102.1900	
23	35.0000	1.0107	-0.2183		1.0340	102.1900	
24	36.0000	0.9775	-0.2112		1.0000	102.1900	

BODY MERIDIAN LINE 6							
	X	Y	Z		RHO	THETA	
1	-0.0000	-0.0000	-0.0000		0.0000	0.0000	
2	1.5000	0.2068	-0.1736		0.2700	130.0000	
3	3.0000	0.3420	-0.2869		0.4464	130.0000	
4	4.5000	0.4553	-0.3820		0.5943	130.0000	
5	6.0000	0.5542	-0.4650		0.7234	130.0000	
6	7.5000	0.6412	-0.5380		0.8370	130.0000	
7	9.0000	0.7173	-0.6019		0.9364	130.0000	
8	10.5000	0.7831	-0.6571		1.0223	130.0000	
9	12.0000	0.8377	-0.7030		1.0936	130.0000	
10	13.5000	0.8793	-0.7379		1.1479	130.0000	
11	15.0000	0.9070	-0.7611		1.1840	130.0000	
12	15.1000	0.9070	-0.7611		1.1840	130.0000	
13	17.5000	0.9070	-0.7611		1.1840	130.0000	
14	20.0000	0.9070	-0.7611		1.1840	130.0000	
15	22.5000	0.9070	-0.7611		1.1840	130.0000	
16	25.0000	0.9070	-0.7611		1.1840	130.0000	
17	27.5000	0.9070	-0.7611		1.1840	130.0000	
18	29.9000	0.9070	-0.7611		1.1840	130.0000	
19	31.0000	0.8993	-0.7546		1.1740	130.0000	
20	32.0000	0.8840	-0.7418		1.1540	130.0000	
21	33.0000	0.8610	-0.7225		1.1240	130.0000	
22	34.0000	0.8304	-0.6968		1.0840	130.0000	
23	35.0000	0.7921	-0.6646		1.0340	130.0000	
24	36.0000	0.7660	-0.6428		1.0000	130.0000	

TRANSFORMED BODY (PRIME-Axis SYSTEM)

MAY 20, 1967

BODY MERIDIAN LINE 7				PHO		THETA	
	X	Y	Z				
1	-0.0000	-0.0000	-0.0000	0.0000	0.0000	0.0000	0.0000
2	1.5000	0.1141	-0.2447	0.2700	155.0000	155.0000	155.0000
3	3.0000	0.1887	-0.4046	0.4464	155.0000	155.0000	155.0000
4	4.5000	0.2512	-0.5386	0.5943	155.0000	155.0000	155.0000
5	6.0000	0.3057	-0.6556	0.7234	155.0000	155.0000	155.0000
6	7.5000	0.3537	-0.7586	0.8370	155.0000	155.0000	155.0000
7	9.0000	0.3957	-0.8487	0.9364	155.0000	155.0000	155.0000
8	10.5000	0.4320	-0.9265	1.0223	155.0000	155.0000	155.0000
9	12.0000	0.4622	-0.9911	1.0936	155.0000	155.0000	155.0000
10	13.5000	0.4951	-1.0404	1.1479	155.0000	155.0000	155.0000
11	15.0000	0.5004	-1.0731	1.1840	155.0000	155.0000	155.0000
12	15.1000	0.5004	-1.0731	1.1840	155.0000	155.0000	155.0000
13	17.5000	0.5004	-1.0731	1.1840	155.0000	155.0000	155.0000
14	20.0000	0.5004	-1.0731	1.1840	155.0000	155.0000	155.0000
15	22.5000	0.5004	-1.0731	1.1840	155.0000	155.0000	155.0000
16	25.0000	0.5004	-1.0731	1.1840	155.0000	155.0000	155.0000
17	27.5000	0.5004	-1.0731	1.1840	155.0000	155.0000	155.0000
18	29.9000	0.5004	-1.0731	1.1840	155.0000	155.0000	155.0000
19	31.0000	0.4962	-1.0640	1.1740	155.0000	155.0000	155.0000
20	32.0000	0.4877	-1.0459	1.1540	155.0000	155.0000	155.0000
21	33.0000	0.4750	-1.0187	1.1240	155.0000	155.0000	155.0000
22	34.0000	0.4581	-0.9824	1.0840	155.0000	155.0000	155.0000
23	35.0000	0.4370	-0.9371	1.0340	155.0000	155.0000	155.0000
24	36.0000	0.4226	-0.9063	1.0000	155.0000	155.0000	155.0000

BODY MERIDIAN LINE 8				PHO		THETA	
	X	Y	Z				
1	-0.0000	-0.0000	-0.0000	0.0000	0.0000	0.0000	0.0000
2	1.5000	0.0000	-0.2700	0.2700	180.0000	180.0000	180.0000
3	3.0000	0.0000	-0.4464	0.4464	180.0000	180.0000	180.0000
4	4.5000	0.0000	-0.5943	0.5943	180.0000	180.0000	180.0000
5	6.0000	0.0000	-0.7234	0.7234	180.0000	180.0000	180.0000
6	7.5000	0.0000	-0.8370	0.8370	180.0000	180.0000	180.0000
7	9.0000	0.0000	-0.9364	0.9364	180.0000	180.0000	180.0000
8	10.5000	0.0000	-1.0223	1.0223	180.0000	180.0000	180.0000
9	12.0000	0.0000	-1.0936	1.0936	180.0000	180.0000	180.0000
10	13.5000	0.0000	-1.1479	1.1479	180.0000	180.0000	180.0000
11	15.0000	0.0000	-1.1840	1.1840	180.0000	180.0000	180.0000
12	15.1000	0.0000	-1.1840	1.1840	180.0000	180.0000	180.0000
13	17.5000	0.0000	-1.1840	1.1840	180.0000	180.0000	180.0000
14	20.0000	0.0000	-1.1840	1.1840	180.0000	180.0000	180.0000
15	22.5000	0.0000	-1.1840	1.1840	180.0000	180.0000	180.0000
16	25.0000	0.0000	-1.1840	1.1840	180.0000	180.0000	180.0000
17	27.5000	0.0000	-1.1840	1.1840	180.0000	180.0000	180.0000
18	29.9000	0.0000	-1.1840	1.1840	180.0000	180.0000	180.0000
19	31.0000	0.0000	-1.1740	1.1740	180.0000	180.0000	180.0000
20	32.0000	0.0007	-1.1540	1.1540	180.0000	180.0000	180.0000
21	33.0000	0.0000	-1.1240	1.1240	180.0000	180.0000	180.0000
22	34.0000	0.0000	-1.0840	1.0840	180.0000	180.0000	180.0000
23	35.0000	0.0000	-1.0340	1.0340	180.0000	180.0000	180.0000
24	36.0000	0.0000	-1.0000	1.0000	180.0000	180.0000	180.0000

POINTS ON FLAT TRANSFORMED WING (PRIME-AXIS SYSTEM) MAY 20, 1967

WING PERCENT CHORD LINE 1, 0.0000

	X	Y	Z
1	10.6700	-0.0000	-0.2500
2	24.4068	5.0000	-0.2500
3	34.3055	8.6030	-0.2500
4	40.2700	10.7740	-0.2500

WING PERCENT CHORD LINE 2, 10.0000

	X	Y	Z
1	11.5910	-0.0000	-0.2500
2	25.3279	5.0000	-0.2500
3	35.2267	8.6030	-0.2500
4	40.2700	10.7740	-0.2500

WING PERCENT CHORD LINE 3, 20.0000

	X	Y	Z
1	12.5120	-0.0000	-0.2500
2	26.2491	5.0000	-0.2500
3	36.1480	8.6030	-0.2500
4	40.2700	10.7740	-0.2500

WING PERCENT CHORD LINE 4, 30.0000

	X	Y	Z
1	13.4330	-0.0000	-0.2500
2	27.1702	5.0000	-0.2500
3	37.0692	8.6030	-0.2500
4	40.2700	10.7740	-0.2500

WING PERCENT CHORD LINE 5, 40.0000

	X	Y	Z
1	14.3540	-0.0000	-0.2500
2	28.0914	5.0000	-0.2500
3	37.9905	8.6030	-0.2500
4	40.2700	10.7740	-0.2500

WING PERCENT CHORD LINE 6, 50.0000

	X	Y	Z
1	15.2750	-0.0000	-0.2500
2	29.0125	5.0000	-0.2500
3	38.9117	8.6030	-0.2500
4	40.2700	10.7740	-0.2500

POINTS ON FLAT TRANSFORMED WING (PRIME-Axis SYSTEM) MAY 20, 1967

WING PERCENT CHORD LINE 7, 60.0000

	X	Y	Z
1	16.1960	-0.0000	-0.2500
2	29.9236	5.0000	-0.2500
3	39.8330	8.6030	-0.2500
4	40.2700	10.7740	-0.2500

WING PERCENT CHORD LINE 8, 70.0000

	X	Y	Z
1	17.1170	-0.0000	-0.2500
2	30.8548	5.0000	-0.2500
3	40.7542	8.6030	-0.2500
4	40.2700	10.7740	-0.2500

WING PERCENT CHORD LINE 9, 80.0000

	X	Y	Z
1	18.0380	-0.0000	-0.2500
2	31.7759	5.0000	-0.2500
3	41.6755	8.6030	-0.2500
4	40.2700	10.7740	-0.2500

WING PERCENT CHORD LINE 10, 90.0000

	X	Y	Z
1	18.9590	-0.0000	-0.2500
2	32.6971	5.0000	-0.2500
3	42.5967	8.6030	-0.2500
4	40.2700	10.7740	-0.2500

WING PERCENT CHORD LINE 11, 100.0000

	X	Y	Z
1	19.8800	-0.0000	-0.2500
2	33.6182	5.0000	-0.2500
3	43.5180	8.6030	-0.2500
4	40.2700	10.7740	-0.2500

MAY 20, 1967
 INTERSECTIONS OF FLAT WING PERCENT CHORD LINES WITH BODY SURFACE
 PHI-THETA ORIGIN IS LOCATED AT (Y,Z) = (0.0000, 0.0000)
 (PRIMED-AXIS SYSTEM)

NO.	PERCENT	X	Y	Z	RHO	THETA
1	0.0000	13.7610	1.1251	-0.2500	1.1525	102.5285
2	10.0000	14.7529	1.1509	-0.2500	1.1777	102.2562
3	20.0000	15.6916	1.1573	-0.2500	1.1840	102.1901
4	30.0000	16.6126	1.1573	-0.2500	1.1840	102.1901
5	40.0000	17.5337	1.1573	-0.2500	1.1840	102.1901
6	50.0000	18.4547	1.1573	-0.2500	1.1840	102.1901
7	60.0000	19.3757	1.1573	-0.2500	1.1840	102.1901
8	70.0000	20.2968	1.1573	-0.2500	1.1840	102.1901
9	80.0000	21.2178	1.1573	-0.2500	1.1840	102.1901
10	90.0000	22.1388	1.1573	-0.2500	1.1840	102.1901
11	100.0000	23.0599	1.1573	-0.2500	1.1840	102.1901

BODY RADIUS AND Z-COORDINATE OF BODY CENTROID VERSUS X-PRIME
MAY 20, 1967

NO.	X-PRIME	RADIUS	Z-PRIME
1	0.0000	0.0000	0.0000
2	0.7243	0.0000	0.0000
3	1.4485	0.1304	0.0000
4	2.1728	0.2607	0.0000
5	2.8970	0.3491	0.0000
6	3.6213	0.4343	0.0000
7	4.3456	0.5077	0.0000
8	5.0698	0.5791	0.0000
9	5.7941	0.6433	0.0000
10	6.5184	0.7057	0.0000
11	7.2426	0.7627	0.0000
12	7.9669	0.8175	0.0000
13	8.6911	0.8670	0.0000
14	9.4154	0.9159	0.0000
15	10.1397	0.9502	0.0000
16	10.8639	1.0017	0.0000
17	11.5882	1.0396	0.0000
18	12.3124	1.0740	0.0000
19	13.0367	1.1049	0.0000
20	13.7610	1.1311	0.0000
21	14.4853	1.1542	0.0000
22	15.2096	1.1720	0.0000
23	15.9339	1.1840	0.0000
24	16.6582	1.1840	0.0000
25	17.3825	1.1840	0.0000
26	18.1068	1.1840	0.0000
27	18.8311	1.1840	0.0000
28	19.5554	1.1840	0.0000
29	20.2797	1.1840	0.0000
30	21.0040	1.1840	0.0000
31	21.7283	1.1840	0.0000
32	22.4526	1.1840	0.0000
33	23.1769	1.1840	0.0000
34	23.9012	1.1840	0.0000
35	24.6255	1.1840	0.0000
36	25.3498	1.1840	0.0000
37	26.0741	1.1840	0.0000
38	26.7984	1.1840	0.0000
39	27.5227	1.1840	0.0000
40	28.2470	1.1840	0.0000
41	28.9713	1.1840	0.0000
42	29.6956	1.1825	0.0000
43	30.4199	1.1757	0.0000
44	31.1442	1.1630	0.0000
45	31.8685	1.1452	0.0000
46	32.5928	1.1226	0.0000
47	33.3171	1.0930	0.0000
48	34.0414	1.0581	0.0000
49	34.7657	1.0252	0.0000
50	35.4900	1.0000	0.0000

BODY PANEL

4P

BODY PANEL ROUTINE

THERE ARE 15 TRANSVERSE VERTICAL PLANES THAT INTERSECT THE BODY
TO DEFINE PANEL LEADING AND TRAILING EDGES

X-INTERCEPTS

13.76097
14.75289
15.69159
16.61262
17.53366
18.45469
19.37572
20.29676
21.21779
22.13882
23.05986
25.00000
27.00000
29.50000
32.41500

BODY PANEL CORNER POINT COORDINATES
1 AND 2 INDICATE BODY PANEL LEADING-EDGE POINTS, 3 AND 4 INDICATE TRAILING-EDGE POINTS

PANEL NO	PARTS	X 1	Y 1	Z 1	X 2	Y 2	Z 2	X 3	Y 3	Z 3	X 4	Y 4	Z 4
1	1	13.761	0.000	1.154	13.761	0.488	1.046	14.753	0.005	1.177	14.753	0.493	1.069
2	1	14.753	0.000	1.178	14.753	0.498	1.068	15.692	0.001	1.184	15.692	0.499	1.073
3	1	15.692	0.000	1.184	15.692	0.500	1.073	16.613	0.000	1.194	16.613	0.500	1.073
4	1	16.613	0.000	1.194	16.613	0.500	1.073	17.534	0.000	1.184	17.534	0.500	1.073
5	1	17.534	0.000	1.184	17.534	0.500	1.073	18.455	0.000	1.184	18.455	0.500	1.073
6	1	18.455	0.000	1.184	18.455	0.500	1.073	19.376	0.000	1.184	19.376	0.500	1.073
7	1	19.376	0.000	1.184	19.376	0.500	1.073	20.297	0.000	1.184	20.297	0.500	1.073
8	1	20.297	0.000	1.184	20.297	0.500	1.073	21.218	0.000	1.184	21.218	0.500	1.073
9	1	21.218	0.000	1.184	21.218	0.500	1.073	22.139	0.000	1.184	22.139	0.500	1.073
10	1	22.139	0.000	1.184	22.139	0.500	1.073	23.060	0.000	1.184	23.060	0.500	1.073
11	1	23.060	0.000	1.184	23.060	0.500	1.073	24.000	0.000	1.184	24.000	0.500	1.073
12	1	24.000	0.000	1.184	24.000	0.500	1.073	25.000	0.000	1.184	25.000	0.500	1.073
13	1	25.000	0.000	1.184	25.000	0.500	1.073	26.000	0.000	1.184	26.000	0.500	1.073
14	1	26.000	0.000	1.184	26.000	0.500	1.073	27.000	0.000	1.184	27.000	0.500	1.073
15	1	27.000	0.000	1.184	27.000	0.500	1.073	28.000	0.000	1.184	28.000	0.500	1.073
16	1	28.000	0.000	1.184	28.000	0.500	1.073	29.000	0.000	1.184	29.000	0.500	1.073
17	1	29.000	0.000	1.184	29.000	0.500	1.073	30.000	0.000	1.184	30.000	0.500	1.073
18	1	30.000	0.000	1.184	30.000	0.500	1.073	31.000	0.000	1.184	31.000	0.500	1.073
19	1	31.000	0.000	1.184	31.000	0.500	1.073	32.000	0.000	1.184	32.000	0.500	1.073
20	1	32.000	0.000	1.184	32.000	0.500	1.073	33.000	0.000	1.184	33.000	0.500	1.073
21	1	33.000	0.000	1.184	33.000	0.500	1.073	34.000	0.000	1.184	34.000	0.500	1.073
22	1	34.000	0.000	1.184	34.000	0.500	1.073	35.000	0.000	1.184	35.000	0.500	1.073
23	1	35.000	0.000	1.184	35.000	0.500	1.073	36.000	0.000	1.184	36.000	0.500	1.073
24	1	36.000	0.000	1.184	36.000	0.500	1.073	37.000	0.000	1.184	37.000	0.500	1.073
25	1	37.000	0.000	1.184	37.000	0.500	1.073	38.000	0.000	1.184	38.000	0.500	1.073
26	1	38.000	0.000	1.184	38.000	0.500	1.073	39.000	0.000	1.184	39.000	0.500	1.073
27	1	39.000	0.000	1.184	39.000	0.500	1.073	40.000	0.000	1.184	40.000	0.500	1.073
28	1	40.000	0.000	1.184	40.000	0.500	1.073	41.000	0.000	1.184	41.000	0.500	1.073
29	1	41.000	0.000	1.184	41.000	0.500	1.073	42.000	0.000	1.184	42.000	0.500	1.073
30	1	42.000	0.000	1.184	42.000	0.500	1.073	43.000	0.000	1.184	43.000	0.500	1.073
31	1	43.000	0.000	1.184	43.000	0.500	1.073	44.000	0.000	1.184	44.000	0.500	1.073
32	1	44.000	0.000	1.184	44.000	0.500	1.073	45.000	0.000	1.184	45.000	0.500	1.073
33	1	45.000	0.000	1.184	45.000	0.500	1.073	46.000	0.000	1.184	46.000	0.500	1.073
34	1	46.000	0.000	1.184	46.000	0.500	1.073	47.000	0.000	1.184	47.000	0.500	1.073
35	1	47.000	0.000	1.184	47.000	0.500	1.073	48.000	0.000	1.184	48.000	0.500	1.073
36	1	48.000	0.000	1.184	48.000	0.500	1.073	49.000	0.000	1.184	49.000	0.500	1.073
37	1	49.000	0.000	1.184	49.000	0.500	1.073	50.000	0.000	1.184	50.000	0.500	1.073
38	1	50.000	0.000	1.184	50.000	0.500	1.073	51.000	0.000	1.184	51.000	0.500	1.073
39	1	51.000	0.000	1.184	51.000	0.500	1.073	52.000	0.000	1.184	52.000	0.500	1.073
40	1	52.000	0.000	1.184	52.000	0.500	1.073	53.000	0.000	1.184	53.000	0.500	1.073
41	1	53.000	0.000	1.184	53.000	0.500	1.073	54.000	0.000	1.184	54.000	0.500	1.073
42	1	54.000	0.000	1.184	54.000	0.500	1.073	55.000	0.000	1.184	55.000	0.500	1.073
43	1	55.000	0.000	1.184	55.000	0.500	1.073	56.000	0.000	1.184	56.000	0.500	1.073
44	1	56.000	0.000	1.184	56.000	0.500	1.073	57.000	0.000	1.184	57.000	0.500	1.073
45	1	57.000	0.000	1.184	57.000	0.500	1.073	58.000	0.000	1.184	58.000	0.500	1.073
46	1	58.000	0.000	1.184	58.000	0.500	1.073	59.000	0.000	1.184	59.000	0.500	1.073
47	1	59.000	0.000	1.184	59.000	0.500	1.073	60.000	0.000	1.184	60.000	0.500	1.073
48	1	60.000	0.000	1.184	60.000	0.500	1.073	61.000	0.000	1.184	61.000	0.500	1.073
49	1	61.000	0.000	1.184	61.000	0.500	1.073	62.000	0.000	1.184	62.000	0.500	1.073
50	1	62.000	0.000	1.184	62.000	0.500	1.073	63.000	0.000	1.184	63.000	0.500	1.073
51	1	63.000	0.000	1.184	63.000	0.500	1.073	64.000	0.000	1.184	64.000	0.500	1.073
52	1	64.000	0.000	1.184	64.000	0.500	1.073	65.000	0.000	1.184	65.000	0.500	1.073
53	1	65.000	0.000	1.184	65.000	0.500	1.073	66.000	0.000	1.184	66.000	0.500	1.073
54	1	66.000	0.000	1.184	66.000	0.500	1.073	67.000	0.000	1.184	67.000	0.500	1.073

55	1	27.000	1.144	0.306	27.000	1.157	-0.250	29.500	1.144	0.306	29.500	1.157	-0.250
56	1	29.500	1.144	0.296	29.500	1.157	-0.240	32.415	1.103	0.295	32.415	1.116	-0.241
57	1	13.761	1.125	-0.250	13.761	0.884	-0.762	14.753	1.146	-0.263	14.753	0.905	-0.752
58	1	14.753	1.151	-0.250	14.753	0.902	-0.757	15.692	1.156	-0.253	15.692	0.908	-0.760
59	1	15.692	1.157	-0.250	15.692	0.907	-0.761	16.613	1.157	-0.250	16.613	0.907	-0.761
60	1	16.613	1.157	-0.250	16.613	0.907	-0.761	17.534	1.157	-0.250	17.534	0.907	-0.761
61	1	17.534	1.157	-0.250	17.534	0.907	-0.761	18.455	1.157	-0.250	18.455	0.907	-0.761
62	1	18.455	1.157	-0.250	18.455	0.907	-0.761	19.376	1.157	-0.250	19.376	0.907	-0.761
63	1	19.376	1.157	-0.250	19.376	0.907	-0.761	20.297	1.157	-0.250	20.297	0.907	-0.761
64	1	20.297	1.157	-0.250	20.297	0.907	-0.761	21.218	1.157	-0.250	21.218	0.907	-0.761
65	1	21.218	1.157	-0.250	21.218	0.907	-0.761	22.139	1.157	-0.250	22.139	0.907	-0.761
66	1	22.139	1.157	-0.250	22.139	0.907	-0.761	23.060	1.157	-0.250	23.060	0.907	-0.761
67	1	23.060	1.157	-0.250	23.060	0.907	-0.761	24.000	1.157	-0.250	24.000	0.907	-0.761
68	1	24.000	1.157	-0.250	24.000	0.907	-0.761	25.000	1.157	-0.250	25.000	0.907	-0.761
69	1	25.000	1.157	-0.250	25.000	0.907	-0.761	26.000	1.157	-0.250	26.000	0.907	-0.761
70	1	26.000	1.157	-0.250	26.000	0.907	-0.761	27.000	1.157	-0.250	27.000	0.907	-0.761
71	1	27.000	1.153	-0.259	27.000	0.911	-0.752	28.000	1.116	-0.241	28.000	0.874	-0.734
72	1	28.000	1.153	-0.259	28.000	0.911	-0.752	29.000	1.116	-0.241	29.000	0.874	-0.734
73	1	29.000	1.153	-0.259	29.000	0.911	-0.752	30.000	1.116	-0.241	30.000	0.874	-0.734
74	1	30.000	1.153	-0.259	30.000	0.911	-0.752	31.000	1.116	-0.241	31.000	0.874	-0.734
75	1	31.000	1.153	-0.259	31.000	0.911	-0.752	32.000	1.116	-0.241	32.000	0.874	-0.734
76	1	32.000	1.153	-0.259	32.000	0.911	-0.752	33.000	1.116	-0.241	33.000	0.874	-0.734
77	1	33.000	1.153	-0.259	33.000	0.911	-0.752	34.000	1.116	-0.241	34.000	0.874	-0.734
78	1	34.000	1.153	-0.259	34.000	0.911	-0.752	35.000	1.116	-0.241	35.000	0.874	-0.734
79	1	35.000	1.153	-0.259	35.000	0.911	-0.752	36.000	1.116	-0.241	36.000	0.874	-0.734
80	1	36.000	1.153	-0.259	36.000	0.911	-0.752	37.000	1.116	-0.241	37.000	0.874	-0.734
81	1	37.000	1.153	-0.259	37.000	0.911	-0.752	38.000	1.116	-0.241	38.000	0.874	-0.734
82	1	38.000	1.153	-0.259	38.000	0.911	-0.752	39.000	1.116	-0.241	39.000	0.874	-0.734
83	1	39.000	1.153	-0.259	39.000	0.911	-0.752	40.000	1.116	-0.241	40.000	0.874	-0.734
84	1	40.000	1.153	-0.259	40.000	0.911	-0.752	41.000	1.116	-0.241	41.000	0.874	-0.734
85	1	41.000	1.153	-0.259	41.000	0.911	-0.752	42.000	1.116	-0.241	42.000	0.874	-0.734
86	1	42.000	1.153	-0.259	42.000	0.911	-0.752	43.000	1.116	-0.241	43.000	0.874	-0.734
87	1	43.000	1.153	-0.259	43.000	0.911	-0.752	44.000	1.116	-0.241	44.000	0.874	-0.734
88	1	44.000	1.153	-0.259	44.000	0.911	-0.752	45.000	1.116	-0.241	45.000	0.874	-0.734
89	1	45.000	1.153	-0.259	45.000	0.911	-0.752	46.000	1.116	-0.241	46.000	0.874	-0.734
90	1	46.000	1.153	-0.259	46.000	0.911	-0.752	47.000	1.116	-0.241	47.000	0.874	-0.734
91	1	47.000	1.153	-0.259	47.000	0.911	-0.752	48.000	1.116	-0.241	48.000	0.874	-0.734
92	1	48.000	1.153	-0.259	48.000	0.911	-0.752	49.000	1.116	-0.241	49.000	0.874	-0.734
93	1	49.000	1.153	-0.259	49.000	0.911	-0.752	50.000	1.116	-0.241	50.000	0.874	-0.734
94	1	50.000	1.153	-0.259	50.000	0.911	-0.752	51.000	1.116	-0.241	51.000	0.874	-0.734
95	1	51.000	1.153	-0.259	51.000	0.911	-0.752	52.000	1.116	-0.241	52.000	0.874	-0.734
96	1	52.000	1.153	-0.259	52.000	0.911	-0.752	53.000	1.116	-0.241	53.000	0.874	-0.734
97	1	53.000	1.153	-0.259	53.000	0.911	-0.752	54.000	1.116	-0.241	54.000	0.874	-0.734
98	1	54.000	1.153	-0.259	54.000	0.911	-0.752	55.000	1.116	-0.241	55.000	0.874	-0.734

BODY PANEL CENTROID AND CONTROL POINT COORDINATES

PANEL	X	Y	Z	X	Y	Z	AREA	THETA- INCLIN	ALPHA- INCLIN
1	14.259	0.246	1.112	14.703	0.249	1.122	0.501	-0.21817	0.02349
2	15.223	0.250	1.126	15.645	0.250	1.128	0.480	-0.21817	0.00619
3	16.152	0.250	1.129	16.567	0.250	1.129	0.472	-0.21817	0.00000
4	17.073	0.250	1.129	17.488	0.250	1.129	0.472	-0.21817	0.00000
5	17.994	0.250	1.129	18.409	0.250	1.129	0.472	-0.21817	0.00000
6	18.915	0.250	1.129	19.330	0.250	1.129	0.472	-0.21817	0.00000
7	19.836	0.250	1.129	20.251	0.250	1.129	0.472	-0.21817	0.00000
8	20.757	0.250	1.129	21.172	0.250	1.129	0.472	-0.21817	0.00000
9	21.678	0.250	1.129	22.093	0.250	1.129	0.472	-0.21817	0.00000
10	22.599	0.250	1.129	23.014	0.250	1.129	0.472	-0.21817	0.00000
11	24.030	0.250	1.129	24.903	0.250	1.129	0.994	-0.21817	0.00000
12	26.000	0.250	1.129	26.900	0.250	1.129	1.025	-0.21817	0.00000
13	28.250	0.250	1.129	29.375	0.250	1.129	1.281	-0.21817	0.00000
14	30.949	0.246	1.108	32.269	0.242	1.090	1.467	-0.21817	-0.01422
15	14.259	0.693	0.902	14.703	0.699	0.912	0.501	-0.65450	0.02349
16	15.223	0.702	0.915	15.645	0.704	0.917	0.480	-0.65450	0.00619
17	16.152	0.704	0.917	16.567	0.704	0.917	0.472	-0.65450	0.00000
18	17.073	0.704	0.917	17.488	0.704	0.917	0.472	-0.65450	0.00000
19	17.994	0.704	0.917	18.409	0.704	0.917	0.472	-0.65450	0.00000
20	18.915	0.704	0.917	19.330	0.704	0.917	0.472	-0.65450	0.00000
21	19.836	0.704	0.917	20.251	0.704	0.917	0.472	-0.65450	0.00000
22	20.757	0.704	0.917	21.172	0.704	0.917	0.472	-0.65450	0.00000
23	21.678	0.704	0.917	22.093	0.704	0.917	0.472	-0.65450	0.00000
24	22.599	0.704	0.917	23.014	0.704	0.917	0.472	-0.65450	0.00000
25	24.030	0.704	0.917	24.903	0.704	0.917	0.994	-0.65450	0.00000
26	26.000	0.704	0.917	26.900	0.704	0.917	1.025	-0.65450	0.00000
27	28.250	0.704	0.917	29.375	0.704	0.917	1.281	-0.65450	0.00000
28	30.949	0.691	0.901	32.269	0.680	0.886	1.467	-0.65450	0.01422
29	14.259	1.010	0.526	14.703	1.019	0.531	0.501	-1.09083	0.02349
30	15.223	1.023	0.532	15.645	1.025	0.534	0.480	-1.09083	0.00619
31	16.152	1.025	0.534	16.567	1.025	0.534	0.472	-1.09083	0.00000
32	17.073	1.025	0.534	17.488	1.025	0.534	0.472	-1.09083	0.00000
33	17.994	1.025	0.534	18.409	1.025	0.534	0.472	-1.09083	0.00000
34	18.915	1.025	0.534	19.330	1.025	0.534	0.472	-1.09083	0.00000
35	19.836	1.025	0.534	20.251	1.025	0.534	0.472	-1.09083	0.00000
36	20.757	1.025	0.534	21.172	1.025	0.534	0.472	-1.09083	0.00000
37	21.678	1.025	0.534	22.093	1.025	0.534	0.472	-1.09083	0.00000
38	22.599	1.025	0.534	23.014	1.025	0.534	0.472	-1.09083	0.00000
39	24.030	1.025	0.534	24.903	1.025	0.534	0.994	-1.09083	0.00000
40	26.000	1.025	0.534	26.900	1.025	0.534	1.025	-1.09083	0.00000
41	28.250	1.025	0.534	29.375	1.025	0.534	1.281	-1.09083	0.00000
42	30.949	1.007	0.524	32.269	0.990	0.516	1.467	-1.09083	-0.01422
43	14.259	1.132	0.026	14.703	1.143	0.026	0.548	-1.54628	0.02338
44	15.223	1.147	0.028	15.645	1.150	0.028	0.522	-1.54628	0.00616
45	16.152	1.150	0.028	16.567	1.150	0.028	0.513	-1.54628	0.00000
46	17.073	1.150	0.028	17.488	1.150	0.028	0.513	-1.54628	0.00000
47	17.994	1.150	0.028	18.409	1.150	0.028	0.513	-1.54628	0.00000
48	18.915	1.150	0.028	19.330	1.150	0.028	0.513	-1.54628	0.00000
49	19.836	1.150	0.028	20.251	1.150	0.028	0.513	-1.54628	0.00000
50	20.757	1.150	0.028	21.172	1.150	0.028	0.513	-1.54628	0.00000
51	21.678	1.150	0.028	22.093	1.150	0.028	0.513	-1.54628	0.00000
52	22.599	1.150	0.028	23.014	1.150	0.028	0.513	-1.54628	0.00000
53	24.030	1.150	0.028	24.903	1.150	0.028	1.080	-1.54627	0.00000
54	26.000	1.150	0.028	26.900	1.150	0.028	1.113	-1.54627	0.00000
55	28.250	1.150	0.028	29.375	1.150	0.028	1.362	-1.54627	0.00000

56	30.949	1.130	0.028	32.269	1.111	0.027	1.594	-1.54627	-0.01415
57	14.259	1.016	-0.500	14.703	1.025	-0.504	0.552	-2.02624	0.02336
58	15.223	1.029	-0.505	15.645	1.032	-0.506	0.532	-2.02624	0.00615
59	16.152	1.032	-0.506	16.567	1.032	-0.506	0.524	-2.02624	0.00000
60	17.073	1.032	-0.506	17.488	1.032	-0.506	0.524	-2.02624	0.00000
61	17.994	1.032	-0.506	18.409	1.032	-0.506	0.524	-2.02624	0.00000
62	18.915	1.032	-0.506	19.330	1.032	-0.506	0.524	-2.02624	0.00000
63	19.836	1.032	-0.506	20.251	1.032	-0.506	0.524	-2.02624	0.00000
64	20.757	1.032	-0.506	21.172	1.032	-0.506	0.524	-2.02624	0.00000
65	21.678	1.032	-0.506	22.093	1.032	-0.506	0.524	-2.02624	0.00000
66	22.599	1.032	-0.506	23.014	1.032	-0.506	0.524	-2.02624	0.00000
67	23.520	1.032	-0.506	24.033	1.032	-0.506	1.104	-2.02624	0.00000
68	24.441	1.032	-0.506	25.054	1.032	-0.506	1.138	-2.02624	0.00000
69	25.362	1.032	-0.506	26.075	1.032	-0.506	1.423	-2.02624	0.00000
70	26.283	1.032	-0.506	27.096	1.032	-0.506	1.629	-2.02624	0.01413
71	27.204	1.032	-0.506	28.117	1.032	-0.506	1.629	-2.02624	0.01413
72	28.125	1.032	-0.506	29.138	1.032	-0.506	0.501	-2.02624	0.02349
73	29.046	1.032	-0.506	30.159	1.032	-0.506	0.480	-2.02624	0.00619
74	30.000	1.032	-0.506	31.180	1.032	-0.506	0.472	-2.02624	0.00000
75	30.949	1.032	-0.506	32.201	1.032	-0.506	0.472	-2.02624	0.00000
76	31.898	1.032	-0.506	33.222	1.032	-0.506	0.472	-2.02624	0.00000
77	32.847	1.032	-0.506	34.243	1.032	-0.506	0.472	-2.02624	0.00000
78	33.796	1.032	-0.506	35.264	1.032	-0.506	0.472	-2.02624	0.00000
79	34.745	1.032	-0.506	36.285	1.032	-0.506	0.472	-2.02624	0.00000
80	35.694	1.032	-0.506	37.306	1.032	-0.506	0.472	-2.02624	0.00000
81	36.643	1.032	-0.506	38.327	1.032	-0.506	0.994	-2.02624	0.00000
82	37.592	1.032	-0.506	39.348	1.032	-0.506	1.025	-2.02624	0.00000
83	38.541	1.032	-0.506	40.369	1.032	-0.506	1.281	-2.02624	0.00000
84	39.490	1.032	-0.506	41.390	1.032	-0.506	1.467	-2.02624	0.01422
85	40.439	1.032	-0.506	42.411	1.032	-0.506	0.501	-2.02624	0.02349
86	41.388	1.032	-0.506	43.432	1.032	-0.506	0.480	-2.02624	0.00619
87	42.337	1.032	-0.506	44.453	1.032	-0.506	0.472	-2.02624	0.00000
88	43.286	1.032	-0.506	45.474	1.032	-0.506	0.472	-2.02624	0.00000
89	44.235	1.032	-0.506	46.495	1.032	-0.506	0.472	-2.02624	0.00000
90	45.184	1.032	-0.506	47.516	1.032	-0.506	0.472	-2.02624	0.00000
91	46.133	1.032	-0.506	48.537	1.032	-0.506	0.472	-2.02624	0.00000
92	47.082	1.032	-0.506	49.558	1.032	-0.506	0.472	-2.02624	0.00000
93	48.031	1.032	-0.506	50.579	1.032	-0.506	0.472	-2.02624	0.00000
94	48.980	1.032	-0.506	51.600	1.032	-0.506	0.472	-2.02624	0.00000
95	49.929	1.032	-0.506	52.621	1.032	-0.506	0.994	-2.02624	0.00000
96	50.878	1.032	-0.506	53.642	1.032	-0.506	1.025	-2.02624	0.00000
97	51.827	1.032	-0.506	54.663	1.032	-0.506	1.281	-2.02624	0.00000
98	52.776	1.032	-0.506	55.684	1.032	-0.506	1.467	-2.02624	0.01422

WING PANEL

8P

WING PANEL ROUTINE

THERE ARE 10 VERTICAL PLANES THAT INTERSECT THE WING TO DEFINE PANEL SIDE EDGES

LEADING-EDGE
Y-INTERCEPT

1.98460
2.81190
3.63920
4.46650
5.29380
6.12110
6.94840
7.77570
8.60300

OUTBOARD CUTTING PLANE

LEADING-EDGE	Y-INTERCEPT	SLOPE
X-INTERCEPT	40.27000	10.77400
		0.00000

ZERO-SLOPE INDICATES STREAMWISE CUTTING PLANE

UNDERFLOW AT 25422 IN MQ

UNDERFLOW AT 25422 IN MQ

UNDERFLOW AT 25422 IN MQ

AIRFOIL COORDINATES ARE USED DIRECTLY BY PROGRAM

WING PANEL CORNER POINT COORDINATES
1 AND 2 INDICATE WING PANEL LEADING-EDGE POINTS, 3 AND 4 INDICATE TRAILING-EDGE POINTS

PANEL NO	PARTS	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
1	1	13.832	1.151	-0.250	16.122	1.985	-0.250	14.753	1.151	-0.250	17.043	1.985	-0.250
2	1	14.771	1.157	-0.250	17.043	1.985	-0.250	15.692	1.157	-0.250	17.965	1.985	-0.250
3	1	15.692	1.157	-0.250	17.965	1.985	-0.250	16.613	1.157	-0.250	18.886	1.985	-0.250
4	1	16.613	1.157	-0.250	18.886	1.985	-0.250	17.534	1.157	-0.250	19.807	1.985	-0.250
5	1	17.534	1.157	-0.250	19.807	1.985	-0.250	18.455	1.157	-0.250	20.728	1.985	-0.250
6	1	18.455	1.157	-0.250	20.728	1.985	-0.250	19.376	1.157	-0.250	21.649	1.985	-0.250
7	1	19.376	1.157	-0.250	21.649	1.985	-0.250	20.297	1.157	-0.250	22.570	1.985	-0.250
8	1	20.297	1.157	-0.250	22.570	1.985	-0.250	21.218	1.157	-0.250	23.491	1.985	-0.250
9	1	21.218	1.157	-0.250	23.491	1.985	-0.250	22.139	1.157	-0.250	24.412	1.985	-0.250
10	1	22.139	1.157	-0.250	24.412	1.985	-0.250	23.060	1.157	-0.250	25.333	1.985	-0.250
11	1	16.122	1.985	-0.250	18.395	2.812	-0.250	17.043	1.985	-0.250	19.316	2.812	-0.250
12	1	17.043	1.985	-0.250	19.316	2.812	-0.250	17.965	1.985	-0.250	20.237	2.812	-0.250
13	1	17.965	1.985	-0.250	20.237	2.812	-0.250	18.886	1.985	-0.250	21.159	2.812	-0.250
14	1	18.886	1.985	-0.250	21.159	2.812	-0.250	19.807	1.985	-0.250	22.080	2.812	-0.250
15	1	19.807	1.985	-0.250	22.080	2.812	-0.250	20.728	1.985	-0.250	23.001	2.812	-0.250
16	1	20.728	1.985	-0.250	23.001	2.812	-0.250	21.649	1.985	-0.250	23.922	2.812	-0.250
17	1	21.649	1.985	-0.250	23.922	2.812	-0.250	22.570	1.985	-0.250	24.843	2.812	-0.250
18	1	22.570	1.985	-0.250	24.843	2.812	-0.250	23.491	1.985	-0.250	25.764	2.812	-0.250
19	1	23.491	1.985	-0.250	25.764	2.812	-0.250	24.412	1.985	-0.250	26.685	2.812	-0.250
20	1	24.412	1.985	-0.250	26.685	2.812	-0.250	25.333	1.985	-0.250	27.606	2.812	-0.250
21	1	18.395	2.812	-0.250	20.668	3.639	-0.250	19.316	2.812	-0.250	21.589	3.639	-0.250
22	1	19.316	2.812	-0.250	20.668	3.639	-0.250	20.237	2.812	-0.250	22.510	3.639	-0.250
23	1	20.237	2.812	-0.250	21.589	3.639	-0.250	21.159	2.812	-0.250	23.431	3.639	-0.250
24	1	21.159	2.812	-0.250	22.510	3.639	-0.250	22.080	2.812	-0.250	24.353	3.639	-0.250
25	1	22.080	2.812	-0.250	23.431	3.639	-0.250	23.001	2.812	-0.250	25.274	3.639	-0.250
26	1	23.001	2.812	-0.250	24.353	3.639	-0.250	23.922	2.812	-0.250	26.195	3.639	-0.250
27	1	23.922	2.812	-0.250	25.274	3.639	-0.250	24.843	2.812	-0.250	27.116	3.639	-0.250
28	1	24.843	2.812	-0.250	26.195	3.639	-0.250	25.764	2.812	-0.250	28.037	3.639	-0.250
29	1	25.764	2.812	-0.250	27.116	3.639	-0.250	26.685	2.812	-0.250	28.958	3.639	-0.250
30	1	26.685	2.812	-0.250	28.037	3.639	-0.250	27.606	2.812	-0.250	29.879	3.639	-0.250
31	1	27.606	3.639	-0.250	28.958	4.466	-0.250	28.510	3.639	-0.250	30.800	4.466	-0.250
32	1	28.510	3.639	-0.250	29.879	4.466	-0.250	29.431	3.639	-0.250	31.721	4.466	-0.250
33	1	29.431	3.639	-0.250	30.800	4.466	-0.250	30.353	3.639	-0.250	32.642	4.466	-0.250
34	1	30.353	3.639	-0.250	31.721	4.466	-0.250	31.274	3.639	-0.250	33.563	4.466	-0.250
35	1	31.274	3.639	-0.250	32.642	4.466	-0.250	32.195	3.639	-0.250	34.484	4.466	-0.250
36	1	32.195	3.639	-0.250	33.563	4.466	-0.250	33.116	3.639	-0.250	35.405	4.466	-0.250
37	1	33.116	3.639	-0.250	34.484	4.466	-0.250	34.037	3.639	-0.250	36.326	4.466	-0.250
38	1	34.037	3.639	-0.250	35.405	4.466	-0.250	34.958	3.639	-0.250	37.247	4.466	-0.250
39	1	35.405	3.639	-0.250	36.326	4.466	-0.250	35.879	3.639	-0.250	38.168	4.466	-0.250
40	1	36.326	3.639	-0.250	37.247	4.466	-0.250	36.800	3.639	-0.250	39.089	4.466	-0.250
41	1	37.247	4.466	-0.250	38.168	5.294	-0.250	37.721	4.466	-0.250	40.010	5.294	-0.250
42	1	38.168	4.466	-0.250	39.089	5.294	-0.250	38.642	4.466	-0.250	40.931	5.294	-0.250
43	1	39.089	4.466	-0.250	40.010	5.294	-0.250	39.563	4.466	-0.250	41.852	5.294	-0.250
44	1	40.010	4.466	-0.250	40.931	5.294	-0.250	40.484	4.466	-0.250	42.773	5.294	-0.250
45	1	40.931	4.466	-0.250	41.852	5.294	-0.250	41.405	4.466	-0.250	43.694	5.294	-0.250
46	1	41.852	4.466	-0.250	42.773	5.294	-0.250	42.326	4.466	-0.250	44.615	5.294	-0.250
47	1	42.773	4.466	-0.250	43.694	5.294	-0.250	43.247	4.466	-0.250	45.536	5.294	-0.250
48	1	43.694	4.466	-0.250	44.615	5.294	-0.250	44.168	4.466	-0.250	46.457	5.294	-0.250
49	1	44.615	4.466	-0.250	45.536	5.294	-0.250	45.089	4.466	-0.250	47.378	5.294	-0.250
50	1	45.536	4.466	-0.250	46.457	5.294	-0.250	46.010	4.466	-0.250	48.299	5.294	-0.250
51	1	46.457	5.294	-0.250	47.378	5.294	-0.250	46.931	4.466	-0.250	49.220	5.294	-0.250
52	1	47.378	5.294	-0.250	48.299	5.294	-0.250	47.852	4.466	-0.250	50.141	5.294	-0.250
53	1	48.299	5.294	-0.250	49.220	5.294	-0.250	48.773	4.466	-0.250	51.062	5.294	-0.250
54	1	49.220	5.294	-0.250	50.141	5.294	-0.250	49.694	4.466	-0.250	51.983	5.294	-0.250

56	1	28.899	5.294	-0.250	31.172	6.121	-0.250	29.820	5.294	-0.250	32.093	6.121	-0.250
56	1	29.820	5.294	-0.250	32.093	6.121	-0.250	30.741	5.294	-0.250	33.014	6.121	-0.250
57	1	30.741	5.294	-0.250	33.014	6.121	-0.250	31.662	5.294	-0.250	33.935	6.121	-0.250
57	1	31.662	5.294	-0.250	33.935	6.121	-0.250	32.583	5.294	-0.250	34.856	6.121	-0.250
58	1	32.583	5.294	-0.250	34.856	6.121	-0.250	33.504	5.294	-0.250	35.777	6.121	-0.250
59	1	33.504	5.294	-0.250	35.777	6.121	-0.250	34.425	5.294	-0.250	36.699	6.121	-0.250
60	1	34.425	5.294	-0.250	36.699	6.121	-0.250	28.408	6.121	-0.250	30.681	6.948	-0.250
61	1	27.487	6.121	-0.250	29.760	6.948	-0.250	29.329	6.121	-0.250	31.602	6.948	-0.250
62	1	28.408	6.121	-0.250	30.681	6.948	-0.250	30.250	6.121	-0.250	32.523	6.948	-0.250
63	1	29.329	6.121	-0.250	31.602	6.948	-0.250	31.172	6.121	-0.250	33.445	6.948	-0.250
64	1	30.250	6.121	-0.250	32.523	6.948	-0.250	32.093	6.121	-0.250	34.366	6.948	-0.250
65	1	31.172	6.121	-0.250	33.445	6.948	-0.250	33.014	6.121	-0.250	35.287	6.948	-0.250
66	1	32.093	6.121	-0.250	34.366	6.948	-0.250	33.935	6.121	-0.250	36.208	6.948	-0.250
67	1	33.014	6.121	-0.250	35.287	6.948	-0.250	34.856	6.121	-0.250	37.129	6.948	-0.250
68	1	33.935	6.121	-0.250	36.208	6.948	-0.250	35.777	6.121	-0.250	38.051	6.948	-0.250
69	1	34.856	6.121	-0.250	37.129	6.948	-0.250	36.699	6.121	-0.250	38.972	6.948	-0.250
70	1	35.777	6.121	-0.250	38.051	6.948	-0.250	30.681	6.948	-0.250	32.954	7.776	-0.250
71	1	29.760	6.948	-0.250	32.033	7.776	-0.250	31.602	6.948	-0.250	33.875	7.776	-0.250
72	1	30.681	6.948	-0.250	32.954	7.776	-0.250	32.523	6.948	-0.250	34.796	7.776	-0.250
73	1	31.602	6.948	-0.250	33.875	7.776	-0.250	33.445	6.948	-0.250	35.718	7.776	-0.250
74	1	32.523	6.948	-0.250	34.796	7.776	-0.250	34.366	6.948	-0.250	36.639	7.776	-0.250
75	1	33.445	6.948	-0.250	35.718	7.776	-0.250	35.287	6.948	-0.250	37.560	7.776	-0.250
76	1	34.366	6.948	-0.250	36.639	7.776	-0.250	36.208	6.948	-0.250	38.481	7.776	-0.250
77	1	35.287	6.948	-0.250	37.560	7.776	-0.250	37.129	6.948	-0.250	39.402	7.776	-0.250
78	1	36.208	6.948	-0.250	38.481	7.776	-0.250	38.051	6.948	-0.250	40.324	7.776	-0.250
79	1	37.129	6.948	-0.250	39.402	7.776	-0.250	38.972	6.948	-0.250	41.245	7.776	-0.250
80	1	38.051	6.948	-0.250	40.324	7.776	-0.250	39.894	7.776	-0.250	42.166	8.603	-0.250
81	1	38.972	7.776	-0.250	41.245	8.603	-0.250	40.815	7.776	-0.250	43.087	8.603	-0.250
82	1	39.894	7.776	-0.250	42.166	8.603	-0.250	41.736	7.776	-0.250	44.008	8.603	-0.250
83	1	40.815	7.776	-0.250	43.087	8.603	-0.250	42.657	7.776	-0.250	44.929	8.603	-0.250
84	1	41.736	7.776	-0.250	44.008	8.603	-0.250	43.578	7.776	-0.250	45.850	8.603	-0.250
85	1	42.657	7.776	-0.250	44.929	8.603	-0.250	44.499	7.776	-0.250	46.771	8.603	-0.250
86	1	43.578	7.776	-0.250	45.850	8.603	-0.250	45.420	7.776	-0.250	47.692	8.603	-0.250
87	1	44.499	7.776	-0.250	46.771	8.603	-0.250	46.341	7.776	-0.250	48.613	8.603	-0.250
88	1	45.420	7.776	-0.250	47.692	8.603	-0.250	47.262	7.776	-0.250	49.534	8.603	-0.250
89	1	46.341	7.776	-0.250	48.613	8.603	-0.250	48.183	7.776	-0.250	50.455	8.603	-0.250
90	1	47.262	7.776	-0.250	49.534	8.603	-0.250	49.104	7.776	-0.250	51.376	8.603	-0.250
91	1	48.183	7.776	-0.250	50.455	8.603	-0.250	50.025	7.776	-0.250	52.297	8.603	-0.250
92	1	49.104	7.776	-0.250	51.376	8.603	-0.250	50.946	7.776	-0.250	53.218	8.603	-0.250
93	1	50.025	7.776	-0.250	52.297	8.603	-0.250	51.867	7.776	-0.250	54.139	8.603	-0.250
94	1	50.946	7.776	-0.250	53.218	8.603	-0.250	52.788	7.776	-0.250	55.060	8.603	-0.250
95	1	51.867	7.776	-0.250	54.139	8.603	-0.250	53.709	7.776	-0.250	55.981	8.603	-0.250
96	1	52.788	7.776	-0.250	55.060	8.603	-0.250	54.630	7.776	-0.250	56.902	8.603	-0.250
97	1	53.709	7.776	-0.250	55.981	8.603	-0.250	55.551	7.776	-0.250	57.823	8.603	-0.250
98	1	54.630	7.776	-0.250	56.902	8.603	-0.250	56.472	7.776	-0.250	58.744	8.603	-0.250
99	1	55.551	7.776	-0.250	57.823	8.603	-0.250	57.393	7.776	-0.250	59.665	8.603	-0.250
100	1	56.472	7.776	-0.250	58.744	8.603	-0.250	58.314	7.776	-0.250	60.586	8.603	-0.250

WING PANEL CENTROID AND CONTROL POINT COORDINATES

PANEL	X	Y	Z	X	Y	Z	AREA	Z THICK	ALPHA-THICK	Z CAMBER	ALPHA-CAMBER
1	15.419	1.561	-0.250	15.934	1.561	-0.250	0.780	-0.13106	0.06738	-0.17193	0.04620
2	16.363	1.569	-0.250	16.778	1.569	-0.250	0.765	-0.09283	0.03510	-0.14713	0.01662
3	17.289	1.571	-0.250	17.703	1.571	-0.250	0.762	-0.06967	0.01634	-0.13461	0.01069
4	18.210	1.571	-0.250	18.624	1.571	-0.250	0.762	-0.05866	0.00011	-0.12665	0.00483
5	19.131	1.571	-0.250	19.545	1.571	-0.250	0.762	-0.06419	0.01523	-0.12404	0.00126
6	20.052	1.571	-0.250	20.466	1.571	-0.250	0.762	-0.08510	-0.02923	-0.12792	-0.00781
7	20.973	1.571	-0.250	21.387	1.571	-0.250	0.762	-0.11931	-0.03690	-0.14046	-0.01879
8	21.894	1.571	-0.250	22.308	1.571	-0.250	0.762	-0.15868	-0.04413	-0.16351	-0.02996
9	22.815	1.571	-0.250	23.229	1.571	-0.250	0.762	-0.20009	-0.05137	-0.19806	-0.04320
10	23.736	1.571	-0.250	24.150	1.571	-0.250	0.762	-0.25001	-0.05876	-0.24687	-0.06070
11	24.657	1.571	-0.250	25.071	1.571	-0.250	0.762	-0.13105	0.06738	-0.17192	0.04620
12	25.578	1.571	-0.250	25.992	1.571	-0.250	0.762	-0.09283	0.03510	-0.14713	0.01662
13	26.500	1.571	-0.250	26.913	1.571	-0.250	0.762	-0.06966	0.01634	-0.13461	0.01069
14	27.421	1.571	-0.250	27.834	1.571	-0.250	0.762	-0.05866	0.00011	-0.12665	0.00483
15	28.342	1.571	-0.250	28.755	1.571	-0.250	0.762	-0.06419	0.01523	-0.12404	0.00126
16	29.263	1.571	-0.250	29.676	1.571	-0.250	0.762	-0.08510	-0.02923	-0.12792	-0.00781
17	30.184	1.571	-0.250	30.597	1.571	-0.250	0.762	-0.11931	-0.03690	-0.14046	-0.01879
18	31.105	1.571	-0.250	31.518	1.571	-0.250	0.762	-0.15868	-0.04413	-0.16351	-0.02996
19	32.026	1.571	-0.250	32.439	1.571	-0.250	0.762	-0.20009	-0.05137	-0.19806	-0.04320
20	32.947	1.571	-0.250	33.360	1.571	-0.250	0.762	-0.25001	-0.05876	-0.24687	-0.06070
21	33.868	1.571	-0.250	34.281	1.571	-0.250	0.762	-0.13105	0.06738	-0.17192	0.04620
22	34.789	1.571	-0.250	35.202	1.571	-0.250	0.762	-0.09283	0.03510	-0.14713	0.01662
23	35.710	1.571	-0.250	36.123	1.571	-0.250	0.762	-0.06966	0.01634	-0.13460	0.01069
24	36.631	1.571	-0.250	37.044	1.571	-0.250	0.762	-0.05866	0.00011	-0.12664	0.00483
25	37.552	1.571	-0.250	37.965	1.571	-0.250	0.762	-0.06419	0.01523	-0.12403	0.00126
26	38.473	1.571	-0.250	38.886	1.571	-0.250	0.762	-0.08510	-0.02923	-0.12791	-0.00781
27	39.394	1.571	-0.250	39.807	1.571	-0.250	0.762	-0.11931	-0.03690	-0.14045	-0.01879
28	40.315	1.571	-0.250	40.728	1.571	-0.250	0.762	-0.15868	-0.04413	-0.16351	-0.02996
29	41.236	1.571	-0.250	41.649	1.571	-0.250	0.762	-0.20009	-0.05137	-0.19806	-0.04320
30	42.157	1.571	-0.250	42.570	1.571	-0.250	0.762	-0.25001	-0.05876	-0.24687	-0.06070
31	43.078	1.571	-0.250	43.491	1.571	-0.250	0.762	-0.13105	0.06738	-0.17192	0.04620
32	44.000	1.571	-0.250	44.412	1.571	-0.250	0.762	-0.09283	0.03510	-0.14712	0.01662
33	44.921	1.571	-0.250	45.333	1.571	-0.250	0.762	-0.06965	0.01634	-0.13460	0.01069
34	45.842	1.571	-0.250	46.254	1.571	-0.250	0.762	-0.05865	0.00011	-0.12664	0.00483
35	46.763	1.571	-0.250	47.175	1.571	-0.250	0.762	-0.06417	0.01523	-0.12403	0.00126
36	47.684	1.571	-0.250	48.096	1.571	-0.250	0.762	-0.08508	-0.02923	-0.12791	-0.00781
37	48.605	1.571	-0.250	49.017	1.571	-0.250	0.762	-0.11930	-0.03690	-0.14045	-0.01879
38	49.526	1.571	-0.250	49.938	1.571	-0.250	0.762	-0.15868	-0.04413	-0.16351	-0.02996
39	50.447	1.571	-0.250	50.859	1.571	-0.250	0.762	-0.20008	-0.05137	-0.19805	-0.04320
40	51.368	1.571	-0.250	51.780	1.571	-0.250	0.762	-0.25001	-0.05876	-0.24687	-0.06070
41	52.289	1.571	-0.250	52.701	1.571	-0.250	0.762	-0.13104	0.06738	-0.17192	0.04620
42	53.210	1.571	-0.250	53.622	1.571	-0.250	0.762	-0.09282	0.03510	-0.14712	0.01662
43	54.131	1.571	-0.250	54.543	1.571	-0.250	0.762	-0.06965	0.01634	-0.13460	0.01069
44	55.052	1.571	-0.250	55.464	1.571	-0.250	0.762	-0.05865	0.00011	-0.12664	0.00483
45	55.973	1.571	-0.250	56.385	1.571	-0.250	0.762	-0.06417	0.01523	-0.12403	0.00126
46	56.894	1.571	-0.250	57.306	1.571	-0.250	0.762	-0.08508	-0.02923	-0.12791	-0.00781
47	57.815	1.571	-0.250	58.227	1.571	-0.250	0.762	-0.11930	-0.03690	-0.14045	-0.01879
48	58.736	1.571	-0.250	59.148	1.571	-0.250	0.762	-0.15868	-0.04413	-0.16351	-0.02996
49	59.657	1.571	-0.250	60.069	1.571	-0.250	0.762	-0.20008	-0.05137	-0.19805	-0.04320
50	60.578	1.571	-0.250	60.990	1.571	-0.250	0.762	-0.25001	-0.05876	-0.24687	-0.06070
51	61.500	1.571	-0.250	61.911	1.571	-0.250	0.762	-0.13104	0.06738	-0.17192	0.04620
52	62.421	1.571	-0.250	62.832	1.571	-0.250	0.762	-0.09282	0.03510	-0.14712	0.01662
53	63.342	1.571	-0.250	63.753	1.571	-0.250	0.762	-0.06965	0.01634	-0.13460	0.01069
54	64.263	1.571	-0.250	64.674	1.571	-0.250	0.762	-0.05865	0.00011	-0.12664	0.00483
55	65.184	1.571	-0.250	65.595	1.571	-0.250	0.762	-0.06417	0.01523	-0.12403	0.00126

56	31.417	5.707	-0.250	31.831	5.707	-0.250	0.762	-0.08507	-0.03923	-0.12791	-0.00781
57	32.338	5.707	-0.250	32.752	5.707	-0.250	0.762	-0.11930	-0.03690	-0.14045	-0.01879
58	33.259	5.707	-0.250	33.674	5.707	-0.250	0.762	-0.15868	-0.04413	-0.16351	-0.02996
59	34.180	5.707	-0.250	34.595	5.707	-0.250	0.762	-0.20008	-0.05137	-0.19805	-0.04320
60	35.101	5.707	-0.250	35.516	5.707	-0.250	0.762	-0.25001	-0.05876	-0.24687	-0.06070
61	36.024	6.535	-0.250	36.498	6.535	-0.250	0.762	-0.13104	0.06738	-0.17191	0.04620
62	37.005	6.535	-0.250	37.420	6.535	-0.250	0.762	-0.09281	0.03510	-0.14712	0.01662
63	38.026	6.535	-0.250	38.341	6.535	-0.250	0.762	-0.06864	0.01634	-0.13459	0.01069
64	39.047	6.535	-0.250	39.262	6.535	-0.250	0.762	-0.05056	0.00011	-0.12663	0.00483
65	40.069	6.535	-0.250	40.183	6.535	-0.250	0.762	-0.06416	-0.01523	-0.12402	-0.00126
66	41.090	6.535	-0.250	41.104	6.535	-0.250	0.762	-0.08507	-0.02923	-0.12790	-0.00781
67	42.111	6.535	-0.250	42.026	6.535	-0.250	0.762	-0.11929	-0.03690	-0.14045	-0.01879
68	43.132	6.535	-0.250	43.047	6.535	-0.250	0.762	-0.15867	-0.04413	-0.16350	-0.02996
69	44.153	6.535	-0.250	44.068	6.535	-0.250	0.762	-0.20008	-0.05137	-0.19805	-0.04320
70	45.174	6.535	-0.250	45.089	6.535	-0.250	0.762	-0.25001	-0.05876	-0.24687	-0.06070
71	46.195	7.362	-0.250	46.110	7.362	-0.250	0.762	-0.13103	0.06738	-0.17191	0.04620
72	47.216	7.362	-0.250	47.025	7.362	-0.250	0.762	-0.09280	0.03510	-0.14711	0.01662
73	48.237	7.362	-0.250	48.141	7.362	-0.250	0.762	-0.06864	0.01634	-0.13459	0.01069
74	49.258	7.362	-0.250	49.162	7.362	-0.250	0.762	-0.05056	0.00011	-0.12663	0.00483
75	50.279	7.362	-0.250	50.183	7.362	-0.250	0.762	-0.06415	-0.01523	-0.12401	-0.00126
76	51.300	7.362	-0.250	51.204	7.362	-0.250	0.762	-0.08507	-0.02923	-0.12790	-0.00781
77	52.321	7.362	-0.250	52.225	7.362	-0.250	0.762	-0.11929	-0.03690	-0.14044	-0.01879
78	53.342	7.362	-0.250	53.246	7.362	-0.250	0.762	-0.15867	-0.04413	-0.16350	-0.02996
79	54.363	7.362	-0.250	54.267	7.362	-0.250	0.762	-0.20008	-0.05137	-0.19805	-0.04320
80	55.384	7.362	-0.250	55.288	7.362	-0.250	0.762	-0.25001	-0.05876	-0.24686	-0.06070
81	56.405	8.189	-0.250	56.319	8.189	-0.250	0.762	-0.13103	0.06738	-0.17191	0.04620
82	57.426	8.189	-0.250	57.339	8.189	-0.250	0.762	-0.09280	0.03510	-0.14711	0.01662
83	58.447	8.189	-0.250	58.360	8.189	-0.250	0.762	-0.06863	0.01634	-0.13458	0.01069
84	59.468	8.189	-0.250	59.381	8.189	-0.250	0.762	-0.05862	0.00011	-0.12662	0.00483
85	60.489	8.189	-0.250	60.402	8.189	-0.250	0.762	-0.06415	-0.01523	-0.12401	-0.00126
86	61.510	8.189	-0.250	61.423	8.189	-0.250	0.762	-0.08506	-0.02923	-0.12790	-0.00781
87	62.531	8.189	-0.250	62.444	8.189	-0.250	0.762	-0.11929	-0.03690	-0.14044	-0.01879
88	63.552	8.189	-0.250	63.465	8.189	-0.250	0.762	-0.15867	-0.04413	-0.16350	-0.02996
89	64.573	8.189	-0.250	64.486	8.189	-0.250	0.762	-0.20008	-0.05137	-0.19805	-0.04320
90	65.594	8.189	-0.250	65.507	8.189	-0.250	0.762	-0.25001	-0.05876	-0.24686	-0.06070
91	66.615	9.327	-0.250	66.528	9.327	-0.250	1.000	-0.17069	0.06738	-0.19794	0.04620
92	67.636	9.327	-0.250	67.549	9.327	-0.250	1.000	-0.14520	0.03510	-0.18141	0.01662
93	68.657	9.327	-0.250	68.570	9.327	-0.250	1.000	-0.12976	0.01634	-0.17306	0.01069
94	69.678	9.327	-0.250	69.591	9.327	-0.250	1.000	-0.12242	0.00011	-0.16775	0.00483
95	70.699	9.327	-0.250	70.612	9.327	-0.250	1.000	-0.12610	-0.01523	-0.16601	-0.00126
96	71.720	9.327	-0.250	71.633	9.327	-0.250	1.000	-0.14004	-0.02923	-0.16860	-0.00781
97	72.741	9.327	-0.250	72.654	9.327	-0.250	1.000	-0.16286	-0.03690	-0.17696	-0.01879
98	73.762	9.327	-0.250	73.675	9.327	-0.250	1.000	-0.18911	-0.04413	-0.19293	-0.02996
99	74.783	9.327	-0.250	74.696	9.327	-0.250	1.000	-0.21672	-0.05137	-0.21537	-0.04320
100	75.804	9.327	-0.250	75.717	9.327	-0.250	1.000	-0.25001	-0.05876	-0.24791	-0.06070

14P

PANEND

TIME 01.599 052067

1A

AERODYNAMIC

SAVE TAPE

JUN 06, 1967

DESCRIPTION OF CASE REQUESTED

SYMMETRICAL CONFIGURATION - PANELS LOCATED ON BOTH SIDES OF X-Z PLANE (SYM = 1.)

CASE = 2. CALCULATE CL, GIVEN SHAPE

CPCALC = 0.

LINEAR CP

POLAR = 0. POLARS NOT REQUESTED

THICK = 1. WING THICKNESS PRESSURES TO BE ADDED

VOUT = 1. VELOCITY COMPONENTS TO BE PRINTED

MACH NUMBER = 1.8000

POINT ABOUT WHICH THE MOMENTS ARE TO BE COMPUTED

X-COORDINATE = 0.0000

Z-COORDINATE = 0.0000

REFERENCE CHORD LENGTH = 1.0000

WING REFERENCE AREA = 89.3750

WING SEMI-SPAN = 1.0000

GIVEN BODY RADII

GIVEN BODY CAMBER

HEIGHT OF WING PLANE ABOVE BODY AXIS = -0.2500

INCLINATION OF BODY AXIS WITH RESPECT TO DEFINING AXIS = 0.0000 DEG.

ANGLE OF ATTACK WITH RESPECT TO BODY AXIS = 6.0000 DEG.

CONSTANT WING CAMBER

GIVEN WING THICKNESS

BODY GEOMETRY	X-STATION	CAMBER	RADIUS	FIRST DERIVATIVE	SECOND DERIVATIVE
	0.0000	0.0000	0.0000	0.1800	-0.0199
	0.7243	0.0000	0.1304	0.1872	0.0398
	1.4485	0.0000	0.2607	0.1512	-0.1393
	2.1728	0.0000	0.3491	0.1142	0.0372
	2.8970	0.0000	0.4343	0.1110	-0.0461
	3.6213	0.0000	0.5077	0.0987	0.0121
	4.3456	0.0000	0.5791	0.0941	-0.0247
	5.0698	0.0000	0.6433	0.0869	0.0048
	5.7941	0.0000	0.7057	0.0826	-0.0168
	6.5184	0.0000	0.7627	0.0769	0.0013
	7.2426	0.0000	0.8175	0.0728	-0.0126
	7.9669	0.0000	0.8679	0.0678	-0.0015
	8.6911	0.0000	0.9159	0.0638	-0.0094
	9.4154	0.0000	0.9602	0.0591	-0.0037
	10.1397	0.0000	1.0017	0.0550	-0.0075
	10.8639	0.0000	1.0396	0.0498	-0.0067
	11.5882	0.0000	1.0740	0.0454	-0.0056
	12.3124	0.0000	1.1049	0.0392	-0.0113
	13.0367	0.0000	1.1311	0.0342	-0.0027
	13.7610	0.0000	1.1542	0.0281	-0.0142
	14.5023	0.0000	1.1720	0.0213	-0.0039
	15.2436	0.0000	1.1840	0.0073	-0.0340
	15.9849	0.0000	1.1840	-0.0019	0.0091
	16.7262	0.0000	1.1840	0.0005	-0.0024
	17.4675	0.0000	1.1840	-0.0001	0.0007
	18.2088	0.0000	1.1840	0.0000	-0.0002
	18.9501	0.0000	1.1840	-0.0000	0.0000
	19.6914	0.0000	1.1840	0.0000	-0.0000
	20.4327	0.0000	1.1840	-0.0000	0.0000
	21.1740	0.0000	1.1840	0.0000	-0.0000
	21.9153	0.0000	1.1840	-0.0000	0.0000
	22.6566	0.0000	1.1840	0.0000	-0.0000
	23.3979	0.0000	1.1840	-0.0000	0.0000
	24.1392	0.0000	1.1840	0.0000	-0.0000
	24.8805	0.0000	1.1840	-0.0000	0.0000
	25.6218	0.0000	1.1840	0.0000	-0.0000
	26.3631	0.0000	1.1840	-0.0000	0.0000
	27.1044	0.0000	1.1840	0.0000	-0.0000
	27.8457	0.0000	1.1840	-0.0000	0.0000
	28.5870	0.0000	1.1840	0.0001	-0.0001
	29.3283	0.0000	1.1840	-0.0003	0.0004
	30.0696	0.0000	1.1825	-0.0050	-0.0016
	30.8109	0.0000	1.1757	-0.0133	-0.0109
	31.5522	0.0000	1.1630	-0.0208	-0.0115
	32.2935	0.0000	1.1452	-0.0269	-0.0090
	33.0348	0.0000	1.1226	-0.0350	-0.0073
	33.7761	0.0000	1.0930	-0.0446	-0.0146
	34.5174	0.0000	1.0581	-0.0475	-0.0114
	35.2587	0.0000	1.0252	-0.0398	0.0038
					0.0170

VELOCITY COMPONENTS ON BODY DUE TO BODY LINE SOURCES AND DOUBLETS

AXIAL (U)	THETA (DEG.)									
	0.0000	22.5000	45.0000	67.5000	90.0000	112.5000	135.0000	157.5000	180.0000	
0.0000	-0.03166	-0.03402	-0.04073	-0.05078	-0.06263	-0.07449	-0.08454	-0.09125	-0.09361	
0.7243	-0.03446	-0.03682	-0.04353	-0.05358	-0.06543	-0.07729	-0.08734	-0.09405	-0.09641	
1.4485	-0.01686	-0.01926	-0.02608	-0.03630	-0.04836	-0.06041	-0.07063	-0.07746	-0.07986	
2.1728	-0.00369	-0.00550	-0.01066	-0.01838	-0.02749	-0.03659	-0.04431	-0.04947	-0.05128	
2.8970	-0.00659	-0.00832	-0.01323	-0.02058	-0.02925	-0.03792	-0.04527	-0.05018	-0.05190	
3.6213	-0.00198	-0.00352	-0.00793	-0.01453	-0.02230	-0.03008	-0.03668	-0.04105	-0.04263	
4.3456	-0.00193	-0.00341	-0.00764	-0.01396	-0.02142	-0.02888	-0.03520	-0.03943	-0.04091	
5.0698	0.00027	-0.00112	-0.00505	-0.01095	-0.01790	-0.02485	-0.03075	-0.03468	-0.03607	
5.7941	0.00087	-0.00046	-0.00423	-0.00987	-0.01653	-0.02320	-0.02884	-0.03261	-0.03394	
6.5184	0.00239	0.00114	-0.00241	-0.00773	-0.01400	-0.02027	-0.02559	-0.02914	-0.03039	
7.2426	0.00305	0.00186	-0.00153	-0.00661	-0.01260	-0.01859	-0.02366	-0.02706	-0.02825	
7.9669	0.00434	0.00322	0.00002	-0.00477	-0.01042	-0.01606	-0.02085	-0.02405	-0.02517	
8.6911	0.00494	0.00387	0.00084	-0.00370	-0.00906	-0.01442	-0.01896	-0.02200	-0.02306	
9.4154	0.00606	0.00505	0.00220	-0.00253	-0.00712	-0.01216	-0.01643	-0.01928	-0.02029	
10.1397	0.00711	0.00576	0.00308	-0.00094	-0.00568	-0.01042	-0.01444	-0.01712	-0.01807	
10.8639	0.00800	0.00713	0.00462	0.00087	-0.00355	-0.00797	-0.01172	-0.01422	-0.01510	
11.5882	0.00871	0.00790	0.00559	0.00213	-0.00196	-0.00604	-0.00950	-0.01181	-0.01263	
12.3124	0.01038	0.00964	0.00753	0.00436	0.00063	-0.00311	-0.00627	-0.00835	-0.00913	
13.0367	0.01105	0.01039	0.00851	0.00569	0.00236	-0.00096	-0.00378	-0.00566	-0.00632	
13.7610	0.01238	0.01180	0.01014	0.00765	0.00472	-0.00179	-0.00070	-0.00236	-0.00294	
14.5023	0.01363	0.01315	0.01177	0.00970	0.00726	0.00481	0.00275	-0.00136	-0.00088	
15.2436	0.01510	0.01472	0.01350	0.01165	0.01417	0.01228	0.01068	0.00961	0.00924	
15.9849	0.01671	0.01631	0.01519	0.01308	0.01707	0.01606	0.01520	0.01463	0.01443	
16.7262	0.01845	0.01815	0.01704	0.01484	0.01883	0.01806	0.01733	0.01681	0.01644	
17.4675	0.02031	0.02001	0.01890	0.01670	0.02067	0.02006	0.01938	0.01900	0.01861	
18.2088	0.02228	0.02208	0.02100	0.01880	0.02287	0.02237	0.02162	0.02131	0.02092	
18.9501	0.02436	0.02416	0.02310	0.02090	0.02487	0.02437	0.02362	0.02331	0.02292	
19.6914	0.02654	0.02634	0.02530	0.02310	0.02697	0.02647	0.02572	0.02541	0.02502	
20.4327	0.02881	0.02861	0.02760	0.02540	0.02927	0.02877	0.02802	0.02771	0.02732	
21.1740	0.03118	0.03098	0.03000	0.02780	0.03167	0.03117	0.03042	0.03011	0.02972	
21.9153	0.03365	0.03345	0.03250	0.03030	0.03417	0.03367	0.03292	0.03261	0.03222	
22.6566	0.03612	0.03592	0.03500	0.03280	0.03667	0.03617	0.03542	0.03511	0.03472	
23.3979	0.03859	0.03839	0.03750	0.03530	0.03917	0.03867	0.03792	0.03761	0.03722	
24.1392	0.04106	0.04086	0.04000	0.03780	0.04167	0.04117	0.04042	0.04011	0.03972	
24.8805	0.04353	0.04333	0.04250	0.04030	0.04417	0.04367	0.04292	0.04261	0.04222	
25.6218	0.04600	0.04580	0.04500	0.04280	0.04667	0.04617	0.04542	0.04511	0.04472	
26.3631	0.04847	0.04827	0.04750	0.04530	0.04917	0.04867	0.04792	0.04761	0.04722	
27.1044	0.05094	0.05074	0.05000	0.04780	0.05167	0.05117	0.05042	0.05011	0.04972	
27.8457	0.05341	0.05321	0.05250	0.05030	0.05417	0.05367	0.05292	0.05261	0.05222	
28.5870	0.05588	0.05568	0.05500	0.05280	0.05667	0.05617	0.05542	0.05511	0.05472	
29.3283	0.05835	0.05815	0.05750	0.05530	0.05917	0.05867	0.05792	0.05761	0.05722	
30.0696	0.06082	0.06062	0.06000	0.05780	0.06167	0.06117	0.06042	0.06011	0.05972	
30.8109	0.06329	0.06309	0.06250	0.06030	0.06417	0.06367	0.06292	0.06261	0.06222	
31.5522	0.06576	0.06556	0.06500	0.06280	0.06667	0.06617	0.06542	0.06511	0.06472	
32.2935	0.06823	0.06803	0.06750	0.06530	0.06917	0.06867	0.06792	0.06761	0.06722	
33.0348	0.07070	0.07050	0.07000	0.06780	0.07167	0.07117	0.07042	0.07011	0.06972	
33.7761	0.07317	0.07297	0.07250	0.07030	0.07417	0.07367	0.07292	0.07261	0.07222	
34.5174	0.07564	0.07544	0.07500	0.07280	0.07667	0.07617	0.07542	0.07511	0.07472	
35.2587	-0.00143	-0.00062	0.00167	0.00510	0.00915	0.01320	0.01663	0.01892	0.01973	

RACIAL(VR)	0.0000	22.5000	45.0000	67.5000	90.0000	112.5000	135.0000	157.5000	180.0000
THETA(DEG.)									
X									
0.0000	0.06980	0.07733	0.09878	0.13087	0.16873	0.20658	0.23867	0.26012	0.26765
0.7243	0.07603	0.08356	0.10501	0.13710	0.17496	0.21281	0.24490	0.26635	0.27388
1.4485	0.04391	0.05152	0.07319	0.10561	0.14387	0.18212	0.21455	0.23621	0.24382
2.1728	0.00905	0.01681	0.03893	0.07202	0.11105	0.15009	0.18318	0.20529	0.21305
2.8970	0.00551	0.01329	0.03545	0.06861	0.10772	0.14683	0.17999	0.20214	0.20992
3.6213	-0.00626	0.00156	0.02383	0.05715	0.09646	0.13576	0.16909	0.19135	0.19917
4.3456	-0.01079	-0.00296	0.01934	0.05272	0.09209	0.13146	0.16484	0.18714	0.19498
5.0698	-0.01777	-0.00991	0.01244	0.04590	0.08538	0.12485	0.15831	0.18066	0.18852
5.7941	-0.02206	-0.01420	0.00819	0.04169	0.08122	0.12074	0.15425	0.17664	0.18450
6.5184	-0.02759	-0.01972	0.00271	0.03628	0.07587	0.11546	0.14902	0.17145	0.17933
7.2426	-0.03165	-0.02377	-0.00131	0.03229	0.07193	0.11157	0.14517	0.16751	0.17551
7.9669	-0.03667	-0.02877	-0.00629	0.02736	0.06705	0.10674	0.14039	0.16287	0.17077
8.6911	-0.04058	-0.03268	-0.01017	0.02351	0.06324	0.10298	0.13666	0.15917	0.16707
9.4154	-0.04529	-0.03738	-0.01485	0.01887	0.05865	0.09843	0.13215	0.15468	0.16259
10.1397	-0.04935	-0.04143	-0.01888	0.01488	0.05469	0.09450	0.12826	0.15081	0.15873
10.8639	-0.05448	-0.04655	-0.02398	0.00981	0.04966	0.08952	0.12330	0.14588	0.15381
11.5882	-0.05896	-0.05103	-0.02843	0.00538	0.04527	0.08516	0.11898	0.14157	0.14951
12.3124	-0.06507	-0.05713	-0.03451	-0.00066	0.03927	0.07920	0.11305	0.13566	0.14361
13.0367	-0.07015	-0.06220	-0.03956	-0.00569	0.03427	0.07423	0.10811	0.13075	0.13870
13.7610	-0.07630	-0.06835	-0.04569	-0.01179	0.02820	0.06819	0.10210	0.12475	0.13271
14.5023	-0.08310	-0.07513	-0.05246	-0.01853	0.02149	0.06151	0.09544	0.11811	0.12607
15.2436	-0.09731	-0.08934	-0.06665	-0.03268	0.00738	0.04744	0.08140	0.10409	0.11206
15.9849	-0.10671	-0.09874	-0.07403	-0.04206	-0.00198	0.03809	0.07207	0.09477	0.10274
16.7262	-0.10419	-0.09622	-0.07352	-0.03955	-0.00053	0.04060	0.07458	0.09728	0.10525
17.4675	-0.10486	-0.09689	-0.07419	-0.04022	-0.00014	0.03993	0.07391	0.09661	0.10458
18.2088	-0.10468	-0.09671	-0.07401	-0.04004	0.00004	0.04011	0.07409	0.09679	0.10476
18.9501	-0.10473	-0.09676	-0.07406	-0.04008	-0.00001	0.04006	0.07404	0.09674	0.10471
19.6914	-0.10472	-0.09675	-0.07405	-0.04007	0.00000	0.04008	0.07405	0.09675	0.10472
20.4327	-0.10472	-0.09675	-0.07405	-0.04008	-0.00000	0.04007	0.07405	0.09675	0.10472
21.1740	-0.10472	-0.09675	-0.07405	-0.04007	0.00000	0.04007	0.07405	0.09675	0.10472
21.9153	-0.10472	-0.09675	-0.07405	-0.04007	0.00000	0.04007	0.07405	0.09675	0.10472
22.6566	-0.10472	-0.09675	-0.07405	-0.04007	0.00000	0.04007	0.07405	0.09675	0.10472
23.3979	-0.10472	-0.09675	-0.07405	-0.04007	0.00000	0.04007	0.07405	0.09675	0.10472
24.1392	-0.10472	-0.09675	-0.07405	-0.04007	0.00000	0.04007	0.07405	0.09675	0.10472
24.8805	-0.10472	-0.09675	-0.07405	-0.04007	0.00000	0.04007	0.07405	0.09675	0.10472
25.6218	-0.10472	-0.09675	-0.07405	-0.04007	0.00000	0.04007	0.07405	0.09675	0.10472
26.3631	-0.10472	-0.09675	-0.07405	-0.04008	0.00000	0.04007	0.07405	0.09675	0.10472
27.1044	-0.10471	-0.09674	-0.07404	-0.04007	0.00001	0.04008	0.07405	0.09675	0.10473
27.8457	-0.10474	-0.09677	-0.07407	-0.04010	-0.00002	0.04005	0.07405	0.09675	0.10470
28.5870	-0.10463	-0.09666	-0.07396	-0.03998	0.00009	0.04017	0.07414	0.09684	0.10481
29.3283	-0.10506	-0.09709	-0.07439	-0.04041	0.00034	0.03973	0.07371	0.09641	0.10438
30.0696	-0.10872	-0.10174	-0.07904	-0.04507	-0.00300	0.03508	0.06905	0.09175	0.09972
30.8109	-0.11810	-0.11013	-0.08743	-0.05347	-0.01340	0.02667	0.06064	0.08334	0.09131
31.5522	-0.12578	-0.11781	-0.09512	-0.06116	-0.02110	0.01895	0.05291	0.07560	0.08357
32.2935	-0.13186	-0.12390	-0.10122	-0.06728	-0.02724	0.01280	0.04674	0.06942	0.07738
33.0348	-0.14009	-0.13214	-0.10948	-0.07556	-0.03556	0.00446	0.03836	0.06102	0.06898
33.7761	-0.14989	-0.14194	-0.11931	-0.08545	-0.04550	-0.00555	0.02832	0.05094	0.05889
34.5174	-0.15255	-0.14461	-0.12201	-0.08818	-0.04828	-0.00838	0.02545	0.04805	0.05599
35.2587	-0.14441	-0.13647	-0.11387	-0.08003	-0.04012	-0.00020	0.03363	0.05624	0.06418

TANGENTIAL(VT)

Y	THETA(DEG.)	0.0000	22.5000	45.0000	67.5000	90.0000	112.5000	135.0000	157.5000	180.0000
0.0000	0.0000	-0.00000	-0.02800	-0.05174	-0.06760	-0.07316	-0.06760	-0.05174	-0.02800	-0.00000
0.7243	0.0000	-0.00000	-0.02800	-0.05174	-0.06760	-0.07316	-0.06760	-0.05174	-0.02800	-0.00000
1.4485	0.0000	-0.00000	-0.02816	-0.05202	-0.06797	-0.07316	-0.06797	-0.05202	-0.02816	-0.00000
2.1728	0.0000	-0.00000	-0.03396	-0.06275	-0.08198	-0.08874	-0.08198	-0.06275	-0.03396	-0.00000
2.8970	0.0000	-0.00000	-0.03384	-0.06252	-0.08168	-0.08842	-0.08168	-0.06252	-0.03384	-0.00000
3.6213	0.0000	-0.00000	-0.03527	-0.06518	-0.08516	-0.09218	-0.08516	-0.06518	-0.03527	-0.00000
4.3456	0.0000	-0.00000	-0.03545	-0.06550	-0.08559	-0.09264	-0.08559	-0.06550	-0.03545	-0.00000
5.0698	0.0000	-0.00000	-0.03615	-0.06680	-0.08728	-0.09447	-0.08728	-0.06680	-0.03615	-0.00000
5.7941	0.0000	-0.00000	-0.03641	-0.06728	-0.08790	-0.09515	-0.08790	-0.06728	-0.03641	-0.00000
6.5184	0.0000	-0.00000	-0.03690	-0.06818	-0.08909	-0.09643	-0.08909	-0.06818	-0.03690	-0.00000
7.2426	0.0000	-0.00000	-0.03718	-0.06870	-0.08976	-0.09716	-0.08976	-0.06870	-0.03718	-0.00000
7.9669	0.0000	-0.00000	-0.03758	-0.06944	-0.09073	-0.09820	-0.09073	-0.06944	-0.03758	-0.00000
8.6911	0.0000	-0.00000	-0.03788	-0.06998	-0.09144	-0.09897	-0.09144	-0.06998	-0.03788	-0.00000
9.4154	0.0000	-0.00000	-0.03822	-0.07063	-0.09228	-0.09988	-0.09228	-0.07063	-0.03822	-0.00000
10.1397	0.0000	-0.00000	-0.03853	-0.07119	-0.09301	-0.10067	-0.09301	-0.07119	-0.03853	-0.00000
10.8639	0.0000	-0.00000	-0.03886	-0.07180	-0.09382	-0.10155	-0.09382	-0.07180	-0.03886	-0.00000
11.5882	0.0000	-0.00000	-0.03920	-0.07244	-0.09465	-0.10245	-0.09465	-0.07244	-0.03920	-0.00000
12.3124	0.0000	-0.00000	-0.03956	-0.07309	-0.09550	-0.10337	-0.09550	-0.07309	-0.03956	-0.00000
13.0367	0.0000	-0.00000	-0.03998	-0.07387	-0.09651	-0.10447	-0.09651	-0.07387	-0.03998	-0.00000
13.7610	0.0000	-0.00000	-0.04034	-0.07454	-0.09759	-0.10542	-0.09759	-0.07454	-0.04034	-0.00000
14.5023	0.0000	-0.00000	-0.04082	-0.07543	-0.09856	-0.10668	-0.09856	-0.07543	-0.04082	-0.00000
15.2436	0.0000	-0.00000	-0.04136	-0.07643	-0.09986	-0.10809	-0.09986	-0.07643	-0.04136	-0.00000
15.9849	0.0000	-0.00000	-0.04229	-0.07814	-0.10210	-0.11051	-0.10210	-0.07814	-0.04229	-0.00000
16.7262	0.0000	-0.00000	-0.04270	-0.07891	-0.10310	-0.11159	-0.10310	-0.07891	-0.04270	-0.00000
17.4675	0.0000	-0.00000	-0.04281	-0.07910	-0.10335	-0.11186	-0.10335	-0.07910	-0.04281	-0.00000
18.2088	0.0000	-0.00000	-0.04269	-0.07889	-0.10307	-0.11156	-0.10307	-0.07889	-0.04269	-0.00000
18.9501	0.0000	-0.00000	-0.04246	-0.07845	-0.10251	-0.11095	-0.10251	-0.07845	-0.04246	-0.00000
19.6914	0.0000	-0.00000	-0.04217	-0.07791	-0.10180	-0.11019	-0.10180	-0.07791	-0.04217	-0.00000
20.4327	0.0000	-0.00000	-0.04186	-0.07735	-0.10106	-0.10939	-0.10106	-0.07735	-0.04186	-0.00000
21.1740	0.0000	-0.00000	-0.04157	-0.07681	-0.10036	-0.10862	-0.10036	-0.07681	-0.04157	-0.00000
21.9153	0.0000	-0.00000	-0.04131	-0.07632	-0.09972	-0.10794	-0.09972	-0.07632	-0.04131	-0.00000
22.6566	0.0000	-0.00000	-0.04108	-0.07591	-0.09918	-0.10735	-0.09918	-0.07591	-0.04108	-0.00000
23.3979	0.0000	-0.00000	-0.04090	-0.07556	-0.09873	-0.10686	-0.09873	-0.07556	-0.04090	-0.00000
24.1392	0.0000	-0.00000	-0.04075	-0.07529	-0.09837	-0.10647	-0.09837	-0.07529	-0.04075	-0.00000
24.8805	0.0000	-0.00000	-0.04063	-0.07507	-0.09808	-0.10616	-0.09808	-0.07507	-0.04063	-0.00000
25.6218	0.0000	-0.00000	-0.04054	-0.07490	-0.09786	-0.10592	-0.09786	-0.07490	-0.04054	-0.00000
26.3631	0.0000	-0.00000	-0.04047	-0.07477	-0.09770	-0.10574	-0.09770	-0.07477	-0.04047	-0.00000
27.1044	0.0000	-0.00000	-0.04041	-0.07468	-0.09757	-0.10561	-0.09757	-0.07468	-0.04041	-0.00000
27.8457	0.0000	-0.00000	-0.04038	-0.07461	-0.09748	-0.10551	-0.09748	-0.07461	-0.04038	-0.00000
28.5870	0.0000	-0.00000	-0.04035	-0.07455	-0.09741	-0.10543	-0.09741	-0.07455	-0.04035	-0.00000
29.3283	0.0000	-0.00000	-0.04032	-0.07451	-0.09735	-0.10537	-0.09735	-0.07451	-0.04032	-0.00000
30.0696	0.0000	-0.00000	-0.04040	-0.07464	-0.09753	-0.10556	-0.09753	-0.07464	-0.04040	-0.00000
30.8109	0.0000	-0.00000	-0.04073	-0.07526	-0.09833	-0.10643	-0.09833	-0.07526	-0.04073	-0.00000
31.5522	0.0000	-0.00000	-0.04125	-0.07623	-0.09960	-0.10780	-0.09960	-0.07623	-0.04125	-0.00000
32.2935	0.0000	-0.00000	-0.04181	-0.07726	-0.10094	-0.10926	-0.10094	-0.07726	-0.04181	-0.00000
33.0348	0.0000	-0.00000	-0.04234	-0.07823	-0.10222	-0.11064	-0.10222	-0.07823	-0.04234	-0.00000
33.7761	0.0000	-0.00000	-0.04294	-0.07935	-0.10367	-0.11222	-0.10367	-0.07935	-0.04294	-0.00000
34.5174	0.0000	-0.00000	-0.04341	-0.08020	-0.10479	-0.11342	-0.10479	-0.08020	-0.04341	-0.00000
35.2587	0.0000	-0.00000	-0.04328	-0.07996	-0.10448	-0.11308	-0.10448	-0.07996	-0.04328	-0.00000

VELOCITY COMPONENTS ON WING PANELS DUE TO BODY PANEL PRESSURE SINGULARITIES

AXIAL (U)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	-0.00162	0.00033	0.00319	0.00195	0.00179	0.00086	-0.00018	0.00012	-0.00147	-0.00103
2	0.00068	0.00436	-0.00288	0.00126	0.00064	-0.00021	0.00003	-0.00133	-0.00112	-0.00249
3	0.00668	0.00803	0.01687	0.00050	-0.00035	-0.00025	-0.00162	-0.00117	-0.00266	-0.00144
4	0.01016	0.00300	0.00032	-0.00016	-0.00074	-0.00242	-0.00129	-0.00277	-0.00135	-0.00108
5	0.00599	0.00136	0.00048	0.00014	-0.00340	-0.00137	-0.00320	-0.00152	-0.00022	-0.00010
6	0.00375	0.00145	-0.00081	-0.00025	-0.00154	-0.00455	-0.00167	-0.00010	-0.00057	-0.00043
7	0.00377	-0.00045	0.00004	-0.00183	-0.00132	-0.00190	-0.00049	-0.00051	0.00049	0.00029
8	0.00073	0.00037	-0.00257	-0.00141	-0.00223	-0.00043	-0.00056	0.00046	0.00030	0.00049
9	0.00132	-0.00295	-0.00115	-0.00266	-0.00029	-0.00063	0.00070	0.00031	0.00002	0.00018
10	-0.00389	-0.00248	-0.00159	0.00019	-0.00079	0.00097	0.00030	0.00001	0.00004	0.00019

TRANSVERSE (V)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	0.00452	0.00007	-0.00488	-0.00352	-0.00343	-0.00199	-0.00031	-0.00064	0.00189	0.00139
2	0.00072	-0.00673	0.00337	-0.00292	-0.00189	-0.00047	-0.00063	0.00159	0.00144	0.00363
3	-0.01002	-0.01350	-0.02684	-0.00210	-0.00056	-0.00042	0.00188	0.00144	0.00385	0.00213
4	-0.01793	-0.00745	-0.00264	-0.00136	-0.00001	0.00287	0.00151	0.00395	0.00201	0.00164
5	-0.01586	-0.00620	-0.00337	-0.00189	0.00397	0.00145	0.00449	0.00223	0.00035	0.00019
6	-0.01600	-0.00743	-0.00166	-0.00135	0.00140	0.00633	0.00240	0.00016	0.00091	0.00069
7	-0.01924	-0.00529	-0.00306	0.00127	0.00123	0.00264	0.00072	0.00083	-0.00069	-0.00037
8	-0.01760	-0.00690	0.00113	0.00089	0.00294	0.00056	0.00087	-0.00066	-0.00042	-0.00070
9	-0.02023	-0.00169	-0.00059	-0.00317	0.00023	0.00095	-0.00101	-0.00044	-0.00001	-0.00024
10	-0.01337	-0.00168	0.00062	-0.00076	0.00109	-0.00144	-0.00042	-0.00001	-0.00004	-0.00027

VERTICAL (W)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	0.02600	0.01023	0.00683	0.00500	0.00497	0.00480	0.00443	0.00422	0.00386	0.00348
2	0.04572	0.01432	0.00763	0.00682	0.00627	0.00554	0.00511	0.00457	0.00424	0.00351
3	0.06508	0.01802	0.01118	0.00880	0.00727	0.00638	0.00556	0.00503	0.00437	0.00368
4	0.08566	0.02214	0.01399	0.01025	0.00844	0.00693	0.00609	0.00522	0.00472	0.00385
5	0.10355	0.02870	0.01633	0.01187	0.00936	0.00766	0.00639	0.00557	0.00487	0.00393
6	0.12660	0.03353	0.01868	0.01328	0.01007	0.00813	0.00680	0.00586	0.00487	0.00391
7	0.14709	0.03801	0.02102	0.01421	0.01096	0.00857	0.00718	0.00584	0.00500	0.00402
8	0.16568	0.04265	0.02247	0.01548	0.01130	0.00907	0.00720	0.00597	0.00502	0.00400
9	0.18273	0.04543	0.02449	0.01594	0.01201	0.00916	0.00737	0.00605	0.00488	0.00400
10	0.19324	0.04899	0.02524	0.01706	0.01215	0.00942	0.00747	0.00591	0.00484	0.00401

VELOCITY COMPONENTS ON WING PANELS DUE TO BODY LINE SOURCES AND DOUBLETS

AXIAL (U)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	0.01160	0.01127	0.00687	0.00506	0.00392	0.00304	0.00243	0.00199	0.00165	0.00136
2	0.01424	0.00795	0.00583	0.00439	0.00335	0.00265	0.00214	0.00177	0.00148	0.00127
3	0.00970	0.00699	0.00502	0.00374	0.00291	0.00233	0.00190	0.00158	0.00134	0.00119
4	0.00877	0.00588	0.00425	0.00324	0.00255	0.00206	0.00170	0.00143	0.00122	0.00112
5	0.00718	0.00496	0.00368	0.00283	0.00226	0.00184	0.00153	0.00130	0.00111	0.00105
6	0.00604	0.00427	0.00320	0.00250	0.00201	0.00165	0.00139	0.00118	0.00102	0.00100
7	0.00516	0.00369	0.00280	0.00221	0.00180	0.00150	0.00126	0.00109	0.00097	0.00093
8	0.00442	0.00321	0.00247	0.00198	0.00162	0.00136	0.00116	0.00101	0.00090	0.00090
9	0.00382	0.00282	0.00220	0.00178	0.00147	0.00125	0.00106	0.00101	0.00093	0.00117
10	0.00333	0.00250	0.00197	0.00161	0.00135	0.00112	0.00167	0.00397	0.00543	0.00220

TRANSVERSE (V)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	0.00543	-0.00701	-0.00546	-0.00487	-0.00423	-0.00351	-0.00296	-0.00253	-0.00219	-0.00185
2	0.00100	-0.00408	-0.00502	-0.00454	-0.00380	-0.00322	-0.00274	-0.00236	-0.00205	-0.00178
3	0.00407	-0.00436	-0.00473	-0.00412	-0.00352	-0.00300	-0.00257	-0.00223	-0.00195	-0.00172
4	0.00249	-0.00411	-0.00438	-0.00388	-0.00332	-0.00283	-0.00244	-0.00212	-0.00186	-0.00167
5	0.00235	-0.00396	-0.00421	-0.00370	-0.00316	-0.00271	-0.00234	-0.00204	-0.00179	-0.00162
6	0.00187	-0.00399	-0.00410	-0.00358	-0.00305	-0.00261	-0.00226	-0.00197	-0.00174	-0.00159
7	0.00128	-0.00404	-0.00404	-0.00350	-0.00298	-0.00255	-0.00220	-0.00193	-0.00175	-0.00153
8	0.00072	-0.00414	-0.00403	-0.00345	-0.00293	-0.00250	-0.00217	-0.00191	-0.00175	-0.00153
9	0.00014	-0.00428	-0.00405	-0.00344	-0.00290	-0.00248	-0.00213	-0.00187	-0.00162	-0.00148
10	-0.00045	-0.00445	-0.00410	-0.00344	-0.00290	-0.00242	-0.00216	-0.00187	-0.00165	-0.00149

VERTICAL (W)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	0.06109	0.02978	0.01711	0.01098	0.00755	0.00546	0.00412	0.00321	0.00258	0.00199
2	0.06317	0.02928	0.01671	0.01066	0.00731	0.00530	0.00401	0.00314	0.00253	0.00197
3	0.06277	0.02888	0.01630	0.01035	0.00712	0.00518	0.00393	0.00309	0.00250	0.00195
4	0.06264	0.02835	0.01591	0.01011	0.00696	0.00508	0.00387	0.00305	0.00247	0.00194
5	0.06200	0.02783	0.01559	0.00991	0.00684	0.00501	0.00383	0.00302	0.00245	0.00192
6	0.06133	0.02739	0.01533	0.00976	0.00675	0.00495	0.00379	0.00300	0.00244	0.00191
7	0.06071	0.02703	0.01513	0.00964	0.00668	0.00491	0.00377	0.00300	0.00242	0.00190
8	0.06017	0.02675	0.01498	0.00956	0.00663	0.00488	0.00374	0.00297	0.00246	0.00190
9	0.05976	0.02654	0.01487	0.00950	0.00660	0.00486	0.00373	0.00297	0.00246	0.00190
10	0.05946	0.02640	0.01480	0.00946	0.00657	0.00484	0.00375	0.00299	0.00253	0.00194

VELOCITY COMPONENTS ON WING PANELS DUE TO WING PANEL PRESSURE SINGULARITIES

AXIAL(U)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	0.08732	0.10456	0.11606	0.12644	0.13618	0.14457	0.15156	0.15736	0.16407	0.26144
2	0.05305	0.06110	0.06789	0.07433	0.07938	0.08339	0.08656	0.08917	0.09606	0.14600
3	0.04340	0.04878	0.05427	0.05829	0.06115	0.06323	0.06459	0.06645	0.08025	0.10417
4	0.03934	0.04306	0.04699	0.04930	0.05076	0.05134	0.05181	0.05411	0.06970	0.07689
5	0.03654	0.03994	0.04170	0.04271	0.04275	0.04248	0.04273	0.04651	0.05846	0.05362
6	0.03577	0.03666	0.03711	0.03667	0.03569	0.03518	0.03513	0.04122	0.04655	0.04124
7	0.03397	0.03334	0.03223	0.03049	0.02937	0.02894	0.02994	0.03709	0.03512	0.03063
8	0.03129	0.02890	0.02609	0.02425	0.02322	0.02304	0.02463	0.03113	0.02443	0.02602
9	0.02686	0.02207	0.01923	0.01770	0.01712	0.01701	0.01929	0.02306	0.01460	0.00915
10	0.01781	0.01315	0.01120	0.01059	0.01008	0.01026	0.01238	0.01301	0.00818	-0.00418

TRANSVERSE(V)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	-0.23989	-0.28726	-0.31885	-0.34737	-0.37414	-0.39718	-0.41638	-0.43232	-0.45077	-0.71827
2	-0.14575	-0.16786	-0.18652	-0.20420	-0.21809	-0.22911	-0.23781	-0.24497	-0.26392	-0.45010
3	-0.11923	-0.13401	-0.14909	-0.16013	-0.16799	-0.17372	-0.17744	-0.18255	-0.22059	-0.37667
4	-0.10808	-0.11830	-0.12910	-0.13545	-0.13944	-0.14104	-0.14235	-0.14864	-0.19149	-0.32161
5	-0.10039	-0.10973	-0.11455	-0.11734	-0.11746	-0.11669	-0.11736	-0.12778	-0.16661	-0.30347
6	-0.09827	-0.10673	-0.11096	-0.10073	-0.09806	-0.09666	-0.09815	-0.11325	-0.12787	-0.29573
7	-0.09333	-0.09159	-0.08854	-0.08375	-0.08067	-0.07942	-0.08226	-0.10190	-0.09647	-0.29359
8	-0.08597	-0.07941	-0.07169	-0.06662	-0.06378	-0.06329	-0.06765	-0.08552	-0.06710	-0.25596
9	-0.07380	-0.06062	-0.05282	-0.04861	-0.04703	-0.04672	-0.05297	-0.06335	-0.04011	-0.30300
10	-0.04893	-0.03611	-0.03076	-0.02908	-0.02769	-0.02819	-0.03399	-0.03573	-0.01696	-0.31729

VERTICAL(W)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	-0.19182	-0.14473	-0.12866	-0.12070	-0.11725	-0.11498	-0.11327	-0.11215	-0.11116	-0.11018
2	-0.21361	-0.14832	-0.12906	-0.12220	-0.11830	-0.11557	-0.11385	-0.11243	-0.11150	-0.11019
3	-0.23257	-0.15162	-0.13220	-0.12387	-0.11910	-0.11628	-0.11421	-0.11284	-0.11159	-0.11035
4	-0.25302	-0.15521	-0.13462	-0.12508	-0.12012	-0.11673	-0.11494	-0.11300	-0.11191	-0.11050
5	-0.27027	-0.16125	-0.13664	-0.12650	-0.12092	-0.11738	-0.11531	-0.11331	-0.11204	-0.11057
6	-0.29265	-0.16564	-0.13873	-0.12775	-0.12154	-0.11780	-0.11531	-0.11358	-0.11202	-0.11054
7	-0.31251	-0.16975	-0.14087	-0.12857	-0.12236	-0.11820	-0.11567	-0.11354	-0.11214	-0.11065
8	-0.33057	-0.17412	-0.14216	-0.12857	-0.12266	-0.11867	-0.11566	-0.11366	-0.11219	-0.11061
9	-0.34721	-0.17669	-0.14408	-0.13015	-0.12333	-0.11873	-0.11582	-0.11377	-0.11213	-0.11062
10	-0.35742	-0.18011	-0.14475	-0.13124	-0.12344	-0.11897	-0.11594	-0.11371	-0.11209	-0.11066

VELOCITY COMPONENTS ON WING PANELS DUE TO WING SOURCES

AXIAL (U)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	-0.01440	-0.00890	-0.00478	-0.00453	0.00006	0.00447	0.00827	0.01187	0.01396	0.02115
2	-0.00055	0.00571	0.00660	0.01170	0.01665	0.02079	0.02464	0.02833	0.03246	0.03324
3	0.00248	0.00525	0.01117	0.01686	0.02146	0.02562	0.02955	0.03261	0.02751	0.03262
4	0.00111	0.00890	0.01577	0.02102	0.02559	0.02983	0.02670	0.02599	0.03168	0.03260
5	0.00358	0.01288	0.01916	0.02431	0.02894	0.02619	0.02523	0.02511	0.03137	0.03163
6	0.00683	0.01516	0.02120	0.02638	0.02410	0.02278	0.02257	0.02200	0.02799	0.03605
7	0.00794	0.01569	0.02170	0.02003	0.01817	0.01782	0.01753	0.01797	0.02221	0.02576
8	0.00975	0.01734	0.01654	0.01377	0.01324	0.01324	0.01153	0.01510	0.01631	0.01904
9	0.01198	0.01277	0.00819	0.00736	0.00726	0.00553	0.00486	0.00956	0.00830	0.01327
10	0.00776	-0.00238	-0.00373	-0.00400	-0.00576	-0.00654	-0.00698	-0.00204	-0.00606	0.00818

TRANSVERSE (V)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	-0.00990	-0.00165	-0.00346	-0.00193	-0.00797	-0.01444	-0.02038	-0.02624	-0.02998	-0.03721
2	-0.03844	-0.03647	-0.03468	-0.04112	-0.04835	-0.05488	-0.06121	-0.06746	-0.06239	-0.07989
3	-0.03705	-0.03405	-0.04107	-0.04940	-0.05674	-0.06370	-0.07048	-0.06598	-0.06220	-0.08955
4	-0.02826	-0.03662	-0.04681	-0.05540	-0.06325	-0.07074	-0.06693	-0.06631	-0.05424	-0.09852
5	-0.02383	-0.03892	-0.04981	-0.05906	-0.06754	-0.06463	-0.06377	-0.06398	-0.04508	-0.10480
6	-0.01972	-0.03741	-0.04929	-0.05935	-0.05767	-0.05646	-0.05663	-0.05614	-0.03320	-0.10924
7	-0.01147	-0.03144	-0.04452	-0.04472	-0.04303	-0.04314	-0.04314	-0.03854	-0.01699	-0.11148
8	-0.00613	-0.02862	-0.03235	-0.02989	-0.02994	-0.03049	-0.02825	-0.02017	-0.00217	-0.11186
9	-0.00225	-0.01687	-0.01301	-0.01300	-0.01356	-0.01139	-0.01062	-0.00006	0.01456	-0.11281
10	0.01124	0.01859	0.01863	0.01804	0.02012	0.02100	0.02147	0.03342	0.04341	-0.11386

VERTICAL (W)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	0.12128	0.12101	0.12101	0.12101	0.12101	0.12101	0.12101	0.12101	0.12101	0.12101
2	0.05126	0.05124	0.05124	0.05124	0.05124	0.05124	0.05124	0.05124	0.05124	0.05124
3	0.02572	0.02572	0.02572	0.02572	0.02572	0.02572	0.02572	0.02572	0.02572	0.02572
4	0.00823	0.00823	0.00823	0.00823	0.00823	0.00823	0.00823	0.00823	0.00823	0.00823
5	-0.00756	-0.00756	-0.00756	-0.00756	-0.00756	-0.00756	-0.00756	-0.00756	-0.00756	-0.00756
6	-0.02223	-0.02223	-0.02223	-0.02223	-0.02223	-0.02223	-0.02223	-0.02223	-0.02223	-0.02223
7	-0.03307	-0.03307	-0.03307	-0.03307	-0.03307	-0.03307	-0.03307	-0.03307	-0.03307	-0.03307
8	-0.04051	-0.04051	-0.04051	-0.04051	-0.04051	-0.04051	-0.04051	-0.04051	-0.04051	-0.04051
9	-0.04775	-0.04775	-0.04775	-0.04775	-0.04775	-0.04775	-0.04775	-0.04775	-0.04775	-0.04775
10	-0.05507	-0.05507	-0.05507	-0.05507	-0.05507	-0.05507	-0.05507	-0.05507	-0.05507	-0.05507

VELOCITY COMPONENTS ON BODY PANELS DUE TO BODY PANEL PRESSURE SINGULARITIES

AXIAL (U)		12.5000		37.5000		62.5000		88.7967		116.0950		142.5000		167.5000	
THETA (DEG.)		12.5000		37.5000		62.5000		88.7967		116.0950		142.5000		167.5000	
ROW NO.		12.5000		37.5000		62.5000		88.7967		116.0950		142.5000		167.5000	
1	0.00000	0.00000	0.00001	0.00003	0.00157	-0.00919	-0.00091	-0.00028							
2	0.00002	0.00056	0.00186	0.01869	-0.02887	-0.02887	-0.00078								
3	0.00191	0.00112	0.00864	0.01959	-0.02301	-0.01412	0.00458								
4	0.00373	0.00749	0.01312	0.02432	-0.01624	-0.00639	-0.00849								
5	0.00523	0.01032	0.01549	0.02487	-0.01378	-0.01207	-0.01398								
6	0.00696	0.01067	0.01737	0.02352	-0.01513	-0.01649	-0.01586								
7	0.00877	0.01164	0.01605	0.02275	-0.01654	-0.01731	-0.01767								
8	0.01063	0.01159	0.01500	0.01999	-0.01666	-0.01814	-0.01809								
9	0.01071	0.01195	0.01474	0.01773	-0.01679	-0.01854	-0.01922								
10	0.01056	0.01213	0.01421	0.01525	-0.01567	-0.01862	-0.01935								
11	0.01035	0.01055	0.00945	0.00297	-0.01311	-0.01619	-0.01871								
12	0.01334	0.01075	0.00494	-0.00197	-0.00752	-0.01062	-0.01215								
13	0.00813	0.00693	0.00446	0.00076	-0.00331	-0.00647	-0.00830								
14	0.00461	0.00386	0.00233	0.00020	-0.00187	-0.00345	-0.00420								

TRANSVERSE (V)

THETA(DEG.)		12.5000	37.5000	62.5000	88.7967	116.0950	142.5000	167.5000
ROW NO.								
1	-0.00000	-0.00001	-0.00003	-0.00521	0.01925	0.00148	0.00031	
2	-0.00009	0.00008	-0.00118	-0.05481	0.07330	0.00122	0.00056	
3	0.00044	-0.00210	-0.00471	-0.10807	0.11521	0.00488	0.00131	
4	0.00331	-0.00296	-0.01780	-0.16279	0.14329	0.00404	-0.00525	
5	-0.00174	-0.00432	-0.02897	-0.21270	0.17291	0.01354	-0.00131	
6	-0.00240	-0.00904	-0.03908	-0.25731	0.20434	0.02431	0.00161	
7	-0.00029	-0.00843	-0.04989	-0.30072	0.23366	0.03397	0.00426	
8	-0.00153	-0.01098	-0.05969	-0.34145	0.26137	0.04130	0.00616	
9	-0.00110	-0.01406	-0.07121	-0.37870	0.28729	0.04935	0.00878	
10	-0.00234	-0.01697	-0.08082	-0.41038	0.31072	0.05880	0.01132	
11	-0.00348	-0.02339	-0.10177	-0.42632	0.34123	0.07418	0.01615	
12	-0.00673	-0.03467	-0.11093	-0.42296	0.35369	0.08204	0.01914	
13	-0.01162	-0.04556	-0.12061	-0.42403	0.35983	0.08715	0.02117	
14	-0.01477	-0.05331	-0.12793	-0.41451	0.33443	0.09281	0.02409	

VERTICAL (W)

THETA(DEG.)		12.5000	37.5000	62.5000	88.7967	116.0950	142.5000	167.5000
ROW NO.								
1	0.00000	0.00001	0.00006	-0.00213	-0.01003	0.00113	0.00007	
2	0.00002	-0.00006	0.00125	-0.00855	-0.04184	0.00623	0.00012	
3	-0.00219	0.00171	-0.00367	-0.01227	-0.06819	-0.00686	0.01779	
4	-0.00479	-0.00548	-0.00755	-0.01936	-0.08609	-0.01059	0.01144	
5	-0.00354	-0.00732	-0.01313	-0.02283	-0.11022	-0.02062	0.00304	
6	-0.00345	-0.00689	-0.01917	-0.03152	-0.12748	-0.03102	-0.00627	
7	-0.00326	-0.01152	-0.02348	-0.03383	-0.14559	-0.04199	-0.01653	
8	-0.00326	-0.01297	-0.02918	-0.03847	-0.16383	-0.05429	-0.02787	
9	-0.00385	-0.01515	-0.03303	-0.04296	-0.18209	-0.06643	-0.03913	
10	-0.00470	-0.01825	-0.03925	-0.04693	-0.19559	-0.07714	-0.05016	
11	-0.00935	-0.02579	-0.04836	-0.04946	-0.21321	-0.09522	-0.07308	
12	-0.02873	-0.04211	-0.05572	-0.05151	-0.21987	-0.10450	-0.08339	
13	-0.04257	-0.05078	-0.05825	-0.05078	-0.22382	-0.11472	-0.09328	
14	-0.05510	-0.06010	-0.06551	-0.10674	-0.27143	-0.12654	-0.10579	

VELOCITY COMPONENTS ON BODY PANELS DUE TO WING PANEL PRESSURE SINGULARITIES

AXIAL (U)		THETA(DEG.)							
		12.5000	37.5000	62.5000	88.7967	116.0950	142.5000	167.5000	
ROW NO.									
1	0.00000	0.00000	0.00000	0.00000	0.02154	-0.01471	0.00000	0.00000	
2	0.00000	0.00000	0.00000	0.01393	0.02308	-0.01590	-0.00937	0.00000	
3	0.00454	0.01110	0.01518	0.02052	0.01437	-0.01385	-0.01009	-0.00946	
4	0.01258	0.01354	0.01606	0.01941	0.01941	-0.01222	-0.01222	-0.01087	
5	0.01335	0.01452	0.01760	0.01905	0.01905	-0.01381	-0.01248	-0.01103	
6	0.01364	0.01566	0.01750	0.01843	0.01843	-0.01340	-0.01270	-0.01150	
7	0.01503	0.01566	0.01727	0.01776	0.01776	-0.01294	-0.01259	-0.01205	
8	0.01532	0.01609	0.01711	0.01697	0.01697	-0.01241	-0.01267	-0.01210	
9	0.01535	0.01608	0.01701	0.01554	0.01554	-0.01148	-0.01249	-0.01198	
10	0.01418	0.01535	0.01601	0.01597	0.01257	-0.00943	-0.01188	-0.01191	
11	0.00871	0.01368	0.00993	0.00407	0.00407	-0.00350	-0.00777	-0.01012	
12	0.00528	0.00769	0.00552	0.00211	0.00211	-0.00184	-0.00441	-0.00560	
13	0.00355	0.00477	0.00340	0.00125	0.00125	-0.00112	-0.00275	-0.00344	
14	0.00000	0.00308	0.00221	0.00082	0.00082	-0.00069	-0.00176	-0.00223	

TRANSVERSE (V)

		THETA(DEG.)							
		12.5000	37.5000	62.5000	88.7967	116.0950	142.5000	167.5000	
ROW NO.									
1	-0.00000	-0.00000	-0.00000	-0.00000	0.01798	-0.02638	-0.00000	-0.00000	
2	-0.00000	-0.00000	0.00908	0.00908	0.08085	-0.08420	-0.01327	-0.00000	
3	0.00427	0.01092	0.02426	0.03477	0.13477	-0.13002	-0.02688	-0.00794	
4	0.00369	0.01478	0.03772	0.06688	0.18068	-0.16866	-0.03529	-0.00885	
5	0.00533	0.01932	0.05093	0.082301	0.22301	-0.20511	-0.04562	-0.01128	
6	0.00693	0.02601	0.06438	0.08230	0.22301	-0.23910	-0.05609	-0.01438	
7	0.00936	0.03194	0.07701	0.30003	0.30003	-0.27176	-0.06567	-0.01921	
8	0.01064	0.03700	0.08876	0.33579	0.33579	-0.30245	-0.07429	-0.01921	
9	0.01220	0.04244	0.10065	0.36870	0.36870	-0.30354	-0.08305	-0.02155	
10	0.01396	0.04794	0.11116	0.39634	0.39634	-0.33328	-0.09084	-0.02409	
11	0.01618	0.05561	0.12538	0.41924	0.41924	-0.36915	-0.09909	-0.02697	
12	0.01743	0.05945	0.12986	0.42185	0.42185	-0.37102	-0.10161	-0.02736	
13	0.01805	0.06060	0.13251	0.42305	0.42305	-0.37197	-0.10303	-0.02786	
14	0.01852	0.06170	0.13402	0.41394	0.41394	-0.34083	-0.10142	-0.02778	

VERTICAL (W)

		THETA(DEG.)							
		12.5000	37.5000	62.5000	88.7967	116.0950	142.5000	167.5000	
ROW NO.									
1	-0.00000	-0.00000	-0.00000	-0.00000	-0.04313	-0.01954	-0.00000	-0.00000	
2	-0.00000	-0.00000	-0.02331	-0.02331	-0.07136	-0.01458	-0.01075	-0.00000	
3	-0.00562	-0.01629	-0.03031	-0.03031	-0.07704	0.00066	-0.00865	-0.00699	
4	-0.01324	-0.01841	-0.03371	-0.03371	-0.07878	0.01676	-0.00428	-0.00220	
5	-0.01162	-0.01748	-0.03440	-0.03440	-0.07607	0.03537	0.00300	-0.00425	
6	-0.00905	-0.01608	-0.03214	-0.03214	-0.07253	0.05426	0.01135	-0.01091	
7	-0.00692	-0.01290	-0.02928	-0.02928	-0.06870	0.07291	0.02016	0.01830	
8	-0.00320	-0.00961	-0.02588	-0.02588	-0.06384	0.09159	0.02934	0.02636	
9	-0.00093	-0.00559	-0.02162	-0.02162	-0.05656	0.11093	0.03889	0.03463	
10	0.00529	-0.00105	-0.01589	-0.01589	-0.04552	0.13085	0.04902	0.04299	
11	0.01630	0.01148	0.00347	0.00347	-0.01032	0.16733	0.07186	0.06131	
12	0.03157	0.02874	0.02157	0.02157	0.01030	0.18712	0.08932	0.07833	
13	0.04344	0.04094	0.03474	0.03474	0.02463	0.20099	0.10194	0.09036	
14	0.05538	0.05435	0.05307	0.05307	0.09444	0.25970	0.11978	0.10431	

VELOCITY COMPONENTS ON BODY PANELS DUE TO WING SOURCES

AXIAL (U)		THETA(DEC.)		12.5000	37.5000	62.5000	88.7967	116.0950	142.5000	167.5000
RCW NO.										
1	-0.00000	-0.00000	-0.00000	-0.00000	-0.00000	-0.01746	-0.01483	-0.00000	-0.00000	-0.00000
2	-0.00000	-0.00000	-0.00000	-0.01181	-0.01010	-0.00962	-0.00962	-0.01002	-0.00000	-0.00000
3	-0.00625	-0.00872	-0.00864	-0.00561	-0.00378	-0.00773	-0.00313	-0.00773	-0.01313	-0.01313
4	-0.01331	-0.01218	-0.00975	-0.00643	-0.00500	-0.00845	-0.00845	-0.00845	-0.00845	-0.00946
5	-0.01091	-0.01024	-0.00846	-0.00524	-0.00167	-0.00228	-0.00228	-0.00228	-0.00652	-0.00652
6	-0.00818	-0.00731	-0.00524	-0.00194	-0.00138	-0.00102	-0.00102	-0.00102	-0.00341	-0.00341
7	-0.00529	-0.00424	-0.00338	-0.00113	-0.00088	-0.00088	-0.00088	-0.00088	-0.00019	-0.00019
8	-0.00221	-0.00106	-0.00093	-0.00085	-0.00085	-0.00085	-0.00085	-0.00085	-0.00085	-0.00085
9	0.00093	0.00191	0.00385	0.00647	0.00888	0.00888	0.00888	0.00888	0.00888	0.00888
10	0.00364	0.00460	0.00517	0.00517	0.00517	0.00517	0.00517	0.00517	0.00517	0.00517
11	0.00839	0.00937	0.00314	0.00253	0.00253	0.00253	0.00253	0.00253	0.00253	0.00253
12	0.00375	0.00358	0.00109	0.00088	0.00088	0.00088	0.00088	0.00088	0.00088	0.00088
13	0.00145	0.00132	0.00050	0.00043	0.00043	0.00043	0.00043	0.00043	0.00043	0.00043
14	0.00066	0.00060	0.00050	0.00050	0.00050	0.00050	0.00050	0.00050	0.00050	0.00050

TRANSVERSE(V)		THETA(DEC.)		12.5000	37.5000	62.5000	88.7967	116.0950	142.5000	167.5000
RCW NO.										
1	-0.00000	-0.00000	-0.00000	-0.00000	-0.00000	-0.01254	-0.01880	-0.00000	-0.00000	-0.00000
2	-0.00000	-0.00000	-0.00000	-0.00686	-0.02478	-0.02478	-0.02478	-0.01151	-0.00000	-0.00000
3	-0.00352	-0.00751	-0.01104	-0.00658	-0.01576	-0.01576	-0.01576	-0.01352	-0.00318	-0.00318
4	-0.00003	-0.00175	-0.00082	-0.000351	-0.00080	-0.00080	-0.00080	-0.00401	-0.00102	-0.00102
5	-0.00004	-0.00082	-0.00043	-0.000233	-0.00239	-0.00239	-0.00239	-0.00269	-0.00069	-0.00069
6	-0.00006	-0.00043	-0.00016	-0.00072	-0.00340	-0.00340	-0.00340	-0.00114	-0.00030	-0.00030
7	0.00004	0.00016	0.00049	0.00107	0.00848	0.00848	0.00848	0.00073	0.00020	0.00020
8	0.00020	0.00049	0.00267	0.01285	0.01778	0.01778	0.01778	0.00254	0.00072	0.00072
9	0.00036	0.00104	0.00409	0.01681	0.01681	0.01681	0.01681	0.00392	0.00103	0.00103
10	0.00042	0.00147	0.00416	0.00863	0.00687	0.00687	0.00687	0.00526	0.00139	0.00139
11	0.00080	0.00288	0.00416	0.00863	0.00687	0.00687	0.00687	0.00276	0.00228	0.00228
12	-0.00007	0.00004	0.00089	0.00215	0.00175	0.00175	0.00175	0.00082	0.00020	0.00020
13	-0.00015	0.00056	0.00115	0.00163	0.00123	0.00123	0.00123	0.00075	0.00023	0.00023
14	0.00013	0.00041	0.00072	0.00086	0.00058	0.00058	0.00058	0.00044	0.00015	0.00015

VERTICAL(W)		THETA(DEC.)		12.5000	37.5000	62.5000	88.7967	116.0950	142.5000	167.5000
RCW NO.										
1	-0.00000	-0.00000	-0.00000	-0.00000	-0.00000	0.03411	-0.02338	-0.00000	-0.00000	-0.00000
2	-0.00000	-0.00000	-0.00000	0.02706	0.01761	0.02711	-0.01888	-0.01357	-0.00000	-0.00000
3	0.00799	0.01358	0.01761	0.01563	0.01123	0.01797	-0.01283	-0.01175	-0.01298	-0.01298
4	0.01648	0.01616	0.01563	0.01207	0.00463	0.00463	-0.00866	-0.01219	-0.01259	-0.01259
5	0.01438	0.01391	0.01207	0.00718	-0.00210	-0.00210	-0.00395	-0.00906	-0.01024	-0.01024
6	0.01150	0.01044	0.00718	0.00204	-0.00809	-0.00809	0.00081	-0.00559	-0.00754	-0.00754
7	0.00817	0.00650	0.00204	-0.00283	-0.00809	-0.00809	0.00509	-0.00193	-0.00450	-0.00450
8	0.00439	0.00223	-0.00283	-0.01259	-0.00836	-0.00836	0.00159	-0.00122	-0.00122	-0.00122
9	0.00038	-0.00183	-0.00704	-0.01662	0.01132	0.01132	0.00469	0.00190	0.00190	0.00190
10	-0.00326	-0.00559	-0.01098	-0.02050	-0.01416	-0.01416	0.00757	0.00464	0.00464	0.00464
11	-0.00495	-0.01261	-0.00845	-0.00371	0.00291	0.00291	0.00636	0.00329	0.00329	0.00329
12	-0.00519	-0.00492	-0.00118	-0.00118	0.00096	0.00096	0.00280	0.00117	0.00117	0.00117
13	-0.00233	-0.00212	-0.00154	-0.00017	-0.00017	-0.00017	0.00049	0.00049	0.00049	0.00049
14	-0.00114	-0.00100	-0.00064	0.00017	-0.00015	-0.00015	0.00049	0.00049	0.00049	0.00049

PRESSURES, FORCES, AND MOMENTS ON ISOLATED BODY

CD = 0.00130 CL = 0.00399 CM = 0.00291

BODY PRESSURE COEFFICIENTS(CP)

THETA(DEG.)	0.0000	22.5000	45.0000	67.5000	90.0000	112.5000	135.0000	157.5000	180.0000
0.0000	0.06332	0.06803	0.08146	0.10156	0.12527	0.14897	0.16907	0.18250	0.18722
0.7243	0.06892	0.07363	0.08706	0.10716	0.13087	0.15458	0.17468	0.18810	0.19282
1.4485	0.03372	0.03851	0.05217	0.07261	0.09672	0.12083	0.14127	0.15492	0.15972
2.1728	0.00738	0.01100	0.02132	0.03676	0.05497	0.07319	0.08863	0.09894	0.10257
2.8970	0.01318	0.01663	0.02645	0.04115	0.05849	0.07583	0.09034	0.10036	0.10381
3.6213	0.00395	0.00705	0.01586	0.02905	0.04461	0.06017	0.07336	0.08217	0.08527
4.3456	0.00386	0.00683	0.01328	0.02292	0.03484	0.04611	0.05576	0.06149	0.06386
5.0698	-0.00053	0.00223	0.01011	0.02190	0.03580	0.04970	0.06149	0.06937	0.07213
5.7941	-0.00174	0.00091	0.00846	0.01975	0.03307	0.04639	0.05768	0.06523	0.06788
6.5184	-0.00478	0.00228	0.00482	0.01546	0.02800	0.04055	0.05118	0.05829	0.06078
7.2426	-0.00610	-0.00372	0.00307	0.01322	0.02520	0.03717	0.04733	0.05411	0.05649
7.9669	-0.00869	-0.00644	-0.00004	0.00953	0.02083	0.03213	0.04170	0.04810	0.05035
8.6911	-0.00988	-0.00775	-0.00168	0.00741	0.01812	0.02884	0.03792	0.04359	0.04612
9.4154	-0.01211	-0.01011	-0.00440	0.00415	0.01423	0.02431	0.03286	0.03857	0.04057
10.1397	-0.01341	-0.01153	-0.00616	0.00188	0.01136	0.02084	0.02888	0.03425	0.03613
10.8639	-0.01601	-0.01425	-0.00924	-0.00175	0.00709	0.01594	0.02343	0.02844	0.03020
11.5882	-0.01743	-0.01581	-0.01118	-0.00426	0.00391	0.01208	0.01900	0.02363	0.02525
12.3124	-0.02077	-0.01928	-0.01505	-0.00812	0.00125	0.00622	0.01255	0.01678	0.01827
13.0367	-0.02210	-0.02078	-0.01701	-0.01138	-0.00473	0.00192	0.00756	0.01132	0.01265
13.7610	-0.02476	-0.02360	-0.02028	-0.01530	-0.00944	-0.00358	-0.00139	0.00471	0.00588
14.5023	-0.02727	-0.02630	-0.02353	-0.01939	-0.01451	-0.00963	-0.00549	-0.00273	-0.00175
15.2436	-0.03020	-0.03744	-0.03531	-0.03211	-0.02833	-0.02456	-0.02136	-0.01922	-0.01847
15.9849	-0.03942	-0.03902	-0.03787	-0.03616	-0.03414	-0.03212	-0.03041	-0.02926	-0.02886
16.7262	-0.02689	-0.02674	-0.02631	-0.02565	-0.02488	-0.02412	-0.02346	-0.02303	-0.02288
17.4675	-0.02161	-0.02163	-0.02167	-0.02174	-0.02182	-0.02189	-0.02196	-0.02200	-0.02202
18.2088	-0.01660	-0.01672	-0.01705	-0.01756	-0.01815	-0.01874	-0.01925	-0.01958	-0.01970
18.9501	-0.01334	-0.01351	-0.01400	-0.01474	-0.01561	-0.01648	-0.01721	-0.01771	-0.01788
19.6914	-0.01089	-0.01108	-0.01163	-0.01246	-0.01343	-0.01441	-0.01523	-0.01578	-0.01598
20.4327	-0.00917	-0.00936	-0.00991	-0.01073	-0.01169	-0.01266	-0.01348	-0.01402	-0.01422
21.1740	-0.00792	-0.00810	-0.00860	-0.00936	-0.01025	-0.01113	-0.01189	-0.01239	-0.01257
21.9153	-0.00701	-0.00716	-0.00760	-0.00826	-0.00904	-0.00982	-0.01048	-0.01092	-0.01108
22.6566	-0.00632	-0.00645	-0.00682	-0.00738	-0.00803	-0.00869	-0.00924	-0.00962	-0.00975
23.3979	-0.00578	-0.00588	-0.00619	-0.00664	-0.00718	-0.00771	-0.00816	-0.00847	-0.00857
24.1392	-0.00533	-0.00542	-0.00566	-0.00602	-0.00645	-0.00687	-0.00723	-0.00747	-0.00756
24.8805	-0.00495	-0.00502	-0.00521	-0.00549	-0.00582	-0.00615	-0.00643	-0.00662	-0.00668
25.6218	-0.00462	-0.00467	-0.00481	-0.00502	-0.00528	-0.00553	-0.00574	-0.00589	-0.00594
26.3631	-0.00431	-0.00435	-0.00446	-0.00462	-0.00481	-0.00500	-0.00516	-0.00527	-0.00531
27.1044	-0.00402	-0.00404	-0.00412	-0.00424	-0.00439	-0.00453	-0.00465	-0.00473	-0.00476
27.8457	-0.00379	-0.00381	-0.00387	-0.00396	-0.00407	-0.00417	-0.00426	-0.00432	-0.00434
28.5870	-0.00339	-0.00340	-0.00345	-0.00352	-0.00360	-0.00368	-0.00375	-0.00379	-0.00381
29.3283	-0.00371	-0.00372	-0.00376	-0.00381	-0.00387	-0.00393	-0.00399	-0.00402	-0.00403
30.0696	-0.00881	-0.00885	-0.00895	-0.00910	-0.00928	-0.00946	-0.00961	-0.00971	-0.00974
30.8109	-0.01632	-0.01646	-0.01687	-0.01747	-0.01817	-0.01888	-0.01948	-0.01988	-0.02002
31.5522	-0.02026	-0.02059	-0.02151	-0.02289	-0.02451	-0.02614	-0.02752	-0.02844	-0.02876
32.2935	-0.02060	-0.02115	-0.02271	-0.02505	-0.02781	-0.03057	-0.03291	-0.03447	-0.03502
33.0348	-0.02260	-0.02341	-0.02569	-0.02912	-0.03315	-0.03719	-0.04062	-0.04290	-0.04371
33.7761	-0.02435	-0.02548	-0.02867	-0.03346	-0.03910	-0.04474	-0.04953	-0.05272	-0.05385
34.5174	-0.01577	-0.01721	-0.02133	-0.02749	-0.03476	-0.04203	-0.04819	-0.05230	-0.05375
35.2587	0.00286	0.00124	-0.00334	-0.01020	-0.01830	-0.02639	-0.03326	-0.03784	-0.03945

INCREMENTAL PRESSURES, FORCES, AND MOMENTS ON BODY PANELS DUE TO WING

CD = 0.00177 CL = 0.01667 CM = -0.36813

BODY PANEL PRESSURE COEFFICIENT(CP)

THETA(DEG.)	12.5000	37.5000	62.5000	88.7967	116.0950	142.5000	167.5000
ROW NO.							
1	-0.00000	-0.00002	-0.00006	-0.01130	0.07745	0.00183	0.00055
2	-0.00004	-0.00112	-0.00800	-0.06334	0.10880	0.04453	0.00156
3	-0.00039	-0.00699	-0.03037	-0.06901	0.08632	0.06386	0.03601
4	-0.00599	-0.01771	-0.03885	-0.07459	0.07625	0.06003	0.06327
5	-0.01533	-0.02922	-0.04925	-0.07783	0.06839	0.06400	0.06898
6	-0.02483	-0.03804	-0.05924	-0.08058	0.06163	0.06895	0.06776
7	-0.03703	-0.04612	-0.06275	-0.08378	0.05739	0.06391	0.06625
8	-0.04748	-0.05323	-0.06649	-0.08168	0.05137	0.05957	0.06076
9	-0.05391	-0.05987	-0.07120	-0.07928	0.04468	0.05445	0.05680
10	-0.05911	-0.06550	-0.07329	-0.07342	0.03328	0.04829	0.05191
11	-0.06585	-0.06719	-0.04911	-0.01974	0.02423	0.03596	0.03773
12	-0.05160	-0.04405	-0.02720	-0.00533	0.01384	0.02459	0.02972
13	-0.02972	-0.02603	-0.01790	-0.00577	0.00704	0.01627	0.02109
14	-0.01763	-0.01510	-0.01010	-0.00291	0.00424	0.00940	0.01174

BODY PANEL SLOPE(DR/DX)

THETA(DEG.)	12.5000	37.5000	62.5000	88.7967	116.0950	142.5000	167.5000
ROW NO.							
1	-0.08032	-0.06116	-0.02643	0.01972	0.06798	0.10500	0.12416
2	-0.09482	-0.07566	-0.04094	0.00491	0.05348	0.09050	0.10965
3	-0.10224	-0.08308	-0.04835	-0.00257	0.04606	0.08308	0.10224
4	-0.10224	-0.08308	-0.04835	-0.00257	0.04606	0.08308	0.10224
5	-0.10224	-0.08308	-0.04835	-0.00257	0.04606	0.08308	0.10224
6	-0.10224	-0.08308	-0.04835	-0.00257	0.04606	0.08308	0.10224
7	-0.10224	-0.08308	-0.04835	-0.00257	0.04606	0.08308	0.10224
8	-0.10224	-0.08308	-0.04835	-0.00257	0.04606	0.08308	0.10224
9	-0.10224	-0.08308	-0.04835	-0.00257	0.04606	0.08308	0.10224
10	-0.10224	-0.08308	-0.04835	-0.00257	0.04606	0.08308	0.10224
11	-0.10224	-0.08308	-0.04835	-0.00257	0.04606	0.08308	0.10224
12	-0.10224	-0.08308	-0.04835	-0.00257	0.04606	0.08308	0.10224
13	-0.10237	-0.08321	-0.04849	-0.00270	0.04593	0.08295	0.10211
14	-0.12598	-0.10682	-0.07209	-0.02631	0.02232	0.05934	0.07850

PRESSURES, FORCES, AND MOMENTS ON WING PANELS IN PRESENCE OF BODY

CD = 0.01949 CL = 0.18361 CM = -5.42608

SPANWISE CD DISTRIBUTION(B/2Q * DD/DY)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
	0.00186	0.00192	0.00201	0.00208	0.00212	0.00215	0.00222	0.00242	0.00260	0.00213

SPANWISE CL DISTRIBUTION(B/2Q * DL/DY)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
	0.01680	0.01779	0.01867	0.01941	0.02002	0.02059	0.02141	0.02305	0.02455	0.02015

UPPER SURFACE WING PANEL PRESSURE COEFFICIENTS(CP)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION	1	2	3	4	5	6	7	8	9	10
	-0.16579	-0.21452	-0.24268	-0.25782	-0.28390	-0.30588	-0.32415	-0.34268	-0.35644	-0.36583
	-0.13484	-0.15824	-0.15489	-0.18337	-0.20003	-0.21325	-0.22674	-0.23586	-0.24208	-0.24603
	-0.12453	-0.13811	-0.17466	-0.15877	-0.17035	-0.18187	-0.18886	-0.18594	-0.21296	-0.27307
	-0.11876	-0.12168	-0.13465	-0.14681	-0.15633	-0.16163	-0.15786	-0.15751	-0.20251	-0.20705
	-0.10660	-0.11828	-0.13002	-0.13998	-0.14111	-0.13828	-0.13257	-0.14280	-0.18144	-0.17239
	-0.10478	-0.11510	-0.12141	-0.13059	-0.12053	-0.11014	-0.11602	-0.12862	-0.14999	-0.14371
	-0.10168	-0.10454	-0.11355	-0.10181	-0.09604	-0.09265	-0.09650	-0.11126	-0.11757	-0.11524
	-0.09239	-0.09964	-0.08509	-0.07717	-0.07169	-0.07441	-0.07352	-0.09540	-0.08590	-0.08092
	-0.08799	-0.06942	-0.05694	-0.04836	-0.05112	-0.04631	-0.07180	-0.06944	-0.05392	-0.04756
	-0.05000	-0.02157	-0.01570	-0.01678	-0.00975	-0.01161	-0.01471	-0.02991	-0.01117	-0.01279

LOWER SURFACE WING PANEL PRESSURE COEFFICIENTS(CP)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION	1	2	3	4	5	6	7	8	9	10
	0.18348	0.20371	0.22155	0.24793	0.26083	0.27240	0.28208	0.28676	0.29986	0.47593
	0.07736	0.08616	0.11668	0.11394	0.111750	0.12032	0.11950	0.12080	0.14217	0.22797
	0.04907	0.05701	0.04242	0.07438	0.07425	0.07106	0.06950	0.07984	0.10821	0.14360
	0.03860	0.05056	0.05332	0.05040	0.04670	0.04373	0.04940	0.05892	0.07631	0.07650
	0.03956	0.04148	0.03677	0.03087	0.02991	0.03162	0.03834	0.04325	0.05240	0.04208
	0.03831	0.03155	0.02705	0.01607	0.02224	0.03060	0.02689	0.03628	0.03620	0.02124
	0.03421	0.02881	0.01538	0.02014	0.02143	0.02299	0.02328	0.03711	0.02290	0.00730
	0.03278	0.01598	0.01929	0.01984	0.02113	0.01774	0.02499	0.02913	0.01181	-0.00084
	0.01947	0.01885	0.01997	0.02243	0.01737	0.02173	0.02534	0.02280	0.00449	-0.01095
	0.02125	0.03102	0.02910	0.02558	0.03058	0.02944	0.03480	0.02213	0.01354	-0.02550

WING PANEL PRESSURE DIFFERENCE(1CL)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	0.34927	0.41823	0.46423	0.50575	0.54473	0.57828	0.60622	0.62944	0.65630	1.04576
2	0.21220	0.24440	0.27157	0.29731	0.31753	0.33357	0.34624	0.35667	0.36426	0.58400
3	0.17360	0.19512	0.21708	0.23315	0.24459	0.25293	0.25835	0.26379	0.27118	0.41667
4	0.15736	0.17224	0.18797	0.19721	0.20303	0.20536	0.20726	0.21042	0.21881	0.28354
5	0.14616	0.15976	0.16679	0.17084	0.17302	0.16990	0.17090	0.18605	0.23384	0.21447
6	0.14309	0.14666	0.14846	0.14666	0.14277	0.14074	0.14292	0.16490	0.18619	0.16495
7	0.13589	0.13335	0.12892	0.12195	0.11746	0.11564	0.11978	0.14937	0.14047	0.12253
8	0.12517	0.11562	0.10438	0.09701	0.09287	0.09216	0.09651	0.12452	0.09771	0.08009
9	0.10746	0.08827	0.07691	0.07079	0.06849	0.06804	0.07714	0.09224	0.05842	0.03661
10	0.07125	0.05259	0.04480	0.04235	0.04033	0.04105	0.04951	0.05205	0.02472	-0.01672

UPPER SURFACE WING PANEL SLOPE(1DZ/DX)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	-0.03734	-0.03734	-0.03734	-0.03734	-0.03734	-0.03734	-0.03734	-0.03734	-0.03734	-0.03734
2	-0.06962	-0.06962	-0.06962	-0.06962	-0.06962	-0.06962	-0.06962	-0.06962	-0.06962	-0.06962
3	-0.08838	-0.08838	-0.08838	-0.08838	-0.08838	-0.08838	-0.08838	-0.08838	-0.08838	-0.08838
4	-0.10461	-0.10461	-0.10461	-0.10461	-0.10461	-0.10461	-0.10461	-0.10461	-0.10461	-0.10461
5	-0.11995	-0.11995	-0.11995	-0.11995	-0.11995	-0.11995	-0.11995	-0.11995	-0.11995	-0.11995
6	-0.13395	-0.13395	-0.13395	-0.13395	-0.13395	-0.13395	-0.13395	-0.13395	-0.13395	-0.13395
7	-0.14162	-0.14162	-0.14162	-0.14162	-0.14162	-0.14162	-0.14162	-0.14162	-0.14162	-0.14162
8	-0.14885	-0.14885	-0.14885	-0.14885	-0.14885	-0.14885	-0.14885	-0.14885	-0.14885	-0.14885
9	-0.15609	-0.15609	-0.15609	-0.15609	-0.15609	-0.15609	-0.15609	-0.15609	-0.15609	-0.15609
10	-0.16348	-0.16348	-0.16348	-0.16348	-0.16348	-0.16348	-0.16348	-0.16348	-0.16348	-0.16348

LOWER SURFACE WING PANEL SLOPE(1DZ/DX)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	-0.17210	-0.17210	-0.17210	-0.17210	-0.17210	-0.17210	-0.17210	-0.17210	-0.17210	-0.17210
2	-0.13982	-0.13982	-0.13982	-0.13982	-0.13982	-0.13982	-0.13982	-0.13982	-0.13982	-0.13982
3	-0.12106	-0.12106	-0.12106	-0.12106	-0.12106	-0.12106	-0.12106	-0.12106	-0.12106	-0.12106
4	-0.10483	-0.10483	-0.10483	-0.10483	-0.10483	-0.10483	-0.10483	-0.10483	-0.10483	-0.10483
5	-0.08949	-0.08949	-0.08949	-0.08949	-0.08949	-0.08949	-0.08949	-0.08949	-0.08949	-0.08949
6	-0.07548	-0.07548	-0.07548	-0.07548	-0.07548	-0.07548	-0.07548	-0.07548	-0.07548	-0.07548
7	-0.06782	-0.06782	-0.06782	-0.06782	-0.06782	-0.06782	-0.06782	-0.06782	-0.06782	-0.06782
8	-0.06059	-0.06059	-0.06059	-0.06059	-0.06059	-0.06059	-0.06059	-0.06059	-0.06059	-0.06059
9	-0.05335	-0.05335	-0.05335	-0.05335	-0.05335	-0.05335	-0.05335	-0.05335	-0.05335	-0.05335
10	-0.04596	-0.04596	-0.04596	-0.04596	-0.04596	-0.04596	-0.04596	-0.04596	-0.04596	-0.04596

WING CAMBER SLOPE(DZ/DX)

SPANWISE STATION	1	2	3	4	5	6	7	8	9	10
CHORDWISE STATION										
1	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472
2	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472
3	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472
4	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472
5	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472
6	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472
7	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472
8	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472
9	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472
10	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472	-0.10472
WING CHORD LENGTHS(C)	9.21046	9.21070	9.21094	9.21118	9.21142	9.21166	9.21190	9.21215	9.21239	6.14167

FORCES AND MOMENTS ON WING-BODY COMBINATION

CO = 0.02256 CL = 0.20427 CM = -5.79131

PCINTS

X	24.00000	Y	4.00000	Z	-1.00000	UP	-0.04104	VP	0.10128	WP	-0.05955	U	0.95346	V	0.10128	M	0.04597	CP	0.00211
24.00000	4.00000	-0.50000	-0.04567	0.12937	-0.08649	0.94806	0.12937	0.01803	0.09133										
24.00000	4.35350	-0.64650	-0.06030	0.15698	-0.04298	0.93422	0.15698	0.00135	0.12661										
24.00000	4.50000	-1.00000	-0.04645	0.11726	-0.01784	0.94807	0.11726	0.08669	0.09590										
24.00000	4.35350	-1.35350	-0.03830	0.08974	-0.03034	0.95622	0.08974	0.07418	0.07661										
24.00000	4.00000	-1.50000	-0.03523	0.07721	-0.04744	0.95899	0.07721	0.05709	0.07187										
24.00000	3.64650	-1.35350	-0.03304	0.07027	-0.06294	0.96148	0.07027	0.04159	0.06609										
24.00000	3.50000	-1.00000	-0.03229	0.07365	-0.07657	0.96224	0.07365	0.02796	0.06457										
24.00000	3.64650	-0.64650	-0.03502	0.08909	-0.08500	0.95950	0.08909	0.01953	0.07004										

GRIDS

COMPUTE** 2**GRIDS

OPTION REQUESTED---RECTANGULAR GRID

X-Z CUT, FOR THIS CUT Y= 1.20000

X	Y	Z	U	V	W	CP
30.000000	1.200000	-1.200000	0.989934E 00	-0.570023E-01	0.104333E 00	0.917638E-02
30.500000	1.200000	-1.200000	0.992241E 00	-0.600857E-01	0.107695E 00	0.456158E-02
31.000000	1.200000	-1.200000	0.995679E 00	-0.635194E-01	0.112374E 00	-0.231379E-02
31.500000	1.200000	-1.200000	0.998674E 00	-0.669344E-01	0.117447E 00	-0.890407E-02
32.000000	1.200000	-1.200000	0.100098E 01	-0.708257E-01	0.122179E 00	-0.129208E-01
32.500000	1.200000	-1.200000	0.100344E 01	-0.752087E-01	0.126561E 00	-0.178279E-01
33.000000	1.200000	-1.200000	0.100548E 01	-0.783316E-01	0.130438E 00	-0.219261E-01
33.500000	1.200000	-1.200000	0.100700E 01	-0.815329E-01	0.134203E 00	-0.249633E-01
34.000000	1.200000	-1.200000	0.100919E 01	-0.860532E-01	0.138596E 00	-0.293384E-01
34.500000	1.200000	-1.200000	0.101167E 01	-0.913022E-01	0.143104E 00	-0.342880E-01
30.000000	1.200000	-0.700000	0.992804E 00	-0.188404E 00	0.132079E 00	0.343511E-02
30.500000	1.200000	-0.700000	0.996728E 00	-0.193886E 00	0.136188E 00	-0.441172E-02
31.000000	1.200000	-0.700000	0.100057E 01	-0.198870E 00	0.140716E 00	-0.120993E-01
31.500000	1.200000	-0.700000	0.100313E 01	-0.203528E 00	0.144857E 00	-0.172204E-01
32.000000	1.200000	-0.700000	0.100498E 01	-0.208356E 00	0.148345E 00	-0.209249E-01
32.500000	1.200000	-0.700000	0.100701E 01	-0.213255E 00	0.151364E 00	-0.249766E-01
33.000000	1.200000	-0.700000	0.100988E 01	-0.217647E 00	0.154221E 00	-0.287181E-01
33.500000	1.200000	-0.700000	0.101073E 01	-0.223207E 00	0.157269E 00	-0.324099E-01
34.000000	1.200000	-0.700000	0.101305E 01	-0.229433E 00	0.160243E 00	-0.370472E-01
34.500000	1.200000	-0.700000	0.101447E 01	-0.235280E 00	0.162273E 00	-0.398961E-01

K-2 CUT, FOR THIS CUT Y= 2.20000

X	Y	Z	U	V	W	CP
30.00000	2.20000	-1.20000	0.990985E 00	-0.341504E-01	0.409533E-01	0.707457E-02
30.50000	2.20000	-1.20000	0.990063E 00	-0.337229E-01	0.427549E-01	0.891712E-02
31.00000	2.20000	-1.20000	0.989512E 00	-0.339817E-01	0.443742E-01	0.100207E-01
31.50000	2.20000	-1.20000	0.990502E 00	-0.344020E-01	0.470522E-01	0.804047E-02
32.00000	2.20000	-1.20000	0.993469E 00	-0.384465E-01	0.503422E-01	0.210673E-02
32.50000	2.20000	-1.20000	0.996106E 00	-0.430525E-01	0.535803E-01	-0.316909E-02
33.00000	2.20000	-1.20000	0.998468E 00	-0.467513E-01	0.569910E-01	-0.789310E-02
33.50000	2.20000	-1.20000	0.100020E 01	-0.497416E-01	0.598296E-01	-0.113549E-01
34.00000	2.20000	-1.20000	0.100210E 01	-0.531640E-01	0.624276E-01	-0.151644E-01
34.50000	2.20000	-1.20000	0.100334E 01	-0.562142E-01	0.646170E-01	-0.176443E-01
30.00000	2.20000	-0.70000	0.993251E 00	-0.364391E-01	0.172873E-01	0.254232E-02
30.50000	2.20000	-0.70000	0.995023E 00	-0.356816E-01	0.195971E-01	0.499710E-02
31.00000	2.20000	-0.70000	0.991038E 00	-0.355215E-01	0.219863E-01	0.536682E-02
31.50000	2.20000	-0.70000	0.993379E 00	-0.370613E-01	0.247158E-01	0.229539E-02
32.00000	2.20000	-0.70000	0.996538E 00	-0.423572E-01	0.276585E-01	-0.403212E-02
32.50000	2.20000	-0.70000	0.999427E 00	-0.469981E-01	0.308784E-01	-0.981105E-02
33.00000	2.20000	-0.70000	0.100107E 01	-0.502949E-01	0.331996E-01	-0.131000E-01
33.50000	2.20000	-0.70000	0.100261E 01	-0.532604E-01	0.353834E-01	-0.161810E-01
34.00000	2.20000	-0.70000	0.100414E 01	-0.565240E-01	0.372569E-01	-0.192370E-01
34.50000	2.20000	-0.70000	0.100539E 01	-0.599930E-01	0.390190E-01	-0.217425E-01

X-Z CUT, FOR THIS CUT Y= 3.20000

X	Y	Z	U	V	W	CP
30.000000	3.200000	-1.200000	0.988189E 00	-0.803656E-02	0.288318E-01	0.126649E-01
30.500000	3.200000	-1.200000	0.989045E 00	-0.877997E-02	0.323951E-01	0.109544E-01
31.000000	3.200000	-1.200000	0.989705E 00	-0.106019E-01	0.350450E-01	0.963442E-02
31.500000	3.200000	-1.200000	0.989551E 00	-0.122944E-01	0.369454E-01	0.994232E-02
32.000000	3.200000	-1.200000	0.989243E 00	-0.122439E-01	0.392729E-01	0.105575E-01
32.500000	3.200000	-1.200000	0.989317E 00	-0.126821E-01	0.415194E-01	0.104095E-01
33.000000	3.200000	-1.200000	0.990214E 00	-0.145600E-01	0.438990E-01	0.861502E-02
33.500000	3.200000	-1.200000	0.992827E 00	-0.192454E-01	0.467426E-01	0.338951E-02
34.000000	3.200000	-1.200000	0.995451E 00	-0.235755E-01	0.497268E-01	-0.185870E-02
34.500000	3.200000	-1.200000	0.997736E 00	-0.263678E-01	0.527333E-01	-0.642898E-02
35.000000	3.200000	-0.700000	0.992424E 00	-0.119636E-01	0.185772E-01	0.419538E-02
35.500000	3.200000	-0.700000	0.992248E 00	-0.129206E-01	0.225627E-01	0.454846E-02
36.000000	3.200000	-0.700000	0.992456E 00	-0.146440E-01	0.261315E-01	0.413249E-02
36.500000	3.200000	-0.700000	0.992345E 00	-0.151453E-01	0.294851E-01	0.439471E-02
37.000000	3.200000	-0.700000	0.991749E 00	-0.144022E-01	0.323928E-01	0.554651E-02
37.500000	3.200000	-0.700000	0.991759E 00	-0.145617E-01	0.351001E-01	0.552632E-02
38.000000	3.200000	-0.700000	0.992862E 00	-0.169365E-01	0.377980E-01	0.331899E-02
38.500000	3.200000	-0.700000	0.995720E 00	-0.219002E-01	0.406324E-01	-0.239646E-02
39.000000	3.200000	-0.700000	0.998451E 00	-0.256426E-01	0.434677E-01	-0.785911E-02
39.500000	3.200000	-0.700000	0.999798E 00	-0.281874E-01	0.457221E-01	-0.105531E-01

OPTION REQUESTED---RECTANGULAR GRID

X-Z CUT, FOR THIS CUT Y= 0.00000

X	Y	Z	U	V	W	C _P
1490.000000	0.000000	-1000.000000	0.994522E 00	0.000000E-38	0.104528E 00	-0.000000E-38
1491.000000	0.000000	-1000.000000	0.994522E 00	0.000000E-38	0.104528E 00	-0.000000E-38
1492.000000	0.000000	-1000.000000	0.994522E 00	0.000000E-38	0.104528E 00	-0.000000E-38
1493.000000	0.000000	-1000.000000	0.994522E 00	0.000000E-38	0.104528E 00	-0.000000E-38
1494.000000	0.000000	-1000.000000	0.994522E 00	0.000000E-38	0.104528E 00	-0.000000E-38
1495.000000	0.000000	-1000.000000	0.994522E 00	0.000000E-38	0.104528E 00	-0.000000E-38
1496.000000	0.000000	-1000.000000	0.994522E 00	0.000000E-38	0.104528E 00	-0.000000E-38
1497.000000	0.000000	-1000.000000	0.993653E 00	0.258450E-11	0.103223E 00	0.173750E-02
1498.000000	0.000000	-1000.000000	0.993357E 00	0.345393E-11	0.102767E 00	0.232914E-02
1499.000000	0.000000	-1000.000000	0.993433E 00	0.310122E-11	0.102949E 00	0.217721E-02
1500.000000	0.000000	-1000.000000	0.993632E 00	0.268112E-11	0.103177E 00	0.177891E-02
1501.000000	0.000000	-1000.000000	0.993701E 00	0.248107E-11	0.103278E 00	0.164109E-02
1502.000000	0.000000	-1000.000000	0.993745E 00	0.230182E-11	0.103365E 00	0.155405E-02
1503.000000	0.000000	-1000.000000	0.993815E 00	0.209944E-11	0.103468E 00	0.141359E-02
1504.000000	0.000000	-1000.000000	0.993892E 00	0.179844E-11	0.103616E 00	0.125941E-02
1505.000000	0.000000	-1000.000000	0.994019E 00	0.150747E-11	0.103766E 00	0.100506E-02
1506.000000	0.000000	-1000.000000	0.994136E 00	0.116058E-11	0.103943E 00	0.771667E-03
1507.000000	0.000000	-1000.000000	0.994262E 00	0.788293E-12	0.104133E 00	0.518991E-03
1508.000000	0.000000	-1000.000000	0.994421E 00	0.331798E-12	0.104362E 00	0.201684E-03
1509.000000	0.000000	-1000.000000	0.994594E 00	-0.182483E-12	0.104622E 00	-0.144498E-03
1510.000000	0.000000	-1000.000000	0.994880E 00	-0.111386E-11	0.105092E 00	-0.716940E-03
1511.000000	0.000000	-1000.000000	0.993486E 00	-0.183734E-11	0.102998E 00	0.207200E-02
1512.000000	0.000000	-1000.000000	0.993035E 00	-0.145243E-11	0.101827E 00	0.297438E-02
1513.000000	0.000000	-1000.000000	0.993066E 00	-0.134618E-11	0.102750E 00	0.291263E-02
1514.000000	0.000000	-1000.000000	0.994060E 00	-0.116481E-11	0.103915E 00	0.923599E-03
1515.000000	0.000000	-1000.000000	0.993543E 00	-0.979960E-12	0.103225E 00	0.195847E-02
1516.000000	0.000000	-1000.000000	0.993713E 00	-0.834508E-12	0.103401E 00	0.161771E-02
1517.000000	0.000000	-1000.000000	0.993533E 00	-0.705972E-12	0.103072E 00	0.197748E-02

1518.000000	0.000000	-1000.000000	0.993257E 00	-0.607332E-12	0.102529E 00	0.253037E-02
1519.000000	0.000000	-1000.000000	0.993488E 00	-0.512281E-12	0.102957E 00	0.206863E-02
1520.000000	0.000000	-1000.000000	0.993474E 00	-0.453906E-12	0.102892E 00	0.209487E-02
1521.000000	0.000000	-1000.000000	0.993223E 00	-0.403420E-12	0.102669E 00	0.259770E-02
1522.000000	0.000000	-1000.000000	0.993347E 00	-0.356067E-12	0.102802E 00	0.234910E-02
1523.000000	0.000000	-1000.000000	0.993378E 00	-0.325649E-12	0.103012E 00	0.228770E-02
1524.000000	0.000000	-1000.000000	0.993599E 00	-0.302837E-12	0.102999E 00	0.186597E-02
1525.000000	0.000000	-1000.000000	0.993732E 00	-0.635104E-12	0.103311E 00	0.157908E-02
1526.000000	0.000000	-1000.000000	0.994017E 00	-0.133060E-11	0.103734E 00	0.100962E-02
1527.000000	0.000000	-1000.000000	0.994185E 00	-0.182383E-11	0.103964E 00	0.673930E-03
1528.000000	0.000000	-1000.000000	0.994433E 00	-0.233242E-11	0.104487E 00	0.177965E-03
1529.000000	0.000000	-1000.000000	0.994606E 00	-0.283740E-11	0.104612E 00	-0.167787E-03
1530.000000	0.000000	-1000.000000	0.994298E 00	-0.241122E-11	0.104301E 00	0.467738E-03
1531.000000	0.000000	-1000.000000	0.992059E 00	0.190878E-11	0.100855E 00	0.492662E-02
1532.000000	0.000000	-1000.000000	0.992202E 00	0.713351E-12	0.100985E 00	0.463922E-02
1533.000000	0.000000	-1000.000000	0.992703E 00	0.367806E-12	0.101772E 00	0.363848E-02
1534.000000	0.000000	-1000.000000	0.993580E 00	0.224168E-12	0.103128E 00	0.188456E-02
1535.000000	0.000000	-1000.000000	0.994623E 00	0.143851E-12	0.104616E 00	-0.203189E-03
1536.000000	0.000000	-1000.000000	0.995711E 00	0.845004E-13	0.106345E 00	-0.237769E-02
1537.000000	0.000000	-1000.000000	0.997737E 00	0.594470E-13	0.109395E 00	-0.443097E-02
1538.000000	0.000000	-1000.000000	0.997040E 00	0.292057E-13	0.108306E 00	-0.503599E-02
1539.000000	0.000000	-1000.000000	0.996286E 00	0.123629E-13	0.107168E 00	-0.352768E-02
1540.000000	0.000000	-1000.000000	0.995767E 00	-0.428882E-14	0.106322E 00	-0.248948E-02
1541.000000	0.000000	-1000.000000	0.995480E 00	-0.154246E-13	0.105904E 00	-0.191680E-02
1542.000000	0.000000	-1000.000000	0.995381E 00	-0.909864E-14	0.105766E 00	-0.171864E-02
1543.000000	0.000000	-1000.000000	0.995216E 00	-0.154823E-13	0.105648E 00	-0.138727E-02
1544.000000	0.000000	-1000.000000	0.995167E 00	-0.264079E-13	0.105424E 00	-0.129014E-02
1545.000000	0.000000	-1000.000000	0.995096E 00	-0.252612E-13	0.105376E 00	-0.114732E-02
1546.000000	0.000000	-1000.000000	0.995021E 00	-0.272281E-13	0.105258E 00	-0.997221E-03
1547.000000	0.000000	-1000.000000	0.994966E 00	-0.306369E-13	0.105162E 00	-0.888878E-03
1548.000000	0.000000	-1000.000000	0.994932E 00	-0.336086E-13	0.105153E 00	-0.819630E-03
1549.000000	0.000000	-1000.000000	0.994999E 00	-0.292328E-13	0.105104E 00	-0.753283E-03

1550.000000	0.000000	-1000.000000	0.994834E 00	-0.377943E-13	0.105097E 00	-0.623869E-03
1551.000000	0.000000	-1000.000000	0.994945E 00	-0.336489E-13	0.105035E 00	-0.645861E-03
1552.000000	0.000000	-1000.000000	0.994823E 00	-0.307934E-13	0.104976E 00	-0.601523E-03
1553.000000	0.000000	-1000.000000	0.994807E 00	-0.304091E-13	0.104914E 00	-0.571202E-03
1554.000000	0.000000	-1000.000000	0.994787E 00	-0.298333E-13	0.104928E 00	-0.530887E-03
1555.000000	0.000000	-1000.000000	0.994774E 00	-0.343509E-13	0.104916E 00	-0.505182E-03
1556.000000	0.000000	-1000.000000	0.994778E 00	-0.303235E-13	0.104808E 00	-0.512955E-03
1557.000000	0.000000	-1000.000000	0.994760E 00	-0.299211E-13	0.104826E 00	-0.475967E-03
1558.000000	0.000000	-1000.000000	0.994714E 00	-0.275570E-13	0.104858E 00	-0.384374E-03
1559.000000	0.000000	-1000.000000	0.994697E 00	-0.280286E-13	0.104854E 00	-0.349372E-03

SYNCHRONIZATION

INITIAL POINT X= 28.00000 Y= 5.00000 Z= 0.25000

INITIAL STEP SIZE= 0.10000

ACTUAL POINTS DETERMINED BY INTEGRATOR

X	Y	Z	U	V	W	CP
10.987316	5.402700	-0.668064	0.995046	0.006203	0.110184	-0.001049
20.284877	5.404234	-0.624006	0.997193	0.002872	0.110724	-0.005343
20.682416	5.405826	-0.579681	0.993749	0.007922	0.111414	0.001545
21.079837	5.411845	-0.534778	0.984898	0.021389	0.112272	0.019249
21.477072	5.422244	-0.489023	0.981797	0.026645	0.114327	0.025451
21.874229	5.431400	-0.442205	0.989436	0.015709	0.117955	0.010172
22.271331	5.433738	-0.394316	1.001270	-0.002067	0.122391	-0.013456
22.668275	5.432495	-0.344974	1.000979	-0.002073	0.126674	-0.012915
23.064974	5.431330	-0.293712	1.002050	-0.004345	0.132302	-0.015056

23.461350	5.428754	-0.240064	1.004213	-0.008811	0.139552	-0.019383
23.457268	5.424185	-0.193278	1.005828	-0.013411	0.149446	-0.022812
24.252515	5.418257	-0.122173	1.005584	-0.017103	0.162943	-0.022124
24.646799	5.409837	-0.055421	1.008895	-0.030369	0.179906	-0.028747
25.039659	5.391396	0.017779	1.023872	-0.071883	0.192456	-0.058700
25.431363	5.351877	0.089136	1.049555	-0.137490	0.171942	-0.110067
25.823183	5.292903	0.142454	1.066037	-0.137870	0.119780	-0.143030
26.214382	5.228767	0.177949	1.066257	-0.168952	0.077428	-0.143471
26.413615	5.198322	0.191037	1.062236	-0.159172	0.064593	-0.135429
26.611240	5.169491	0.202193	1.057136	-0.147844	0.055496	-0.125227
26.809205	5.142563	0.211942	1.052795	-0.137822	0.048494	-0.116527
27.007400	5.117588	0.220588	1.050377	-0.131857	0.043156	-0.112306
27.205743	5.093065	0.228229	1.051292	-0.126303	0.037817	-0.111170
27.404185	5.069060	0.234835	1.051910	-0.125638	0.032715	-0.113541
27.503431	5.057170	0.237837	1.052205	-0.124555	0.030267	-0.114777
27.603694	5.045361	0.240608	1.052205	-0.122674	0.028092	-0.115367
27.701977	5.033690	0.243170	1.051936	-0.122674	0.026261	-0.114829
27.801287	5.022173	0.245573	1.051235	-0.120221	0.024695	-0.113427
27.900628	5.010980	0.247841	1.050308	-0.117450	0.023324	-0.111572
28.000000	5.000000	0.250000	1.049007	-0.114446	0.022308	-0.108970
28.099404	4.989298	0.252073	1.047557	-0.111229	0.021443	-0.106071
28.198841	4.978891	0.254075	1.045977	-0.107864	0.020750	-0.102910
28.298309	4.968782	0.256021	1.044426	-0.104585	0.020165	-0.099808
28.397807	4.958959	0.257917	1.043027	-0.101553	0.019624	-0.097010
28.497331	4.949388	0.259761	1.041493	-0.099079	0.018988	-0.094941
28.596876	4.940024	0.261546	1.041130	-0.096895	0.018377	-0.093215
28.696301	4.921528	0.263492	1.037990	-0.090486	0.017508	-0.086936
28.795840	4.905236	0.268257	1.034521	-0.083666	0.016703	-0.079997
28.895301	4.889674	0.271340	1.032016	-0.078192	0.015662	-0.074987
28.994665	4.875044	0.274324	1.029269	-0.072299	0.014854	-0.069455
29.093640	4.861623	0.277149	1.026388	-0.065880	0.014295	-0.063732
29.192732	4.849149	0.279851	1.026099	-0.063353	0.013356	-0.063155
29.291528	4.825964	0.284894	1.023474	-0.055961	0.012562	-0.057904
29.390547	4.805197	0.289654	1.022061	-0.050755	0.011794	-0.055077
29.4891483	4.786218	0.294090	1.020762	-0.045995	0.010977	-0.052480
29.587411	4.769498	0.298411	1.017634	-0.038642	0.011385	-0.046224
29.685883	4.755883	0.303199	1.013864	-0.030568	0.013180	-0.038683
29.784648	4.745411	0.308839	1.010218	-0.022514	0.015340	-0.031392
29.883670	4.737928	0.315315	1.007587	-0.015503	0.017241	-0.026130
29.982451	4.729947	0.322484	1.006204	-0.009962	0.018788	-0.023364
30.081357	4.722927	0.330531	1.004304	-0.005071	0.022156	-0.019565
30.180241	4.728807	0.340093	1.002548	-0.000726	0.025719	-0.016053
30.279090	4.725292	0.351065	1.000854	0.003059	0.029224	-0.012665
30.377933	4.721079	0.363413	0.999623	0.005627	0.032510	-0.010202
30.476756	4.713593	0.377012	0.999362	0.006662	0.035403	-0.009681
30.575578	4.706259	0.391682	0.999874	0.006489	0.037902	-0.010705
30.674334	4.755738	0.423579	1.002912	0.002524	0.041966	-0.016781
30.7730971	4.741210	0.458446	1.003994	0.001667	0.045449	-0.018944
30.871877	4.727117	0.495797	1.005117	0.000308	0.048457	-0.021190
30.970694	4.741710	0.535409	1.006293	-0.001370	0.051155	-0.023522
31.06948	4.740098	0.576863	1.007677	-0.002540	0.053226	-0.026311
31.168276	4.738626	0.619970	1.006302	-0.000392	0.055618	-0.023559

INITIAL POINT X= 2R.00000 Y= 5.00000 Z= -0.50000

INITIAL STEPSIZE= 0.20000

ACTUAL POINTS DETERMINED BY INTEGRATOR

X	Y	Z	U	V	M	CP
19.698917	4.075370	-1.139750	0.972324	0.048993	0.105959	0.044396
20.096007	4.044373	-1.095409	0.979819	0.041466	0.113158	0.029407
20.492882	4.074200	-1.047399	0.990244	0.029943	0.123197	0.008556
20.889555	4.071875	-0.997935	0.984249	0.041377	0.123574	0.020546
21.285893	4.091317	-0.947604	0.979215	0.053890	0.126354	0.030613
21.681760	4.115202	-0.895503	0.967105	0.063297	0.130097	0.036833
22.077143	4.145166	-0.842638	0.968244	0.083765	0.127958	0.052556
22.471904	4.184523	-0.791738	0.956466	0.108908	0.120303	0.076153
22.865814	4.235175	-0.744226	0.944695	0.134197	0.108785	0.099835
23.259922	4.295291	-0.701279	0.936667	0.152540	0.096284	0.115309
23.651492	4.362117	-0.663647	0.931889	0.163437	0.082754	0.125266
24.044130	4.431424	-0.631578	0.931378	0.164016	0.069720	0.126287
24.437351	4.499592	-0.604574	0.934768	0.158168	0.058890	0.119508
24.831480	4.563946	-0.581788	0.939977	0.148597	0.049201	0.109090
25.226391	4.624811	-0.563404	0.942073	0.142464	0.038778	0.104898
25.621729	4.683964	-0.549000	0.941836	0.140588	0.030109	0.105372
26.017152	4.743250	-0.537799	0.940027	0.141896	0.023517	0.108990
26.412621	4.802608	-0.528668	0.940777	0.138787	0.019494	0.107490
26.808545	4.859032	-0.521158	0.944713	0.129047	0.017444	0.099618
27.205162	4.910416	-0.517548	0.947702	0.122854	0.017103	0.093641
27.602408	4.956720	-0.513976	0.951136	0.116384	0.017088	0.086772
28.000000	5.000000	-0.500000	0.953846	0.110950	0.017033	0.081152
28.398881	5.020872	-0.496736	0.957520	0.106956	0.016894	0.077352
28.797811	5.041294	-0.493601	0.957585	0.097002	0.014813	0.073873
29.196803	5.061118	-0.490560	0.958377	0.093734	0.014542	0.072290
29.595889	5.080184	-0.487562	0.959682	0.089885	0.014336	0.069681
29.995004	5.098526	-0.484622	0.960098	0.087344	0.013966	0.068047
30.394177	5.116470	-0.481774	0.959772	0.085768	0.013466	0.069499
30.792684	5.135003	-0.478308	0.960789	0.079901	0.012833	0.067466
31.191328	5.153051	-0.4751207	0.960474	0.075856	0.011568	0.068095
31.590194	5.171210	-0.4721207	0.963466	0.066898	0.009553	0.062113
31.989124	5.189470	-0.469166	0.965668	0.059332	0.007663	0.057708
32.388137	5.207870	-0.466327	0.969282	0.050747	0.006109	0.050479
32.787264	5.226442	-0.463642	0.973078	0.042319	0.004438	0.042891
33.186474	5.245157	-0.461042	0.975500	0.036995	0.003399	0.038767
33.585820	5.263970	-0.458678	0.975500	0.034084	0.001561	0.038044
33.985282	5.282818	-0.456517	0.977796	0.028089	0.000183	0.033451
34.384766	5.301727	-0.454530	0.979896	0.022754	-0.000203	0.029652
34.784253	5.320713	-0.452505	0.981920	0.016208	-0.000704	0.025203
35.183711	5.339771	-0.450565	0.984105	0.009251	0.000063	0.020834
35.583151	5.358894	-0.448677	0.986774	0.001643	0.001761	0.015496
35.982574	5.378074	-0.446877	0.989527	-0.006780	0.006123	0.009950
36.381971	5.397317	-0.445102	0.990841	-0.011946	0.012933	0.007362
36.781286	5.416519	-0.443361	0.991611	-0.015048	0.018927	0.005822
37.180518	5.435781	-0.441649	0.992885	-0.018256	0.024059	0.003274
37.579669	5.455098	-0.439986	0.994806	-0.023089	0.028687	-0.000569
37.978744	5.474374	-0.438344	0.996855	-0.028974	0.033140	-0.004266
38.377811	5.493661	-0.436738	0.998029	-0.034834	0.037468	-0.007014
38.776878	5.512952	-0.435160	1.000213	-0.043872	0.051986	-0.011382
39.175945	5.532244	-0.433616	1.002077	-0.045360	0.082024	-0.015110
39.575012	5.551536	-0.432100	1.003691	-0.045481	0.099092	-0.018339
40.000000	5.570828	-0.430616	1.005040	0.012659	0.079237	-0.021037

INITIAL POINT X= 15.40000 Y= 1.50000 Z= 0.00000

INITIAL STEP SIZE= 0.10000

ACTUAL POINTS DETERMINED BY INTEGRATOR

X	Y	Z	U	V	W	CP
-0.089190	0.840364	-1.598771	0.994522	0.000000	0.104528	-0.000000
0.308619	0.840764	-1.556260	0.994522	0.000000	0.104528	-0.000000
0.706428	0.840364	-1.514448	0.994522	0.000000	0.104528	-0.000000
1.104237	0.840364	-1.472637	0.994522	0.000000	0.104528	-0.000000
1.502045	0.840364	-1.430826	0.994522	0.000000	0.104528	-0.000000
1.899892	0.840692	-1.389466	0.994522	0.000000	0.104528	-0.000000
2.297559	0.839562	-1.348055	0.994522	0.000000	0.104528	-0.000000
2.695897	0.842815	-1.310216	0.972407	0.000000	0.104528	-0.000000
3.094768	0.84107	-1.282155	0.963962	0.029581	0.075499	0.044229
3.493754	0.867528	-1.257040	0.964660	0.029581	0.062694	0.061119
3.892621	0.890602	-1.229988	0.971772	0.033271	0.081395	0.059723
4.291407	0.893838	-1.201745	0.971996	0.031279	0.088455	0.045500
4.690212	0.909987	-1.175472	0.965810	0.041835	0.067595	0.045052
5.089449	0.927192	-1.148772	0.972684	0.042617	0.062712	0.051425
5.488758	0.945317	-1.121370	0.973003	0.046507	0.066529	0.043674
5.888171	0.965645	-1.094442	0.972109	0.051831	0.066657	0.043037
6.287634	0.987338	-1.068940	0.974093	0.057117	0.065717	0.044825
6.687070	1.010212	-1.038556	0.974828	0.054329	0.064432	0.040855
7.086162	1.034818	-1.008632	0.974927	0.057915	0.070238	0.039388
7.485195	1.060734	-0.979659	0.976313	0.062150	0.071805	0.039189
7.884278	1.087671	-0.948296	0.977386	0.064867	0.075186	0.036419
8.283361	1.115849	-0.915622	0.977906	0.067630	0.078720	0.034272
8.682441	1.145045	-0.881345	0.979147	0.070761	0.082164	0.033232
9.081524	1.174792	-0.845148	0.980452	0.072727	0.086735	0.030750
9.480605	1.205154	-0.807023	0.981233	0.074150	0.091769	0.028140
9.879686	1.235946	-0.766846	0.982339	0.075730	0.096708	0.026578
10.278767	1.266690	-0.724386	0.983753	0.076394	0.102238	0.024365
10.677848	1.297210	-0.679602	0.984822	0.076050	0.108262	0.021538
11.076929	1.327364	-0.632491	0.986822	0.075498	0.114207	0.019399
11.476010	1.356667	-0.582961	0.989518	0.074251	0.120275	0.017208
11.875091	1.384740	-0.531010	0.987445	0.071703	0.126635	0.014153
12.274172	1.411482	-0.476746	0.988836	0.068589	0.132829	0.011372
12.673253	1.434554	-0.420258	0.989943	0.065151	0.138692	0.009157
13.072334	1.45403	-0.361626	0.991529	0.060316	0.144505	0.005986
13.471415	1.46931	-0.301564	0.993333	0.054423	0.002377	0.002377
13.870496	1.479875	-0.240104	0.994010	0.051542	0.150025	0.001024
14.269577	1.489238	-0.178714	0.994592	0.048642	0.152528	-0.000140
14.668658	1.497975	-0.117132	0.995110	0.045689	0.154871	-0.001177
15.067739	1.505951	-0.055230	0.995771	0.042387	0.157056	-0.002498
15.466820	1.513199	-0.006231	0.996529	0.038803	0.159131	-0.004015
15.865901	1.519598	-0.042714	0.997342	0.035008	0.161072	-0.005641
16.264982	1.525594	-0.079204	1.000904	0.032122	0.163348	-0.012764
16.664063	1.521562	-0.117132	1.017068	-0.002438	0.160088	-0.045093
17.063144	1.518650	-0.090738	1.025004	-0.025495	0.153498	-0.060965
17.462225	1.515839	-0.066231	1.026714	-0.032067	0.147403	-0.064385
17.861306	1.512594	-0.052320	1.026690	-0.034725	0.141428	-0.064336
18.260387	1.509230	-0.038904	1.025505	-0.036484	0.136782	-0.061967
18.659468	1.505942	-0.025833	1.023627	-0.033129	0.133899	-0.058210
19.058549	1.502638	-0.012925	1.021328	-0.030833	0.132693	-0.053612
19.457630	1.500000	0.000000	1.016966	-0.026069	0.134562	-0.044889
19.856711	1.497618	0.013199	1.014519	-0.023337	0.135663	-0.039995
20.255792	1.495367	0.026457	1.014064	-0.023005	0.135587	-0.039084
20.654873	1.493081	0.039672	1.014674	-0.023956	0.134840	-0.040304
21.053954	1.490677	0.052777	1.015682	-0.025280	0.133558	-0.042321
21.453035	1.488143	0.065722	1.016871	-0.026673	0.131795	-0.044698

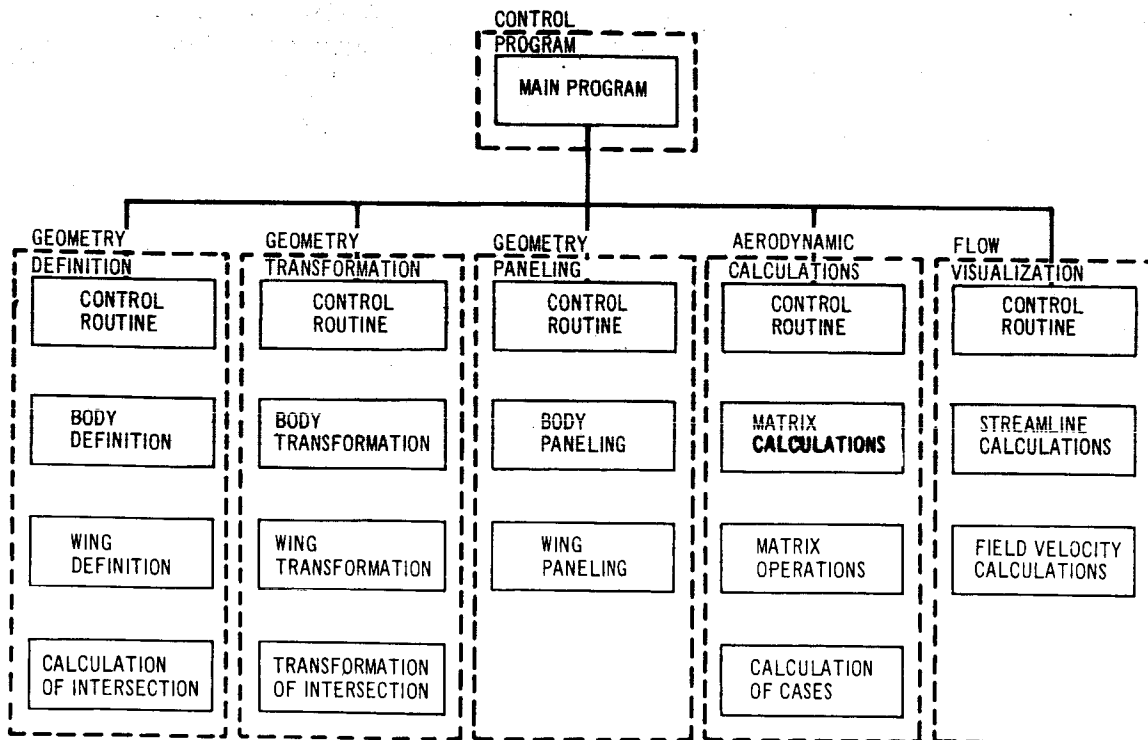
15.994669	1.485474	0.078460	1.018230	-0.028116	0.129585	-0.047417
16.193055	1.479737	0.103151	1.021235	-0.030778	0.123998	-0.053426
16.391582	1.473560	0.126575	1.024361	-0.032714	0.117182	-0.059678
16.590246	1.467325	0.148799	1.026946	-0.031178	0.112284	-0.060847
16.789016	1.461563	0.170182	1.028592	-0.028083	0.108196	-0.060120
16.987880	1.456476	0.190847	1.023709	-0.024276	0.104762	-0.058373
17.186825	1.452170	0.210904	1.023794	-0.019955	0.101553	-0.056545
17.385858	1.448744	0.230241	1.024301	-0.015144	0.098861	-0.054958
17.584236	1.444854	0.249884	1.028934	-0.004837	0.096911	-0.053558
18.183013	1.444639	0.297174	1.035921	0.006061	0.094728	-0.052798
18.382051	1.449404	0.324441	1.034550	0.018446	0.091786	-0.050056
18.581142	1.454859	0.349823	1.030407	0.027767	0.083794	-0.047170
19.180249	1.470097	0.373851	1.023886	0.030978	0.079846	-0.046772
19.379429	1.482481	0.396230	1.021962	0.028834	0.075137	-0.046880
20.178690	1.495563	0.418712	1.027490	0.034633	0.069463	-0.045936
20.378015	1.509343	0.435398	1.027267	0.036271	0.065490	-0.045490
20.577403	1.523493	0.452343	1.025810	0.036014	0.062023	-0.045273
21.176844	1.537880	0.467843	1.026858	0.038801	0.056734	-0.044672
21.376325	1.553401	0.481066	1.028306	0.040574	0.051664	-0.043759
22.175857	1.565007	0.492479	1.030095	0.039104	0.047237	-0.042146
22.375467	1.583656	0.502302	1.031866	0.036400	0.043514	-0.040689
22.575133	1.597566	0.510909	1.031347	0.034108	0.041219	-0.039351
23.174807	1.611651	0.518771	1.029961	0.036626	0.0419361	-0.0370879
23.374470	1.626328	0.526092	1.028192	0.039391	0.0418543	-0.0367341
24.174095	1.642184	0.533035	1.027721	0.042056	0.0416900	-0.0364397
24.373656	1.659410	0.540322	1.021656	0.044600	0.042313	-0.0364269
24.573075	1.678274	0.550731	1.014604	0.049122	0.039965	-0.040164
25.172354	1.697967	0.564469	1.009718	0.050553	0.037906	-0.039392
25.371521	1.719074	0.580614	1.007229	0.050754	0.043503	-0.0375415
26.170608	1.737994	0.598843	1.006198	0.049462	0.048389	-0.023352
26.369635	1.757227	0.619013	1.005081	0.047420	0.053349	-0.021118
26.568634	1.775710	0.640426	1.004429	0.046001	0.053263	-0.023815
27.167665	1.793624	0.661711	1.005942	0.044130	0.055096	-0.022841
27.366663	1.811021	0.684033	1.004991	0.044086	0.057237	-0.020939
28.165595	1.828825	0.707190	1.003829	0.045875	0.059325	-0.018614
28.364452	1.847217	0.731157	1.002969	0.046133	0.061252	-0.016895
28.563272	1.865340	0.755937	1.001990	0.044660	0.063365	-0.014937
29.162749	1.882749	0.781576	1.001187	0.042833	0.065359	-0.013370
29.361839	1.899685	0.807964	1.000406	0.042603	0.067019	-0.011768

4. PROGRAM RECORDS

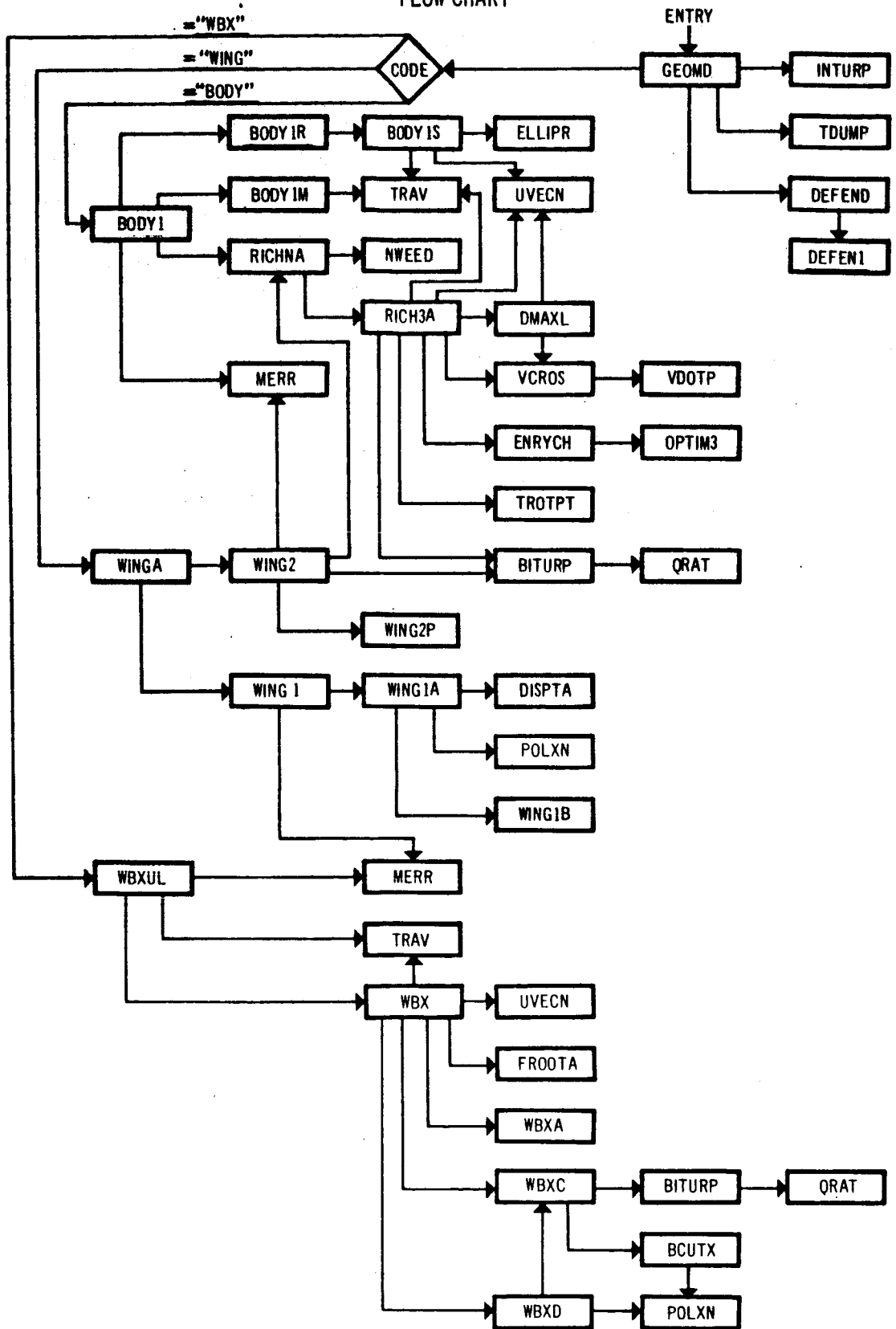
4.1 Flow Charts

A program flow chart, supplemented by flow charts of each of the five main program sections, and a program overlay structure diagram are presented in this section.

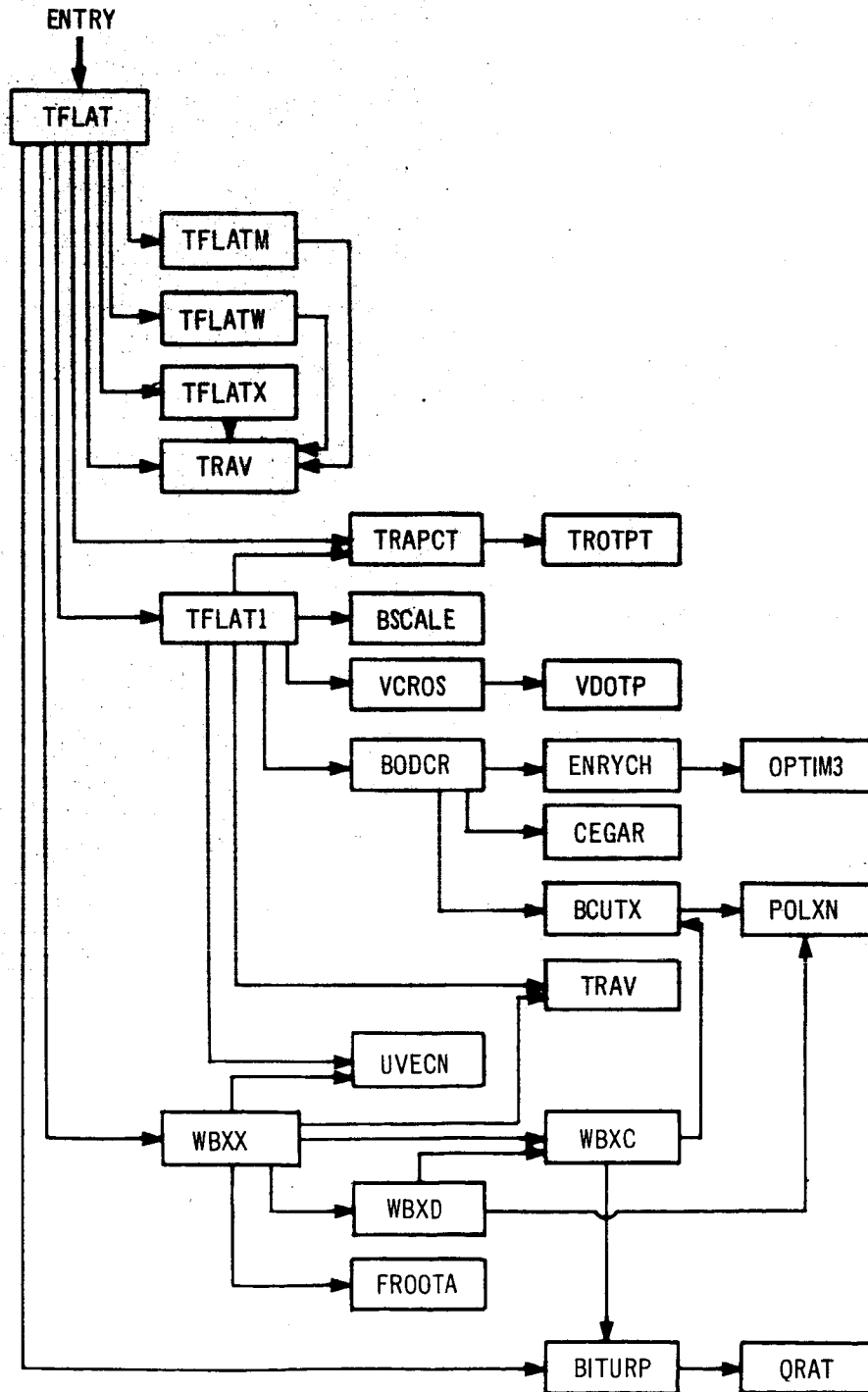
PROGRAM FLOW CHART



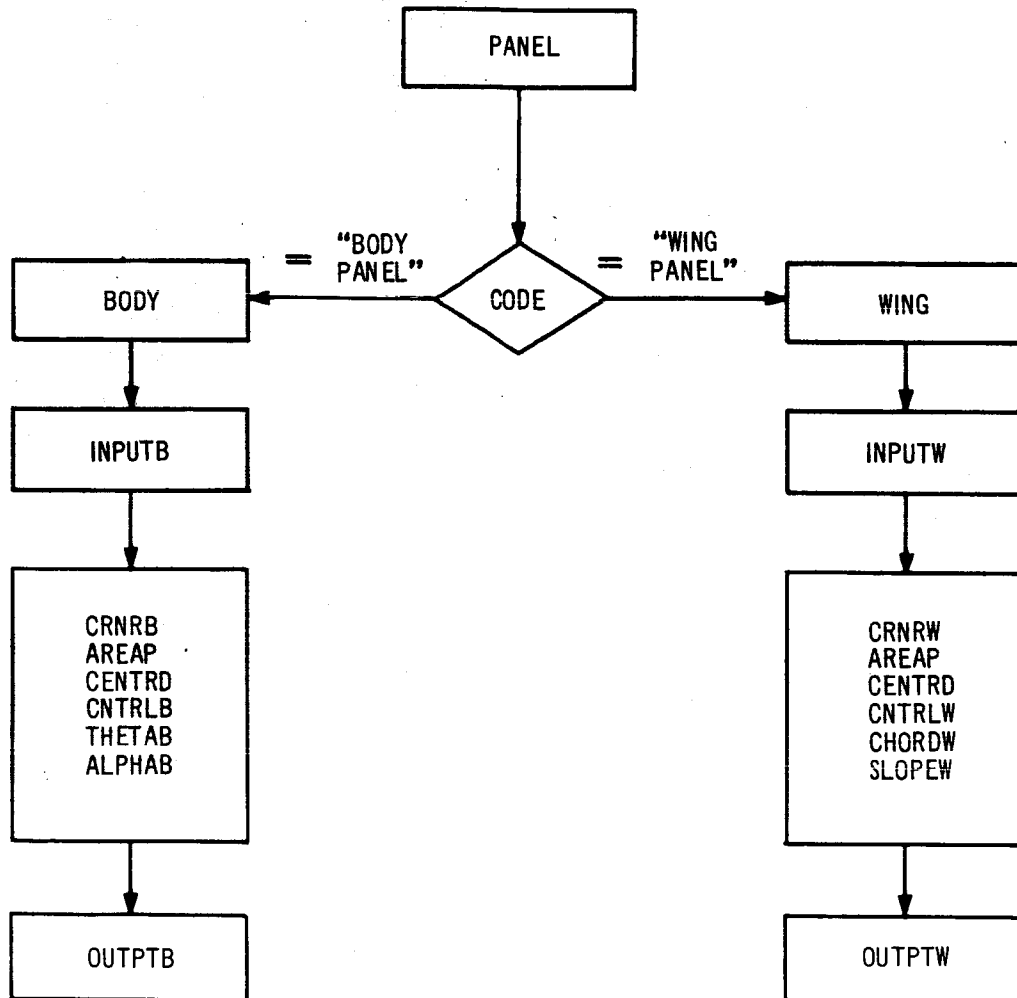
GEOMETRY DEFINITION SECTION FLOW CHART



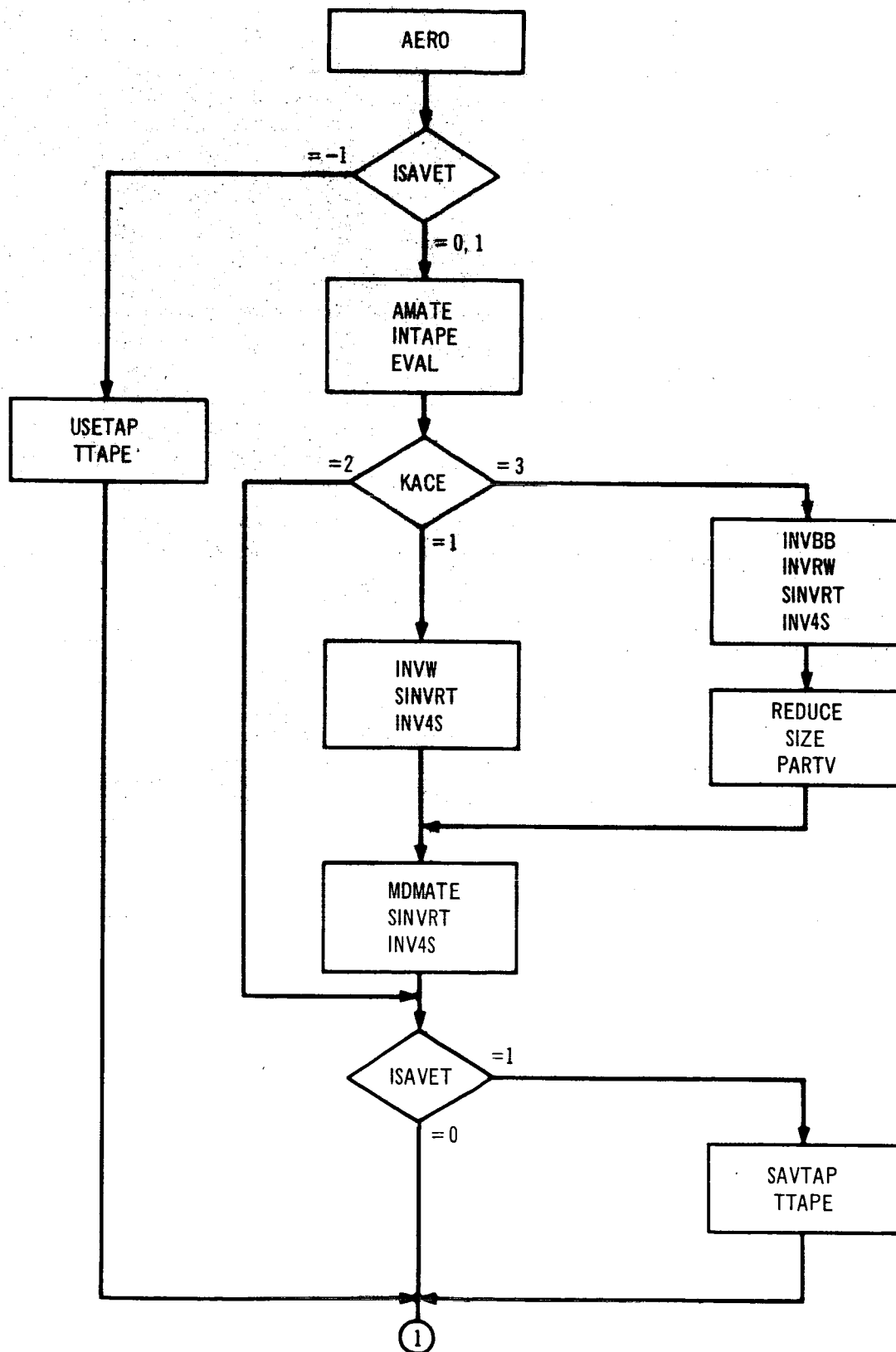
GEOMETRY TRANSFORMATION SECTION FLOW CHART

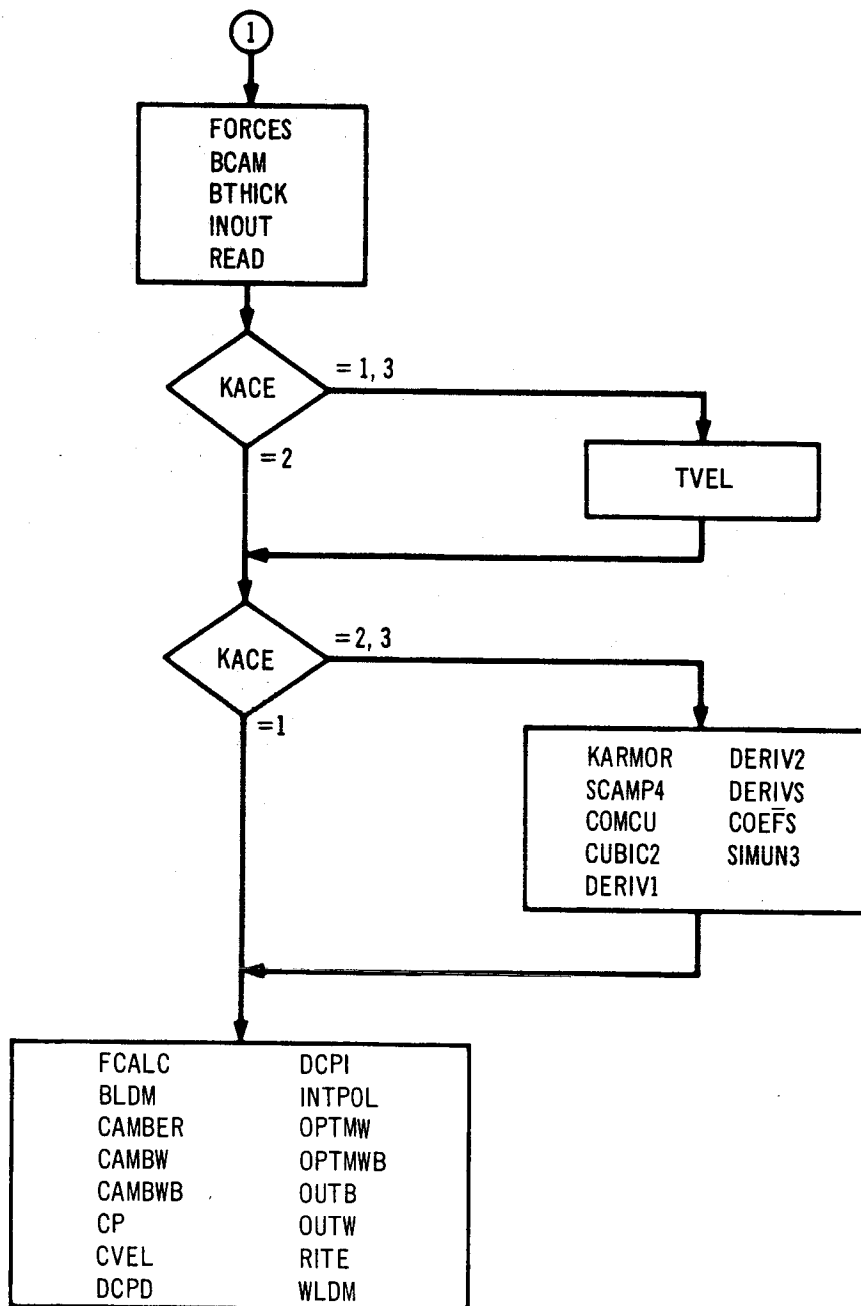


GEOMETRY PANELING SECTION
FLOW CHART

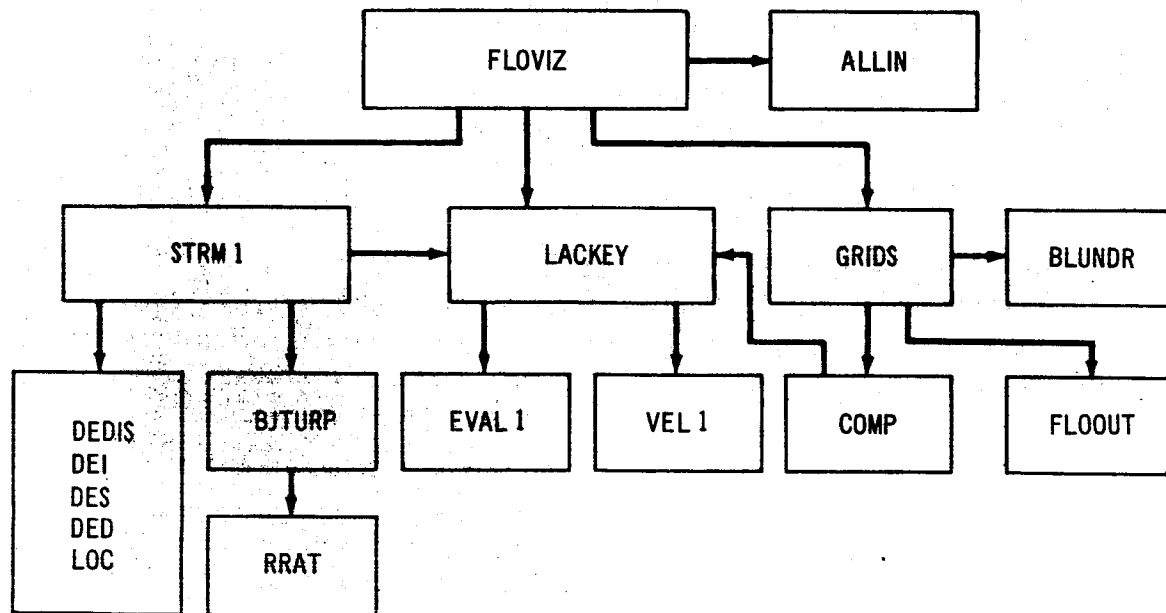


AERODYNAMIC SECTION FLOW CHART

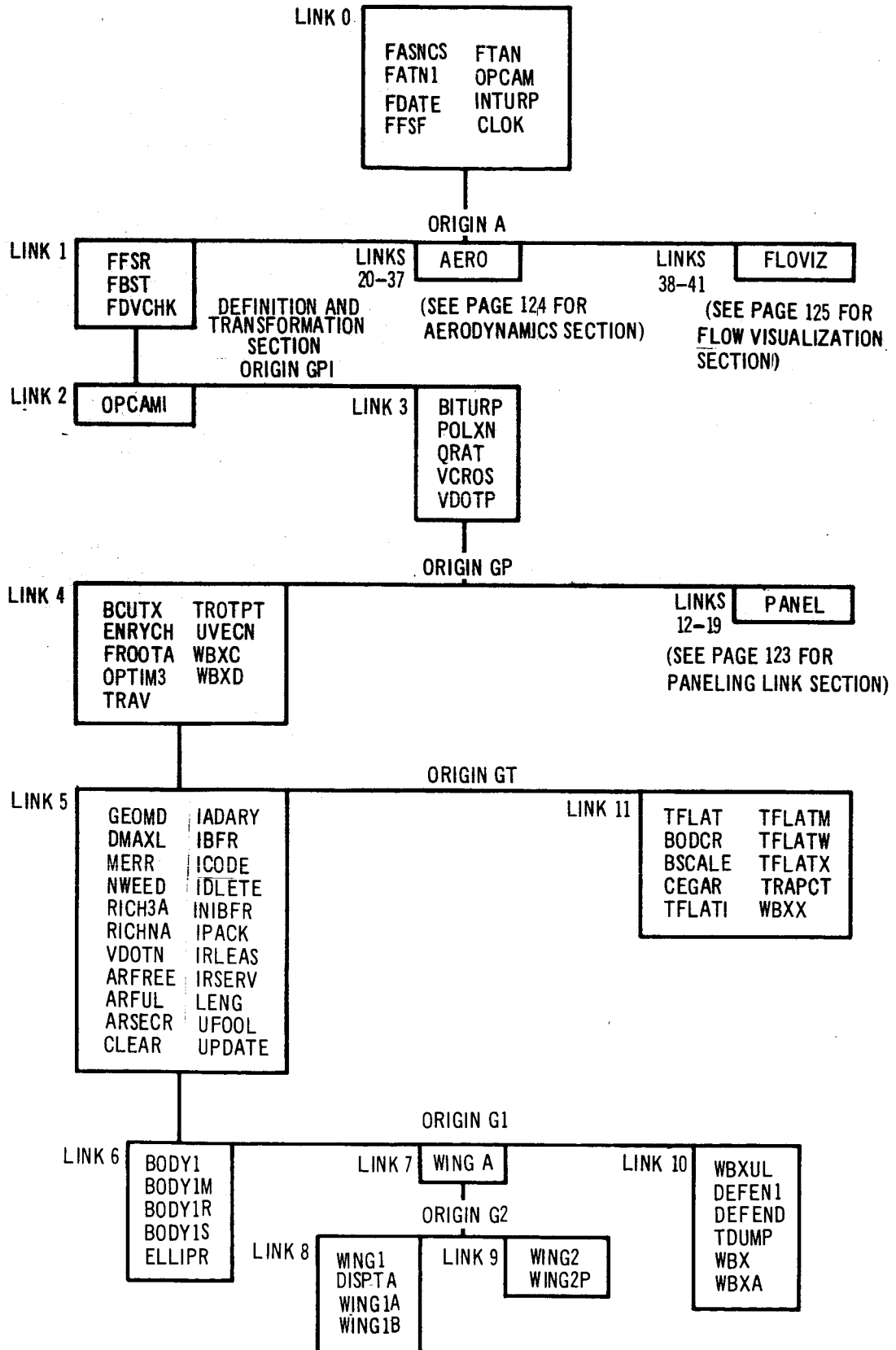




FLOW VISUALIZATION SECTION
FLOW CHART

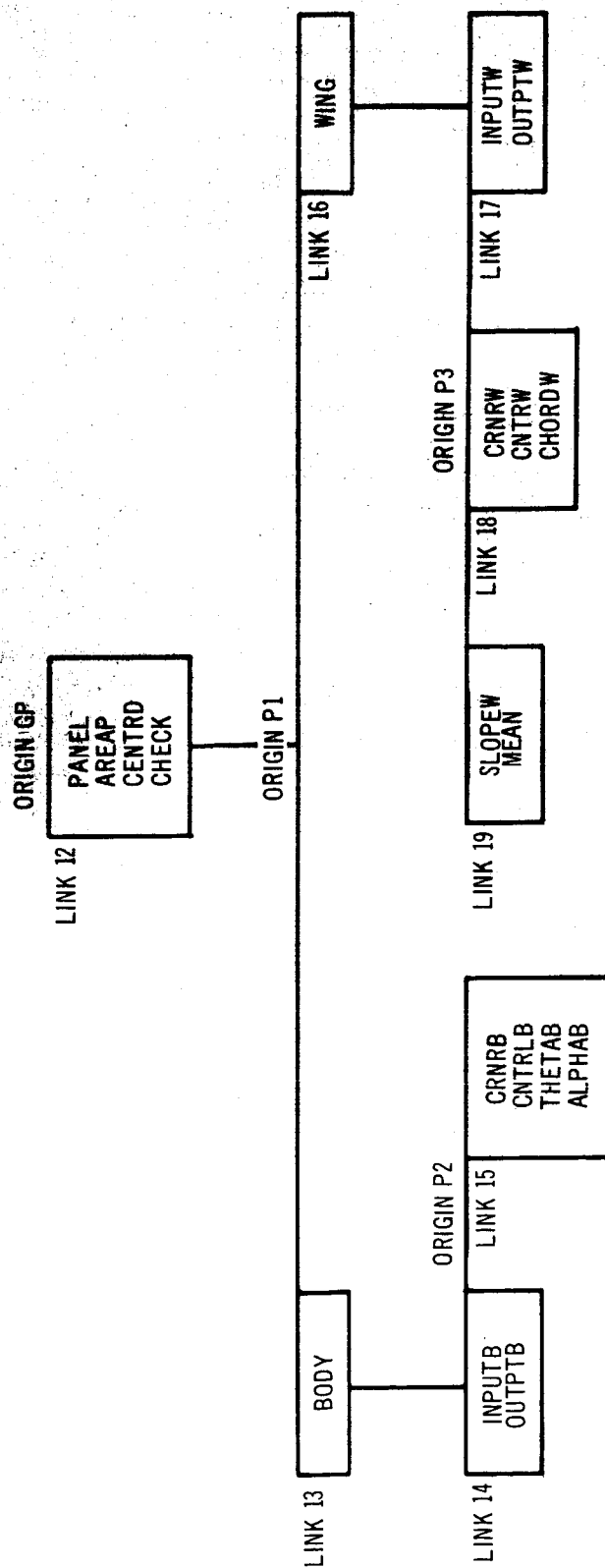


PROGRAM OVERLAY STRUCTURE

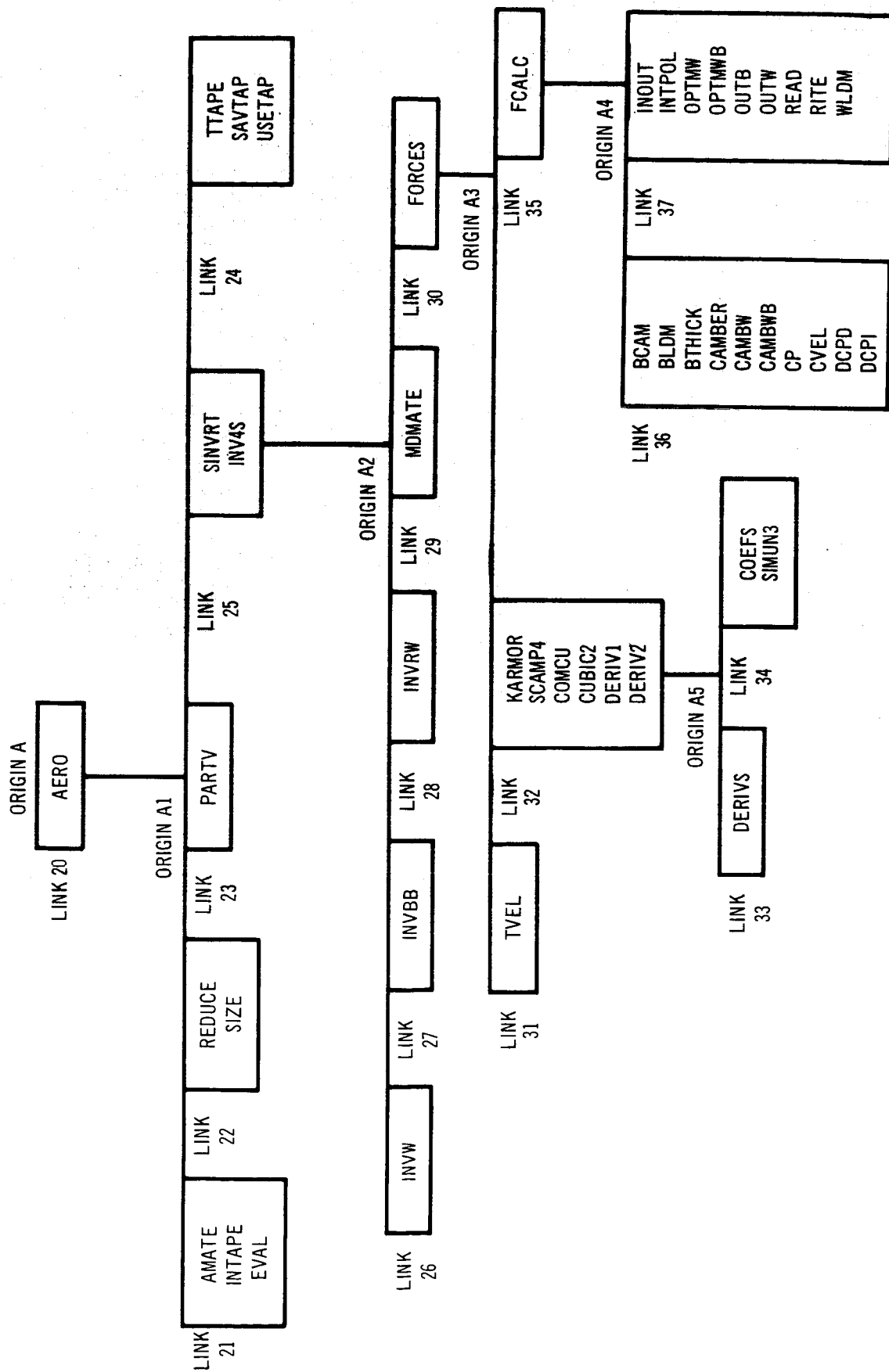


PROGRAM OVERLAY STRUCTURE (CONT)

PANELING SECTION

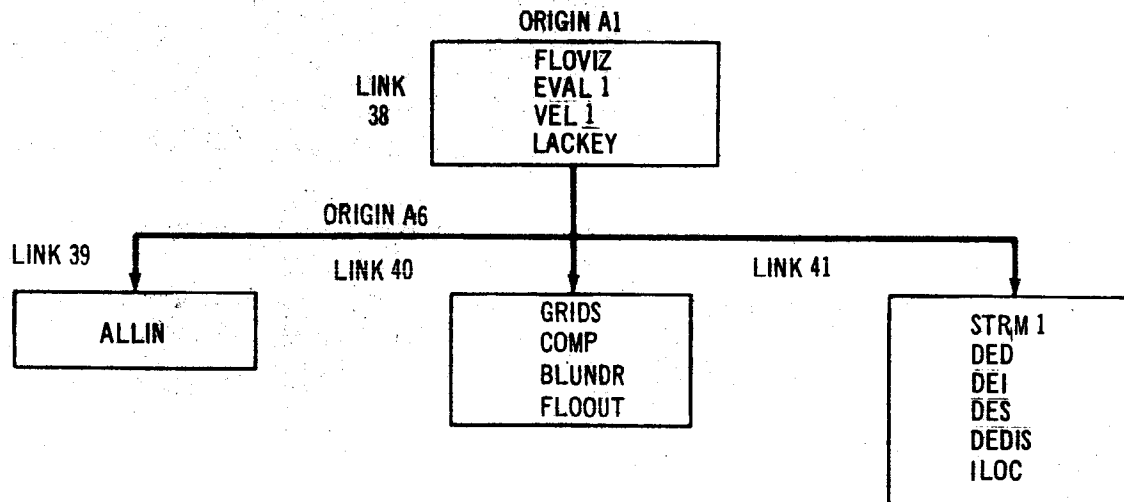


AERODYNAMICS SECTION



PROGRAM OVERLAY STRUCTURE (CONT)

FLOW VISUALIZATION SECTION



4.2 Subroutine Descriptions

The subroutines listed alphabetically in the accompanying index (with the exceptions noted) are discussed in this section.

Subroutine Index

<u>Subroutine</u>	<u>Page</u>	<u>Subroutine</u>	<u>Page</u>
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ALLIN	133	CLEAR	(See Appendix A)
ALPHAB	135	CLOK	181
AMATE	137	CNTRLB	182
AREAP	139	CNTRLW	185
ARFREE	(See Appendix A)	COEFS	187
ARFUL	(See Appendix A)	COMCU	190
ARSECR	(See Appendix A)	COMP	193
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BCUTX	145	CUBIC2	205
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BLDM	149	DCPD	209
BLUNDR	151	DCPI	210
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BODY	154	DEDIS	(See Appendix C)
BODY1	157	DEFEN1	212
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BODY1S	163	DERIV1	215
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<u>Subroutine</u>	<u>Page</u>	<u>Subroutine</u>	<u>Page</u>
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FASNCS	228	LOC	281
FCALC	229	MDMATE	282
FDATE	233	MEAN	285
FFSF	234	MERR	286
FFSR	235	NWEED	287
FLOOUT	237	OPCAM	288
FLOVIZ	239	OPCAMI	290
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FROOTA	244	OPTMW	294
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IPACK	(See Appendix A)	SIZE	334
IRLEAS	(See Appendix A)	SLOPEW	335
IRSERV	(See Appendix A)	STRM1	340
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<u>Subroutine</u>	<u>Page</u>	<u>Subroutine</u>	<u>Page</u>
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TFLAT	344	VDOTP	371
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TRAV	358	WBXX	386
TROTPT	359	WING	389
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UNLOAD	364	WING2	400
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UVECN	368	WLDM	414
VCROS	369		

SUBJECT: FORTRAN IV Subroutine ACOS
(See subroutine FASNCS)

SUBJECT:

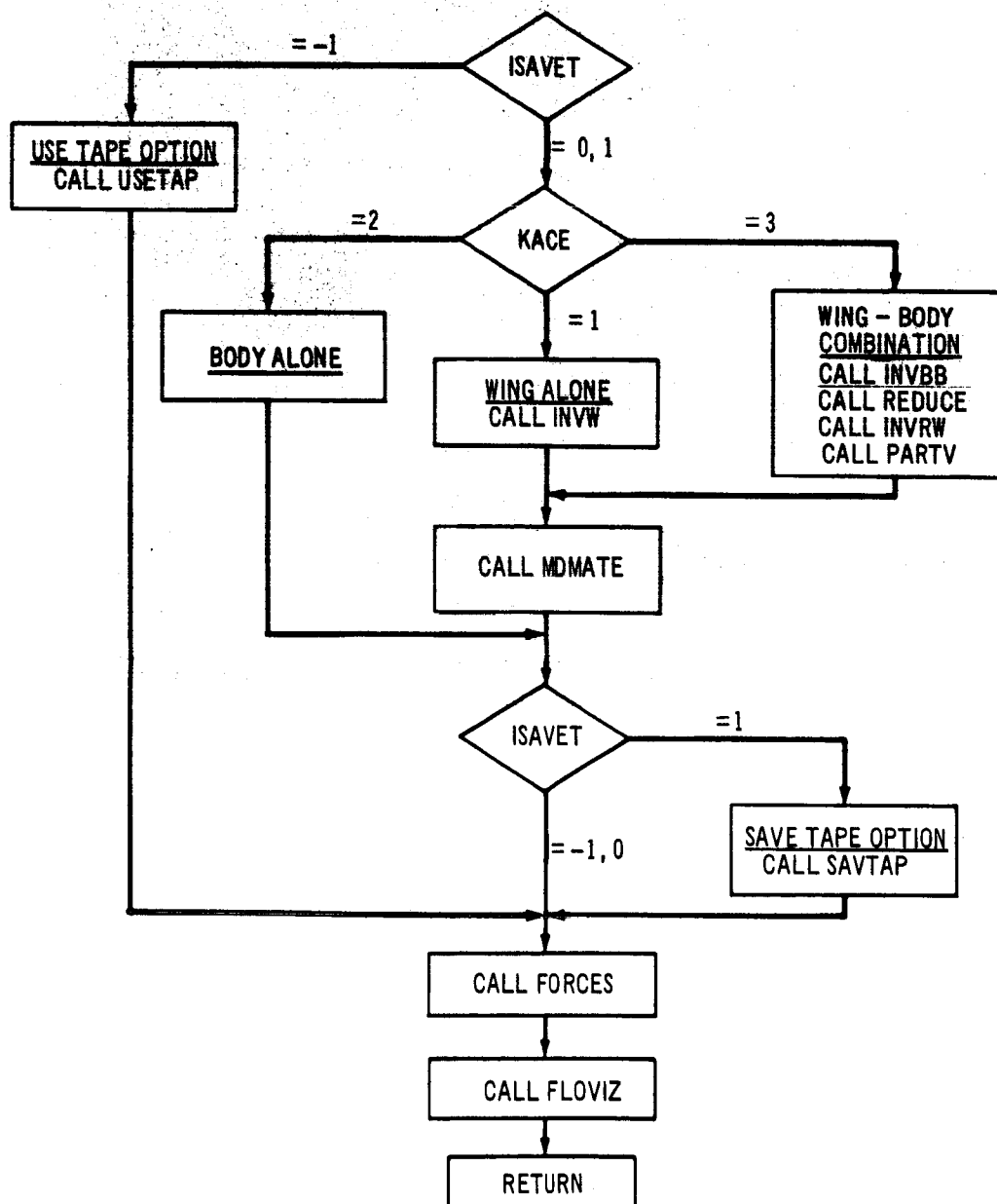
FORTTRAN IV Subroutine AERO

PURPOSE:

To control the flow through the Aerodynamics section of the program.

METHOD:

The flow to the main subroutines of the aerodynamics links is controlled by this subroutine for the three possible configurations (wing alone, body alone, and wing-body combinations).



USAGE:

CALL AERO

**COMMON DATE(2), NTAPEA, NTAPEB, NTAPEC,
NTAPED, NTAPEE, NTAPEF, NTAPEI, NTAPEO,
NBODY, NWING, XMACH, SYM, KACE**

Input: NTAPEC = Logical number of the tape on
which geometrical data and
aerodynamic matrices can be
written and saved for later
computer runs.

KACE = Code that indicates type of
configuration.

= 1, wing alone.

= 2, body alone.

= 3, wing-body combination.

**SUBPROGRAM
CALLED:**

**INTURP
USETAP
AMATE
INWV
INVBB
REDUCE
INVRW
PARTV
MDMATE
SAVTAP
FORCES
FLOVIZ
UNLOAD**

ERROR RETURNS:

None

RES TR ICTIONS:

None

STORAGE

$240_8 = 360_{10}$

SUBJECT: **FORTTRAN IV Subroutine ALLIN**

PURPOSE: **To read a save tape to obtain necessary geometric and computational results from earlier parts of the program for use by EVAL1 and VEL1.**

METHOD: **The tape is read according to the format given in Appendix D .**

USAGE: **CALL ALLIN (NTA)**

COMMON /FLOV1/ KACE, NPANEL, NBODY, NWIN,
 NBODYS, NWINGS, NROW, XMACH, SYM

COMMON /FLOV2/ X, Y, Z, NPART, ALPHAS,
 THETA, XBB, R, WT, T, TC, SST,
 CHORD

COMMON /FLOV3/ T 11, TC 11

COMMON /BA/ XB (210), YB (210), ZB (210)

COMMON /BB/ XC (210), YC (210), ZC (210)

DIMENSION X (210, 3, 4), Y (210, 3, 4), Z (210, 3, 4)

DIMENSION NROW (2), NPART (210)

DIMENSION ALPHAS (210), THETAS (210), CHORD (210)

DIMENSION XBB (50), R (50), WT (120)

DIMENSION T (50), TC (50), SST (210)

Inputs: **NTA = logical tape number of save tape**
 XB = X-coordinate of boundary point
 YB = Y-coordinate of boundary point
 ZB = Z-coordinate of boundary point
 XC = X coordinate of centroid of panels
 YC = Y coordinate of centroid of panels
 ZC = Z coordinate of centroid of panels

The arrays described above are not referenced and are included merely as a convenience for future modifications.

**SUBPROGRAMS
CALLED:**

FSF

ERROR RETURNS: None

RESTRICTIONS: Assumes that the save tape is written in proper format.

STORAGE: $2200_8 = 1172_{10}$

SUBJECT:

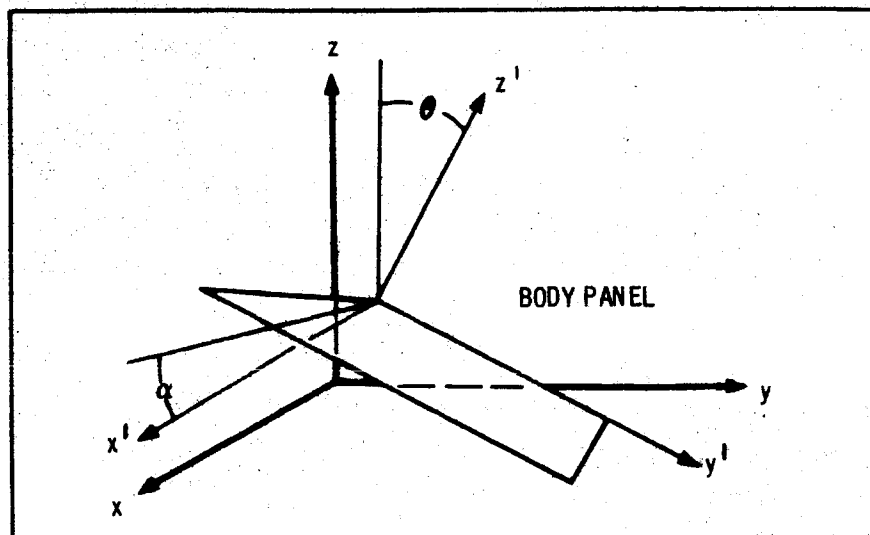
FORTAN IV Subroutine ALPHAB

PURPOSE:

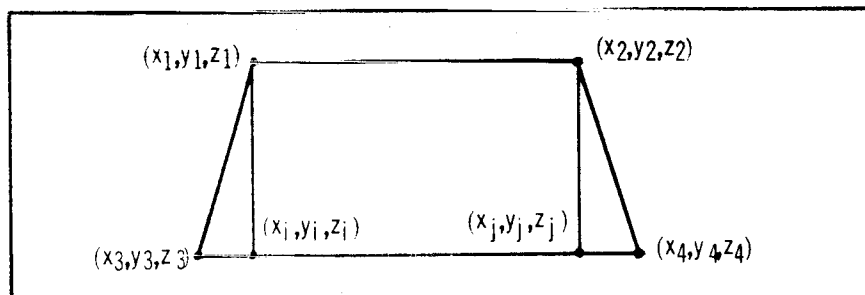
To calculate body panel alpha-incidence angles.

METHOD:

The program calculates the panel alpha-incidence angle by use of a geometric function. For an arbitrary body panel,



the incidence angle, α , is the angle of the panel in the x' , y' , z' coordinate system of the panel as viewed down the y' -axis. The x' -axis of this system is parallel to the x -axis of the body coordinate system, though this is not true for the y' and z' axes for a panel of nonzero θ -inclination. For a body panel defined as follows,



the α -incidence angle is calculated by the following formula, which involves the inclination angle θ ,

$$\alpha = \tan^{-1} \left[\frac{(z_1 - z_i) \cos \theta - (y_1 - y_i) \sin \theta}{(x_1 - x_i)} \right]$$

USAGE: **COMMON** (See subroutine OPCAMI for unlabeled **COMMON** description)

COMMON /COM1/ (See subroutine **PANEL**)

Input: **NPER1**
 NPLN1

COMMON /COM2/ (See subroutine **BODY**)

Input: **KPANEL**
 XCOR
 YCOR
 ZCOR
 XINT
 YINT
 ZINT
 THETA

Output: **ALPHA**

CALL ALPHAB

SUBPROGRAMS

CALLED:

ATAN	}	Built-in functions
SIN		
COS		

ERROR RETURNS: **None**

STORAGE: **362₁₀ = 552₈**

SUBJECT:

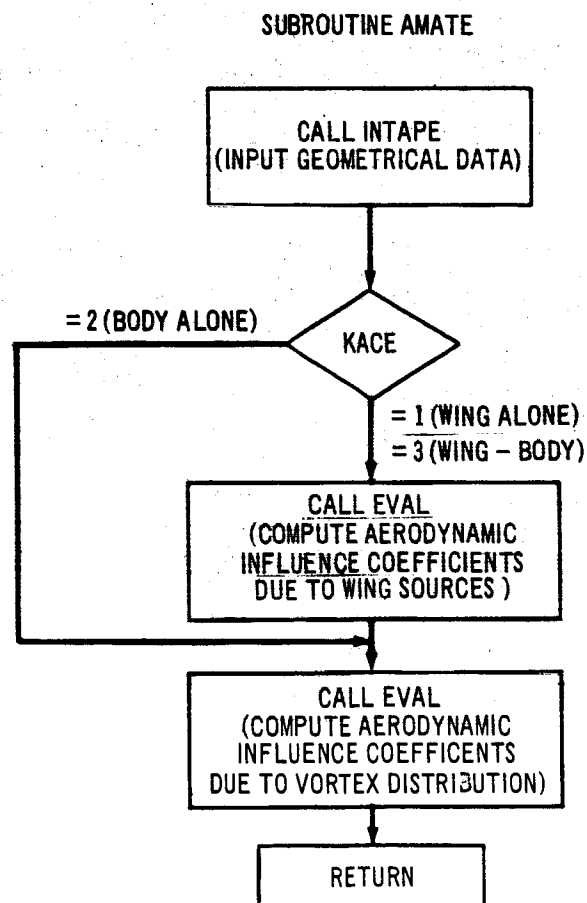
FORTRAN IV Subroutine AMATE

PURPOSE:

To control the flow through a section of the aerodynamic links of the program.

METHOD:

The flow is given in the following diagram.



USAGE:**CALL AMATE**

COMMON DATE(2), NTAPEA, NTAPEB, NTAPEC,
NTAPED, NTAPEE, NTAPEF, NTAPEI, NTAPEO,
NBODY, NWIN, XMACH, SYM, KACE

COMMON /BLOCK/ ALPHAS(210), AREA(210),
A(210), ALPHAC(110), ALPHAT(110), CHORD(210),
ISYM, NPART(210), NPANEL, NROW(2),
THETA(210), TAIL, U(210), V(210), VPM(210),
VV(210), VPMM(210), W(210), WPM(210), WW(210),
WPMM(210), X(210, 3, 4), XBAR(210), XC(210),
Y(210, 3, 4), YBAR(210), YC(210), Z(210, 3, 4),
ZBAR(210), ZC(210)

Input: KACE = Code that indicates type of configuration.

= 1, wing alone.

= 2, body alone.

= 3, wing-body combination.

NBODY= Number of body panels.

XC = Array of panel control point coordinates.

XBAR = Array of panel centroid coordinates.

**SUBPROGRAMS
CALLED:**

INTAPE

EVAL

ERROR RETURNS:

None

RESTRICTIONS:

None

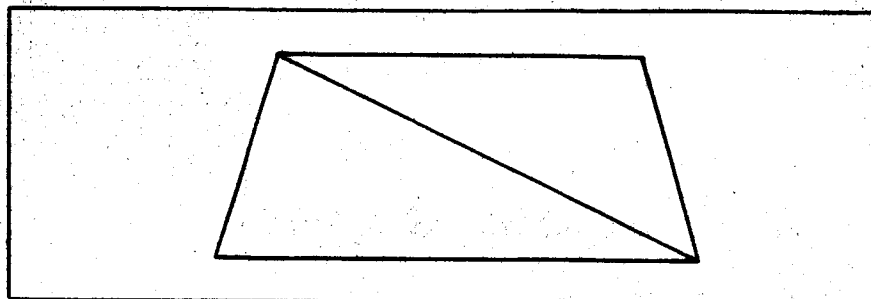
STORAGE:

$12282_{10} = 27772_8$

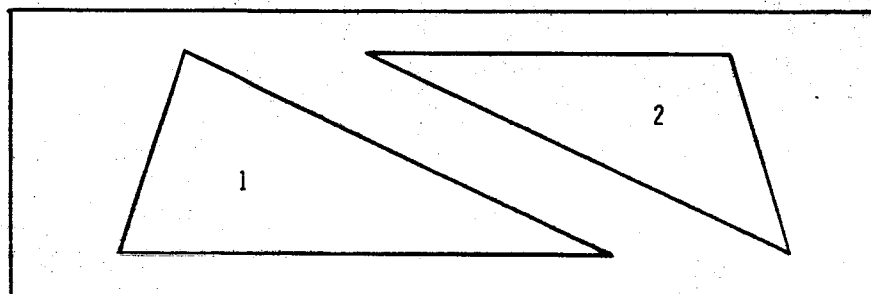
SUBJECT: FORTRAN IV Subroutine AREAP

PURPOSE: To calculate the area of a panel.

METHOD: Area S of a panel is obtained by dividing panel into two triangular subpanels, using a vector cross-product routine to calculate the area of each subpanel and summing these two results for the area of the panel. For example, a quadrilateral panel,



is divided into two subpanels, thus:



and areas S_1 and S_2 of each subpanel are calculated and summed for panel area S .

$$S_1 + S_2 = S$$

The subroutine also calculates ratio R of area S_1 of subpanel 1, to panel area S ,

$$R = \frac{S_1}{S}$$

This value is used in other subroutines.

USAGE: DIMENSION X(16, 16), Y(16, 16), Z(16, 16), S(15, 15),
R(15, 15)

$\left. \begin{array}{l} X \\ Y \\ Z \end{array} \right\} =$ x, y, and z coordinates of panel corner points.

S = Panel area.

R = Ratio of subpanel area to panel area.

CALL AREAP (X, Y, Z, S, R, NC, NR)

Input: $\left. \begin{array}{c} X \\ Y \\ Z \end{array} \right\} \text{ (see above)}$

NC = Number of panel columns.

NR = Number of panel rows.

Output: $\left. \begin{array}{c} S \\ R \end{array} \right\} \text{ (see above)}$

SUBPROGRAM

CALLED: VCROS

ERROR RETURNS: None

STORAGE: $239_{10} = 357_8$

SUBJECT: FORTRAN IV Subroutine ASIN
(See subroutine FASNCS)

SUBJECT: **FORTTRAN IV Function ATN1**

PURPOSE: **To compute the arctangent, in radians.**

METHOD: **This function has been replaced by the standard built-in
function ATAN2 with a \$NAME control card.**

SUBJECT: FORTRAN IV Subroutine BCAM

PURPOSE: To compute camber slopes at body panel control points from a given body camber shape.

METHOD: The camber shape is specified by a table of z (camber) vs. x (body source control station). This table is converted to a second table of Δz vs. x :

$$\Delta z_i = \frac{z_{i+1} - z_i}{x_{i+1} - x_i}$$

Slope α_c (camber slope) at x_c (body panel control point) is contained by interpolation:

$$\alpha_{c_j} = \Delta z_{i+1} + \frac{x_c - x_i - 1}{x_i - x_{i-1}} \times (\Delta z_i - \Delta z_{i-1})$$

USAGE: CALL BCAM (NBODYS, NROWB, XB, ZDELTA, XC, DZDXB, ACB)

DIMENSION XB(55), ZDELTA(55), XC(100), DZDXB(55), ACB(55)

Input: NBODYS = Number of body source control stations.

NROWB = Number of rows of body panels.

XB = Array of x-coordinates of body source control stations.

ZDELTA = Array of camber shapes at the body source control stations.

XC = Array of x-coordinates of body panel control points.

DZDXB = Dummy array.

Output: ACB = Array of camber slopes at the body panel control points.

SUBPROGRAMS CALLED:

None

ERROR RETURNS: None

RESTRICTIONS: NBODYS \leq 55

STORAGE: $132_{10} = 204_8$

SUBJECT: FORTRAN IV Subroutine BCUTX

PURPOSE: To find the intersections of a set of body meridian lines with a plane normal to the x-axis.

METHOD: Subroutine POLXN is used to find the intersection of each meridian line with the plane.

USAGE: DIMENSION B(1), A(2, N)
CALL BCUTX (B, N, X, EP, NA, A)

Input: B = Array of body meridian line points, with header (see subroutine WBXUL).
N = Number of body meridian lines.
X = Body station. The plane will be taken as $x = X$.
EP = A tolerance used by POLXN in finding intersections.

Output: NA = Number of points in A. $NA \leq N$.
A = Array of points (y_i, z_i) in section. These points are in 1-to-1 correspondence with meridian lines only if each meridian line intersects the plane.

SUBPROGRAM CALLED: POLXN

ERROR RETURNS: None

RESTRICTIONS: N must be greater than zero. If a meridian line has multiple plane intersections, the first intersection found will be used.

STORAGE: $133_{10} = 205_8$

SUBJECT: FORTRAN IV Subroutine BITURP

PURPOSE: Given a table of y versus x and a value of x, to find the corresponding value of y by either linear or biquadratic interpolation.

METHOD: Let n be the number of points (x_i, y_i) in the given table. Let X be the given value of x for which the corresponding Y is desired. If $n = 2$, the linear interpolation mode is selected (even if biquadratic interpolation was requested). If $x_1 < x_n$, the table is searched from top to bottom; otherwise the search is from bottom to top. If X is outside the table range, an error code is set and Y is returned as y_1 or y_n (depending on whether X is closer to x_1 or x_n). If $X = x_i$ then no interpolation is necessary and $Y = y_i$. Otherwise, the table interval that contains X is located. For linear interpolation, the calculation of Y is trivial.

Y may be found by biquadratic interpolation if X does not lie in the first or last table interval. For illustration of the method, assume that $x_2 < X < x_3$. Fit a quadratic $Q_2(x)$ to the points (x_i, y_i) , $i = 1, 2, 3$ and another quadratic $Q_3(x)$ to the points (x_i, y_i) , $i = 2, 3, 4$. Find the slopes $Q'_2(x_2)$ and $Q'_3(x_3)$. Fit a cubic to the points (x_2, y_2) and (x_3, y_3) with the corresponding slopes $Q'_2(x_2)$ $Q'_3(x_3)$. Evaluate the cubic at $x = X$ to find Y.

However, Y is actually computed by the following interpolating formula (which has a continuous first derivative), mathematically equivalent to the above method:

$$Y = \frac{(x_3 - X)Q_2(X) + (X - x_2)Q_3(X)}{x_3 - x_2}$$

$Q_2(X)$ and $Q_3(X)$ are found by subroutine QRAT.

If X lies in the first or last interval of the table, biquadratic interpolation cannot be used. Y is therefore computed by quadratic interpolation.

USAGE: DIMENSION X(1), Y(1), NU(3)

CALL BITURP (X, Y, I, N, K, XI, YI, NU)

Input: X = Location of the first x-coordinate in the table.

Y = Location of the first y-coordinate in the table.

- I** = Skip number; that is, the spacing of table values in the X and Y arrays. For example, $I = 1$ if $X = (x_1, x_2, \dots)$ and $Y = (y_1, y_2, \dots)$; however, if x and y are stored in a single array, say $W = (x_1, y_1, x_2, y_2, \dots)$, then $I = 2$ and the subroutine call would be `CALL BITURP (W, W(2), 2, ...)`.
- N** = Number of points in the table.
- K** = Interpolation code ($K = 1$ if linear interpolation; $K = 2$ if biquadratic interpolation).
- XI** = The given value of x for which the corresponding value of y is desired.
- NU** = Error indicator array: `NU(1)` is not used, on input. `NU(2)` is an output tape number on which to write a message if an error is detected; no message is written if $NU(2) \leq 0$. `NU(3)` is an error message limiter; if an error is detected, $NU(3) = NU(3) - 1$. Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.

Output: **YI** = Interpolated value of y (if $NU(1) = 0, 1, \text{ or } 2$).

NU = Error indicator array: $NU(1) = 0$ if success; $= -1$ if $I \leq 0$; $= -2$ if $N < 2$; $= -3$ if $x_1 = x_n$; $= 1$ or 2 if X is outside the table range; $= 3$ or 4 if a quadratic could not be formed (because two points near the line $x = X$ have the same x-coordinate. `NU(2)` is not an output. `NU(3)` is reduced by one if an error was detected.

SUBPROGRAM

CALLED:

QRAT

RESTRICTIONS:

BITURP does not check the X array to see that it is monotonic. Weird results may be obtained if it is not monotonic in the neighborhood of the interpolating interval for biquadratic interpolation.

STORAGE:

$375_{10} = 567_8$

SUBJECT:

**FORTRAN IV Subroutine BJTURP
(See Subroutine BITURP)**

SUBJECT: FORTRAN IV Subroutine BLDM

PURPOSE: To compute the coefficients of lift, drag, and pitching moment for the region of the body represented by panels.

METHOD: The force normal to the panel is given as the product of the dynamic pressure, surface pressure coefficient, and panel area:

$$F_i = q \cdot C_{p_i} \cdot A_i$$

Resolving into the components normal and parallel to the free stream yields the lift and drag

$$L_i = - F_i \cdot \cos \theta_i$$

$$D_i = F_i \cdot n_i$$

where n_i is the component of velocity normal to the x-axis and θ_i is the angle between the plane of the panel and a panel parallel to the x-y plane.

The moment of force with respect to a point (x, 0, z) is given by

$$M_i = - L_i (\bar{x}_i - x) + D_i (\bar{z}_i - z)$$

where \bar{x}_i , \bar{z}_i are the x and z coordinates of the panel centroid.

Finally, the coefficients of lift, drag, and moment on the body panels are given by

$$C_L = \frac{1}{q \cdot S_W} \sum_{i=1}^{NM} L_i$$

$$C_D = \frac{1}{q \cdot S_W} \sum_{i=1}^{NM} D_i$$

$$C_M = \frac{1}{q \cdot S_W} \sum_{i=1}^{NM} M_i$$

where S_W is the wing reference area, and NM is the number of body panels.

USAGE: CALL BLDM(NM, XP, ZP, RFAREA, AREA, XBAR, ZBAR, ALPHAM, THETAM, CPM, CL, CD, CM)

DIMENSION AREA(NM), XBAR(NM), ZBAR(NM),
ALPHAM(NM), THETAM(NM), CPM(NM)

Input: NM = Number of body panels.

XP = x-coordinate of the point about which the pitching moments are to be calculated.

ZP = z-coordinate of the point about which the pitching moments are to be calculated.

RFAREA = Wing reference area.

AREA = Array of body panel areas.

XBAR = Array of body panel centroid x-coordinates.

ZBAR = Array of body panel centroid z-coordinates.

ALPHAM = Array of the velocity components normal to the x-axis.

THETAM = Array of angles between the plane of the panel and a plane parallel to the x-y plane.

CPM = Array of panel surface pressure coefficients.

Output: CL = Coefficient of lift.

CD = Coefficient of drag.

CM = Coefficient of pitching moment.

SUBPROGRAM

CALLED: COS (Built-in function)

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $118_{10} = 166_8$

SUBJECT: FORTRAN IV Function BLUNDR

PURPOSE: This routine is used to prevent the overflow of arrays in GRIDS.

METHOD: Compares the product of increment parameters IX, IY, IZ against NMAX as indicated by MODE (see Subroutine GRIDS).

USAGE: IF (BLUNDR (IX, IY, IZ, MODE, NMAX).NE.O.)
RETURN

Input: IX = x - increment parameters.
IY = y - increment parameters.
IZ = z - increment parameters.
MODE = Indicates the planar cut to be taken;
the total number of points in such a
plane must be less than NMAX.
NMAX = The maximum dimension of the GP and
VLS arrays.

Output: BLUNDR = 0. acceptable inputs.
= 1. unacceptable inputs.

A message is written on the output tape if
BLUNDR = 1

**SUBROUTINES
CALLED:** None

ERROR RETURNS: See Output above.

RESTRICTIONS: None

STORAGE: $135_{10} = 217_8$

SUBJECT: FORTRAN IV Subroutine BODCR

PURPOSE: To find the area, equivalent radius, and centroid of a body section.

METHOD: It is assumed that the body is symmetrical about a plane parallel to the x-z plane, and that only one side of the body is given. The body is specified by a set of meridian lines (subroutine WBXUL). Subroutine BCUTX is used to find the y-z coordinates of the meridian lines at a given value of x. These coordinates form the two-dimensional points of a body section. A test is made to see that the y-coordinates of the first and last points are the same within a given tolerance. The average of these two values is used for the centroid y-coordinate. Subroutine ENRYCH is called and, if a given quantity CHD is greater than zero, additional points on the section are interpolated. The centroid and area of the section are found by subroutine CEGAR. The area is then doubled to make it apply to the entire body section. If the area is smaller than a given tolerance, the z-coordinate of the centroid is taken as the average of the z-coordinates of the first and last points in the section; otherwise, the value found by CEGAR is used. The z-coordinate of the centroid is set to zero if it is smaller than a given tolerance. The section radius is found by averaging the distances from the centroid to each meridian line; if the radius is less than a given tolerance, it is set to zero.

USAGE: DIMENSION B(1), EP(5), S(2, N), E(MAXE), NU(3)
 CALL BODCR (B, N, X, EP, CHD, MAXE, S, E, NE, Y, Z, AREA, RAD, NU)

Input: B = Body meridian line array, with header (see subroutine WBXUL).
 N = Number of meridian lines.
 X = Body station (x-coordinate section).
 EP = Array of tolerances.
 CHD = Tolerance that regulates the number of points interpolated by ENRYCH (affects only AREA and Z).
 MAXE = Length of array E.

NU = Error indicator array. NU(1) is not used on input. NU(2) is an output tape number on which to write a message if an error is detected; no message is written if $NU(2) \leq 0$. NU(3) is an error message limiter; if an error is detected, $NU(3) = (NU(3) - 1)$. Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.

Output: S = Array of points (y_i, z_i) in section.
 E = Scratch array.
 NE = Number of elements in enriched array.
 Y = y-coordinate of centroid.
 Z = z-coordinate of centroid.
 AREA = Area of entire section (twice area of the half-section).
 RAD = Equivalent radius.
 NU = Error indicator array. NU(1) = 0 if success.

SUBPROGRAMS CALLED
 ENRYCH
 CEGAR
 SQRT (Built-in function)
 BCUTX

ERROR RETURNS: A message is written if an error is detected. NU = 1 if the number of points in the section (found by BCUTX) is less than N or less than 2. An error of NU = 2, 4, or 5 is from ENRYCH. If an error code of 3 was returned by ENRYCH, NU is set to zero but a message is written.

RESTRICTIONS: CHD should be zero if the section is symmetrical about a horizontal plane or if there are less than eight meridian lines.

STORAGE: $486_{10} = 746_8$

SUBJECT: FORTRAN IV Subroutine BODY

PURPOSE: To serve as a control program for the body paneling sub-routines.

METHOD: Program uses a series of FORTRAN IV language "CALL" statements to call the required body paneling subroutines.

The program contains the following labeled COMMON statement that occurs in all lower level body paneling subroutines, COMMON /COM2/ NPLNB, NPLNW, JLEAD, JTRAIL, IMID, NPTS(16), X(16, 90), Y(16, 90), Z(16, 90), XCEPT(21), XCEPTB(21), XCEPTW(16), YCEPTW(16), ZCEPTW(16), CODEBW(16), KPANEL(15, 20), XCOR(16, 21), YCOR(16, 21), ZCOR(16, 21), XINT(15, 20, 2), YINT(15, 20, 2), ZINT(15, 20, 2), XCEN(15, 20), YCEN(15, 20), ZCEN(15, 20), XCON(15, 20), YCON(15, 20), ZCON(15, 20), AREA(15, 20), ARAT(15, 20), THETA(15, 20), ALPHA(15, 20), CHORD(15, 20)

NPLNB = Number of cutting planes to intersect the body fore and aft of the body-wing intersection region.

NPLNW = Number of cutting planes to intersect the body in the body-wing intersection region.

JLEAD }
JTRAIL } = Codes for internal program control.
IMID }

NPTS = Number of points on the successive body meridian lines that define the body.

X }
Y } = x, y, and z coordinates of points
Z } on body meridian lines.

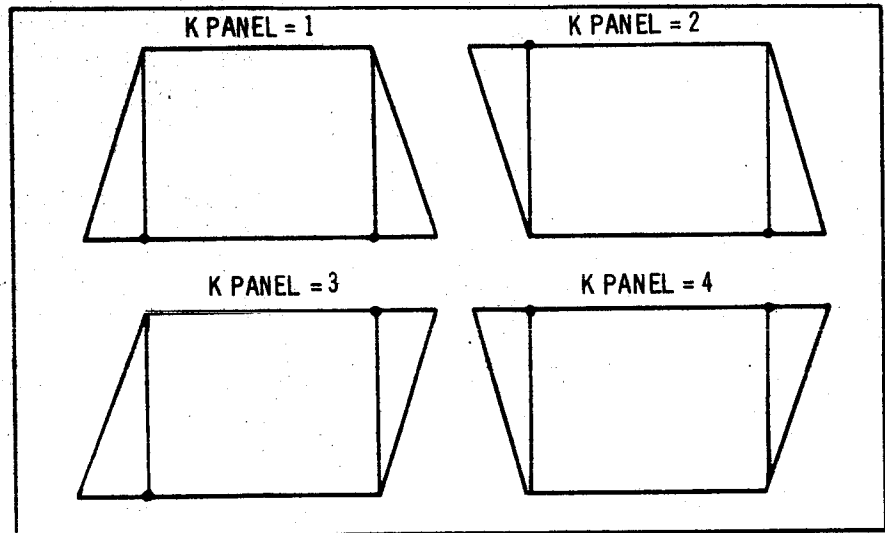
XCEPT = x intercepts of all body cutting planes.

XCEPTB = x intercepts of those body cutting planes that intersect fore and aft of the body-wing intersection region.

XCEPTW }
YCEPTW } = x, y, and z coordinates of the inter-
ZCEPTW } sections with the body of those wing per-
cent lines that define body cutting planes.

CODEBW = Codes that indicate wing percent lines that are to define body cutting planes in body-wing intersection region.

KPANEL = Code for body panel type. If KPANEL (I, J) = 1, both additional subpanel corner points are located on panel trailing edge. If KPANEL(I, J) = 2, inboard point is on leading edge, and outboard point is on trailing edge. If KPANEL (I, J) = 3, inboard point is on trailing edge and outboard point is on leading edge. If KPANEL(I, J) = 4, both points are on leading edge.



XCOR }
YCOR } = x, y, and z coordinates of body
ZCOR } panel corner points.

XINT }
YINT } = x, y, and z coordinates of additional
ZINT } subpanel corner points.

XCEN }
YCEN } = x, y, and z coordinates of body
ZCEN } panel centroid.

XCON }
YCON } = x, y, and z coordinates of body
ZCON } panel control point.

AREA = Body panel area.

ARAT = Ratio of subpanel area to panel area.

THETA = Body panel theta-inclination angle.

ALPHA = Body panel alpha-incidence angle.

CHORD = Body panel streamwise chord length.

USAGE: **COMMON** (See subroutine OPCAMI for description of unlabeled **COMMON**)

CALL BODY

SUBPROGRAMS

CALLED:

INPUTB
CRNRB
AREAP
CENTRD
CNTRLB
THETAB
ALPHAB
OUTPTB

ERROR RETURNS: Error message indicates whether error occurred in calculation of body panel geometry.

STORAGE: $152_{10} = 230_8$

SUBJECT: FORTRAN IV Subroutine BODY1

PURPOSE: To read data cards that specify a body surface and generate three-dimensional points on body meridian lines.

METHOD: A body surface is specified by a set of defining sections normal to the X axis. Points on defining sections are given in polar coordinate form (ρ , θ) or in rectangular coordinates (y , z). The number of points must be the same for all sections (except for zero-area sections). For convenience, several options are available for specifying section points (see Input Data Format, 3.3, card 6D).

Three-dimensional points on the i^{th} body meridian line are formed by selecting the i^{th} point at each defining section. Additional points are interpolated (if requested) so that straight-line connections between adjacent points will represent a smooth curve as closely as specified.

USAGE: DIMENSION DAT(2), B(1), AXIS(2), TITLE(12), NU(3)
LOGICAL LGDEF(3, 6)

CALL BODY1 (DAT, LI, LO, B, LSTA, NSTA, LBPL,
MBPL, NBPL, LTHETS, AXIS, TITLE,
LGDEF, NU)

Input: DAT = Date (alphameric).
LI = Input tape number.
LO = Output tape number.
B = Buffer for variable-length arrays.
NU = Error indicator array: NU(1) is not used, on input. NU(2) is an output tape number on which to write a message if an error is detected; no message is written if $\text{NU}(2) \leq 0$. NU(3) is an error message limiter; if an error is detected, $\text{NU}(3) = (\text{NU}(3) - 1)$. Then if $\text{NU}(3) > 0$ and $\text{NU}(2) > 0$, an error message is written.

Output: B = Buffer for variable-length arrays.
LSTA = The set of body-defining stations (x-values) starts in B(LSTA).

NSTA = Number of body-defining stations.
LBPL = The body meridian line array, with header, starts in B(LBPL). See Appendix D for the array format.
MBPL = Number of meridian lines.
NBPL = Number of cells in meridian-line array.
LTHETS = The standard set of θ values (in degrees) corresponding to meridian lines, starts in B(LTHETS).
AXIS = y and z coordinates of the body main axis.
TITLE = Body title (alphanumeric).
LGDEF = LGDEF(1, 3) is set to .TRUE., LGDEF(2, 3) is set to .TRUE. if the body meridian lines are successfully computed.
NU = Error-indicator array. NU(1) is zero if no errors were detected. NU(3) may have been changed if an error was found (see INPUT, above).

**SUBPROGRAMS
CALLED:**

RICHNA
 BODY1M
 BODY1R
 MERR
 IDLETE
 IRLEAS
 IRSERV
 IPACK

} (See Appendix A)

ERROR RETURNS: Function MERR is used to write an error message "ERROR i, CODE j IN SUBROUTINE BODY1 DURING GEOMETRIC DEFINITION" if an error is detected.

<u>i</u>	<u>j</u>	<u>Explanation</u>
1	0	The number of defining sections (BNS, card 4D) or the number of meridian lines (BTHETA) is less than 2 or greater than 150.

<u>i</u>	<u>i</u>	<u>Explanation (cont)</u>
2	0	BNS * BTHETA is so large that the storage required for the meridian-line points (even with no enriching) is greater than the storage available in array B.
3	1	The code for the type of body section (SCODE, card 6D) is less than 0 or greater than 6.
3	2	SCODE = 3 (elliptical section), but a semi-axis is zero.
4	k	Meridian lines have been formed, but error k was detected in subroutine RICHNA.
5	0	Machine or program error of undetermined origin.

RESTRICTIONS:

The storage buffer, B, for variable-length arrays must have been initialized by subroutine INIBFR (Appendix A) or its equivalent.

STORAGE:

$$568_{10} = 1070_8$$

SUBJECT: FORTRAN IV Subroutine BODY1M

PURPOSE: To write body meridian line points on an output tape.

METHOD: This is primarily an output routine for BODY1. The meridian lines are given in a single array with the format described in Appendix D. The polar coordinates of each point are computed in a plane normal to the x axis with polar origin at the body axis. Points that lie in a body defining section (within 0.0001) are identified by an asterisk.

USAGE: DIMENSION B(1), AXIS(2), TITLE(12), DAYT(2), STA(1)
CALL BODY1M (B, NB, AXIS, TITLE, DAYT, LO, STA)

Input: B = Array of meridian lines, with header.
NB = Number of meridian lines.
AXIS = y, z coordinates of main body axis.
TITLE = Title (alphameric).
DAYT = Date (alphameric).
LO = Output tape number.
STA = Array of defining stations X-values).

Output: Printout on tape LO.

SUBPROGRAMS CALLED: ATN1
SQRT (Built-in function)
TRAV

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $373_{10} = 565_8$

SUBJECT: FORTRAN IV Subroutine BODY1R

PURPOSE: To read and write data that specify body defining sections, and form three-dimensional points on body meridian lines.

METHOD: The number of body-defining sections, number of meridian lines, the Y and Z coordinates of the body axis, and a standard set of angles are given. Each section lies in a station plane (normal to the X axis). A meridian line of three-dimensional points on the body surface is formed by selecting corresponding points from each station. Let
 NPT = number of meridian lines = number of two-dimensional points per section = number of angles in the standard set.
 Subroutine BODY1R is called for each section to read data cards and compute NPT three-dimensional points on the body surface. These points are then stored in meridian-line order. Results for each section are written on an output tape.

USAGE: **DIMENSION** BAXIS(2), TITLE(12), DAT(2), THETS(NPT), THETA(NPT), RHO(NPT), PT(3, NPT), BPL(3, NSTA, NPT), STA(NSTA)

CALL BODY1R (LI, LO, NPT, NSTA, BAXIS, TITLE, DAT, THETS, THETA, RHO, PT, BPL, STA, NU)

Input: LI = Input tape number.
 LO = Output tape number.
 NPT = Number of meridian lines.
 NSTA = Number of defining sections (stations).
 BAXIS = Y, Z coordinates of main body axis.
 TITLE = Title (alphameric).
 DAT = Date (alphameric).
 THETS = Array of standard angles, in degrees.

Scratch: THETA }
 RHO } = Storage for θ , ρ , and point coordinates (used at each section).
 PT }

Output: BPL = Points on meridian lines.
 STA = Array of defining stations (X coordinates).

NU = Error indicator, which is zero for success.

SUBPROGRAM

CALLED: BODY1S

ERROR RETURNS: If NU \neq 0, see BODY1S.

RESTRICTIONS: Tape LI must be properly positioned and contain NSTA sets of data for BODY1S.

STORAGE: $368_{10} = 560_8$

SUBJECT: FORTRAN IV Subroutine BODY1S

PURPOSE: To read body-defining section data cards and compute points on the body section.

METHOD: Data cards are described in section 3.3. The code for section type is checked for validity; then the indicated operation is carried out.

USAGE: **DIMENSION** BAXIS(2), THETS(NPT), SECAX(2),
 THETA(NPT), RHO(NPT), PT(3, NPT)

CALL BODY1S (LI, BAXIS, NPT, THETS, SECAX, SCODE,
 THETA, RHO, PT, NU)

Input: LI = Input tape number.

BAXIS = Y, Z coordinates of the main body axis.

NPT = Number of points in section.

THETS = Array of angles, in degrees, which are used for SCODE = 1, 2, and 3.

PT = See OUTPUT, below; used as input only if SCODE = 0.

Output: SECAX = Y, Z coordinates of the section origin (ρ , θ origin).

SCODE = Code for type of section (read from card).

0. This section is identical to the previous section, except for X-coordinates. Store the station value (read from card) as the X-coordinate for each point in PT.
1. Read NPT values of ρ from cards. Use with the THETS array to compute Y, Z coordinates of points on the section.
2. Circular section. Use the radius (read from card) as ρ , and THETS to compute section points.
3. Section is a rectangular ellipse. Use the semi-axes (read from card) to construct ellipse. Find

ρ 's corresponding to THETS.
Construct points on section.

4. Circular section, but read NPT values of θ from cards instead of using THETS.
5. Read NPT values of ρ from cards, then read NPT values of θ from cards.
6. The y, z coordinates of the section points are given. Find corresponding ρ , θ coordinates; but if any ρ is zero, use corresponding θ from THETS.

THETA = Array of θ values (in degrees) corresponding to each section point (same as THETS for SCORE = 1, 2, 3).

RHO = Array of ρ values.

PT = Array of points (x, y, z coordinates) in section.

NU = Error indicator, which is zero for success.

SUBPROGRAMS
CALLED:

ATN1
UVECN
ELLIPR
SIN (Built-in function)
TRAV
COS (Built-in function)

ERROR RETURNS: NU = 1 if SCORE < 0 or SCORE > 6.
NU = 2 if SCORE = 3 and a semi-axis is zero.

RESTRICTIONS: Input tape LI is assumed to be correctly positioned and to contain valid data. Angles are measured from the vertical, and it is assumed that $0 \leq \theta \leq 180$. The ρ - θ origin is at SECAX.

STORAGE: $439_{10} = 667_8$

SUBJECT: FORTRAN IV Subroutine BSCALE

PURPOSE: To scale body meridian lines so that each line extends from $x = 0$ to $x = x_E$, where x_E is given. The y and z coordinates are unchanged.

METHOD: The x-coordinates of the points on each meridian line are scaled as follows:

$$x' = (x - x_1) x_E / (x_L - x_1)$$

where $x_1 = x$ of first point, $x_L = x$ of last point.

USAGE: DIMENSION B(1)

CALL BSCALE (B, NB, XEND, NU)

Input: B = Meridian line array (see subroutine TFLAT1).

NB = Number of meridian lines.

XEND = x_E .

Output: B = Scaled meridian line array.

NU = Error indicator. NU = 0 if success.
NU = k if $x_L - x_1 = 0$ for the kth meridian line.

SUBPROGRAM

CALLED: None

ERROR RETURNS See Output

RESTRICTIONS: None

STORAGE: $125_{10} = 175_8$

SUBJECT: FORTRAN IV Subroutine BTHICK

PURPOSE: To compute thickness slopes at body panel control points from a given body radii distribution.

METHOD: The radii distribution is specified by a table of r (radius) vs. x (body source control station). This table is used to obtain a second table of Δr vs. x :

$$\Delta r_i = \frac{r_{i+1} - r_i}{x_{i+1} - x_i}$$

from which α_T (thickness slope) at x_c (body panel control point) are calculated by interpolation:

$$\alpha_{T_j} = \Delta r_{i-1} + \left(\frac{x_c - x_{i-1}}{x_i - x_{i-1}} \right) \cdot (\Delta r_i - \Delta r_{i-1})$$

USAGE: CALL BTHICK (NBODYS, NBODY, NROWB, XB, R, XC, ALPHA, THETA)

DIMENSION XB(55), R(55), XC(100), ALPHA (55), THETA(55)

Input: NBODYS = Number of body source control stations.

NBODY = Number of body panels.

NROWB = Number of rows of body panels.

XB = Array of x-coordinates of body source control stations.

R = Array of radii at the body source control stations.

XC = Array of x-coordinates of body panel control points.

ALPHA = Dummy array.

Output: THETA = Array of thickness slopes at the body panel control points.

SUBPROGRAMS CALLED:

None

ERROR RETURNS: None

RESTRICTIONS:

NBODYS ≤ 55

NBODY ≤ 100

STORAGE:

$180_{10} = 264_8$

SUBJECT:

FORTRAN IV Subroutine CAMBER

PURPOSE:

To compute the wing surface shape, given the wing surface slopes.

METHOD:

The wing surface shape is computed column-by-column from the inboard column of wing panels to the outboard column. For a given column of wing panels, the surface shape is obtained panel-by-panel from the wing leading edge to the trailing edge. If i specifies panel row and j the column, then the surface shape is calculated:

$$s_{i,j} = \left\{ \sum_{k=1}^j \alpha_{w_{i,k}} \cdot c_{i,k} \right\} / C_i$$

where

 $s_{i,j}$ = panel surface shape. $\alpha_{w_{i,j}}$ = panel surface slope. $c_{i,j}$ = panel chord length. C_i = panel column chord length.**USAGE:**

CALL CAMBER (NCOLW, NROWW, CHORD, ALPHAW, CSHAPE, CHORDL)

DIMENSION: CHORD(110), ALPHAW(110), CSHAPE(110), CHORDL(110)

Input: NCOLW = Number of columns of wing panels.

NROWW = Number of rows of wing panels.

CHORD = Array of wing panel chord lengths.

ALPHAW = Array of wing surface slopes.

CHORDL = Dummy array.

Output: CSHAPE = Array of wing surface shapes.

SUBPROGRAMS**CALLED:**

None

ERROR RETURNS:

None

RESTRICTIONS: $(\text{NCOLW} \cdot \text{NROWW}) \leq 110$

STORAGE: $139_{10} = 213_8$

SUBJECT: FORTRAN IV Subroutine CAMBW

PURPOSE: To compute the velocity components normal to the x-axis on the wing panels, given the matrix of the aerodynamic influence coefficients and the pressure difference across the panels.

METHOD: The velocity components are given by

$$n_{w_i} = \sum_{i=1}^{NW} \sum_{j=1}^{NW} A_{WW_{ij}} \cdot p_{w_j}$$

where A_{WW} is the matrix of aerodynamic influence coefficients (influence on the wing, due to the wing) and p_w is the pressure difference across each wing panel.

USAGE: CALL CAMBW (NW, NT, A, CL, ALPHAW)

DIMENSION A(NW), CL(NW), ALPHAW(NW)

Input: NW = Number of wing panels.

NT = Logical tape number on which A_{WW} is stored.

A = Dummy array used by the subroutine.

CL = Array of pressure differences.

Output: ALPHAW = Array of velocity components.

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $90_{10} = 132_8$

SUBJECT:

FORTRAN IV Subroutine CAMBWB

PURPOSE:

In the presence of a body, to compute the velocity components on the wing, normal to the x-axis.

METHOD:

The velocity component on the wing panel i is given by

$$n_{w_i} = \sum_{j=1}^{NW} A_{R_{ij}} \cdot p_{w_j} + \sum_{j=1}^{NB} D_{ij} \cdot n_{B_j}$$

where

A_R = The matrix of the reduced aerodynamic influence coefficients,

p_w = The pressure difference across wing panels,

D = The matrix formed by the product.

$$A_{WB} \cdot A_{BB}^{-1}$$

where A_{WB} = A partition of the aerodynamic influence coefficients matrix resulting from the influence of the body on the wing.

A_{BB} = The partition resulting from the influence of the body on the body.

n_B = The velocity component on the body normal to the x-axis.

USAGE:

DIMENSION A(NW), CLW(NW), ALPHAB(NB), ALPHAW(NW)
CALL CAMBWB (NB, NW, NTAPEX, NTAPEY, A, CLW, ALPHAB, ALPHAW)

Input: NB = Number of body panels.
 NW = Number of wing panels.
 NTAPEX = Logical tape number on which A_R is stored.
 NTAPEY = Logical tape number on which D is stored.
 A = Dummy array used by the subroutine.
 CLW = Array of the pressure differences across wing panels.
 ALPHAB = Array of velocity components on the body, normal to the x-axis.

Output: ALPHAW = Array of velocity components on the wing, normal to the x-axis.

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $144_{10} = 220_8$

SUBJECT: FORTRAN IV Subroutine CEGAR

PURPOSE: To find the area and the centroid (center of gravity) of a polygon.

METHOD: Given n points $(x_i, y_i; i = 1, \dots, n)$ that are the vertices of a polygon, the area of the polygon is given by the magnitude of A , where

$$A = 1/2 \sum_{i=1}^n (y_{i+1} + y_i) (x_{i+1} - x_i)$$

where x_{n+1}, y_{n+1} are set equal to x_1, y_1 by the subroutine to ensure that the polygon is closed. If any two or more of the points (x_i, y_i) coincide, no difficulty will result in the calculation of the centroid, and the area as long as the resulting polygon is a simple closed curve.

The coordinates of the centroid are given by,

$$\bar{x} = \sum_{i=1}^n (x_{i+1}^2 + x_i^2 + x_{i+1} x_i) (y_{i+1} - y_i) / (-6A), \text{ and}$$

$$\bar{y} = \sum_{i=1}^n (y_{i+1}^2 + y_i^2 + y_{i+1} y_i) (x_{i+1} - x_i) / (6A)$$

USAGE: DIMENSION P(2, n+1), CG(2)
 CALL CEGAR (N, P, A, CG)

Input: N = the number of points, n.
 P = the array of points (x_i, y_i) that are the vertices of the polygon.

Output: A = the magnitude of the area of the polygon.
 CG = the centroid of the area, (\bar{x}, \bar{y}) .

RESTRICTIONS: The polygon must be a simple closed curve, (i.e., the polygonal arc cannot cross itself).

ERROR RETURNS: If the area of the polygon is zero, then the subroutine sets the coordinates of the centroid equal to zero.

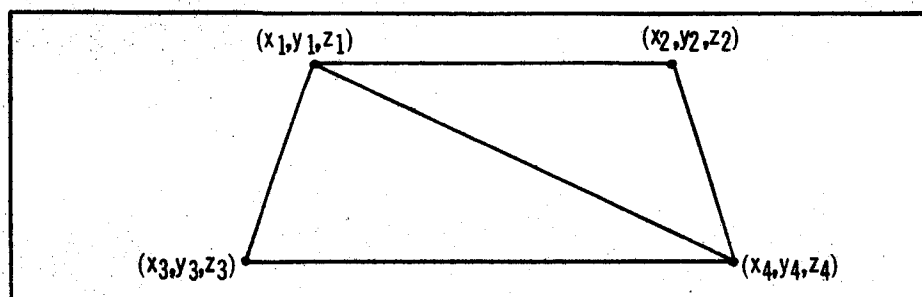
Because, in the calculation of \bar{x} and \bar{y} , A is used as a divisor, considerable error could result in the values obtained for \bar{x} and \bar{y} when A is close to zero. Overflow could also occur for small values of A .

STORAGE: $229_{10} = 345_8$

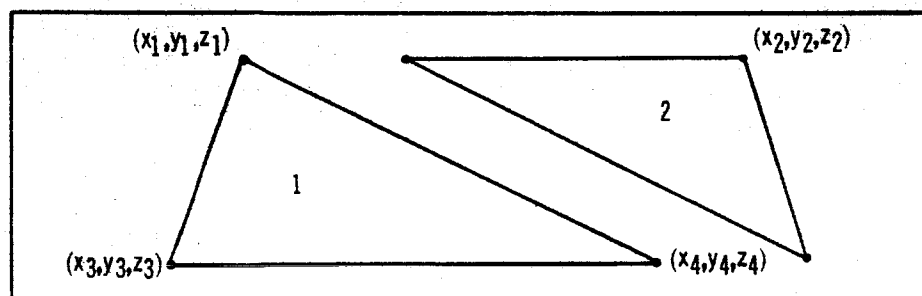
SUBJECT: FORTRAN IV Subroutine CENTRD

PURPOSE: To calculate coordinates of a panel centroid.

METHOD: Centroid coordinates of a panel are calculated by dividing panel into two subpanels, locating a centroid on each subpanel, and averaging coordinates of the two centroids with appropriate weighting factor. For example, a given quadrilateral panel:



is subdivided into two subpanels, thus:



and a centroid is calculated for each subpanel using standard formulae. For subpanel 1 of the above example,

$$\bar{x}_1 = x_1 + \frac{2}{3} \left(x_3 + \frac{1}{2} (x_4 - x_3) - x_1 \right)$$

$$\bar{y}_1 = y_1 + \frac{2}{3} \left(y_3 + \frac{1}{2} (y_4 - y_3) - y_1 \right)$$

$$\bar{z}_1 = z_1 + \frac{2}{3} \left(z_3 + \frac{1}{2} (z_4 - z_3) - z_1 \right)$$

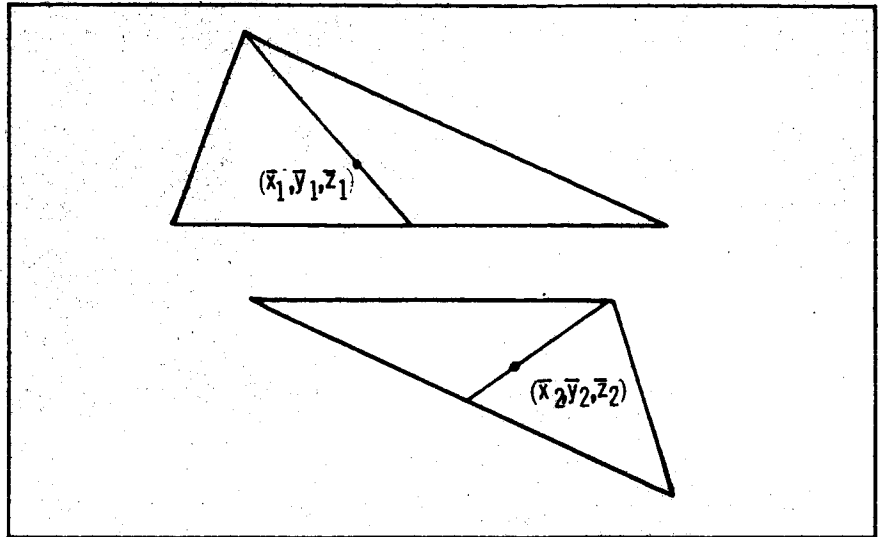
Similarly for subpanel 2,

$$\bar{x}_2 = x_2 + \frac{2}{3} \left(x_1 + \frac{1}{2} (x_4 - x_1) - x_2 \right)$$

$$\bar{y}_2 = y_2 + \frac{2}{3} \left(y_1 + \frac{1}{2} (y_4 - y_1) - y_2 \right)$$

$$\bar{z}_2 = z_2 + \frac{2}{3} \left(z_1 + \frac{1}{2} (z_4 - z_1) - z_2 \right)$$

This is shown in the following sketch,



A weighting factor is used to average coordinates of centroids of the two subpanels and derive coordinates of panel centroid. The weighting factor is merely the ratio of the area of sub-panel 1 to the panel area (see subroutine AREAP). That is,

$$\bar{x} = \bar{x}_2 + R(\bar{x}_1 - \bar{x}_2)$$

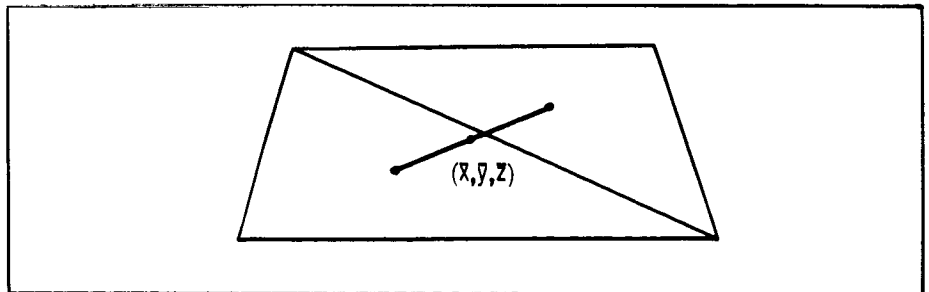
$$\bar{y} = \bar{y}_2 + R(\bar{y}_1 - \bar{y}_2)$$

$$\bar{z} = \bar{z}_2 + R(\bar{z}_1 - \bar{z}_2)$$

and,

$$R = \frac{S_1}{S}$$

This is shown below,



USAGE:

DIMENSION X(16, 16), Y(16, 16), Z(16, 16), R(15, 15),
XC(15, 15), YC(15, 15), ZC(15, 15)

$\left. \begin{matrix} X \\ Y \\ Z \end{matrix} \right\} = \text{x, y, and z-coordinates of panel corner points.}$

R = Ratio of subpanel area to panel area.

$\left. \begin{matrix} XC \\ YC \\ ZC \end{matrix} \right\} = \text{x-, y-, and z-coordinates of panel centroid.}$

CALL CENTRD (X, Y, Z, R, XC, YC, ZC, NC, NR)

Input: $\left. \begin{matrix} X \\ Y \\ Z \\ R \end{matrix} \right\} \text{ (see above)}$

NC = Number of panel columns.

NR = Number of panel rows.

Output: $\left. \begin{matrix} XC \\ YC \\ ZC \end{matrix} \right\} \text{ (see above)}$

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

STORAGE: $298_{10} = 452_8$

SUBJECT: FORTRAN IV Subroutine CHECK

PURPOSE: To check if a sequence $\{x_i\}$ of numbers is monotonic increasing (or decreasing).

METHOD: The given sequence $\{x_i\}$ can be one of four types:

- 1) Monotonic increasing; i.e., $x_i \leq x_{i+1}$
- 2) Strictly monotonic increasing; i.e., $x_i < x_{i+1}$
- 3) Monotonic decreasing; i.e., $x_i \geq x_{i+1}$
- 4) Strictly monotonic decreasing; i.e., $x_i > x_{i+1}$

The program calling sequence includes a code that indicates which type the sequence should be. The program consists of a "do-loop" involving an "if" statement that checks the sequence accordingly.

USAGE: CALL CHECK (X, N, K, L, N6)

Input: X = Sequence to be checked.

N = Number of elements in sequence $\{x_i\}$.

K = Code indicating sequence type that $\{x_i\}$ should be. If $K = 1$, $\{x_i\}$ should be monotonic increasing sequence. If $K = 2$, $\{x_i\}$ should be strictly monotonic increasing sequence. If $K = -1$, $\{x_i\}$ should be monotonic decreasing sequence. If $K = -2$, $\{x_i\}$ should be strictly monotonic decreasing sequence.

N6 = Output tape unit.

Output: L = Error code. If $L = 0$, $\{x_i\}$ successfully checked. If $L = 1$, error occurred.

SUBPROGRAM CALLED: None

ERROR RETURNS: See above

RESTRICTIONS: The sequence $\{x_i\}$ must be a sequence of floating point numbers.

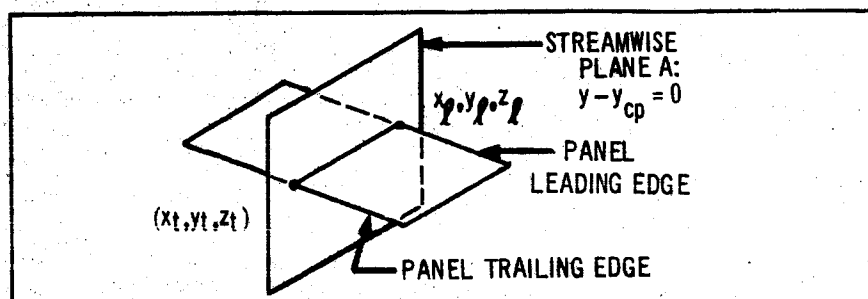
STORAGE: $237_{10} = 355_8$

SUBJECT: FORTRAN IV Subroutine CHORDW

PURPOSE: To calculate the length of a streamwise chord through the wing panel control point.

METHOD: The program calculates the length of the streamwise chord by use of a basic distance formula.

The chord is located by construction of a streamwise plane (A) normal to the plane of the panel and passing through the panel control point. This is shown in the following sketch:



The line of intersection of this plane and the original panel is the desired chord, and the chord length is calculated,

$$L = x_t - x_l$$

USAGE: COMMON (See subroutine OPCAMI for unlabeled COMMON description)

COMMON /COM1/ (See subroutine PANEL)

Input: NPER1
NPLN1

COMMON /COM2/ (See subroutine WING)

Input: XCOR
YCOR
ZCOR
YCON

Output: CHORD

CALL CHORDW

SUBPROGRAM
CALLED:

POLXN

ERROR RETURNS: Error messages indicate if error occurred in use of sub-routine POLXN to calculate chord intercepts.

STORAGE: $418_{10} = 642_8$

SUBJECT: **FORTRAN IV Subroutine CLOK**

PURPOSE: **To find the time of day.**

METHOD: **This is a dummy subroutine which returns blanks. An appropriate change may be made at the user's installation to return the true time and date.**

USAGE: **CALL CLOK (TIME, DATE)**

Output: TIME = Time of day (alphameric).

DATE = Date (alphameric).

SUBPROGRAM

CALLED: **None**

ERROR RETURNS: **None**

RESTRICTIONS: **None**

STORAGE: **23₁₀ = 27₈**

SUBJECT:

FORTRAN IV Subroutine CNTRLB

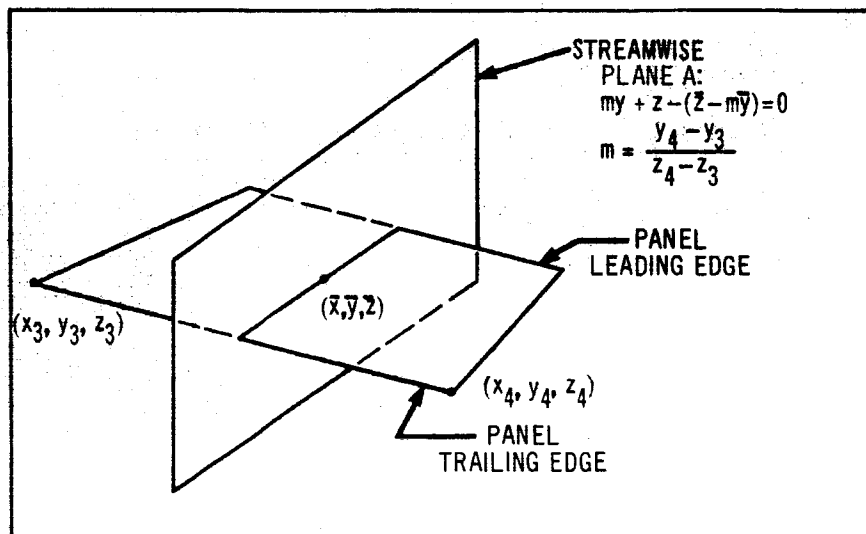
PURPOSE:

To calculate the coordinates of a body panel control point and the length of a streamwise chord through the control point.

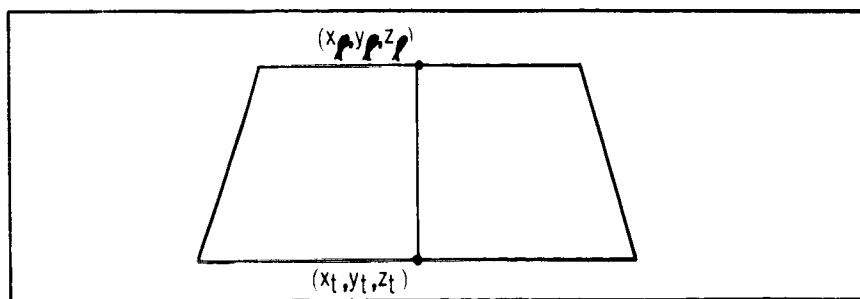
METHOD:

The coordinates of a body panel control point are calculated by locating a streamwise chord through the panel centroid, determining the intercepts of this chord with the panel leading and trailing edges, and using a specified input constant to average these coordinates and locate the control point along the chord.

To find the chord that is required, the program constructs a streamwise plane (A) normal to the plane of the panel and through the panel centroid. For example,



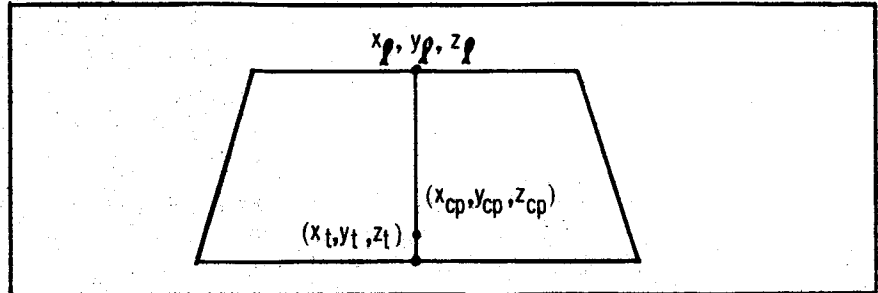
The intersection of this plane with the given panel defines the chord that is needed, and the chord length is calculated using a standard distance formula. For the above example,



and,

$$L = \left[(x_t - x_l)^2 + (y_t - y_l)^2 + (z_t - z_l)^2 \right]^{1/2}$$

The control point coordinates are then calculated by using an input constant, c , and averaging the chord intercepts.

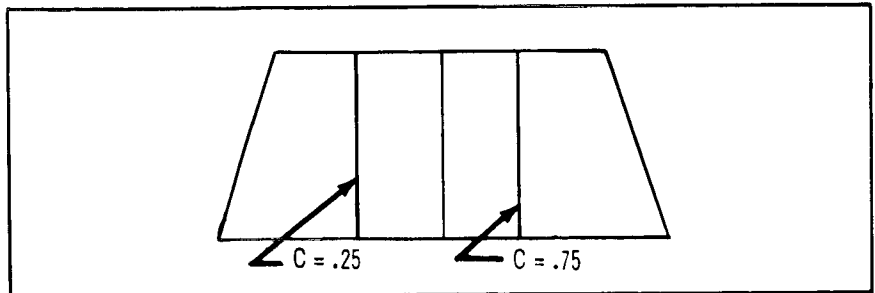


$$x_{cp} = x_l + c \cdot (x_t - x_l)$$

$$y_{cp} = y_l + c \cdot (y_t - y_l)$$

$$z_{cp} = z_l + c \cdot (z_t - z_l)$$

As noted above, the location of the panel control point along the streamwise chord is controlled by an input constant, c , (fraction). In addition and as an option, a second constant can be employed as input to change the spanwise location of the chord on which the control point is calculated. For a case in which the option is not used, the streamwise chord is constructed through the panel centroid; thus is located at approximately 50 percent in the spanwise direction. But for a case in which this option is used, this spanwise percent value can be changed to an arbitrary one, say 25 or 75 percent.



USAGE: **COMMON** (See subroutine OPCAMI for unlabeled **COMMON** description).

CONTROL /COM1/ (See subroutine **PANEL**)

Input: **KODEC**
 XPER
 YPER
 NPER1
 NPLN1

Output: **KODEB**

COMMON /COM2/ (See subroutine **BODY**)

Input: **XCOR**
 YCOR
 ZCOR
 YCEN
 ZCEN

Output: **XCON**
 YCON
 ZCON
 CHORD

CALL CNTRLB

SUBPROGRAMS **POLXN**
CALLED: **SQRT** (Built-in function)

ERROR RETURNS: Error message indicates if error has been encountered in use of subroutine **POLXN** to calculate chord intercepts.

STORAGE: $484_{10}^{>} = 744_8$

SUBJECT:

FORTRAN IV Subroutine CNTRLW

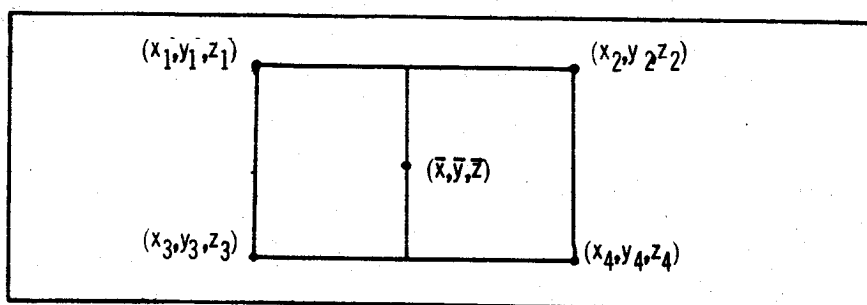
PURPOSE:

To calculate the coordinates of a wing panel control point.

METHOD:

The coordinates of a wing panel control point are calculated by defining a constant, c_1 , that locates the control point in the spanwise direction, and a second constant, c_2 , that locates it in the streamwise direction. The latter constant, c_2 , is always given as input data, though the former constant, c_1 , can be given as input or calculated by the program as a function of the centroid location.

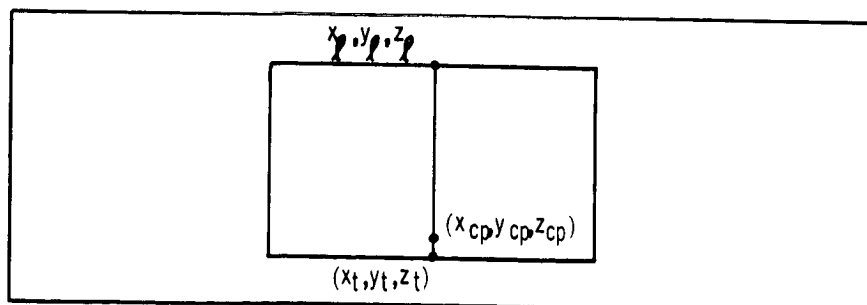
The two constants are used to average the panel corner point coordinates and derive the control point coordinates. As an example, a wing panel is defined,



The constant, c_2 , is given as input and the constant, c_1 , is either given as input or calculated by the program. For the latter case,

$$c_1 = \frac{\bar{y} - y_1}{y_2 - y_1}$$

These constants are then used to average the four corner point coordinates and obtain the control point coordinates,



$$\begin{aligned}
x_{cp} &= x_l + c_2 \cdot (x_t - x_l) \\
x_l &= x_1 + c_1 \cdot (x_2 - x_1) \\
x_t &= x_3 + c_1 \cdot (x_4 - x_3) \\
y_{cp} &= y_l + c_2 \cdot (y_t - y_l) \\
y_l &= y_1 + c_1 \cdot (y_2 - y_1) \\
y_t &= y_3 + c_1 \cdot (y_4 - y_3) \\
z_{cp} &= z_l + c_2 \cdot (z_t - z_l) \\
z_l &= z_1 + c_1 \cdot (z_2 - z_1) \\
z_t &= z_3 + c_1 \cdot (z_4 - z_3)
\end{aligned}$$

USAGE: COMMON (See subroutine OPCAMI for unlabeled COMMON description)

COMMON /COM1/ (See subroutine PANEL)

Input: KODEC
 XPER
 YPER
 KSTART
 KEND
 NPER1
 NPLN1

COMMON /COM2/ (See subroutine WING)

Input: XCOR
 YCOR
 ZCOR
 YCEN

Output: XCON
 YCON
 ZCON

CALL CNTRLW

**SUBPROGRAM
 CALLED:**

AMAX (Built-in function)

ERROR RETURNS: Error message indicates if error occurred in calculation of panel control point.

STORAGE: 735₁₀ = 1337₈

SUBJECT:

FORTRAN IV Subroutine COEFS

PURPOSE:

To compute the axial force coefficient, normal force coefficient and pitching moment coefficient on a body.

METHOD:

For the axial force coefficient,

$$C_A = \frac{1}{S} \int_0^l r \cdot \frac{dr}{dx} \left[\int_0^{2\pi} C_p d\theta \right] dx;$$

for the normal force coefficient,

$$C_N = \frac{1}{S} \int_0^l r \left[\int_0^{2\pi} C_p \cos \theta d\theta \right] dx$$

and for the pitching moment coefficient,

$$C_M = \frac{1}{S\bar{c}} \int_0^l x \cdot r \left[\int_0^{2\pi} C_p \cos \theta d\theta \right] dx$$

where x = x-coordinate of body station. r = Body radius at body station. $\frac{dr}{dx}$ = Body surface first derivative at body station. C_p = Pressure coefficient at a body station and on a body meridian line. θ = Angle of body meridian line. l = Body length. S = Reference area. \bar{c} = Reference chord length.

For each coefficient, subroutine SIMUN3 is first used to obtain a value for the integral around the body (with respect to θ) at each body station and then for the integral along the body axis (with respect to x). This result is multiplied by the appropriate constant to obtain the final value.

USAGE:

For the axial force coefficient:

**CALL SCX (XB, R, FD, THETAB, CPBB, NFT, NLT,
NTHETA, XP, ZP, C, IRROR)**

For the normal force coefficient:

**CALL SCN (XB, R, FD, THETAB, CPBB, NFT, NLT,
NTHETA, XP, ZP, C, IRROR)**

For the pitching moment coefficient:

**CALL SCM (XB, R, FD, THETAB, CPBB, NFT, NLT,
NTHETA, XP, ZP, C, IRROR)**

**DIMENSION XB(55), R(55), FD(55), THETAB(10),
CPBB(10,55)**

Input: **XB** = Array of x-coordinates of body
 stations.

R = Array of body radii at body stations.

FD = Array of body surface first
 derivatives at body stations.

THETAB = Array of θ -angles of body meridian
 lines.

CPBB = Array of pressure coefficients.

NFT } = Index codes.
 NLT }

NTHETA = Number of body meridian lines.

XP } = x and y coordinates of point about
 ZP } which pitching moment coefficient
 is to be computed.

C = Coefficient (axial force, normal
 force or pitching moment).

IRROR = Error return

 = 0 — success

 = 0 — error occurred in numerical
 integration of subroutine
 SIMUN3

SUBPROGRAMS**CALLED:****SIMUN3****COS (Built-in-function)****ERROR RETURNS:**

Three types of errors are indicated. If fewer than three points are input to subroutine SIMUN3, ERROR = 1. If subroutine SCAMP4, which is called by subroutine SIMUN3, detects an error, ERROR = 2. If subroutine SIMUN3 detects an error in calculating the integral of the function defined by the input points, ERROR = 3. Otherwise, if the call is successful, ERROR = 0.

RESTRICTIONS: $3 \leq (\text{NLT-NFT} + 1) \leq 55$ **STORAGE:** $491_{10} = 753_8$

SUBJECT: FORTRAN IV Subroutine COMCU

PURPOSE: To fit a composite cubic through n points (x_i, y_i) i.e., a separate cubic between each pair of adjacent points, such that the $n - 1$ cubics are so determined that each matches its neighbors in function value and in the first two derivatives.

METHOD: Rather than solve simultaneously for the $4(n - 1)$ cubic coefficients, the approach here is to solve simultaneously for the slopes of the composite cubic at the given n points. Thus a linear system of order n , rather than $4n - 4$, is involved. It can be shown that a necessary and sufficient condition for continuity of the second derivative is that:

$$(x_{i+1} - x_i)y'_{i-1} + 2(x_{i+1} - x_{i-1})y'_i + (x_i - x_{i-1})y'_{i+1} = \frac{3}{(x_i - x_{i-1})(x_{i+1} - x_i)} \left[(x_i - x_{i-1})^2 (y_{i+1} - y_i) + (x_{i+1} - x_i)^2 (y_i - y_{i-1}) \right]$$

for $i = 2, 3, \dots, n - 1$.

This yields $n - 2$ equations in the n unknowns, y'_i , $i = 1, 2, \dots, n$. For the 1st and n th equations of the linear system, the boundary conditions on y'_1 and y'_n are used. This has been generalized to permit any combination of a given y' or y'' at the end points, e.g., y'_1 and y''_n can be given as the boundary conditions. The second derivative of a cubic through two points can be expressed as a function of the first derivatives and of the given point coordinates as follows:

$$\frac{x_2 - x_1}{2} y''_1 = 3 \frac{y_2 - y_1}{x_2 - x_1} - 2y'_1 - y'_2$$

and

$$\frac{x_n - x_{n-1}}{2} y''_n = -3 \frac{y_n - y_{n-1}}{x_n - x_{n-1}} + y'_{n-1} + 2y'_n$$

Whether the boundary conditions involve first or second derivatives (or both), and no matter what the spacing of the x_i (so long as the x_i form a strictly monotone sequence), the coefficient matrix of the linear system is

tridiagonal (all elements are zero except on the principal diagonal, the first subdiagonal, and the first superdiagonal). When n is large, a considerable time saving and an enormous storage saving can result if the special structure of this matrix is taken advantage of. Hence this subroutine stores the matrix elements in $4n$ locations (as opposed to n^2) and then solves the system.

The actual coefficients of the $n - 1$ cubics of the composite cubic are not found by COMCU. Since on any subinterval $x_1, x_1 + 1$ a cubic is uniquely determined by the known two points and two slopes, the calling program can find the four coefficients of each cubic independently and may often need to do so for only one of the $n - 1$ cubics. In any case, the subroutine CUBIC2 specifically finds a cubic, given two points and the slope at each point.

USAGE:

CALL COMCU (DA, DB, S, X, Y, L, M, N, NDA, NDB)

DIMENSION S(400), X(400), Y(400)

Input: X = Array of x-ordinates of input points.

Y = Array of y-ordinates of input points.

N = Number of input points.

NDA = Order (1 or 2) of derivative at X(1).

NDB = Order (1 or 2) of derivative at X(N).

DA = Value of derivative at X(1).

DB = Value of derivative at X(N).

L = Code.

= 1, if single precision is to be used.

= 2, if double precision is to be used.

Output: S = Array of first derivatives.

M = Error return

= 0 — success

≠ 0 — error detected

SUBPROGRAMS**CALLED:** None**ERROR RETURNS:** If overflow occurred, $M = 1$. Otherwise, $M = 0$.**RESTRICTIONS:** The x-abcissae must form a strictly monotone sequence. $N \leq 400$ **STORAGE:** $1496_{10} = 2730_8$

SUBJECT: FORTRAN IV Subroutine COMP

PURPOSE: To compute the velocity components at an array of points.

METHOD: An array of points is input, and calls to velocity computation routine are made.

USAGE: DIMENSION GP(3, IC), VLS (4, IC)
CALL COMP (GP, VLS, IC)

Input: IC = Number of points in the GP array.
GP(1, I) = x-coordinate of Ith point.
GP(2, I) = y-coordinate of Ith point.
GP(3, I) = z-coordinate of Ith point.

Output: VLS(1, I) = u-velocity component at Ith point.
VLS(2, I) = v-velocity component at Ith point.
VLS(3, I) = w-velocity component at Ith point.
VLS(4, I) = c_p-velocity component at Ith point.

SUBROUTINE CALLED: LACKEY

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $89_{10} = 131_8$

SUBJECT:

FORTRAN IV Subroutine CP

PURPOSE:

To compute the pressures coefficients by either the linear or nonlinear equation, given the velocity components in the x , y , and z directions at each of the panels.

METHOD:

For the linear pressure coefficient,

$$C_p = -2u$$

and for the nonlinear pressure coefficient,

$$C_p = -2u + \beta^2 u^2 - v^2 - w^2$$

where

u = velocity component in the x-direction.

v = velocity component in the y-direction.

w = velocity component in the z-direction.

$$\beta = M^2 - 1$$

USAGE:

CALL CP (K, NP, XMACH, CPCALC, U, V, W, CPP)

DIMENSION U(NP), V(NP), W(NP), CPP(NP)

Input: K = Code

= 0, for wing panels.

= 1, for body panels.

NP = Number of panels.

XMACH = Mach number.

CPCALC = Calculation option.

= 0., calculation of pressure coefficients to use linear equation.

= 1., calculation of pressure coefficients to use nonlinear equation.

U = Array of velocity components in
x-direction.

V = Array of velocity components in
y-direction.

W = Array of velocity components in
z-direction.

Output: CPP = Array of pressure coefficients,

SUBPROGRAMS

CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $156_{10} = 234_8$

SUBJECT:

FORTRAN IV Subroutine CRNRB

PURPOSE:

To calculate body panel (and secondary panel) corner point coordinates.

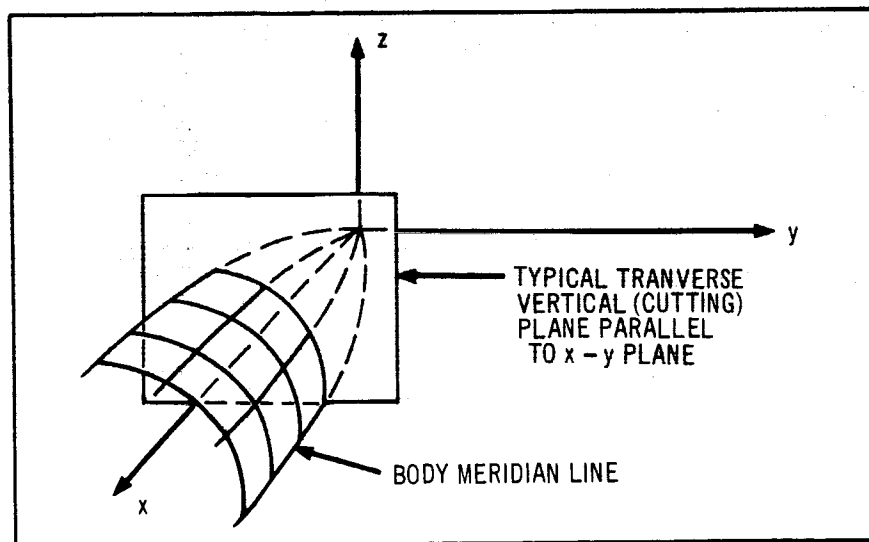
METHOD:

In general, a body panel is defined by four corner points. A program restriction requires either that the panel have streamwise inboard and outboard edges, or that it be subdivided so that its secondary panels have streamwise edges. To satisfy this condition, additional points are located on the panel leading and/or trailing edge.

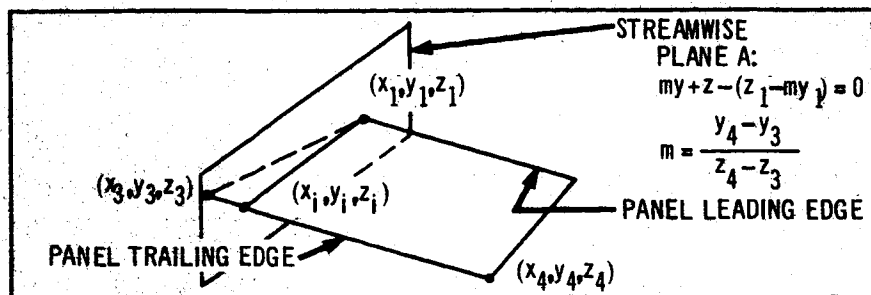
The program calculates the four panel corner points by intersecting with the body meridian lines a series of parallel transverse vertical (cutting) planes. The equations for these planes have the general form,

$$x - c_i = 0,$$

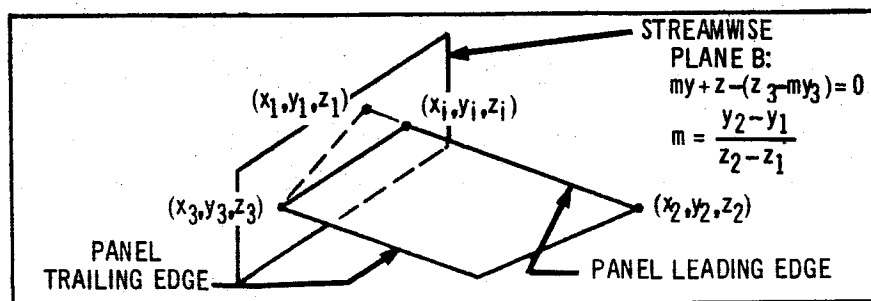
for which c_i is the i^{th} intercept as given on input cards. This is shown in the following sketch:



The program calculates the additional panel points by constructing planes normal to the plane of the panel and through a panel corner point, and intersecting these planes with the panel leading and trailing edges. At most, two such constructions are necessary for each of the two required points. To obtain the first point, the program constructs a streamwise plane (A) normal to the panel trailing edge and through the inboard leading edge corner point and attempts to intersect this plane with the panel trailing edge:

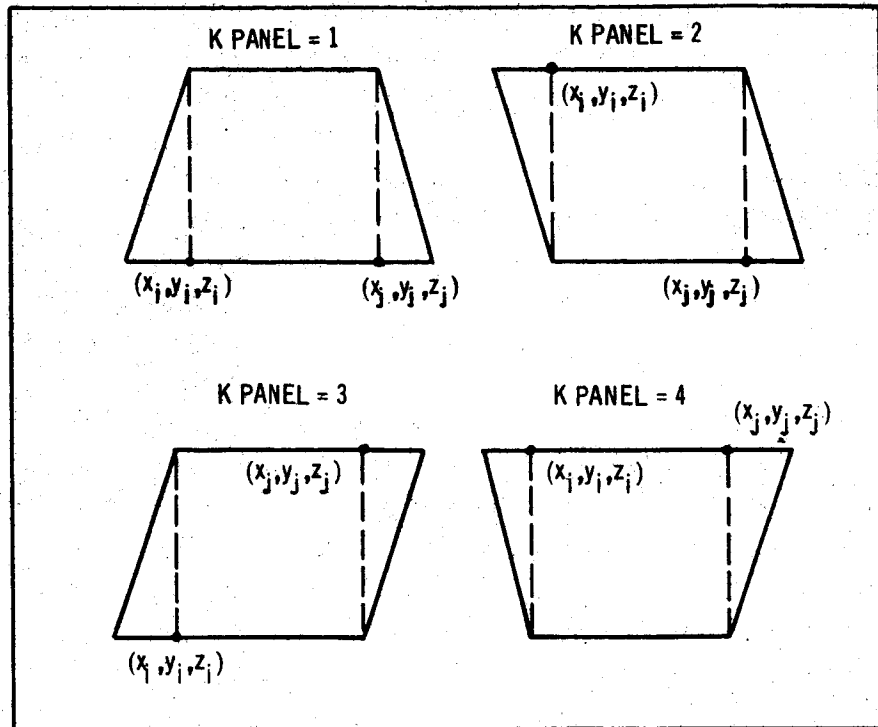


If an intersection with the trailing edge is obtained, this point is defined to be the first of the two required points. Should no intersection be calculated, the program then constructs a streamwise plane normal to the panel leading edge and through the inboard trailing edge corner point and attempts to intersect this plane with the panel leading edge:



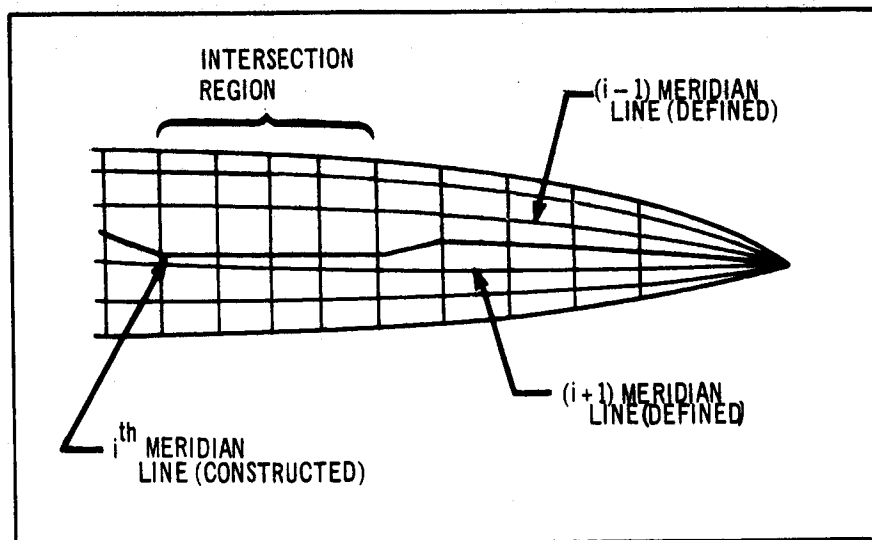
If the previous construction has failed, then this construction yields an intersection, and the point is defined to be the first of the two required points. The calculations used to obtain the second of the two points are identical to those given above except that the planes that are constructed pass through outboard rather than inboard corner points.

As both, either, or neither of these two points can occur on the panel leading (or trailing) edge, four panel configurations are possible, and a code is assigned for each panel. These codes are the following:



These codes are used in later subprograms.

In certain cases the body-wing intersection line does not coincide with a body meridian line, and an additional meridian line is constructed. In the intersection region proper, points on this additional line are defined to be the intersection points; elsewhere, fore and aft of the intersection region, points are obtained by averaging the corresponding points on the two adjacent body meridian lines. This is shown in the following sketch:



USAGE:

COMMON (See subroutine OPCAMI for unlabeled **COMMON** description).

Input: NWRITE

COMMON /COM1/ (See subroutine PANEL)

Input: KOPTB
KINT
XI
YI
ZI
NPER
NPER1
NPLANE
NPLN1

Output: KSTART
KEND

COMMON /COM2/ (See subroutine BODY)

Input: NPLNB
NPLNW
JLEAD
JTRAIL
NPTS
X
Y
Z
XCEPT
XCEPTW
YCEPTW
ZCEPTW

Output: IMID
KPanel
XCOR
YCOR
ZCOR
XINT
YINT
ZINT

CALL CRNRB

**SUBPROGRAM
CALLED:**

POLXN

ERROR RETURNS:

Error messages indicate if panel or secondary panel
corner points not correctly calculated.

STORAGE:

$1282_{10} = 2402_8$

SUBJECT:

FORTRAN IV Subroutine CRNRW

PURPOSE:

To calculate wing panel (and secondary panel) corner point coordinates.

METHOD:

In general, a wing panel is defined by four corner points. To satisfy a program restriction that either a panel have streamwise inboard and outboard edges or that it be subdivided so that its secondary panels have streamwise edges, an additional point is determined in the following two cases:

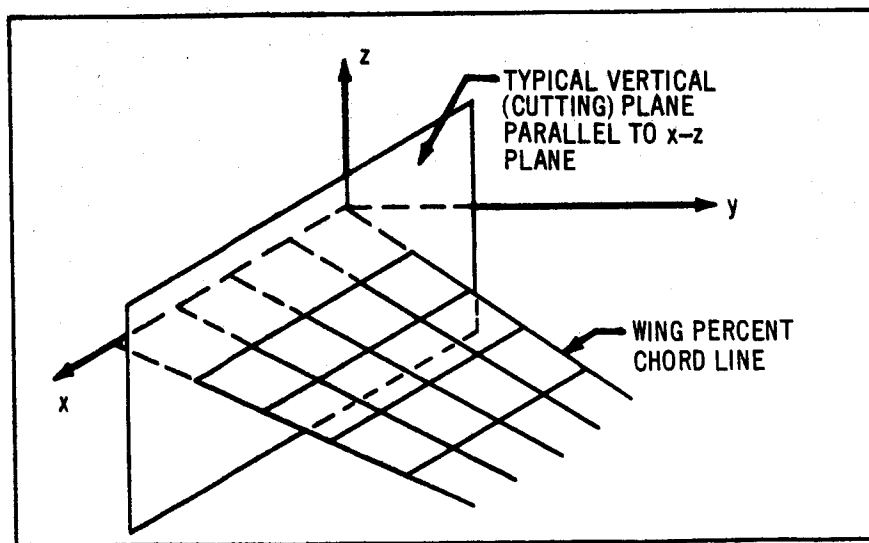
- 1) For panels on the inboard column if the body and wing intersect in a nonstreamwise line;
- 2) For panels on the outboard column if the outboard wing edge is a nonstreamwise edge.

All other panels have streamwise edges and are not subpaneled.

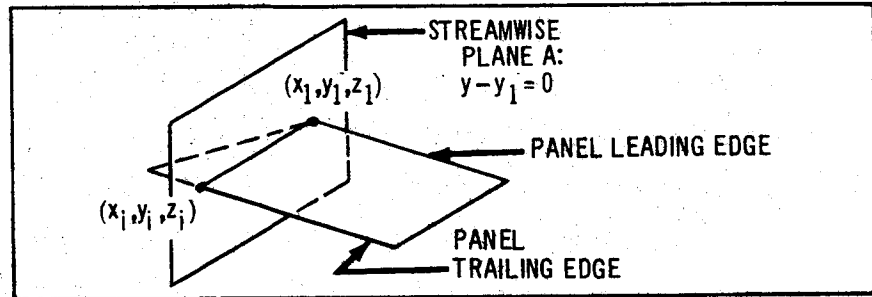
The program calculates the four panel corner points by intersecting with the wing percent chord lines a series of vertical (cutting) planes. The equations for these planes have the general form,

$$y - c_i = 0,$$

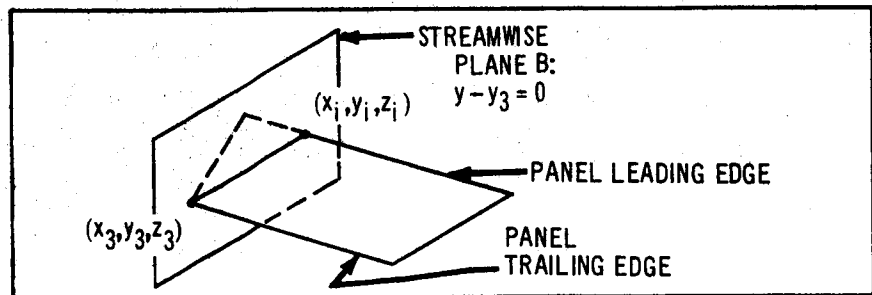
for which c_i is the i^{th} intercept as given on input cards. This is shown in the following sketch.



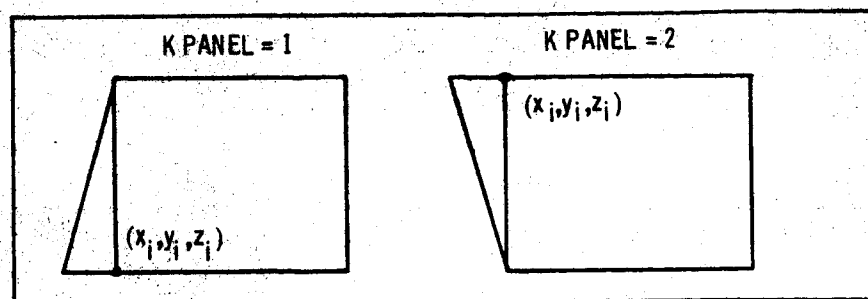
The program calculates the additional panel point, in those cases indicated above, by constructing planes normal to the plane of the panel and through a panel corner point, and by intersecting these planes with the panel leading or trailing edges. Two such constructions, at most, are required to obtain this point. The program first constructs a plane (A) normal to the panel and through a leading edge corner point and attempts to intersect this plane with the panel trailing edge.



If an intersection with the trailing edge is found, it is then defined to be that additional panel point. If no intersection is calculated, the program constructs a plane (B) normal to the panel and through a trailing edge corner point and attempts to intersect this plane with the leading edge.



As this additional point can be on either the leading or trailing edge a code is determined and assigned for any such panel.



USAGE:

COMMON (See subroutine OPCAMI for unlabeled **COMMON** description).

Input: NWRITE

COMMON /COM1 / (See subroutine PANEL)

Input: KOPTW
KINT
XI
YI
ZI
NPER
NPER1
NPLANE
NPLN1

Output: KSTART
KEND

COMMON /COM2 / (See subroutine WING)

Input: LJ
NPTS
X
Y
Z
KPNT
VALUE
YCEPT
SLOPE

Output: KPANEL
XCOR
YCOR
ZCOR
XINT
YINT
ZINT

CALL CRNRW

SUBPROGRAM
CALLED:

POLXN

ERROR RETURNS: Error messages indicate if panel (or secondary panel)
corner points not calculated.

STORAGE:

$926_{10} = 1636_8$

SUBJECT: FORTRAN IV Subroutine CUBIC2

PURPOSE: To fit a cubic to two points, being given the slope at each.

METHOD: The subroutine sets up the system of four simultaneous equations expressing the four given conditions and solves it for the coefficients of the cubic.

USAGE: CALL CUBIC2 (X, Y, D, C, M)

DIMENSION X(2), Y(2), D(2), C(4)

Input: X = Array of x-coordinates.
 Y = Array of y-coordinates.
 D = Array of first derivatives.

Output: C = Array of cubic coefficients.
 M = Error return.
 = 1 — success
 ≠ 1 — error detected

SUBPROGRAMS CALLED: None

ERROR RETURNS: If M = 2, overflow occurred. If M = 3, X(1) = X(2). Otherwise call is successful and M = 1.

RESTRICTIONS: X(1) ≠ X(2)

STORAGE: $146_{10} = 222_8$

SUBJECT: **FORTRAN IV Subroutine CVEL**

PURPOSE: **To compute the velocity components due to a given pressure difference, given the velocity components resulting from a unit pressure difference across panels.**

METHOD: **The velocity components resulting from a unit pressure difference across the influencing panels are computed and stored on tape previous to calling of this subroutine. Then the velocity components resulting from a given pressure difference across the influencing panels are found by**

$$u_i = \sum_{j=1}^N U_{ij} \cdot P_j$$

$$v_i = \sum_{j=1}^N V_{ij} \cdot P_j$$

$$w_i = \sum_{j=1}^N W_{ij} \cdot P_j$$

where U_{ij} , V_{ij} , and W_{ij} are the velocity components in the x, y, and z directions respectively at panel i induced by panel j, and p_j is the given pressure differences across the influencing panel.

USAGE: **CALL CVEL(M, N, NT, A, B, C, CL, U, V, W)**

DIMENSION A(M), B(M), C(M), U(N), V(N), W(N)

Input: M = Number of influenced panels.

N = Number of influencing panels.

NT = Logical tape number on which the velocity components due to unit pressure differences are stored.

A = Dummy array used by the subroutine.

B = Dummy array used by the subroutine.

C = Dummy array used by the subroutine.

CL = Array of given pressure differences.

Output: U = Array of velocity components in the x-direction.
V = Array of velocity components in the y-direction.
W = Array of velocity components in the z-direction.

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $129_{10} = 201_8$

SUBJECT:

FORTRAN IV Subroutine DATE

(See subroutine FDATE)

SUBJECT: **FORTRAN IV Subroutine DCPD**

PURPOSE: **To compute the pressure difference across the wing panels.**

METHOD: **The pressure difference across a wing panel i is given by:**

$$p_{W_i} = \sum_{j=1}^{NM} A_{R_{ij}}^{-1} \cdot n_{W_i}$$

where A_R^{-1} = The inverse of the reduced aerodynamic influence coefficients matrix.

n_W = The velocity component of the wing, normal to the x-axis.

USAGE: **CALL DCPD (NM, NTAPEX, A, ALPHAM, CLM)**

DIMENSION **A(NM), ALPHAM(NM), CLM(NM)**

Input: **NM** = Number of wing panels.

NTAPEX = Logical tape number, of which A_R^{-1} is stored.

A = Dummy array used by the sub-routine.

ALPHAM = Array velocity components on wing panels normal to the x-axis.

Output: **CLM** = Array of the pressure difference across wing panels.

SUBPROGRAM

CALLED: **None**

ERROR RETURNS: **None**

RESTRICTIONS: **None**

STORAGE **$90_{10} = 132_8$**

SUBJECT: FORTRAN IV Subroutine DCPI

PURPOSE: In the presence of a wing, to compute the pressure difference across a body panel.

METHOD: The pressure difference is given by:

$$p_{B_i} = \sum_{j=1}^{NB} A_{BB_{ij}}^{-1} \cdot n_{B_j} + \sum_{j=1}^{NW} E_{ij} \cdot p_{W_j}$$

where A_{BB}^{-1} = The inverse of a partition of the aerodynamic influence coefficients resulting from the influence of the body on the body.

n_B = The velocity component normal to the x-axis, on the body.

E = The matrix formed by the product,

$$A_{BB}^{-1} \cdot A_{BW}$$

where A_{BW} = The partition of the aerodynamic influence coefficients matrix resulting from the influence of the wing on the body.

p_W = The pressure difference across the wing panels.

USAGE: CALL DCPI (NB, NW, NTAPEX, A, ALPHAB, CLW, CLB)

DIMENSION A(NW), ALPHAB(NB), CLW(NW), CLB(NB)

Input: NB = Number of body panels.

NW = Number of wing panels.

NTAPEX = Logical tape number on which A_{BB}^{-1} and E are stored.

A = Dummy array used by the subroutine.

ALPHAB = Array of velocity components on the body, normal to the x-axis.

CLW = Array of the pressure difference across wing panels.

Output: CLB = Array of the pressure difference across the body panels.

SUBPROGRAM

CALLER: None

ERROR RETURNS: None

RESTRICTIONS None

STORAGE: $143_{10} = 217_8$

SUBJECT: FORTRAN IV Subroutine DEFEN1

PURPOSE: To write records on the Geometry Definition binary tape.

METHOD: The format of the binary tape to be written is shown in Appendix D. Each time that DEFEN1 is called it writes two records. Record A consists of ten fixed-point words. Record B contains either nine words or $K - J + 1$ words, where K and J are given. A ten-word array, IREC, is given. If $IREC(3) \neq 0$, then record B consists of nine words, which are zeros, and record A has the following format:

word 1	IREC(1)
word 2	0
word 3	IREC(3)
words 4-10	0

However, if $IREC(3) = 0$, then IREC is written as record A and the specified part of a given array is written as record B.

USAGE: DIMENSION B(1), IREC(10)

CALL DEFEN1 (B, J, K, LTAPE, IREC)

Input: B = B(J) through B(K) is to be written on LTAPE.

J = Subscript.

K = Subscript.

LTAPE = Tape number.

IREC = Array to be written on LTAPE (see METHOD, above).

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

RESTRICTIONS: LTAPE is assumed to be correctly positioned.

STORAGE: $128_{10} = 200_8$

SUBJECT: FORTRAN IV Subroutine DEFEND

PURPOSE: To prepare records for the Geometry Definition tape and to monitor tape writing.

METHOD: This subroutine is used by subroutine GEOMD to transfer data from core to tape. If wing-body intersections are not requested, GEOMD calls DEFEND at the end of the case to write records 1-18 (see Appendix D). But if intersections are requested, GEOMD first calls DEFEND to write records 1-10, then finds intersections, and finally calls DEFEND again to write records 11-18.

USAGE: **DIMENSION** B(1), LK(3, 9)
 LOGICAL LGDEF(3, 6), LGTAPE
 CALL DEFEND (B, LK, LO, LTAPE, LGDEF, LGTAPE, INTWB)

Input: **B** = Storage buffer for variable-length arrays.

LK = Array that describes contents of B. Consider LK(i, j). The index j refers to a data array as follows:

<u>i</u>	<u>Data array</u>
1	Upper wing percent lines
2	Lower wing percent lines
3	Upper wing percent lines (part outside body)
4	Lower wing percent lines (part outside body)
5	Body meridian lines
6	Body stations
7	Wing planform (leading and trailing edge points)
8	Upper wing-body intersections
9	Lower wing-body intersections

A data array is stored starting in B(LK(1, j)). The number of elements

in the data array is LK(3, j). The number of percent lines (j = 1, 2, 3, 4) or meridian lines (j = 5) is LK(2, j). The number of airfoils is LK(2, 7). LK(2, j) is not used for j = 6, 8, 9.

LO = Output tape number.

LTAPE = Binary tape number.

LGDEF = Logical array of problem status (see subroutine GEOMD).

LGTAPE = .TRUE. if records are to be written on LTAPE, .FALSE. if not.

INTWB = If INTWB < 0, LTAPE is to be rewound and records 1-10 written. If INTWB > 0, records 11-18 and an EOF are to be written. If INTWB = 0, records 1-18 and an EOF are to be written.

Output: LGDEF = If LGDEF(1, i) and LGDEF(2, i) are both true, LGDEF(3, i) is set to .TRUE. to indicate that the corresponding data array has been written on LTAPE.

SUBPROGRAM

CALLED: DEFEN1

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $373_{10} = 565_8$

SUBJECT: FORTRAN IV Function DERIV1

PURPOSE: To find the first derivative of the quadratic through three given points at a specified one of these points. This provides a good approximation to the slope of a function at a point, particularly if the other two points used are nearby.

METHOD: The subroutine simply finds the unique polynomial of degree two through the given points then evaluates its first derivative at the specified point.

USAGE: D = DERIV1 (X, Y, N)
 DIMENSION X(3), Y(3)

Input: X = Array of x-coordinates.
 Y = Array of y-coordinates.
 N = Code.
 = 1, 2 or 3 indicating point at which derivative is desired.

SUBPROGRAMS CALLED: None

ERROR RETURNS: None

RESTRICTIONS: The x-coordinates must be distinct, but need not be in any order of evenly spaced.

STORAGE: $129_{10} = 201_8$

SUBJECT: FORTRAN IV Function DERIV2

PURPOSE: To find the second derivative of the cubic through four given points (x_1 , y_1) at an arbitrary point whose x-coordinate is given.

METHOD: The subprogram simply finds the unique polynomial of degree three through the given points, then evaluates its second derivative at the desired x , which need not be one of the four given x_i .

USAGE: $D = \text{DERIV2}(X, Y, XX)$

DIMENSION $X(4), Y(4)$

Input: X = Array of x-coordinates.

Y = Array of y-coordinates.

XX = x-coordinate of point at which second derivative is desired.

SUBPROGRAMS CALLED: None

ERROR RETURNS: None

RESTRICTIONS: The x-coordinates must be distinct but can be in any order and unevenly spaced.

STORAGE: $167_{10} = 247_8$

SUBJECT: FORTRAN IV Subroutine DERIVS

PURPOSE: Given a set of n points (x_i , y_i), to obtain the first and second derivatives at each of the points.

METHOD: Subroutine SCAMP4 is used to fit a chain of cubics of the general form:

$$y = C_0 + C_1x + C_2x^2 + C_3x^3$$

to the set of points and calculate the first derivative at each point from the equation:

$$y' = C_1 + 2C_2x + 3C_3x^2.$$

The second derivative at each point is obtained from the equation:

$$y'' = 2C_2 + 6C_3x.$$

USAGE: CALL DERIVS (XB, R, NBODYYS, FD, SD)

DIMENSION XB(NBODYYS), R(NBODYYS), FD(NBODYYS), SD(NBODYYS)

Input: XB = Array of x-abcissae.

R = Array of y-ordinates.

NBODYYS = Number of points.

Output: FD = Array of first derivatives.

SD = Array of second derivatives.

SUBPROGRAM CALLED: SCAMP4

ERROR RETURNS: None

RESTRICTIONS: The array of x-abcissae must form a strictly monotone sequence.

STORAGE: $301_{10} = 455_8$

SUBJECT: FORTRAN Function DISPTA

PURPOSE: To find the distance between two points in N-space.

METHOD: Standard

USAGE: D = DISPTA (P, Q, N)
 DIMENSION P(N), Q(N)
 Input: P = Array of coordinates of one point.
 Q = Array of coordinates of other point.
 N = Dimension of space.
 Output: D = Distance between points P and Q.

SUBPROGRAM
CALLED: SQRT (Built-in function)

ERROR RETURNS: None

RESTRICTIONS: N > 0

STORAGE: $50_{10} = 62_8$

SUBJECT: FORTRAN IV Subroutine DMAXL

PURPOSE: Given a set of points in 3-space, to find which point is farthest from the line through the end-points.

METHOD: Let P_1 and P_N be the first and last points, and let \bar{u} be a unit vector from \bar{P}_1 to \bar{P}_N . For each intermediate point P_i , find the vector $\bar{v} = \bar{P}_i - \bar{P}_1$. Then the distance from P_i to the line $P_1 P_N$ is the magnitude of the cross-product of \bar{u} and \bar{v} . The point P_j farthest from the line is selected. If there is more than one such point, the first is selected.

USAGE: DIMENSION P(3, N), U(3)
 CALL DMAXL (P, N, DIST, J, U, NU)

Input: P = Array of points.
 N = Number of points in P.

Output: DIST = Distance from point P_j to the line $P_1 P_N$.
 J = Subscript of point P_j (that is, the desired point is $P(i, J)$, $i = 1, 3$).
 U = Unit vector directed from P_1 to P_N .
 NU = Error indicator, which is zero for success.

SUBPROGRAMS CALLED: UVECN
 VCROS

ERROR RETURNS: NU = 1 if N = 2,
 = -1 if N < 2,
 = -2 if P_1 and P_N are coincident.

RESTRICTIONS: None

STORAGE: $139_{10} = 213_8$

SUBJECT: FORTRAN IV Subroutine ELLIPR

PURPOSE: Given the horizontal and vertical semi-axes of a rectangular ellipse and the angle of a radius vector to find the length of the vector and the corresponding point on the ellipse.

METHOD: The sine and cosine of the angle (measured in a clockwise direction from the + y axis) are given. The required quantities are computed in a standard manner.

USAGE: CALL ELLIPR (A, B, SIN, COS, RHO, X, Y, NU)

Input: A = Horizontal semi-axis.
B = Vertical semi-axis
SIN = Sine of angle.
COS = Cosine of angle.

Output: RHO = Length of radius vector.
X = x-coordinate.
Y = y-coordinate.
NU = Error code, which is zero if successful.

SUBPROGRAM

CALLED: SQRT (Built-in function)

ERROR RETURNS: NU = 1 if either of the semi-axes is zero.
NU = 2 if the radius vector has zero length. (This indicates that SIN = COS = 0.)

RESTRICTIONS: None

STORAGE: $83_{10} = 123_8$

SUBJECT: FORTRAN IV Subroutine ENRYCH

PURPOSE: Given a set of points that lie on a smooth curve, to interpolate additional points so spaced that between each pair of points the distance from the chord to the assumed interpolation curve is less than a given tolerance.

METHOD: For each set of four consecutive points, subroutine OPTIM3 is called to interpolate additional points. Because OPTIM3 measures error between a chord and arc in a y direction, x and y are reversed for each set of four consecutive points if the range of y is greater than the range of x. Also, signs are reversed if necessary to make the equivalent x_i strictly increasing before calling OPTIM3. The inverse operations are performed after OPTIM3 does the interpolation.

USAGE: DIMENSION A(NI), B(NI), C(NO), NU(3)
CALL ENRYCH (A, B, NI, EPS, C, NO, NU)

Input: A = Array of independent variable coordinates.

B = Array of dependent variable coordinates.

NI = Number of pairs, A_i , B_i .

EPS = Arc-chord tolerance.

NO = Length of array C.

NU(2) = Logical output tape number on which to write error comments, if any.

NU(3) = Error message limiter and counter. If an error occurs for which a message is normally written, NU(3) is first reduced by one. The message is then written only if both NU(2) and NU(3) are greater than zero.

Output: C = Array of A_i , B_i pairs interspersed with interpolated pairs. If $NI < 4$ or $EPS \leq 0$, no interpolation takes place; then C contains A_i , B_i , $NO = 2*NI$, and $NU = 0$.

NO = Number of elements in the C array.

NU = 0 — success.

= 2 — at least one set of four consecutive points (A_i , B_i) is not strictly monotonic in either x or y.

- = 3 — more than 199 interpolated points are required between two consecutive points (A_i , B_i) in order to satisfy the given value of EPS. This may be due to (1) a very small value of EPS, or (2) a "wild" interpolating cubic between two points (points too "rough" or too far apart in that region).
- = 4 — C array is too small.
- = 5 — the input value of NO is less than $2*NI$.

**SUBPROGRAM
CALLED:**

OPTIM3

ERROR RETURNS:

If an error is encountered in any interpolating interval ($NU = 2$ or 3), an error message is written if $NU(2)$ and $NU(3) > 0$, no points are interpolated in that interval, and the routine continues. The value of NU returned is that of the last error encountered (if any).

RESTRICTIONS:

For every set of four consecutive points, either the independent variable coordinates or the dependent variable coordinates must be strictly monotonic. Since OPTIM3 uses cubic or quadratic interpolation, some input arrays may cause rather extreme swings in the output array. This may usually be corrected by supplying more input points in the swing region. In general, the output array of points will lie on a curve that maintains first derivative continuity. However, this may not be true if an x,y reversal (see METHOD, above) is required for some but not all sets of four points; appropriate scaling of one variable before entry (preferably by a power of 2) will ensure that either no set or all sets of four consecutive points will be reversed.

STORAGE:

$975_{10} = 1717_8$

SUBJECT: FORTRAN IV Subroutine EVAL

PURPOSE: To compute the matrix of the aerodynamic influence coefficients, the velocity components due to a surface distribution of vorticity, and the velocity components due to a surface distribution of sources in the reference plane of the wing.

METHOD: The equations in this subroutine are given in detail in the Appendix B of Part I.

USAGE: CALL EVAL (NI, XCPT, THKW)

COMMON DATE(2), NTAPEA, NTAPEB, NTAPEC,
NTAPED, NTAPEE, NTAPEF, NTAPEI, NTAPEO, NBODY,
NWIN, XMACH, SYM, KACE

COMMON/BLOCK/ALPHAS (210), AREA (210), A (210),
ALPHAC (110), ALPHAT (110), CHORD (210), ISYM,
NPART (210), NPANEL, NROW (2), THETA (210), TAIL,
U (210), V (210), VPM (210), VV (210), VPMM (210),
W (210), WPM (210), WW (210), WPMM (210), X (210,
3, 4), XBAR (210), XC (210), Y (210, 3, 4), YBAR (210),
YC (210), Z (210, 3, 4), ZBAR (210), ZC (210)

Input: NI = Index that indicates start of influencing panels.

XCPT = Array of panel control point coordinates.

THKW = 0., indicates the aerodynamic influence coefficients and velocity components due to vortices are to be computed.

≠ 0. indicates the velocity components due to wing sources are to be computed.

XMACH = Mach number.

SYM = Configuration symmetry condition.

KACE = 1, indicates body-alone case.

= 2, indicates wing-alone case.

= 3, indicates wing-body combination case.

NBODY = Number of body panels.
NWING = Number of wing panels.
NPANEL = Total number of panels.
NTAPEA = Logical number of tape on which the aerodynamic influence coefficients or normal velocity components on the body due to wing sources are written.
NTAPEB = Logical number of tape on which the velocity components are written.
X = Array of x-coordinates of the panel corner points.
Y = Array of y-coordinates of the panel corner points.
Z = Array of z-coordinates of the panel corner points.
THETA = Array of θ angles (angle between the plane of the panel and a plane parallel to the x-y plane).
ALPHAS = Array of the panel slopes, $\frac{dz}{dx}$

Output: IF THKW = 0.

A = Matrix of the aerodynamic influence coefficients.
U = Velocity components in the x-direction due to vortex distribution.
V = Velocity components in the y-direction due to vortex distribution.
W = Velocity components in the z-direction due to vortex distribution.

If THKW \neq 0.

A = Normal velocity components on the body due to wing sources.

U = Velocity components in the x-direction due to wing sources.

V = Velocity components in the y-direction due to wing sources.

W = Velocity components in the z-direction due to wing sources.

**SUBROUTINES
CALLED:**

ACOS	}	(Built-in functions)
TAN		
ALOG		
SQRT		
COS		
SIN		

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $3337_{10} = 6411_8$

SUBJECT: FORTRAN IV Subroutine EVAL1

PURPOSE: To compute velocity components due to a surface distribution of sources in the reference plane of the wing.

METHOD: The equations in this subroutine are given in detail in Appendix B of Part I.

USAGE: COMMON/FLOV1/KACE, NPANEL, NBODY, NWING, NBODYS, NROW (2), XMACH, SYM

COMMON/FLOV2/X(210, 3, 4), Y(210, 3, 4), Z(210, 3, 4), NPART(210), ALPHAS(210), THETA(210), XBB(50), R(50), WT(120), T(50), TC(50), SST(210), CHORD(210)

CALL EVAL1 (NI, THKW, XB, YB, ZB, U, V, W, NSTOP)

DIMENSION C(4), Q(4), CPM(4), RPM(4), RTMM(4), CPMM(4), BBETAM(4)

Input: NI = Index to indicate starting point of influencing panels.

NSTOP = Index to indicate end point of influencing panels.

THKW = 0. velocity components due to vorticies to be calculated.

= 1. velocity components due to sources to be computed.

XB = x-coordinate of field point.

YB = y-coordinate of field point.

ZB = z-coordinate of field point.

NPANEL = total number of panels.

SYM = 0. nonsymmetric configuration

= 1. symmetric configuration

XMACH = Mach number.

X = array of x-coordinates of panel corner points.

Y = array of y-coordinates of panel corner points.

Z = array of z-coordinates of panel corner points.
NPART = array containing the number of parts on each panel.
THETA = array of θ -angles (angle between the plane of the panel and a plane parallel to the x-y plane).
ALPHAS = array of panel slopes, $\frac{dz}{dx}$.
SST = array of panel vortex strengths.
WT = array of panel source strengths.
Output: U = u-component of perturbation velocity.
V = v-component of perturbation velocity.
W = w-component of perturbation velocity.

**SUBPROGRAMS
CALLED:**

ACOSH
 ALOG
 SIN
 TAN
 SQRT

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $2603_{10} = 5053_8$

SUBJECT: FORTRAN IV Subroutine FASNCS

PURPOSE: To compute the arc sine and/or the arc cosine of a normalized floating point argument.

METHOD: The arc sine and arc cosine are calculated as follows:

- 1) for $0 \leq x \leq 1$, $\text{arc cos } x = (1 - x)^{1/2} a(x)$
- 2) for $-1 \leq x < 0$, $\text{arc cos } x = \pi - (1 - |x|)^{1/2} a(|x|)$
- 3) for $0 \leq x \leq 1$, $\text{arc sin } x = \pi/2 - (1 - x)^{1/2} a(x)$
- 4) for $-1 \leq x < 0$, $\text{arc sin } x = -\pi/2 + (1 - |x|)^{1/2} a(|x|)$

where $a(x)$ is approximated by an eighth degree polynomial. For x from 1 to -1, the subroutine gives the arc sine in radians from $\pi/2$ to $-\pi/2$, and the arc cosine in radians from 0 to π .

USAGE: The subroutine FASNCS has two entry points, ASIN and ACOS; the function names ASIN (X) and ACOS (X) are used in FORTRAN arithmetic expressions.

SUBPROGRAM

CALLED: SQRT (Built-in functions)

ERROR RETURNS: None

RESTRICTIONS: $|x| \leq 1$. If $|x| > 1$, then an error message is printed. The subroutine is accurate to 8 decimal places, with the following exceptions in the arc sine:

$ x < 0.0015$	6 decimal figures
$0.0015 \leq x < 0.002$	7 decimal figures

STORAGE: $109_{10} = 155_8$

SUBJECT:

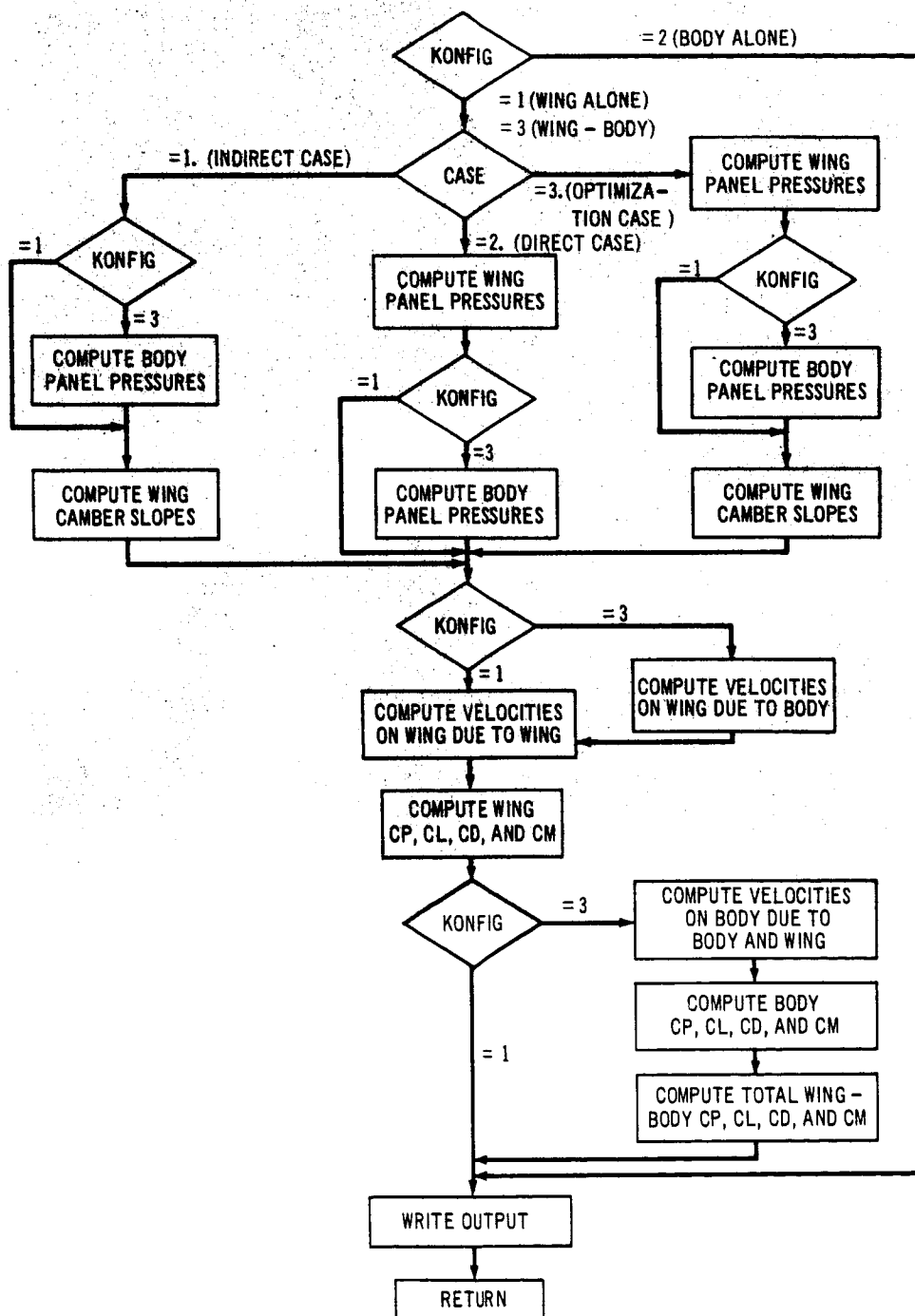
FORTRAN IV Subroutine FCALC

PURPOSE:

To compute pressures, forces, and moments.

METHOD:

This subroutine is called by the subroutine FORCES to compute the pressures, forces and moments for the different cases of wing alone, body alone, and wing-body configurations.



USAGE:

CALL FCALC

COMMON DATE (2), NTAPEA, NTAPEB, NTAPEC,
NTAPED, NTAPEE, NTAPEF, NTAPEI, NTAPEO,
NBODY, NWIN, XMACH, SYM, KACE

COMMON/AVAR/A (210), ACB (21), ABX (100), AWX
(110), AREA (210), ARN (2), ARWT (20), ALPHA (210),
ALPHAB (210), ALPHAS (210), ALPHAT (110),
ALPHAW (110), ALPHAX (110), AWX (110), ALPHAA,
ALPHAD, ARA, ARADEG, ARB, ARW, ARAS, AT, AAA

COMMON/BVAR/B (210), BBCL, BBCLD, BBCM

COMMON/CVAR/C (210), CHORD (210), CL (210), CPBB
(55, 10), CPNN (55, 10, 2), CLS (210), CDR, CASE,
CPCALC, CBAR, CONSNT, CLBAR, CLX, CLM, CDM

COMMON/DVAR/D (210), DZDXB (55), DADEG, DARAD

COMMON/IVAR/IPOLAR

COMMON/KVAR/KASE, KONFIG, KPOLAR

COMMON/NVAR/NFMT (9), NROW (2), NS, NPANEL,
NACEL, NROWB, NROWW, NCOLW, NBODYS,
NTHETA, NTHETS, NXLE, NRG, NPOLAR, NCLX

COMMON/PVAR/POLAR

COMMON/RVAR/R (55), RN (55, 2), RATIOX, RFAREA

COMMON/SVAR/SEMIS, SLC

COMMON/TVAR/TITLE (12), THETA (210), THETAB
(10), THETAS (9), THETAN (10, 2), TCL (10), TCD
(10), TCM (10), THICK, TWIST

COMMON/UVAR/UBWT (100), UWBT (110), UWWT
(110), UNCL (210, 2)

COMMON/VVAR/VBWT (100), VWBT (110), VWWT (110),
VNCL (210, 2), VOUT

COMMON/WVAR/WBWT (100), WWBT (110), WWWT
(110), WNCL (210, 2)

COMMON/XVAR/XBAR (210), XC (210), XNI (2), XNXN
(2), XNTN (2), XB (55), XN (55, 2), XNNCD (2), XNNCL
(2), XNNCM (2), XYZ (3), XCL (10), XCD (10),
XNACEL, XP, XCPBAR

COMMON/YVAR/YBAR (210), YC (210), YNI (2)

COMMON/ZVAR/ZBAR (210), ZC (210), ZNI (2),
ZDELTA (55), ZDN (55, 2), ZP, ZA

Output: Body-alone case

BBCD = Body coefficient of drag.

BBCL = Body coefficient of lift.

BBCM = Body coefficient of pitching
moment.

CPBB = Body pressure coefficients.

Wing-alone case

WCD = Wing coefficient of drag.

WCL = Wing coefficient of lift.

WCM = Wing coefficient of pitching
moment.

WSCD = Spanwise distribution of wing drag.

WSCL = Spanwise distribution of wing lift.

CPU = Upper surface wing pressure
coefficient.

CPL = Lower surface wing pressure
coefficient.

CP = Wing pressure difference.

= CPL - CPU

ALPHAU = Upper surface wing panel slopes.

ALPHAL = Lower surface wing panel slopes.

CHORD = Wing panel chord lengths.

Wing-body combination case

Note: In addition to the output given above for the body-alone and wing-alone case, the following output of incremental pressures, forces, and moments on the body due to the wing are given for this case:

BWCD = Incremental coefficient of drag.
 BWCL = Incremental coefficient of lift.
 BWCM = Incremental coefficient of pitching moment.
 CPB = Increment pressure coefficients.
 and also for the total wing-body configuration:
 WBCD = Total coefficient of drag.
 WBCL = Total coefficient of lift.
 WBCM = Total coefficient of pitching moment.

**SUBROUTINES
CALLED:**

CAMBW
 DCPI
 CAMBWB
 DCPD
 OPTMW
 OPTMWB
 CVEL
 RITE
 CP
 INTPOL
 CAMBER
 WLDM
 BLDM
 OUTB
 OUTW
 FSF
 SQRT (Built-in function)

ERROR RETURNS: None

RESTRICTIONS: NBODY \leq 100
 NWING \leq 110

STORAGE: $5440_{10} = 12500_8$

SUBJECT: FORTRAN IV Subroutine FDATE

PURPOSE: To make the date of the run available for printout.

METHOD: The FORTRAN monitor places the current date in core as a BCD word. The first two characters are the month, the second two characters are the day, and the last two characters are the year. This date is printed at the top of each page of a listing.

USAGE: CALL DATE(A, B)

The date, in BCD, is stored and arranged as follows:

Location A = XXXbYY

Location B = ,b19ZZ

where XXX represents a three-character abbreviation for the month, b represents a blank, and YY and ZZ represent the day and year, respectively.

DATE may be used as a function. If so used, the BCD word XXYZZZ is left in the accumulator upon exit from the subroutine,

C = DATE(A, B).

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

STORAGE: $41_{10} = 51_8$

SUBJECT: FORTRAN IV Subroutine FFSF

PURPOSE: To enable the FORTRAN program to move past end-of-file marks on FORTRAN written binary tapes, and to skip entire files.

METHOD: The first two words of each record on the designated logical tape unit are read using the IOCS read routine. If the second word is the Hollerith literal "TAPEND," the error code is set equal to the number of files remaining in the file count. Whenever end-of-file is encountered by the IOCS read subroutine, the file count is reduced by one. When the file count reaches zero, the error code is set to zero, and the subroutine returns to the main program. The tape is then positioned just beyond the end-of-file mark, ready to read the first record in the next file. A file count of zero or one will move past one end-of-file mark to the beginning of the next file on the tape. A file count of two will pass two end-of-file marks, thereby skipping the remainder (if any) of the current file and the next file in its entirety.

USAGE: CALL FSF (NFILE, LTAPE, LERROR)

Input: NFILE = The file count described above; the number of files to space forward.

LTAPE = The logical tape unit to be used.

LERROR = Error code. If LERROR = 0, subroutine successful. If LERROR = n, n > 0, n indicates the number of unspaced files.

SUBPROGRAMS

CALLED: IOCS
FVIO

ERROR RETURNS: None

RESTRICTIONS: If TAPEND indicator was written when the tape was written, FFSF will not read past the TAPEND signal. If not, it is possible to run off the end of the tape.

STORAGE: $52_{10} = 64_8$

SUBJECT: FORTRAN IV Subroutine FFSR

PURPOSE: To move a designated FORTRAN binary tape forward a specified number of logical records while indicating whether end-of-file was reached.

METHOD: Logical Records (FSR)

The first word in each physical record on the designated tape unit is examined using the IOCS read routine, and if the address is nonzero, the specified record count is reduced by one. If an end-of-file is encountered, the tape is back-spaced so that the end-of-file mark is, in effect, not passed, and the error code is set equal to the number of records remaining to be read. If no end-of-file is encountered, reading continues until the record count reaches zero; zero is stored in the error code and the subroutine returns to the calling program. No redundancy checking is done.

Physical Records (FSPR)

The method is the same as for a logical record except that the record count is reduced by each physical record spaced forward and the first word of each record is not examined.

USAGE:

CALL FSR (N, LTAPE, LERROR)

Input: N = Number of FORTRAN logical records to forward space. Zero means no spacing.

LTAPE = Logical tape unit.

LERROR = Error code.

CALL FSPR (NP, LTAPE, LERROR)

Input: NP = Number of physical records to forward space. Zero means no spacing.

LTAPE = Logical tape unit.

LERROR = Error code.

**SUBPROGRAMS
CALLED:**

IOCS
FVIO

RESTRICTIONS: This routine will not proceed beyond an end-of-file mark on tape.

STORAGE: $53_{10} = 65_8$

SUBJECT: FORTRAN IV Subroutine FLOOUT

PURPOSE: To provide optional output of perturbation velocity components and pressure coefficients due to the various singularities — wing pressure singularities, body pressure singularities, wing source singularities, and body line sources and doublets — at points in the near flow field.

METHOD: The velocity contributions are written on four different scratch tapes; one for each type by subroutine LACKEY. Depending upon the type of case — wing along, wing-body or body alone — the velocity components are read in and the pressure coefficients are calculated according to the CPCALC option (see subroutine LACKEY).

Appropriate titles are printed defining which singularities' contributions are being presented. The x, y, z coordinates of the point in question, followed by the u, v, w, velocity components and the pressure coefficients due to that singularity are written on the output tape.

USAGE: COMMON /FLOV4/ COSARA, SINARA, XMACH2, BT2
 COMMON /FLOV5/ N1, N2, N3, N4
 COMMON /THICK/ THKW, ARA, CPCALC, CAMN, POP
 COMMON /INTGA/ GP(3, 500), VLS(4, 500)

CALL FLOOUT (IC)

Input:	IC	=	number of points and velocity components to be output.
	COSARA	=	cosine of angle of attack
	SINARA	=	sine of angle of attack
	XMACH2	=	(Mach Number) ²
	BT2	=	XMACH2-1
	N1	}	= four logical tape numbers of scratch tapes on which the velocity components have been written.
	N2		
	N3		
	N4		
	THKW	}	= see subroutine LACKEY for description.
	ARA		
	CPCALC		
	CAMN		
	POP		= 0., special printout not requested.
			≠ 0., special printout is requested.

GP

= scratch array used for
x, y, z coordinates.

VLS

= scratch array used for
u, v, w, and pressure
coefficients.

SUBPROGRAMS
CALLED:

None

ERROR RETURNS:

None

RESTRICTIONS:

Due to the limitations on the dimension of the scratch
arrays, this routine is restricted to maximum of 500
points in the flow field. If more than 500 points are
given, the output is printed for the first 500.

STORAGE:

$575_{10} = 1077_8$

SUBJECT: FORTRAN IV Subroutine FLOVIZ

PURPOSE: Control routine of the Flow Visualization section.

METHOD: A control word is read from the input tape to determine the option selected. The control word must be one of GRIDS, STREAMLINES, or POINTS. If the control word is not one of the above, control is returned to the calling routine.

Once a control word is recognized, input of data continues and the appropriate option is selected.

USAGE: CALL FLOVIZ

DIMENSION X(210, 3, 4), Y (210, 3, 4), Z (210, 3, 4),
NROW (2), NPART (210)

DIMENSION ALPHAS (210), THETA (210)

DIMENSION XBB (50), R (50), WT (120)

DIMENSION T (50), TC (50), SST (210), CHORD (210)

COMMON/FLOV1/KACE, NPANEL, NBODY, NWIN, NWING,
NBODYS, NWINGS, NROW, XMACH, SYM

COMMON/FLOV2/X, Y, Z, NPART, ALPHAS, THETA,
XBB, R, WT, T, TC, SST, CHORD

COMMON/FLOV4/COSARA, SINARA, XMACH2, BT2

COMMON/FLOV5/N1, N2, N3, N4

COMMON/GRIDA/MODE, DX, DY, DZ, IX, IY, IZ, XO,
YO, ZO, XA, YA, ZA, LIT

COMMON/INTGA/DUM (3500)

COMMON/THICK/THKW, ARA, CPCALC, CAMN, POP

COMMON DAT (4), N8, DUUM (3), N5, N6, DUUUM (5)

DATA GRID/6HGRIDS /, STREAM/6HSTREAM/,
POINT/6HPOINTS/

**SUBPROGRAMS
CALLED:**

ALLIN
GRIDS
FLOOUT
STRM1
LACKEY
SQRT

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $908_{10} = 1614$

SUBJECT:

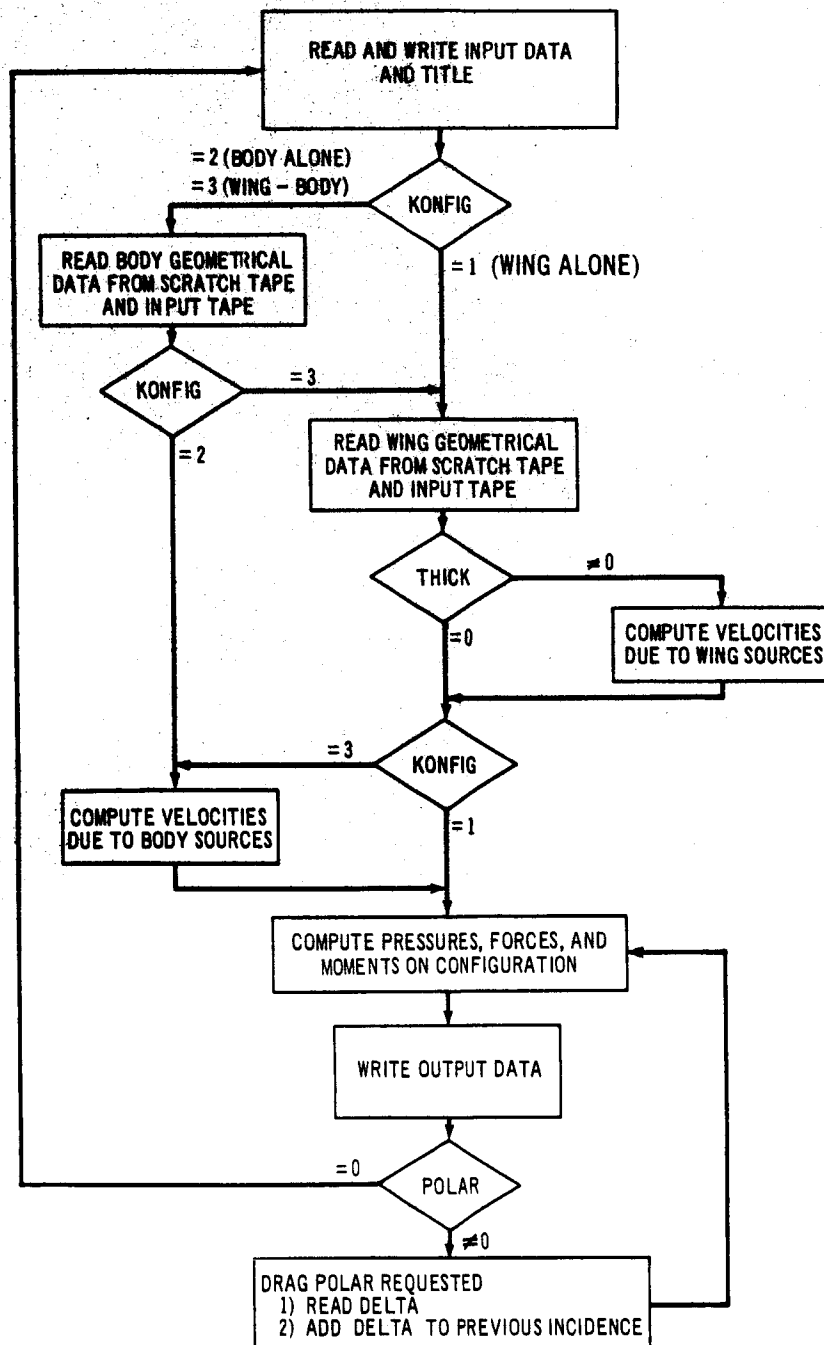
FORTTRAN IV Subroutine FORCES

PURPOSE:

Control routine for computing pressures, forces, and moments.

METHOD:

The input data cards for a given case are read and other subroutines are called as required to perform the requested calculations.



USAGE:

CALL FORCES

**COMMON DATE (2), NTAPEA, NTAPEB, NTAPEC,
NTAPED, NTAPEE, NTAPEF, NTAPEI, NTAPEO,
NBODY, NWIN, XMACH, SYM, KACE**

**COMMON/AVAR/A (210), ACB (21), ABX (100), AWW
(110), AREA (210), ARN (2), ARWT (20), ALPHA (210),
ALPHAB (210), ALPHAS (210), ALPHAT (110),
ALPHAW (110), ALPHAX (110), AWW (110), ALPHAA,
ALPHAD, ARA, ARADEG, ARB, ARW, ARAS, AT, AAA**

COMMON/BVAR/ B (210), BBCL, BBCLD, BBCLM

**COMMON/CVAR/ C (210), CHORD (210), CL (210),
CPBB (55, 10), CPNN (55, 10, 2), CLS (210), CDR,
CASE, CPCALC, CBR, CONSNT, CLBR, CLX, CLM,
CDM**

COMMON/DVAR/ D (210), DZDXB (55), DADEG, DARAD

COMMON/IVAR/IPOLAR

COMMON/KVAR/KASE, KONFIG, KPOLAR

**COMMON/NVAR/NFMT (9), NROW (2), NS, NPANEL,
NACEL, NROWB, NROWW, NCOLW, NBDYS, NTHETA,
NTHETS, NXLE, NRG, NPOLAR, NCLX**

COMMON/PVAR/POLAR

COMMON/RVAR/ R (55), RN (55, 2), RATIOX, RFAREA

COMMON/SVAR/SEMIS, SLC

**COMMON/TVAR/TITLE (12), THETA (210), THETAB
(10), THETAS (9), THETAN (10, 2), TCL (10), TCD
(10), TCM (10), THICK, TWIST**

**COMMON/UVAR/UBWT (100), UWT (110), UWT
(110), UNCL (210, 2)**

**COMMON/VVAR/VBWT (100), VWT (110), VWT
(110), VNCL (210, 2), VOUT**

**COMMON/WVAR/WBWT (100), WWT (110), WWT
(110), WNCL (210, 2)**

**COMMON/XVAR/XBAR (210), XC (210), XNI (2), XNXN
(2), XNTN (2), XB (55), XN (55, 2), XNCD (2), XNCL
(2), XNCLM (2), XYZ (3), XCL (10), XCD (10), XNCL,
XP, XCPBAR**

COMMON/YVAR/YBAR (210), YC (210), YNI (2)

COMMON/ZVAR/ZBAR (210), ZC (210), ZNI (2),
ZDELTA (55), ZDN (55, 2), ZP, ZA

Input: See Aerodynamic Card Set of Input Data Format
(section 3.3)

**SUBPROGRAMS
CALLED:**

INOUT
READ
BCAM
BTHICK
TVEL
KARMOR
FCALC
FSF
COS (built-in function)

ERROR RETURNS: None

RESTRUCTIONS: NBODY ≤ 100
NWING ≤ 110

STORAGE: $1020_{10} = 23732_8$

SUBJECT: FORTRAN Subroutine FROOTA

PURPOSE: To find the root of a single-valued function $f(x)$.

METHOD: FROOTA is designed to be called repeatedly until a root is found within a given tolerance. On initial call it is given two points on the function; these two points bracket the root. FROOTA computes two values of x (estimates of the root location) and returns with a code indicating that it wishes to be called again. Calling program finds function values corresponding to the two root estimates and calls FROOTA a second time. FROOTA determines which points now bracket the root, computes new root estimates, and returns. Process continues until FROOTA signals that root has been found.

Root estimates are made as follows: (a) the first root is estimated by assuming the function to be linear between the bracketing points, and (b) the second root is estimated by bisecting the bracketing interval. A root is located when (1) exact root is found, (2) bracketing interval becomes smaller than given tolerance, or (3) root estimate made on the basis of linear interpolation is identical to x -value of bracketing point.

USAGE:

DIMENSION R(10)

R(9) = 0.

R(10) = Tolerance

R(1) = $\left\{ \begin{array}{l} \\ \end{array} \right.$ Initial bracketing values of x
R(3) = $\left\{ \begin{array}{l} \\ \end{array} \right.$

DO α I = 1, 50

R(2) = Function value corresponding to R(1)

R(4) = Function value corresponding to R(3)

CALL FROOTA(R, J)

IF (J) β , γ , α

α CONTINUE

β error exit

γ success exit. Root is in R(1).

Input: (First call only. Assume root bracketed by x_a , x_b where $x_a > x_b$ or $x_a < x_b$.)

R(1) = x_a

R(2) = $f(x_a)$

R(3) = x_b

R(4) = $f(x_b)$

R(9) = 0.

R(10) = Tolerance (in x), which may be zero

Input: (2nd and succeeding calls)

R(2) = $f(R(1))$

R(4) = $f(R(3))$

Output: R(1) = Root estimate if J = 1

= Root if J = 0

R(3) = Root estimate if J = 1

R(5) = x_c

R(6) = $f(x_c)$

R(7) = x_d

R(8) = $f(x_d)$

} where x_c and x_d are values of
x which currently bracket the
root ($x_c < x_d$).

R(9) = Number of times that FROOTA has been
called.

J = 0 The root has been found.

= 1 The root has not yet been located.

= -2 R(9) < 0.

= -3 $f(x_a) * f(x_b) > 0$ on the first call,
which means that the root is not bracketed.

SUBPROGRAM

CALLED:

None

RESTRICTIONS:

Function values at limits of initial interval must not have the same sign. Function must be continuous over interval. It may have a number of roots but, of course, FROOTA will only find one. Last six elements of R-array must not be changed between successive calls for a particular case.

STORAGE:

$186_{10} = 272_8$

SUBJECT: FORTRAN IV Subroutine FSF
(See Subroutine FFSF)

SUBJECT:

FORTRAN IV Subroutine FSR

(See Subroutine FFSR)

SUBJECT: FORTRAN IV Subroutine FTAN

PURPOSE: To compute the tangent of a floating point radian argument.

METHOD: The tangent function is computed as follows:

- 1) if $0 \leq |x| \leq 10^{-4}$ radians, $\tan x = x$
- 2) if $10^{-4} < |x| \leq \pi/4$ radians,

$$\tan x = \frac{x}{1} - \frac{x^2}{3} - \frac{x^2}{5} - \frac{x^2}{7} - \frac{x^2}{9} - \frac{x^2}{11}$$
- 3) if $\pi/4 < |x| < \pi/2$ radians, and
 - a) $x > 0$, then $\tan x = \frac{1}{\tan(\pi/2 - x)}$
 - b) $x < 0$, then $\tan x = \frac{1}{\tan(\pi/2 - |x|)}$

USAGE: The function name TAN(X) is used in an arithmetic expression where the argument X is a FORTRAN expression.

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: X is restricted: $|X| < 2^{26} \cdot \pi$ and not within two bits of an odd multiple of $\pi/2$.
 If $|X| > 2^{26} \cdot \pi$ an error message is given.
 If the argument is within two bits of an odd multiple of $\pi/2$, an error message is given.
 The accuracy is at least 8 significant digits for $0 \leq x \leq \pi$ radians, at least 7 significant digits for $\pi < x \leq 2\pi$ and at least 6 significant digits otherwise.

STORAGE: $124_{10} = 174_8$

SUBJECT: FORTRAN IV Subroutine GEOMD

PURPOSE: To control subprograms that deal with the first phase of wing-body geometry.

METHOD: A buffer is set up (see Appendix A) that is used by all lower-level subroutines for all variable-length storage arrays. Data cards are read by subroutine INTURP until a valid command (in columns 1-6) is found. After any command except DEFEND is executed, data cards are again read until another valid command is encountered; a DEFEND command returns control to the calling program. For a command BODY (or BODY), subroutine BODY1 is called to read body definition data and compute points on body meridian lines. A command WING (or WING) results in a call of subroutine WINGA to read wing definition data and compute points on wing percent lines. A WBX command is used to find the intersections of previously defined wing percent lines with a body surface. The TDUMP command sets a code which will later result in a printout of the contents of the definition tape. A NOTAPE (or NOTAPE) command sets a code to suppress the writing of a definition tape (see Appendix D).

USAGE: DIMENSION DATE(2)

 COMMON /LGEOMD/ LGDEF(3, 6)

 LOGICAL LGDEF

 CALL GEOMD (DATE, LI, LO, LER, LTAPE)

Input: DATE = Date (alphameric).

 LI = Input tape number.

 LO = Output tape number.

 LER = Output tape number for error comments.

 LTAPE = Definition tape number.

Output: LDGEF = Logical array describing which definitions were requested and completed.
 LGDEF(i, j) is .TRUE. if the i^{th} statement is true for the j^{th} component.
 j^{th} component

1. Upper wing surface percent lines.
2. Lower wing surface percent lines.

3. Body surface meridian lines.
4. Wing planform points.
5. Intersections of upper wing percent lines with body surface.
6. Intersections of lower wing percent lines with body surface.

ith statement

1. This component requested.
2. This component successfully computed.
3. This component successfully computed and the results written on LTape.

SUBPROGRAMS

CALLED:

CLEAR } (See Appendix A)
 INIBFR }
 TDUMP }
 DEFEND }
 BODY1 }
 INTURP }
 WINGA }
 WBXUL }

ERROR RETURNS: The LGDEF array will reflect any errors detected. Lower-level subroutines write error messages on tape LER.

RESTRICTIONS:

The suggested order for commands is BODY, WING, WBX, DEFEND. The minimum set of commands is BODY, DEFEND (or WING, DEFEND). The last command must always be DEFEND. NOTAPE must be placed before WBX (if present). BODY, ..., WING or WING, ..., BODY must precede WBX. A required set of data cards (see Input Data Format, 3.3) must follow each command except TDUMP, NOTAPE, and DEFEND.

STORAGE:

$10289_{10} = 24061_8$

SUBJECT:

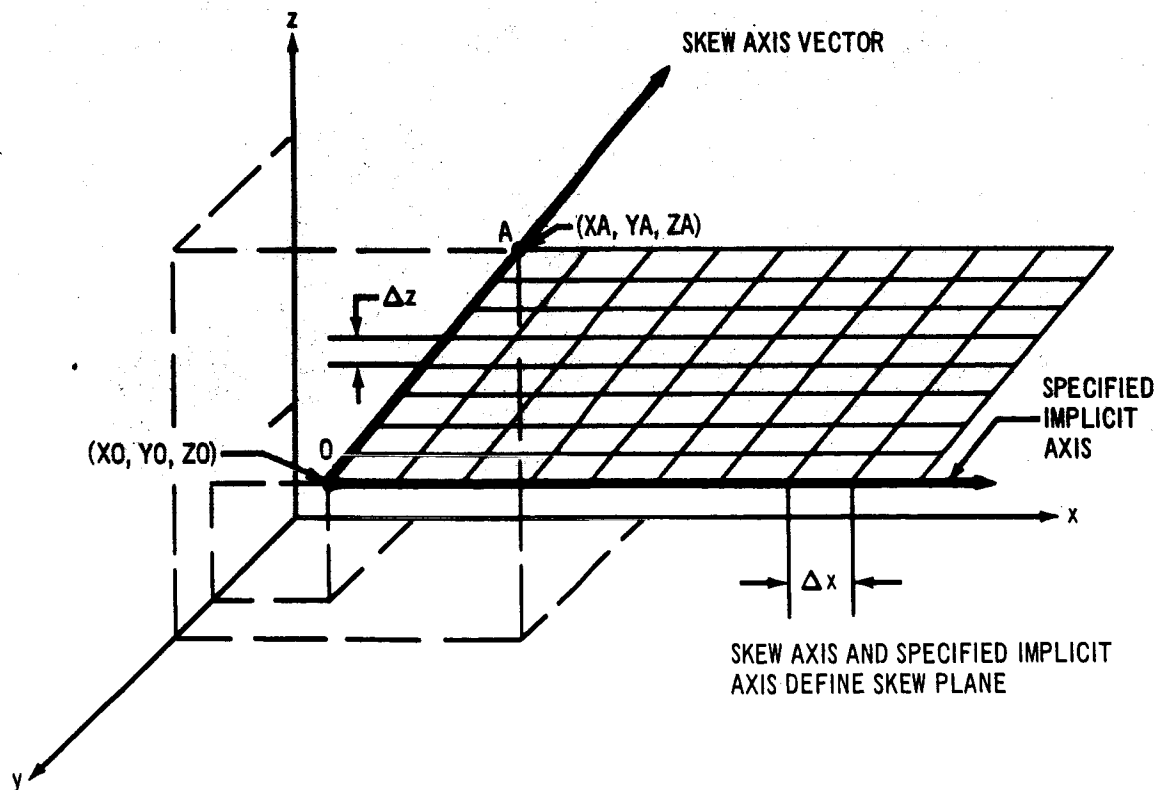
FORTRAN IV Subroutine GRIDS

PURPOSE:

Computes two- and three-dimensional grids, and two-dimensional skew grids. Field velocity components and C_p 's are computed at the grid lattice points.

METHOD:

The input data described below under USAGE defines the rectangular-grid system. The two-dimensional skew grid is defined by one of the implicit axis (user specified) and by a vector formed by the requested grid origin point, and another input point that may be anywhere in the space of interest. The grid lattice in this case is specified by incremental distances given along an implicit axis and by projections of incremental distances given along one of the implicit axes on the vector-defined axis as shown in the sketch below:



USAGE:

**COMMON/GRIDA/MODE, DX, DY, DZ, IX,IY, IZ, XO,
YO, ZO, XA, YA, ZA, LIT**

COMMON/INTGA/GP (3, NMAX), VLS (4, NMAX)

CALL GRIDS

DX	= length of increment in x-direction.
DY	= length of increment in y-direction.
DZ	= length of increment in z-direction.
IX	= number of increments in x-direction.
IY	= number of increments in y-direction.
IZ	= number of increments in z-direction.
XO	= x-coordinate of grid origin.
YO	= y-coordinate of grid origin.
ZO	= z-coordinate of grid origin.
XA	= x-coordinate of skew grid vector point.
YA	= y-coordinate of skew grid vector point.
ZA	= z-coordinate of skew grid vector point.
LIT	= a BCD character x, y, or z, defines the implicit axis to be used in the skew grid computation.
MODE	= 1, output as y-z planar cuts. = 2, output as x-z planar cuts. = 3, output as x-y planar cuts. = 4, skew grid.
GP (I, J)	= a scratch array used to contain the coordinate of a 2-d planar cut.
VLS (I, J)	= a scratch array used to contain the points in the above array.

Outputs: The coordinates, the actual velocities, a normalized velocity vector, and the C_p at each point of the grid are written on the output tape.

**SUBPROGRAM
CALLED:**

COMP
BLUNDR
FLOOUT
SQRT

ERROR RETURNS: See RESTRICTIONS below.

RESTRICTIONS: The product of the increment parameters for a cut must be less than 500. Grids will not be calculated and an error message is written on the output tape if the above is related.

STORAGE: $1144_{10} = 2214_8$

SUBJECT: FORTRAN IV Subroutine INOUT

PURPOSE: To print out all input aerodynamic data.

METHOD: The input data is written on the output tape for subsequent off-line printing.

USAGE: CALL INOUT (NTAPEO, KASE, CPCALC, POLAR, THICK, VOUT, RFAREA, XP, ZP, XMACH, SYM)

Input: NTAPEO = Logical number of output tape.
KASE = Code that selects case option.
CPCALC = Code that selects pressure coefficient calculation option.
POLAR = Code that selects drag polar option.
THICK = Code that selects wing thickness option.
VOUT = Code that selects velocity components printout option.
RFAREA = Half wing reference area.
XP = x-coordinate of point about which the pitching moments are to be computed.
ZP = z-coordinate of point about which the pitching moments are to be computed.
XMACH = Mach number.
SYM = Configuration symmetry condition.

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $472_{10} = 730_8$

SUBJECT: FORTRAN IV Subroutine INPUTB

PURPOSE: To read body definition and transformation data from scratch tapes as provided by previous program section and to read body paneling data from input cards.

METHOD: Program uses direct read tape statements to obtain body definition and transformation from scratch tapes (see Appendix D for tape format). Similarly program reads input tape directly for body paneling input card data.

USAGE: COMMON (See subroutine OPCAMI for unlabeled COMMON description).

Input: ND1
ND4
NREAD
NWRITE

COMMON /COM1/ (See subroutine PANEL)

Output: KOPTB
KINT
XI
YI
ZI
NPER
NPER1
NPLANE
NPLN1

COMMON /COM2/ (See subroutine BODY)

Output: NPLNB
NPLNW
JLEAD
JTRAIL
NPTS
X
Y
Z
XCEPT
XCEPTB
XCEPTW
YCEPTW
ZCEPTW
CODEBW

CALL INPUTB

CALLED: FSR
CHECK

ERROR RETURNS: Error message indicates whether body cutting planes are incorrectly defined on input cards. Error messages also indicate whether size of subscripted array is exceeded by input card data or by data on scratch tapes.

STORAGE: $5972_{10} = 13524_8$

SUBJECT: FORTRAN IV Subroutine INPUTW

PURPOSE: To read wing definition and transformation data from scratch tape as provided by previous program section and to read wing paneling data from input cards. Program reads input cards that define wing cutting planes, and, if an option is used, program reads actual upper and lower airfoil surface coordinates from which wing camber and thickness are calculated.

METHOD: Program uses standard read tape instructions to obtain wing definition from scratch tapes (see Appendix D for tape format). Similarly program reads input tape for wing paneling card data.

USAGE: COMMON (See subroutine OPCAMI for unlabeled COMMON description).

Input: ND4
NREAD
NWRITE

COMMON /COM1/ (See subroutine PANEL for description)

Output: KOPTW
KOPTF
NUMS
NPER
NPER1
NPLANE
NPLN1

COMMON /COM2/ (See subroutine WING for description)

Output: NPTS
X
Y
Z
KPNT
VALUE
YCEPT
SLOPE

CALL INPUTW

SUBPROGRAMS CALLED: FSR
CHECK

ERROR RETURNS: Error messages indicate if size of subscripted array is exceeded by data on input cards or on scratch tapes.

STORAGE: $5946_{10} = 13472_8$

SUBJECT: FORTRAN IV Subroutine INTAPE

PURPOSE: To input geometrical data to the aerodynamic links of the program.

METHOD: The geometrical data are read into the aerodynamic links of the program from binary scratch tapes generated in the geometry links. The format of the tape that transfers the panel geometry from the paneling links is described in Appendix D. The geometry of the isolated body is transferred from the transformation links. The format of this tape is given in Appendix D.

USAGE: CALL INTAPE

COMMON DATE (2), NTAPEA, NTAPEB, NTAPEC, NTAPED, NTAPEE, NTAPEF, NTAPEI, NTAPEO, NBODY, NWING, XMACH, SYM, KACE

COMMON/BLOCK/ALPHAS (210), AREA (210), A (210), ALPHAC (110), ALPHAT (110), CHORD (210), ISYM, NPART (210), NPANEL, NROW (2), THETA (210), TAIL, U (210), V (210), VPM (210), VV (210), VPMM (210), W (210), WPM (210), WW (210), WPMM (210)

DIMENSION X (210, 3, 4), XBAR (210), XC (210), Y (210, 3, 4), YBAR (210), YC (210), Z (210, 3, 4), ZBAR (210), ZC (210)

Input: NBODY = Number of body panels.

NWING = Number of wing panels.

NTAPEB = Logical tape number from which isolated body geometry data is read.

NTAPEC = Logical tape number from which panel geometry data is read and on which panel geometry data is rewritten in a different format for use in the aerodynamics links.

NTAPED = Logical tape number from which additional isolated body geometry data is read.

SUBPROGRAM:

CALLED: None

ERROR RETURNS: None

RESTRICTIONS:

$NBODY \leq 100$

$NWING \leq 110$

STORAGE:

$1260_{10} = 2354_8$

SUBJECT: **FORTRAN IV Subroutine INTPOL**

PURPOSE: The drag of an individual panel may be obtained by multiplying the panel pressure by the product of the average downwash over the panel and the area. The program calculates panel pressure and downwash (n_1) at the control point. As the control point is normally located at 95 percent of the panel chord, the downwash at this point is often greater than the average downwash of the panel. Thus it is necessary to interpolate for the average downwash of the panel in calculating the drag.

METHOD: For the first panel of any chordwise column, the average downwash is obtained by a linear extrapolation of the downwash at the control points of the first two panels.

$$\bar{n}_1 = n_1 + \frac{(\bar{R} - R) (n_2 - n_1)}{1 + R \left(\frac{C_2}{C_1} - 1 \right)}$$

where R = The location of the control point as a fraction of the local panel chord.

\bar{R} = The location of the point as a fraction of the local panel chord at which the downwash used in drag calculations is to be found.

C = The local chord length of the panels.

For the remainder of the panels in any chordwise column of panels, the downwash is obtained by a linear interpolation of the downwash of the adjacent panels.

$$\bar{n}_i = n_i + \frac{C_i}{C_{i-1}} \frac{(\bar{R} - R) (n_i - n_{i-1})}{1 + R \left(\frac{C_i}{C_{i-1}} - 1 \right)}$$

USAGE: **CALL INTPOL (NM, NROW, RATIOX, RATIOD, CHORD, ALPHAM, ALPHAD)**

DIMENSION **CHORD(NM), ALPHAM(NM), ALPHAD(NM)**

Input: **NM** = Total number of panels on wing or body.

NROW = Number of panels in a chordwise column.

RATIOX = Location of the control point as a fraction of the local panel chord.

RATIOD = Location of the point as a fraction of the local panel chord at which the downwash is to be found.

CHORD = Array of the local chord lengths of the panels.

ALPHAM = Array of panel downwash at the control point locations.

Output: **ALPHAD** = Array of interpolated panel downwash values.

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $177_{10} = 261_8$

SUBJECT: FORTRAN IV Function INTURP

PURPOSE: To read and write a data card, then find which word in a given table is the same as the first word in the data card.

METHOD: Let LI be the input tape and LO the output tape. INTURP reads the next data card on LI with FORMAT (13A6, A2). If LO > 0, the contents of the card are written on LO with FORMAT (1H0,14A6). A fixed-point comparison is made between the first word on the card and each word in the table until a match is found or the end of the table is reached. The function value returned is the position in the table that matched the first word in the data card, or else zero if no match was found.

USAGE: DIMENSION T(N)
K = INTURP (T, N, LI, LO)
T = Table.
N = Number of words in T.
LI = Input tape.
LO = Output tape.
K = Function value.

EXAMPLE: A data deck might have three types of data cards, each group with a header card having a code word in the first six columns, and perhaps comments in the remaining columns. Assume the code words are BODY, WING, and DEFINE. A portion of the program could be written as follows:

```

DIMENSION T(3)
DATA T/4HBODY, 4HWING, 6HDEFINE/

10  K = INTURP (T, 3, 5, 6)
    IF (K) 10, 10, 20
20  GO TO (100, 200, 300), K

```

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $98_{10} = 142_8$

SUBJECT: FORTRAN IV Subroutine INVBB

PURPOSE: For the wing-body case, to preprocess the aerodynamic influence coefficients matrix.

$$\begin{bmatrix} A_{BB} & A_{BW} \\ A_{WB} & A_{WW} \end{bmatrix}$$

where

A_{BB} = The influence on the body due to the body

A_{WB} = The influence on the wing due to the body

A_{BW} = The influence on the body due to the wing

A_{WW} = The influence on the wing due to the wing

by inverting A_{BB} and partitioning A_{WB} in preparation for reduction of the matrix (subroutine REDUCE).

METHOD: The portion of the aerodynamic influence coefficients resulting from the influence of the body is read from logical tape NTAPEA by columns into core. A_{WB} is written immediately on logical tape NTAPED. A_{BB} is inverted in core by the single precision inversion subroutine SINVRT. The matrix inverse is then stored on NTAPED behind A_{WB} . Both matrices are written by columns as a logical record. Logical tape NTAPED is rewound and NTAPEA is left at the position of the last read instruction.

USAGE: CALL INVBB

COMMON DATE(2), NTAPEA, NTAPEB, NTAPEC,
NTAPED, NTAPEE, NTAPEF, NTAPEI, NTAPEO, NBODY,
NWING, XMACH, SYM, KACE

DIMENSION ABB(115, 115), AWB(110)

Input: NTAPEA = Logical number of scratch tape.
NTAPED = Logical number of scratch tape.
NTAPEO = Logical number of output tape.
NBODY = Number of body panels.
NWING = Number of wing panels.
A = Aerodynamic influence coefficients matrix on logical tape NTAPEA.

Output: AWB

= Partition of the aerodynamic influence coefficients matrix resulting from the influence of the body on the wing written on logical tape NTAPED.

ABB⁻¹

= Inverse of the partition of the aerodynamic influence coefficients matrix resulting from the influence of the body on the body written on logical tape NTAPED.

SUBPROGRAM

CALLED:

SINVRT (see Appendix B)

ERROR RETURNS:

If an error occurs in the inversion of the matrix, the message "ERROR IN INVERSION OF BODY MATRIX" will be written on the output tape. The values for IRR1, IRR2, and SCALE returned by subroutine SINVRT are also written on the output tape.

RESTRICTIONS:

The matrix to be inverted must not exceed the order 110.

STORAGE:

$13566_{10} = 32402_8$

SUBJECT: FORTRAN IV Subroutine INVRW

PURPOSE: For the wing-body case, to invert the reduced aerodynamic influence coefficients matrix.

METHOD: The reduced aerodynamic influence coefficients matrix is read from logical tape NTAPEE into core. The matrix is inverted in core by the single-precision inversion subroutine SINVRT. The matrix inverse is then stored on logical tape NTAPEE behind original matrix with an end-of-file separating the two matrices. An end-of-file is also written after the inverted matrix. The tape is then rewound.

USAGE: CALL INVRW

COMMON DATE(2), NTAPEA, NTAPEB, NTAPEC,
NTAPED, NTAPEE, NTAPEF, NTAPEI,
NTAPEO, NBODY, NWING, XMACH, SYM,
KACE

DIMENSION ARWW(115, 115)

Input: NTAPEE = Logical number of scratch tape.
NWING = Number of wing panels.
ARWW = Reduced aerodynamic influence coefficients matrix.

Output: ARWW⁻¹ = Inverse of the reduced aerodynamic influence coefficients matrix.

SUBPROGRAM CALLED: SINVRT (see Appendix B)

ERROR RETURNS: If an error occurs in the inversion of the matrix, the message "ERROR IN INVERSION OF REDUCED MATRIX" will be written on the output tape. The values of IRR1, IRR2, and SCALE returned by subroutine SINVRT are also written on the output tape.

RESTRICTIONS: The matrix to be inverted must not exceed the order 110.

STORAGE: $13427_{10} = 32163_8$

SUBJECT: FORTRAN IV Subroutine INVW

PURPOSE: For the wing-alone case, to invert the aerodynamic influence coefficients matrix and to store both the matrix and its inverse on a scratch tape.

METHOD: The aerodynamic influence coefficients matrix previously computed is read from logical tape NTAPEA into core and simultaneously stored on logical tape NTAPEE, where NTAPEA and NTAPEE are logical tape numbers of scratch tapes stored in COMMON. The matrix in core is inverted by a single precision inversion Subroutine SINVRT. The inverse is stored behind the original matrix on logical tape NTAPEE with an end-of-file mark separating the two matrices. An end-of-file mark is also written after the inverted matrix. Both tapes are then rewound.

USAGE: CALL INVW

COMMON DATE(2), NTAPEA, NTAPEB, NTAPEC,
NTAPED, NTAPEE, NTAPEF, NTAPEI,
NTAPEO, NBODY, NWING, XMACH, SYM,
KACE

DIMENSION AWW(115, 115)

Input: AWW = Aerodynamic influence coefficients
matrix on logical tape NTAPEA.

Output: AWW = Aerodynamic influence coefficients
matrix written on logical tape NTAPEE.

AWW^{-1} = Inverse aerodynamic influence coefficients matrix written on logical tape NTAPEE.

SUBPROGRAM CALLED: SINVRT (See Appendix B)

ERROR RETURNS: If an error occurs in the inversion of the matrix the message ERROR IN INVERSION OF WING ONLY MATRIX will be written on the output tape. The values for IRR1, IRR2, and SCALE as returned by subroutine SINVRT are also written on the output tape.

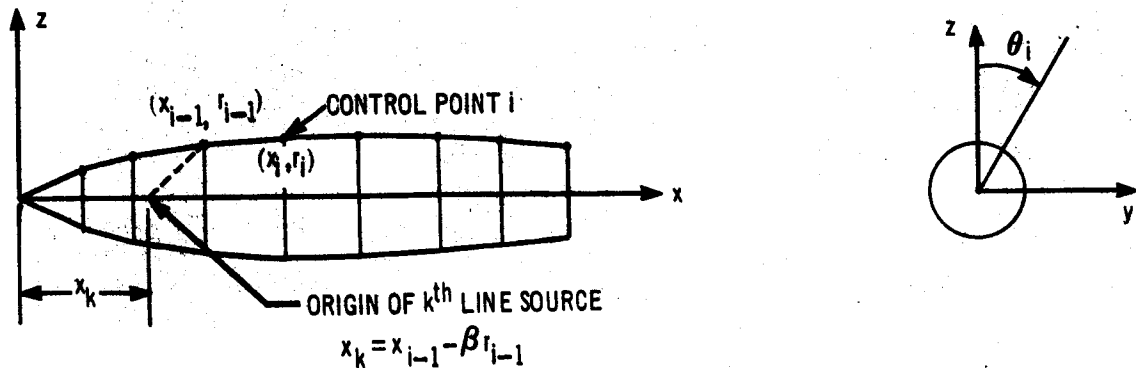
RESTRICTIONS: The matrix must not exceed the order 110.

STORAGE: $13467_{10} = 32233_8$

SUBJECT: FORTRAN IV Subroutine KARMOR

PURPOSE: For the isolated body, to compute the velocity components and the resulting pressures, forces, and moments induced by the body sources and doublets.

METHOD: The body, considered to be made up of a series of K parabolic arcs, is defined by a radius r and camber Δz at each body station x along the body axis.



A linearly varying source is placed at the nose of the body ($i = 1$) to give the proper conical tip. The strength of this source is determined by the tangency condition at the nose:

$$T_{S1} = \frac{\tan \delta}{\sqrt{\cot^2 \delta - \beta^2} + \tan \delta \cosh^{-1} \left(\frac{\cot \delta}{\beta} \right)}$$

where δ is the semi-vertex of the nose.

A quadratically varying source, also placed at the nose, satisfies the boundary condition at $i = 1$:

$$a_{BBS1} T_{S1} + a_{BBS2_{11}} T_{S2_1} = \left(\frac{dr}{dx} \right)_1 \left[1 + u_{BBS1} T_{S1} + u_{BBS2_{11}} T_{S2_1} \right]$$

which yields:

$$T_{S2_1} = \frac{\left(\frac{dr}{dx} \right)_1 - \left[a_{BBS1} - \left(\frac{dr}{dx} \right)_1 u_{BBS1} \right] T_{S1}}{a_{BBS2_{11}} - \left(\frac{dr}{dx} \right)_1 u_{BBS2_{11}}}$$

where

$$a_{BBS1_{ik}} = \frac{\sqrt{(x_i - x_k)^2 - \beta^2 r_i^2}}{r_i}$$

$$a_{BBS2_{ik}} = \frac{1}{r_i} \left\{ (x_i - x_k) \sqrt{(x_i - x_k)^2 - \beta^2 r_i^2} - \beta^2 r_i^2 \cosh^{-1} \frac{x_i - x_k}{\beta r_i} \right\}$$

$$u_{BBS1_{ik}} = - \cosh^{-1} \frac{x_i - x_k}{\beta r_i}$$

$$u_{BBS2_{ik}} = 2 \sqrt{(x_i - x_k)^2 - \beta^2 r_i^2} - 2 (x_i - x_k) \cosh^{-1} \frac{x_i - x_k}{\beta r_i}$$

$$r_i = \sqrt{y_i^2 + z_i^2}$$

In general, the strength of the quadratically varying source of the i th segment is given by:

$$TS2_i = \frac{\left(\frac{dr}{dx} \right)_i \left[a_{BBS1_{i1}} - \left(\frac{dr}{dx} \right)_i u_{BBS1_{i1}} \right] TS1 - \sum_{k=1}^{i-1} \left[a_{BBS2_{ik}} - \left(\frac{dr}{dx} \right)_i u_{BBS2_{ik}} \right] TS2_k}{a_{BBS2_{ii}} - \left(\frac{dr}{dx} \right)_i u_{BBS2_{ii}}}$$

The end of a closing body presents a special problem since the influence coefficients cannot be evaluated on the axis. The boundary condition on the net source strength at the end of a closing body must be used. The manner in which the strength of the source varies along the axis and the strengths of the previously evaluated sources are known. Therefore, at the end of a closing body, $i = \text{NBODYYS}$ and $r_i = 0$:

$$(x_{\text{NBODYYS}} - x_1) T_{S1} + \sum_{k=1}^{\text{NBODYYS}} (x_{\text{NBODYYS}} - x_k)^2 T_{S2_k} = 0$$

which yields:

$$T_{S2_{\text{NBODYYS}}} = \frac{-(x_{\text{NBODYYS}} - x_1) T_{S1} - \sum_{k=1}^{\text{NBODYYS}-1} (x_{\text{NBODYYS}} - x_k)^2 T_{S2_k}}{\left[x_{\text{NBODYYS}} - (x - \beta r)_{\text{NBODYYS}-1} \right]^2}$$

It should be noted that the k^{th} line source is located at the distance:

$$x_k = x_{i-1} - \beta r_{i-1}$$

from the nose of the body.

The strengths of the doublets are determined in a similar manner. In terms of the aerodynamic influence coefficients, the boundary condition is written:

$$\left(\frac{dr}{dx} \right)_i \left[u_{\text{BBD1}_{i1}} T_{D1} + \sum_{k=1}^K u_{\text{BBD2}_{ik}} T_{D2_k} \right] =$$

$$a_{\text{BBD1}_{i1}} T_{D1} + \sum_{k=1}^K a_{\text{BBD2}_{ik}} T_{D2_k} + \left(\alpha - \frac{dz_c}{dx} \right)_i \cos \theta_i$$

where $(\alpha - \frac{dz}{dx})$ is the local angle-of-attack, and

$$a_{BBD1_{ik}} = \frac{\cos \theta_i}{2r_i^2} \left\{ \beta^2 r_i^2 \cosh^{-1} \frac{x_i - x_k}{\beta r_i} \right. \\ \left. + (x_i - x_k) \sqrt{(x_i - x_k)^2 - \beta^2 r_i^2} \right\}$$

$$a_{BBD2_{ik}} = -\frac{\cos \theta_i}{r_i^2} \left\{ \left[\frac{(x_i - x_k)^2 - 4\beta^2 r_i^2}{3} \right] \right.$$

$$\left. \sqrt{(x_i - x_k)^2 - \beta^2 r_i^2} + (x_i - x_k) \beta^2 r_i^2 \cosh^{-1} \frac{x_i - x_k}{\beta r_i} \right\}$$

$$u_{BBD1_{ik}} = \frac{\cos \theta_i}{r_i} \sqrt{(x_i - x_k)^2 - \beta^2 r_i^2}$$

$$u_{BBD2_{ik}} = \frac{\cos \theta_i}{r_i} \left\{ (x_i - x_k) \sqrt{(x_i - x_k)^2 - \beta^2 r_i^2} \right. \\ \left. - \beta^2 r_i^2 \cosh^{-1} \frac{x_i - x_k}{\beta r_i} \right\}$$

Since both $u_{BBD_{ik}}$ and $a_{BBD_{ik}}$ are functions of $\cos \theta_i$, these two terms are redefined

$$u'_{BBD_{ik}} = u_{BBD_{ik}} / \cos \theta_i$$

$$a'_{BBD_{ik}} = a_{BBD_{ik}} / \cos \theta_i$$

and

$$\left(\alpha - \frac{dz_c}{dx} \right)_1 = - \left[a'_{BBD1_{11}} - \left(\frac{dr}{dx} \right)_1 u'_{BBD1_{11}} \right] T_{D1} -$$

$$\sum_{k=1}^K \left[a'_{BBD2_{ik}} - \left(\frac{dr}{dx} \right)_i u'_{BBD2_{ik}} \right] T_{D2_k}$$

Again, a linearly varying doublet is placed at the nose of the body, the strength of which is given by:

$$T_{D1} = \frac{- \left(\alpha - \frac{dz_c}{dx} \right)_{\text{nose}}}{\frac{\beta}{2} \left[\sqrt{\cot^2 \delta - \beta^2} + \beta \cosh^{-1} \left(\frac{\cot \delta}{\beta} \right) + \tan \delta \left(\sqrt{\cot^2 \delta - \beta^2} \right) \right]}$$

A quadratically varying doublet is also placed at the nose

$$T_{D2_1} = \frac{- \left(\alpha - \frac{dz_c}{dx} \right)_1 + \left[a'_{BBD1_{11}} - \left(\frac{dr}{dx} \right)_1 u'_{BBD1_{11}} \right] T_{D1}}{a'_{BBD2_{11}} - \left(\frac{dr}{dx} \right)_1 u'_{BBD2_{11}}}$$

and at all subsequent body stations

$$T_{D2_i} = \frac{-\left(\alpha - \frac{dz_c}{dx}\right)_i + \left[a'_{BBD1_{i1}} - \left(\frac{dr}{dx}\right)_i u'_{BBD1_{i1}} \right] T_{D1} + \sum_{k=1}^{i-1} \left[a'_{BBD2_{ik}} - \left(\frac{dr}{dx}\right)_i u'_{BBD2_{ik}} \right] T_{D2_k}}{a'_{BBD2_{ii}} - \left(\frac{dr}{dx}\right)_i u'_{BBD2_{ii}}}$$

At the end of a closing body, a quadratically varying doublet is defined:

$$T_{D2_{NBODYYS}} = \frac{-\left(x_{NBODYYS} - x_1\right) T_{D1} - \sum_{k=1}^{NBODYYS-1} \left(x_{NBODYYS} - x_k\right)^2 T_{D2_k}}{\left[x_{NBODYYS} - (x - \beta r)_{NBODYYS-1}\right]^2}$$

The pressure coefficients on the body due to the line sources and doublets are calculated using one of three formulas (as specified by an input).

For the linear pressure coefficient,

$$C_p = -2u_{B_i};$$

for the nonlinear pressure coefficient,

$$C_p = -2u_{B_i} + \beta^2 u_{B_i}^2 - v_{r_{B_i}}^2 - v_{\theta_{B_i}}^2$$

and for the "exact" isentropic pressure coefficient,

$$C_p = \frac{2}{\gamma M^2} \left\{ \left[1 - \frac{\gamma-1}{2} M^2 \left(2u_{B_i}^2 + u_{B_i}^2 + v_{r_{B_i}}^2 + v_{\theta_{B_i}}^2 \right) \right]^{\frac{\gamma}{\gamma-1}} - 1 \right\}$$

where

$$u_{B_i} = u_{BBS1_{i1}} T_{S1} + \sum_{k=1}^K u_{BBS2_{ik}} T_{S_k} + u_{BBD1_{i1}} T_{D1} +$$

$$\sum_{k=1}^K u_{BBD2_{ik}} T_{D_k}$$

$$v_{r_{B_i}} = v_{r_{BBS1_{i1}}} T_{S1} + \sum_{k=1}^K v_{r_{BBS2_{ik}}} T_{S_k} + v_{r_{BBD1_{i1}}} T_{D1} +$$

$$\sum_{k=1}^K v_{r_{BBD2_{ik}}} T_{D_k}$$

$$v_{\theta_{B_i}} = v_{\theta_{BBS1_{i1}}} T_{S1} + \sum_{k=1}^K v_{\theta_{BBS2_{ik}}} T_{S_k} + v_{\theta_{BBD1_{i1}}} T_{D1} +$$

$$\sum_{k=1}^K v_{\theta_{BBD2_{ik}}} T_{D_k}$$

and

$$\beta = M^2 - 1$$

$$\gamma = 1.4$$

The lift, drag, and pitching moments on the body due to the line sources and doublets are calculated neglecting any interference effects from the wing. Such interference terms are added later. These forces are determined by integrating the pressures over the body. It is convenient to resolve the aerodynamic forces acting on a body into an axial force X, a normal force N, and a pitching moment M about the nose. The corresponding dimensionless coefficients are given by:

$$C_{X_B} = \frac{X}{qS} = \frac{1}{S} \int_0^1 r \cdot \frac{dr}{dx} \int_0^{2\pi} C_p d\theta dx ;$$

$$C_{N_B} = \frac{N}{qS} = \frac{1}{S} \int_0^1 r \int_0^{2\pi} C_p \cos \theta d\theta dx;$$

$$C_{M_{B_0}} = \frac{M}{qS\bar{c}} = \frac{1}{S\bar{c}} \int_0^1 x \cdot r \int_0^{2\pi} C_p \cos \theta d\theta dx.$$

These coefficients are evaluated in subroutine COEFS using a numerical integration technique.

The total lift, drag, and pitching moments about an arbitrary point are obtained by an appropriate resolution of forces:

$$C_{L_B} = C_{N_B} \cos \alpha - C_{X_B} \sin \alpha$$

$$C_{D_B} = C_{N_B} \sin \alpha + C_{X_B} \cos \alpha$$

$$C_{M_B} = C_{M_{B_0}} + \bar{x} C_{N_B} - \bar{z} C_{X_B},$$

where the moments are computed about the point (\bar{x}, \bar{z}) , \bar{c} is the reference chord length, and S is the reference area. The forces and moments are computed for the half-body only.

USAGE:

CALL KARMOR (NBODYS, NTHETA, XN, YN, ZN, CPCALC, VOUT, ARA, XP, ZP, RFAREA, XB, R, THETAB, ZDELTA, XC, YC, ZC, THETA, U, VV, WW, AN1, CPB, BBCL, BBCD, BBCM)

COMMON DATE (2), NTAPEA, NTAPEB, NTAPEC, NTAPEB, NTAPEE, NTAPEF, NTAPEI, NTAPEO, NBODY, NWING, XMACH, SYM, KACE

DIMENSION XB (NBODYS), R (NBODYS), THETAB (NTHETA), ZDELTA (NBODYS), XC (NBODY + NWING), YC (NBODY + NWING), ZC (NBODY + NWING), THETA (NTHETA), U (NWING), VV (NWING), WW (NWING), AN1 (NWING), CPB (NBODYS, NTHETA)

Input: NBODYS = Number of body stations.
 NTHETA = Number of body meridian lines (or θ 's).
 XN }
 YN } = x-, y- and z-coordinates of body
 ZN } nose.
 CPCALC = Code.
 = 0., calculation of pressure coefficients
 to use linear equation.
 = 1., calculation of pressure coefficients
 to use nonlinear equation.
 = 2., calculation of pressure coefficients
 to use "exact" isentropic equation.
 VOUT = Code.
 = 0., velocity components are not to be
 printed.
 = 1., velocity components are to be
 printed.
 ARA = Angle-of-attack of body with respect
 to freestream.
 XP }
 ZP } = x- and z-coordinates of point about
 which pitching moments are to be
 computed.
 RFAREA = Reference area.
 XB = Array of x-coordinates of body stations.
 R = Array of body radii at body stations.
 THETAB = Array of θ -angles of body meridian
 lines.
 ZDELTA = Array of body cambers at body station
 XC = Array of panel control point
 x-coordinates.
 YC = Array of panel control point
 y-coordinates.
 ZC = Array of panel control point
 z-coordinates.
 THETA = Scratch array.
 NBODY = Number of body panels.
 NWING = Number of wing panels.
 XMACH = Mach number.
 U = Array of x-components of velocity on
 the wing panels due to the body sources
 and doublets.
 VV = Array of y-components of velocity on
 the wing panels due to the body sources
 and doublets.
 WW = Array of z-components of velocity on
 the wing panels due to the body sources
 and doublets.
 AN1 = Array of normal components of velocity
 on the wing panels due to the body
 sources and doublets.
 CPB = Array of pressure coefficients.
 BBCL = Lift of the body.

BBCD = Drag of the body.
 BBCM = Pitching moment of the body.

SUBPROGRAMS CALLED: ALOG
 SQRT
 COS
 SIN
 ATN1
 FSF
 DERIVS
 COEFS

} = (Built-in functions)

ERROR RETURNS: None

RESTRICTIONS: NBODYS \leq 55
 NBODY \leq 100
 NWING \leq 110

STORAGE: $5163_{10} = 12053_8$

SUBJECT: FORTRAN IV Subroutine LACKEY

PURPOSE: Computes perturbation velocities and pressure coefficients at field points due to sources and vortices on the wings and due to vortices on the bodies. When required, the freestream velocity components are added to the results to yield the total velocity at the field point. The user selects the pressure coefficient calculation equations from among linear, nonlinear, or "exact" isentropic.

METHOD: This subroutine calls EVAL1, and VEL1 to compute the perturbation velocities. The pressure coefficient is then computed from the appropriate equation.

Linear: $C_p = -2u$

Nonlinear: $C_p = -2u + \beta^2 u^2 - v^2 - w^2$

Exact Isentropic: $C_p = \frac{1.42857}{M^2} \left\{ \left[1 + 2 M^2 (1 - Q^2) \right]^{\frac{7}{2}} - 1 \right\}$

where

u = velocity component in the x-direction.

v = velocity component in the y-direction.

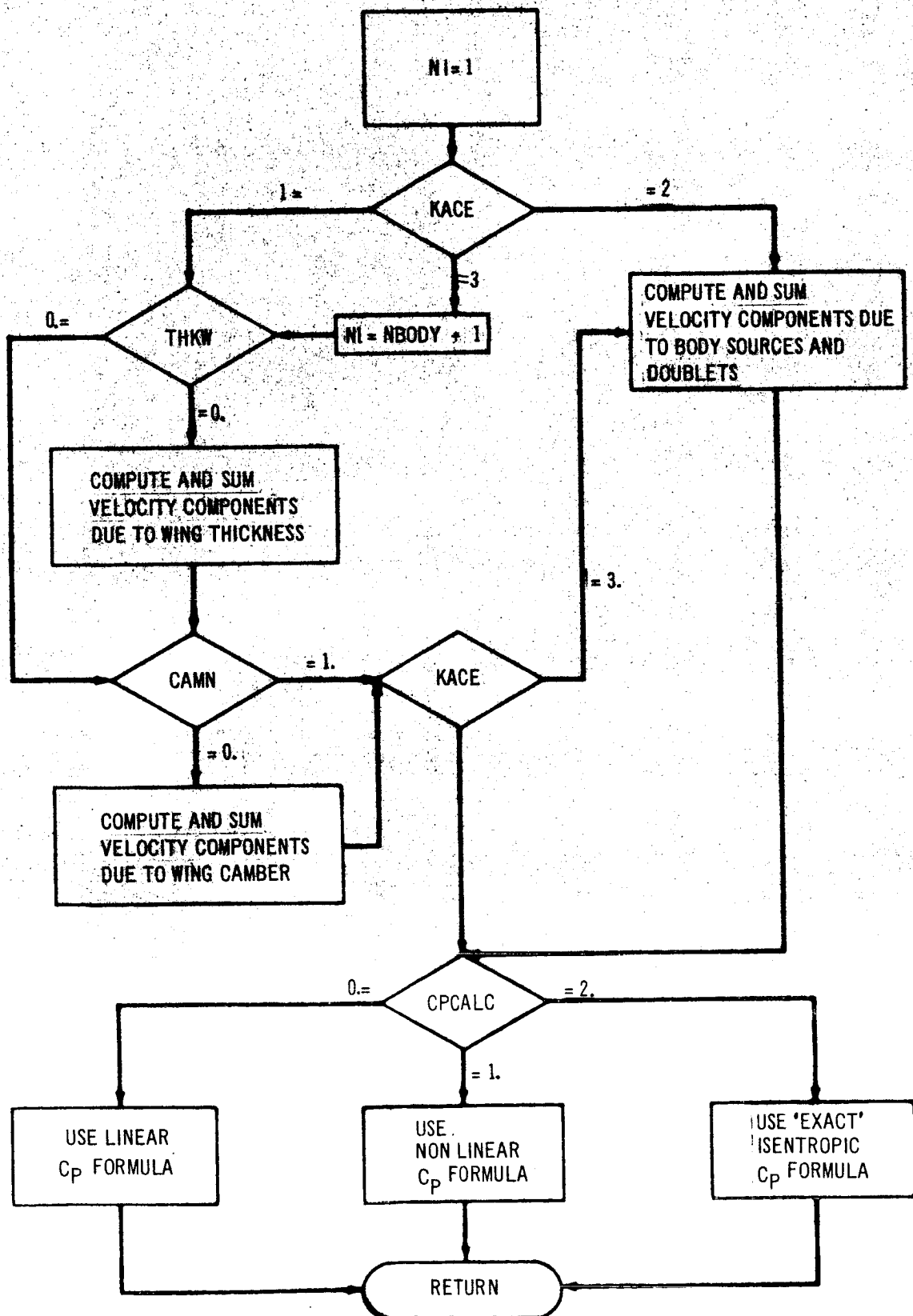
w = velocity component in the z-direction.

M = Mach number.

α = angle of attack.

$$Q^2 = (u + \cos \alpha)^2 + v^2 + (w + \sin \alpha)^2$$

A flow chart of the routine follows.



USAGE:

COMMON/THICK/THKW, ARA, CPCALC, CAMN, POP
COMMON/FLOV1/KACE, NBODY, DUM (5), XMACH
COMMON/FLOV5/N1, N2, N3, N4
CALL LACKEY (ISTR, XB, YB, ZB, U, V, W, CP)

Input: THKW = 1. indicates a thick wing.
 = 0. camber only.

ARA = angle of attack in radians.

CPCALC = 0. linear equations used for C.
 1. nonlinear equations used for C.
 2. "exact" isentropic equations
 used for C.

CAMN = 0. indicates velocity components
 due to camber to be computed.
 = 1. indicates velocity components
 due to camber not to be computed.

KACE = 1 wing alone.
 = 2 body alone.
 = 3 wing and body.

NBODY = number of vortex panels on body.

XMACH = Mach number.

XB = x-coordinate of field point.

YB = y-coordinate of field point.

ZB = z-coordinate of field point.

ISTR = 1. indicates freestream velocity
 to be added to velocity components.
 = 0. indicates freestream velocity
 not to be added at field point.

N1	}	= 4 logical tape numbers on which velocity components due to the various singularities are written for use by FLOOUT.
N2		
N3		
N4		

Output:	U	= x-direction velocity component.
	V	= y-direction velocity component.
	W	= z-direction velocity component.
	CP	= C_p at field point.

SUBPROGRAMS

CALLED:	EVAL1
	VEL1

ERROR RETURN:	None
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RESTRICTIONS:	None
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STORAGE:	$428_{10} = 654_8$
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SUBJECT: MAP Function LOC

PURPOSE: To determine the absolute machine address of a variable or first location of an array. This routine is used only in the streamline integration package by DEDIS.

METHOD: Using machine hardware instructions and standard system conventions, the address of the argument is returned in the AC to the calling program.

USAGE: INTEGER VARADD

VARADD = LOC (VAR)

Input: VAR = any array or variable name.

Output: VARADD = contains the address of VAR.

SUBPROGRAMS CALLED: None

RESTRICTIONS: None

STORAGE: $4_{10} = 4_8$

SUBJECT: FORTRAN IV Subroutine MDMATE

PURPOSE: To compute the matrix resulting from the application of the Lagrange multipliers technique in minimizing the drag for given wing constraints.

METHOD: The minimum drag of a wing in the presence of a body for given wing C_L and pitching moment may be determined by applying the method of Lagrange multipliers to the system of equations defining the drag. A function F is defined in terms of the pressure difference of the wing panels, p_{W_i} , and the auxiliary variables (Lagrange multipliers) λ_1 and λ_2 .

$$F = D + \lambda_1 (L - \bar{L}) + \lambda_2 (M - \bar{M})$$

The condition for minimum drag for the constraints that $L = \bar{L}$ and $M = \bar{M}$ is found by setting the partial derivatives of F with respect to the variable p_{W_i} , λ_1 , and λ_2 equal to zero. The result is the following system of linear equations, and the pressure difference across the wing panels may now be determined for minimum drag.

$$\begin{bmatrix} -2A_1 a_{11} & -(A_1 a_{12} + A_2 a_{21}) & \dots & -A_1 & -x_1 A_1 \\ -(A_2 a_{21} + A_1 a_{12}) & & & -A_2 & . \\ . & & & . & . \\ . & & & . & . \\ . & & & -A_N - x_N A_N & . \\ -A_1 & . & -A_N & 0 & 0 \\ -x_1 A_1 & . & -x_1 A_N & 0 & 0 \end{bmatrix} \cdot \begin{Bmatrix} p_{W_1} \\ p_{W_2} \\ . \\ . \\ p_{W_N} \\ \lambda_1 \\ \lambda_2 \end{Bmatrix} = \begin{Bmatrix} A_1(\bar{n}_1 + \bar{n}_{B_1}) \\ A_2(\bar{n}_2 + \bar{n}_{B_2}) \\ . \\ . \\ A_N(\bar{n}_N + \bar{n}_{B_N}) \\ \bar{L} \\ \bar{M} \end{Bmatrix}$$

where \bar{n}_i = The downwash on the wing due to the body sources.

\bar{n}_{B_i} = The downwash on the wing resulting from the cancelation of normal velocity on the body due to the wing thickness.

If only the lift is constrained, the row and column of the matrix corresponding to λ_2 are omitted and p_{W_i} is found by inverting as before.

In this subroutine, the coefficients of the system of equations are computed and the inverses for the two cases are stored on a scratch tape in preparation for wing optimization by a later link. The matrices are stored with an end-of-file mark separating them.

USAGE:

CALL MDMATE

COMMON DATE(2), NTAPEA, NTAPEB, NTAPEC,
NTAPED, NTAPEE, NTAPEF, NTAPEI, NTAPEO,
NBODY, NWING, XMACH, SYM, KACE

DIMENSION WW(115, 115), XBAR(210), AREA(210)

Input: XBAR = Array of panel centroid x-coordinates.

AREA = Array of panel areas.

NBODY = Number of body panels.

NWING = Number of wing panels.

WW = Reduced matrix of the aerodynamic influence coefficients.

NTAPEE = Logical tape number from which the reduced matrix of the aerodynamic influence coefficients is read.

NTAPEA = Logical tape number on which the drag minimization matrices is stored.

Output: WW = Drag minimization matrix written on NTAPEA.

WW^{-1} = Inverse of the drag minimization matrix constrained for wing lift written on NTAPEA.

WW^{-1} = Inverse of the drag minimization matrix constrained for wing lift and pitching moment written on NTAPEA.

SUBPROGRAM

CALLED:

SINVRT (see Appendix B)

ERROR RETURNS:

If an error occurs in the inversion of the matrix, a message will be written on the output tape "ERROR IN INVERSION OF DRAG MINIMIZATION MATRIX" followed by the error codes from subroutine SINVRT.

RESTRICTIONS: The matrix to be inverted must not exceed the order 112.

STORAGE: $14218_{10} = 33612_8$

SUBJECT: FORTRAN IV Subroutine MEAN

PURPOSE: To smooth a set of data points defining a single-valued function of one variable.

METHOD: A sliding operation that deals with four points at a time $((x_i, y_i), i = 1, 2, 3, 4)$ is employed. Points whose ordinates may be changed are the interior two points at each setting of the operation. The abscissae of the input points are not changed. A straight line is drawn from (x_1, y_1) to (x_3, y_3) and another straight line from (x_2, y_2) to (x_4, y_4) . If the abscissa of the intersection of these two lines lies in the interval (x_2, x_3) , then the points are left as is, and the operation slides over one point and begins anew. If the lines are parallel or if the abscissa of the intersection is outside (x_2, x_3) , then new ordinates y_2 and y_3 are calculated. An ordinate on the first line is evaluated at the abscissa x_2 ; similarly an ordinate on the second line is evaluated at the abscissa x_3 . The new values y_2 and y_3 are the mean values of the original ordinates and new ordinates so calculated.

This operation slides along the set of points until all interior points have been subjected to smoothing. Five such passes made over the curve at each call of MEAN.

USAGE: CALL MEAN (X, Y, N)

Input: X = Array of abscissae; a strictly monotone sequence
Y = Array of ordinates to be smoothed
N = Number of points

Output: Y = Smoothed ordinates (the first and last points are not subjected to smoothing)

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: The abscissae must be strictly monotonic; thus vertical slopes are excluded.

STORAGE: $163_{10} = 243_8$

SUBJECT: FORTRAN IV Function MERR

PURPOSE: To write error messages for subroutines in the geometric definition portion of the program.

METHOD: An error array NU is given. NU(1) is an error code that should be the same as a given success code IOK if an error condition does not exist. NU(2), if greater than zero, is the number of an output tape on which an error message can be written. NU(3) is an error message limiter; a message is not to be written unless NU(3) is greater than 1. M is an error message number.

If NU(1) = IOK, the function value (K) is set to zero, and no further action is necessary. Otherwise, NU(3) is decreased by 1; then if NU(2) ≤ 0 or if NU(3) ≤ 0 , K is set to -1 and return is made to the calling program. Otherwise, the following message is written:

"ERROR i, CODE j, IN SUBROUTINE xxxxxx DURING GEOMETRIC DEFINITION"

where i = M, j = NU(1), and xxxxxx is the given name of the subroutine in which the error occurred.

USAGE: DIMENSION NU(3)

K = MERR (NU, IOK, M, SR)

Input: NU = Error array.

IOK = Success code.

M = Error message number.

SR = Subroutine name (alphanumeric).

Output: Message on error tape.

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $87_{10} = 127_8$

SUBJECT: FORTRAN IV Function NWEED

PURPOSE: To remove excess points from an array of points in m-space.

METHOD: Each point is compared with the previous point. If all corresponding coordinates are the same with given tolerances, that point is eliminated by shifting the balance of the array and reducing the number of points by 1. However, if the last point is too near its neighbor, the neighbor is discarded and the last point retained.

USAGE: DIMENSION A(M, N), EP(M)
 NN = NWEED (A, N, M, EP)

Input: A = Given array of points.
 N = Number of points in A.
 M = Space dimension.
 EP = Array of tolerances, one for each coordinate.

Output: A = Weeded array of points.
 NN = Number of points in the weeded array (NN may have the same storage location as N).

SUBPROGRAM
 CALLED: None

ERROR RETURNS: None

RESTRICTIONS: N > 1 and M > 0. If any EP(i) ≤ 0, no weeding will be done. For weeding only on selected coordinates, EP is set to some large value for the remaining coordinates.

STORAGE: 153₁₀ = 231₈

SUBJECT: **FORTTRAN IV Program OPCAM**

PURPOSE: To interpret data commands and control flow through the Program for Analysis and Design of Supersonic Wing-Body Combinations.

METHOD: The program first calls subroutine OPCAMI, which carries out the following operations: (1) assigns logical tape numbers to tape symbols (in COMMON); (2) obtains the data and places it in COMMON; (3) writes the program title on the output tape; (4) transfers the data cards to a scratch tape, which is then used as the input tape for the remainder of the program; (5) writes the data cards on the output tape.

Then function INTURP is used to read a data card, to write its contents on the output tape, and to see whether it is a command card. A command card has the words DEFINE, DEF1NE, PANEL, AERODY, ARE0DY, END OF or END OF in columns 1-6; the contents of the remaining columns are written on the output tape but are not otherwise used. If the data card is a command card, the appropriate action is taken; otherwise, successive cards are read until a command card is found (this feature permits the insertion of comment cards or blank cards immediately before any command card).

The command DEFINE (or DEF1NE) results in a call to subroutine GEOMD. On return, data cards are again read until a command card is encountered. If any GEOMD data cards were not read because of error, they will be listed by INTURP.

Subroutine TFLAT is called when a PANEL card is read. If TFLAT detects an error, it skips over data cards until the input tape is positioned just in front of a DEFINE or END OF card; OPCAM then goes on to process this card in the usual way. But if TFLAT signals success, then the argument NOBODY (set by TFLAT) is examined. If NOBODY = -1, meaning a body-alone case, OPCAM goes on to read the next data card; otherwise, OPCAM calls subroutine PANEL.

OPCAM calls subroutine AERO when an AERODY (or AER0DY) card is read. An END OF (or END OF) card results in program termination.

SUBPROGRAMS
CALLED:

AERO
CLOK
GEOMD
INTURP
TFLAT
PANEL
OPCAM1

ERROR RETURNS:

Program errors are dealt with in the program section where they occur.

RESTRICTIONS:

Each time that INTURP reads and writes a data card, OPCAM writes (on the same line, near the right margin) the word TIME followed by the time of day. The time of day is found by a subroutine CLOK. The basic program deck contains a dummy subroutine CLOK which merely returns blanks. A proper subroutine CLOK may replace the dummy at the installation where the program is used.

STORAGE:

$152_{10} = 230_8$

SUBJECT: FORTRAN IV Subroutine OPCAMI

PURPOSE: To perform initialization chores for the main program OPCAM.

METHOD: Tape symbols are assigned as follows:

<u>Symbol</u>	<u>Tape Number</u>	<u>Description</u>
LIN	5	System input tape.
LO	6	System output tape.
LI	9	Input tape used by remainder of program.
LA	1	Scratch tapes.
LB	2	
LC	3	
LD	4	
LE	7	
LF	8	

Subroutine DATE is called to obtain the date. A title is written on the output tape. Tape LI is rewound. Then all data cards are read with FORMAT(13A6, A2) from tape LIN, written on tape LO with FORMAT(1H 14A6), and written on tape LI with FORMAT(13A6, A2); the last data card is signaled by the word END OF or END 0F (in case the letter O is mistakenly keypunched as the number zero) in columns 1-6. Then an EOF is written on tape LI, and it is rewound.

USAGE: COMMON DAT(2), LA, LB, LC, LD, LE, LF, LI, LO
CALL OPCAMI

Output: DAT = Date (alphameric)

LA	} Scratch tape numbers.
LB	
LC	
LD	
LE	

LF = Scratch tape number.

LI = Input tape number.

LO = Output tape number.

SUBPROGRAM

CALLED: DATE

ERROR RETURNS: None

RESTRICTIONS: An END OF card must be placed at the end of the data deck. If the END OF card does not appear in the data deck, the job will be terminated by the EOF on the system input tape. If the END OF card is not the physically last card, only the data preceding it will be read by the remainder of the program.

STORAGE: $235_{10} = 353_8$

SUBJECT:FORTRAN IV Subroutine **OPTIM3****PURPOSE:**

Given four successive points on the graph of a function of a single variable, to generate additional points between one selected pair of the given points, the spacing of the additional points to be such that straight-line segments joining them will represent the given function with a prescribed maximum error.

METHOD

Four successive arguments x_i and their respective ordinates y_i are input to the subroutine, together with a tolerance z and integer k to indicate the interval (x_k, x_{k+1}) to consider. **OPTIM3** then generates the biquadratic interpolating function described in subroutine **BITURP**. This function is a linear combination of two quadratics on the interval (x_2, x_3) , hence it is there a cubic; on either of the other possible intervals it is a quadratic. In any case, the function has a continuous first derivative, unlike a Lagrangian interpolation polynomial of any order.

Having generated the interpolation function ϕ , **OPTIM3** computes its function value y , its slope S , and its radius of curvature R , all at some particular x (at x_k in the first instance). In a small neighborhood of (x, y) the function ϕ can be represented by a circular arc of radius R , tangent at (x, y) to ϕ . **OPTIM3** then computes the central angle of that arc so that the arc and its chord have a maximum separation, in the y -direction, of z . Then the x -component Δx of that chord is the distance from the current argument x to the next argument (unless x_{k+1} has been reached), and the process continues.

USAGE:**DIMENSION** $X(4), Y(4), A(200), B(200)$ **CALL** **OPTIM3** (X, Y, Z, A, B, K, L, M)

Input: X = Array of x -coordinates of given points.
 Y = Array of y -coordinates of given points.
 Z = Allowable tolerance (in y direction).
 K = Subscript of x at lower end of interval to be interpolated.

Output: A = Array of x -coordinates of interpolated points.
 $A(1) = X(K), A(2) = x$ of first interpolated point, etc.

B = Array of y-coordinates of interpolated points.
B(1) = Y(K), B(2) = y of first interpolated point, etc.

L = One more than the number of interpolated points generated by the routine.

M = Error indicator, which is 1 if success.

SUBPROGRAMS
CALLED:

ACOS }
ATAN } (Built-in functions)
COS }
SQRT }

ERROR RETURNS: M = 0 if X(1) = X(4); M = 2 if L = 200 and more points are needed.

RESTRICTIONS: The x_i must form a strictly monotonic sequence, though not necessarily equally spaced. Note that the A and B arrays contain the first given point, but not the last.

STORAGE: $594_{10} = 1122_8$

SUBJECT: FORTRAN IV Subroutine OPTMW

PURPOSE: For wing alone, to compute the pressure difference across wing panels for a wing optimized for minimum drag.

METHOD: The method is outlined in the description of subroutine MDMATE. From the matrix inverse computed in MDMATE, the following multiplication yields the pressure difference across the panels.

$$\begin{Bmatrix} p_{W_1} \\ p_{W_2} \\ \vdots \\ p_{W_N} \\ \lambda_1 \\ \lambda_2 \end{Bmatrix} = \begin{bmatrix} -2A_1 a_{11} & -(A_1 a_{12} + A_2 a_{21}) & \dots & -A_1 & -x_1 A_1 \\ -(A_2 a_{21} + A_1 a_{12}) & \cdot & & -A_2 & \cdot \\ \cdot & \cdot & & \cdot & \cdot \\ \cdot & \cdot & & \cdot & \cdot \\ \cdot & \cdot & & -A_N & -x_N A_N \\ -A_1 & \cdot & \cdot & -A_N & 0 & 0 \\ -x_1 A_1 & \cdot & \cdot & -x_1 A_N & 0 & 0 \end{bmatrix}^{-1} \begin{Bmatrix} 0 \\ 0 \\ \cdot \\ \cdot \\ 0 \\ \bar{L} \\ \bar{M} \end{Bmatrix}$$

If only the lift is constrained, the row and column of the matrix corresponding to λ_2 is omitted and p_{W_i} is found as before.

USAGE: CALL OPTMW(NW, NTAPEX, A, B, CONSNT, CLBAR, XCPBAR, RFAREA, AREA, CL)

DIMENSION A(1), B(1), AREA(1), CL(1)

Input: NW = Number of wing panels.

NTAPEX = Logical number of tape from which the inverse of the minimum drag matrix is read.

A = Dummy array used by the subroutine.

B = Dummy array used by the subroutine.

CONSNT = 0., indicates wing optimization for wing C_L constraint.

= 1., indicates wing optimization for wing C_L and pitching moment constraints.

CLBAR = Wing coefficient of lift constraint.

XCPBAR = x-coordinate of the wing center of pressure constraint.

RFAREA = Wing reference area.

AREA = Array of wing panel areas.

Output: CL = Array of the pressure difference across the wing panels optimized for minimum drag.

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $131_{10} = 203_8$

SUBJECT:

FORTRAN IV Subroutine OPTMWB

PURPOSE:

In the presence of a body, to compute the pressure difference across wing panels for a wing optimized for minimum drag.

METHOD:

The method is outlined in the description of subroutine MDMATE. From the matrix inverse computed in MDMATE the following multiplication is carried out yielding the pressure difference across the panels.

$$\begin{Bmatrix} p_{W1} \\ p_{W2} \\ \vdots \\ p_{WN} \\ \lambda_1 \\ \lambda_2 \end{Bmatrix} = \begin{bmatrix} -2A_1 a_{11} & -(A_1 a_{12} + A_2 a_{21}) & \dots & -A_1 & -x_1 A_1 \\ -(A_2 a_{21} + A_1 a_{12}) & & & -A_2 & \cdot \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ \vdots & \vdots & \vdots & -A_N & x_N A_N \\ -A_1 & \cdot & -A_N & 0 & 0 \\ -x_1 A_1 & \cdot & -x_1 A_N & 0 & 0 \end{bmatrix}^{-1} \begin{Bmatrix} A_1(\bar{n}_1 + \bar{n}_{B1}) \\ A_2(\bar{n}_2 + \bar{n}_{B2}) \\ \vdots \\ A_N(\bar{n}_N + \bar{n}_{BN}) \\ \bar{L} \\ \bar{M} \end{Bmatrix}$$

where \bar{n}_i = The downwash on the wing due to body sources
sources
NBODY

$n_{B_i} = \sum_{j=1}^{NBODY} D_{ij} \cdot (-n_{B_j})$ is the downwash on the wing due to the cancellation of the normal velocity on the body due to wing thickness.

D_{ij} = The interference influence coefficients matrix.

n_{B_j} = Downwash on the body due to wing sources

$\bar{L} = C_L \cdot S_W$ is the lift constraint

$\bar{M} = \bar{X} \cdot \bar{C}_L \cdot S_W$ is the pitching moment constraint

If only the lift is constrained, the row and column of the matrix corresponding to λ_2 is omitted and p_{W_i} is found as before.

CALL OPTMWB(NW, NB, NTAPEX, NTAPEY, THICK,
A, B, ALPHA, ABX, ALPHAX, AREA, CONSNT, CLBAR,
XCPBAR, RFAREA, CL)

DIMENSION A(1), B(1), ALPHA(1), ABX(1), ALPHAX(1),
AREA(1), CL(1)

Input: NW = Number of wing panels.
NB = Number of body panels.
NTAPEX = Logical number of the tape from
which the inverse of the minimum
drag matrix is read.
NTAPEY = Logical number of the tape from
which D is read.
THICK = 0., wing thickness effects not to be
included.
= 1., wing thickness effects to be in-
cluded.
A = Dummy array used by the sub-
routine.
B = Dummy array used by the sub-
routine.
ALPHA = Dummy array used by the sub-
routine.
ABX = Array of normal on the body due to
a given wing thickness distribution.
ALPHAX = Array of downwash values on the
wing due to body sources.
AREA = Array of panel areas.
CONSNT = 0., wing optimization for wing C_L
constraint
= 1., wing optimization for wing C_L
and pitching moment constraints.
CLBAR = Wing coefficient of lift constraint.
XCPBAR = x-coordinate of the wing center of
pressure constraint.
RFAREA = Wing reference area.
Output: CL = Array of the pressure difference
across the wing panels optimized
for minimum drag.

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $239_{10} = 357_8$

SUBJECT: FORTRAN IV Subroutine OUTB

PURPOSE: To print out the data for body panels in a prescribed format.

METHOD: The data for the region of the body represented by panels are printed in the following format:

THETA (DEG.)	θ_1	θ_2	. . .	θ_{NTHETA}
ROW NO.				
1	$Z_{1,1}$	$Z_{1,2}$. . .	$Z_{1,NTHETA}$
2	$Z_{2,1}$.
3	.			.
.	.			.
.	.			.
.	.			.
NROW	$Z_{NROW,1}$. . .	$Z_{NROW,NTHETA}$

The numbers running horizontally represent the angles, θ around the body starting at the crown line and proceeding to the keel line. The numbers running vertically represent the rows of panels starting from the furthest forward panel and working aft.

USAGE: CALL OUTB (NTAPEO, NBODY, NTHETA, NROWB, THETA, Z)

DIMENSION Z(NBODY), THETA(NTHETA)

Input: NTAPEO = Logical number of output tape.

 NBODY = Number of body panels.

 NTHETA = Number of θ angles.

 NROWB = Number of rows of panels.

 THETA = θ angles.

 Z = Data to be output.

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $119_{10} = 167_8$

SUBJECT: **FORTRAN IV Subroutine OUTPTB**

PURPOSE: To write body paneling data on output tape as printout and on scratch tape for use in other program sections.

METHOD: Program uses direct write tape statements to write body paneling data on output tape and on scratch tape (see Appendix D for tape format). Program uses a tolerance of ± 0.00001 and sets all small negative and positive values equal to 0. Program also checks and eliminates any trivial secondary panel parts. An input tolerance is used for this check.

USAGE: **COMMON** (See subroutine OPCAMI for unlabeled **COMMON** description).

 Input: **NTAPE2**
 NWRITE

 Output: **NBODY**

COMMON /COM1/ (See subroutine **PANEL**)

 Input: **NPER**
 NPER1
 NPLANE
 NPLN1

COMMON /COM2/ (See subroutine **BODY**)

 Input: **KPANEL**
 XCOR
 YCOR
 ZCOR
 XINT
 YINT
 ZINT
 XCEN
 YCEN
 ZCEN
 XCON
 YCON
 ZCON
 AREA
 THETA
 ALPHA
 CHORD

CALL OUTPTB

SUBPROGRAM

CALLED: SQRT (Built-in function)

ERROR RETURNS: None

STORAGE: $1392_{10} = 2560_8$

SUBJECT: FORTRAN IV Subroutine OUTPTW

PURPOSE: To write wing paneling data on output tape as printout and on scratch tape for use in other program sections.

METHOD: Program uses direct write tape statements to write wing paneling data on output tape and on scratch tape (see Appendix D for tape format). Program uses a tolerance of ± 0.00001 and sets all small negative and positive values equal to 0. Program also checks all secondary panel parts of two-part panels on inboard and outboard columns and eliminates any "small" parts. An input tolerance is used for this check.

USAGE: COMMON (See subroutine OPCAMI for unlabeled COMMON description).

Input: NTAPE2
NWRITE

Output: NWING

COMMON /COM1/ (See subroutine PANEL)

Input: **KSTART**
 KEND
 NPER
 NPER1
 NPLANE
 NPLN1

COMMON /COM2/ (See subroutine WING)

Input: KPANEL
 XCOR
 YCOR
 ZCOR
 XINT
 YINT
 ZINT
 XCEN
 YCEN
 ZCEN
 XCON
 YCON
 ZCON
 AREA
 THETA
 ALPHA
 CHORD

CALL OUTPTW

SUBJECT: FORTRAN IV Subroutine OUTW

PURPOSE: To print out the data for wing panels in a prescribed format.

METHOD: The data for the wing panels are output in the following format:

SPANWISE STATION	1	2	3	.	.	.	NCOL
CHORDWISE STATION							
1	$Z_{1,1}$	$Z_{1,2}$	$Z_{1,NCOL}$
2	$Z_{2,1}$						
3	.						.
.	.						.
.	.						.
.	.						.
NROW	$Z_{NROW,1}$	$Z_{NROW,NCOL}$

The numbers running horizontally represent NCOL columns of panels from inboard to outboard, and the numbers running vertically represent NROW rows of panels from the leading to the trailing edge.

USAGE: CALL OUTW (NTAPEO, NWING, NCOLW, NROWW, Z)

DIMENSION Z(NWING)

Input: NTAPEO = Logical number of output tape.

 NWING = Number of wing panels.

 NCOLW = Number of chordwise columns of panels.

 NROWW = Number of rows of panels in a chordwise column.

 Z = Data to be output.

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $119_{10} = 167_8$

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

STORAGE: $1612_{10} = 3114_8$

SUBJECT: FORTRAN IV Subroutine PANEL

PURPOSE : To serve as control program for geometry paneling sub-routines.

METHOD: Program first reads control card used in later subroutines to calculate coordinates of panel control point. Program then reads control card containing literal name and transfers to appropriate subroutine. Either the program transfers to the subroutine BODY or to the subroutine WING, or the program returns to the subroutine OPCAM.

The program contains the following labeled COMMON statement that occurs in all lower level geometry paneling subroutines:

```
COMMON/COM1/KODEB, KODEW, KODEWU, KODEI,
KODEC, XPER, YPER, KOPTB, KOPTW, KOPTF,
NUMS, KTYPE, KSTART, KEND, KINT, XI(16),
YI(16), ZI(16), NPER, NPER1, NPLANE,
NPLN1
```

KODEB = Code for body definition error.

KODEW = Code for wing definition error.

KODEWU = Code for error in wing thickness (or camber) calculations.

KODEI = Code for body-wing intersection definition error.

KODEC = Code for panel control point location. If KODEC = 0, panel control point is located on the streamwise chord through the panel centroid. If KODEC = 1, input value for YPER is used to locate control point.

XPER = Fraction of local streamwise panel chord at which panel control point is located.
 $0. \leq XPER \leq 1.$

YPER = Fraction of local spanwise panel chord at which panel control point is located.
 $0. < YPER \leq 1.$
NOTE: If YPER = 0, panel control point is located on the streamwise chord through the panel centroid.

KOTPB = Code for additional body panel card input.
 If **KOTPB** = 1, body panel corner points
 are input on cards. If **KOTPB** = 0, other-
 wise.

KOPTW = Code for additional wing panel card input.
 If **KOPTW** = 1, wing panel corner points
 are input on cards. If **KOPTW** = 0,
 otherwise.

KOPTF = Code for additional wing panel card input.
 If **KOPTF** = 1, actual wing surface coordi-
 nates are input on cards. If **KOPTF** = 0,
 otherwise.

NUMS = Number of airfoil sections for which wing
 surface coordinates are read as additional
 card input.

KTYPE }
KSTART } = Codes for internal program control.
KEND }

KINT = Code for body-wing intersection. If
KINT = 1, body-wing intersection has been
 requested and calculated. If **KINT** = 0,
 otherwise.

XI }
YI } = x, y, z coordinates of body-wing
ZI } intersection.

NPER = Number of columns of panels plus one.

NPER1 = Number of columns of panels.

NPLANE = Number of rows of panels plus one.

NPLN1 = Number of rows of panels.

USAGE:

COMMON (See subroutine OPCAMI for unlabeled **COMMON** description).

Input: **NTAPE1**
 NTAPE2
 ND1
 NREAD
 NWRITE

CALL PANEL

SUBPROGRAMS

CALLED:

WING

BODY

INTURP

ERROR RETURNS:

Error messages indicate whether error occurred in reading various geometry definitions from scratch tape.

STORAGE:

$11208_{10} = 25710_8$

SUBJECT: FORTRAN IV Subroutine PARTV

PURPOSE: To partition velocity components due to the surface distribution of vorticity in preparation for use in later aerodynamic links.

METHOD: The velocity components are read from a scratch tape written by subroutine EVAL in the following form, where a column is written as a logical record.

$$\begin{bmatrix} U_{BB} & U_{BW} \\ V_{BB} & V_{BW} \\ W_{BB} & W_{BW} \\ U_{WB} & U_{WW} \\ V_{WB} & V_{WW} \\ W_{WB} & W_{WW} \end{bmatrix}$$

where the subscripts are given:

BB = Influence on the body due to the body

WB = Influence on the wing due to the body

BW = Influence on the body due to the wing

WW = Influence on the wing due to the wing

The velocity components are reordered to a partitioned form with an end-of-file separating the partitions.

$$\begin{bmatrix} U_{BB} \\ V_{BB} \\ W_{BB} \end{bmatrix} \begin{bmatrix} U_{WB} \\ V_{WB} \\ W_{WB} \end{bmatrix} \begin{bmatrix} U_{BW} \\ V_{BW} \\ W_{BW} \end{bmatrix} \begin{bmatrix} U_{WW} \\ V_{WW} \\ W_{WW} \end{bmatrix}$$

USAGE:

CALL PARTV

COMMON DATE(2), NTAPEA, NTAPEB, NTAPEC,
NTAPED, NTAPEE, NTAPEF, NTAPEI, NTAPEO,
NBODY, NWIN, XMACH, SYM, KACE

DIMENSION U(110), V(110), W(110), UU(110), VV(110),
WW(110)

Input: NTAPEB = Logical tape number from which the
velocity components are read.

NTAPED = Logical tape number on which the
velocity components are written.

NWING = Number of wing panels.

NBODY = Number of body panels.

U, V, W = Velocity components in random
order on logical tape NTAPED.

Output: U, V, W = Velocity components in a specified
order written on logical tape NTAPED.

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

RESTRICTIONS: $0 < \text{NBODY} \leq 100$

$0 < \text{NWING} \leq 110$

STORAGE: $1099_{10} = 2113_8$

SUBJECT: FORTRAN IV Subroutine POLXN

PURPOSE: To find the intersections of an m-dimensional polygonal arc and a plane (or line, if $m = 2$). A polygonal arc is defined as a set of points consecutively connected by straight lines.

METHOD: Consider any two consecutive points in the polygonal arc P, say P_i and P_{i+1} . If P_i (or P_{i+1}) lies within a given distance EP of the plane, it is said to lie in the plane. If one point lies in the plane, that point is returned as an intersection. If both points P_i and P_{i+1} lie in the plane (i.e., the line segment $\overline{P_i P_{i+1}}$ is contained in the plane), only the end points of that line segment are returned as intersections. If P_i and P_{i+1} lie on opposite sides of the plane, the intersection of the line segment $\overline{P_i P_{i+1}}$ with the plane is returned. The subroutine stops processing points when a specified maximum number of intersections has been found. The point subscripts associated with any intersection are also returned.

USAGE: DIMENSION C(M+1), P(M, N), Q(M, MAX), LQ(2, MAX)
CALL POLXN (C, P, M, N, EP, MAX, Q, LQ, L)

Input: C = Coefficients of the plane
 $C_1x_1 + C_2x_2 + \dots + C_Mx_M + C_{M+1} = 0.$
P = Array of point coordinates
 $x_{11}, x_{21}, \dots, x_{M1}, x_{12}, x_{22}, \dots, x_{M2}, \dots$
M = Dimension of hyperspace.
N = Number of points in P.
EP = Tolerance.
MAX = Maximum number of intersections to be found.

Output: Q = Array of intersection points.
LQ = Array of point numbers of points in P that are adjacent to points in Q; for instance, if an intersection in Q is between the fourth and fifth points of P, the corresponding elements of LQ are (4, 5); if point i in P lies in the plane (or within distance EP from it), then the point i appears in Q,

and the corresponding elements in LQ
are (i, i).

L = Number of intersection points in Q;
L = 0 if no intersections are found.

SUBPROGRAM

CALLED: SQRT (Built-in function)

ERROR RETURNS: L will be returned as -1 if $M \leq 0$, or if $MAX \leq 0$, or if
all of the coefficients C are zero.

RESTRICTIONS: If any points are identical and lie in the plane, each such
point will be returned as an intersection.

STORAGE: $268_{10} = 414_8$

SUBJECT: FORTRAN IV Subroutine QRAT

PURPOSE: To find the coefficients of the quadratic that passes through three given points, and optionally to evaluate the quadratic at a given value of x .

METHOD: The quadratic equation is

$$y = C_1 + C_2 x + C_3 x^2$$

Let (x_i, y_i) , $i = 1, 2, 3$ be the three given points. Then if no two points have the same x -coordinate,

$$C_3 = \left(\frac{y_3 - y_2}{x_3 - x_2} - \frac{y_2 - y_1}{x_2 - x_1} \right) / (x_3 - x_1)$$

$$C_2 = (y_3 - y_1) / (x_3 - x_1) - C_3 (x_3 + x_1)$$

$$C_1 = y_2 - (C_2 + C_3 x_2) x_2$$

The quadratic is evaluated for a given value of x if a code is positive.

USAGE: DIMENSION X(1), Y(1), C(3)

CALL QRAT(X, Y, IXY, KODE, XI, YI, C, NU)

Input: X = Location of the x -coordinate of the first point.

 Y = Location of the y -coordinate of the first point.

 IXY = Skip number for X and Y. IXY = location of w_{i+1} minus the location of w_i , where w is either x or y and $i = 1$ or 2 . For example, IXY = 1 if X and Y are each dimensioned 3. Or if an array $W = (x_1, y_1, x_2, y_2, x_3, y_3)$ then CALL QRAT (W, W(2), 2, ...) may be used to avoid shifting x_i and y_i to separate arrays

 KODE = If KODE > 0, the quadratic (if found) will be evaluated at $x = XI$ and the result stored in YI. Otherwise, XI and YI are not used.

 XI = See KODE.

Output: YI = See KODE.
 C = Array of quadratic coefficients
 C = (C₁, C₂, C₃).
 NU = An error code that is zero if QRAT is
 successful.

SUBPROGRAM

CALLED: None

ERROR RETURNS: NU = 1 if any two of the given points have the same x-
 coordinate.

RESTRICTIONS: IXY may not be zero; it may be negative if the point coor-
 dinates are stored in descending core locations.

STORAGE: $157_{10} = 235_8$

SUBJECT: FORTRAN IV Subroutine READ

PURPOSE: To provide, as options, three methods of inputting an array of values.

METHOD: The subroutine allows control over the form of input to the program by means of a literal word on a data card. Two words are stored in the program Data Dictionary. The first control word is CONSTANT, of which the first six letters CONSTA are stored. The second word is GIVEN. If the word on the data card matches either of the two control words, transfer in the program is made accordingly. The third option is provided by arbitrary letters in the first six columns of the input card. The three options provided are:

- 1) If the first data card contains CONSTANT, the program expects one additional data card on which the first field (columns 1-10) contains a value. This value is then set in the array S.
- 2) If the first data card contains GIVEN, the program expects to read an array of values off a specified logical tape unit.
- 3) If the data card contains any arbitrary alphanumeric characters, the program expects to read an array of values from data cards punched in a seven-field, ten-digit format.

USAGE: CALL READ (NTAPEI, NTAPEO, NTAPEC, NM, S)
 DIMENSION S(NM), DICT(2)

Input: NTAPEI = Logical number of input tape.
 NTAPEO = Logical number of output tape.
 NTAPEC = Logical number of scratch tape, if option 2.
 NM = Number of values in the input array.

Output: S = Array of values.

SUBPROGRAM CALLED: INTURP

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $131_{10} = 203_8$

SUBJECT:

FORTRAN IV Subroutine REDUCE

PURPOSE:

To form the "reduced" aerodynamic influence coefficients matrix and three additional matrices in preparation for use in later links.

METHOD:

The aerodynamic influence coefficients matrix is composed of the normal velocity components induced by a unit pressure difference on each panel.

The matrix may be written in terms of the sub-matrices

$$\begin{bmatrix} A_{BB} & A_{BW} \\ A_{WB} & A_{WW} \end{bmatrix} \cdot \begin{Bmatrix} p_B \\ p_W \end{Bmatrix} = \begin{Bmatrix} -n_{BWS} \\ \frac{dZc}{dx} - (\alpha) - n_{WB} \end{Bmatrix}$$

where

- A_{BB} = The influence on the body due to the body
- A_{WB} = The influence on the wing due to the body
- A_{BW} = The influence on the body due to the wing
- A_{WW} = The influence on the wing due to the wing
- n_{BWS} = The normal velocity component on the body due to wing sources
- $\frac{dZc}{dx}$ = The slope of the wing panels
- α = The angle of attack
- n_{WB} = The normal velocity component on the wing due to the body

The matrix equation is solved for p_B and p_W .

$$\begin{aligned} \{p_B\} &= -[A_{BB}]^{-1} \{n_{BWS}\} + [A_{BW}] \{p_W\} \\ \{p_W\} &= [A_R]^{-1} \{ [A_{WB}] [A_{BB}]^{-1} \{n_{BWS}\} + \left\{ \frac{dZc}{dx} - \alpha - n_{WB} \right\} \} \end{aligned}$$

$$\text{where } [A_R] = [A_{WW}] - [A_{WB}] [A_{BB}]^{-1} [A_{BW}]$$

is referred to as the "reduced" aerodynamic matrix.

The "reduced" matrix is then written on logical tape NTAPPE.

The additional matrices formed are

$$\begin{aligned} [D] &= [A_{WB}] [A_{BB}]^{-1} \\ \text{and } [E] &= [A_{BB}] [A_{BW}] \end{aligned}$$

Three matrices are written on logical tape NTAPEF in the order $[A_{BB}]^{-1}$, $[D]$, $[E]$ with an end-of-file written after each matrix.

USAGE:

CALL REDUCE

COMMON DATE(2), NTAPEA, NTAPEB, NTAPEC, NTAPED, NTAPEE, NTAPEF, NTAPEI, NTAPEO, NBODY, NWIN, XMACH, SYM, KACE

DIMENSION: AB(100), ABB(100, 100), AWB(110, 100), ABW(100, 25), AWW(100, 25), E(100, 25), D(110)

EQUIVALENCE (ABB, AWB)

Input: NWING = Number of wing panels.
 NBODY = Number of body panels.
 NTAPEA = Logical number of tape from which the aerodynamic influence coefficients are read.
 NTAPED = Logical number of tape from which $[A_{WB}]$ and $[A_{BB}]^{-1}$ are read.
 NTAPEE = Logical number of tape on which the reduced aerodynamic influence coefficients matrix is written.
 NTAPEF = Logical number of tape on which $[A_{BB}]^{-1}$, $[D]$, and $[E]$ are written.
 AWB = Matrix $[A_{WB}]$
 ABB = Matrix $[A_{BB}]^{-1}$
 ABW = Matrix $[A_{BW}]$
 AWW = Matrix $[A_{WW}]$
 Output: AWW = Matrix $[A_R]$
 ABB = Matrix $[A_{BB}]^{-1}$
 D = Matrix $[D]$
 E = Matrix $[E]$

SUBPROGRAM

CALLED: None

ERROR RETURNS: None

RESTRICTIONS: NWING \leq 110

NBODY \leq 100

STORAGE: 19564₁₉ = 46152₈

SUBJECT: FORTRAN IV Subroutine RICH3A

PURPOSE: Given a sparse array of points on a space curve, to compute a dense array.

METHOD: A given tolerance, CHD, regulates the number of additional points to be generated on the space curve. Between adjacent points in the dense array, the maximum distance between arc and chord will be approximately less than CHD. (However, if $CHD \leq 0$ or if there are fewer than four points in the sparse array, no interpolation takes place and the dense array will be identical to the sparse array.)

The given sparse-array points are projected into a plane. Additional points are interpolated in this plane by subroutine ENRYCH (using the tolerance CHD). An inverse projection is then performed, mapping the two-dimensional points back to the original three-space.

A more detailed description of the enriching process follows. As a first step the sparse array of points is transformed to an X', Y', Z' coordinate system. The transformation is determined by a given code, KD. Let $P_1 (x_1, y_1, z_1)$ be the first point in the given sparse array P , and $P_n (x_n, y_n, z_n)$ be the last point. If $KD = 0$, the $X' Y' Z'$ origin is at P_1 , and the X' axis passes through P_n ; the $X' Z'$ plane contains the point in P farthest from the line $P_1 P_n$. If $KD = 1$ or 2 , the $X' Y' Z'$ origin is at $(x_1, y_1, 0)$, and the X' axis passes through the point $(x_n, y_n, 0)$; the Z' axis is parallel to the Z axis. In the next step, the $X' Z'$ coordinates of the points are treated as two-dimensional points by subroutine ENRYCH to produce a dense array of points. To find the corresponding Y' coordinate of each point, a two-dimensional interpolation is made by subroutine BITURP: the interpolation table contains the sparse array X' and Y' coordinates, with X' as the independent variable. For each dense array point the Y' coordinate is interpolated from the table. The interpolation is linear if $KD = 1$, or biquadratic if $KD = 0$ or 2 . In the final step, the dense array X', Y', Z' coordinates are transformed to the original X, Y, Z system.

USAGE: DIMENSION $P(3, N), Q(3, N), A(3, MAX/3), NU(3)$
CALL RICH3A ($N, P, Q, KD, MAX, CHD, NA, A, NU$)

Input: N = Number of points in P .
 P = Array of given points (sparse array).

KD = Code (see METHOD, above).
 MAX = Maximum number of elements that may be stored in the A-array.
 CHD = Chord-height tolerance that determines the spacing of interpolated points (see ENRYCH)
 NU = Error indicator array: NU(1) is not used on input. NU(2) and NU(3) are used only by ENRYCH and BITURP. NU(2) is an output tape number on which to write a message if an error is detected; no message is written if $NU(2) \leq 0$. NU(3) is an error message limiter; if an error is detected, $NU(3) = (NU(3) - 1)$. Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.
 Output: Q = Scratch array that may occupy the same storage space as P if P need not be preserved.
 NA = Number of points in the A-array.
 A = Array of enriched points (dense array).
 NU = Error indicator array: NU(1) = 0 if success. NU(3) is discussed above.

SUBPROGRAMS
CALLED:

UVECN
 VCROS
 DMAXL
 ENRYCH
 BITURP
 TROTPT
 SQRT (Built-in function)
 TRAV

ERROR RETURNS: NU = -2, if KD = 0 and the endpoints of P are coincident.
 NU = -1 (corresponding to error code 3 from ENRYCH) if more than 200 interpolated points would be required between two points in P: either CHD is too small or the points in P (after projection) are ill-conditioned. RICH3A adds no interpolated points in this interval, and continues.
 NU = 1, 4, 5, or 6 if MAX is too small. NU = 2 (error 2 from ENRYCH) if four consecutive points in P (after

transformation to the X', Y' system) are not strictly monotonic in either X' or Y' . $NU = 7$ if $KD = 1$ or 2 and the endpoints of P have the same X and Y coordinates. $NU = 11, 12, 13$, or 14 (BITURP errors 1, 2, 3, or 4) if an error was detected during the inverse projection (see METHOD, above); this can happen only if the given sparse array is ill-conditioned. $NU = 21$ if an error occurs when finding the projection plane.

RESTRICTIONS: After transformation to the X', Y', Z' system (see METHOD, above), the given sparse array points must be monotonic in X' ; no two X' coordinates may be the same. Since only the projections of the given points on the $X'-Z'$ plane are enriched, too few points may be generated if the given points do not lie approximately in the plane.

STORAGE: $509_{10} = 775_8$

SUBJECT: FORTRAN IV Subroutine RICHNA

PURPOSE: To enrich (interpolate additional points) a set of body meridian lines or wing percent lines.

METHOD: A given array A of length MAX contains M arrays of N three-dimensional points each. Each array will be called a percent line. Since array A is also used for output, all the points are first shifted to the end of A. A given code, KOD, determines the type of interpolation (see subroutine RICH3A). If $KOD \neq 0$, all points in each percent line are checked; a comment is written for each point having X and Y coordinates that are nearly the same (within a given tolerance EPS) as those of the previous point but for which the Z-coordinates are different. Then all percent lines are screened by function NWEED to remove any points too close to the preceding point; If $KOD = 0$, all three coordinates must nearly match the previous point before a point is removed. But if $KOD > 0$, only the X and Y coordinates must nearly match; thus any points for which a comment was written will be removed.

(NOTE: $KOD = 0$ for body meridian lines; $KOD = 0, 1$, or 2 for wing percent lines.) If a given tolerance CHD is less than or equal to 0, no additional points will be interpolated. A "header" or "table of contents" is inserted at the beginning of array A; this is followed by the point coordinates. The format of the completed array A is given in Appendix D.

USAGE: DIMENSION A(MAX), P(M), NU(3)

CALL RICHNA (A, MAX, M, N, P, EPS, CHD, KOD, NA, NU)

Input: A = Array of M percent lines of N points each.
MAX = Length of array A.
M = Number of percent lines.
N = Number of points in each percent line.
P = Array of labels that are angles (if body meridian lines) or percent values (if wing percent lines); these are used in the "header" of the final array (see Appendix D).
EPS = Tolerance of test for coincident points.

CHD = Chord-arc tolerance that controls the number of interpolated points. See subroutine RICH3A.

KOD = Code which determines type of interpolation (see KD in subroutine RICH3A).

NU = Error indicator array: NU(1) is not used on input. NU(2) is an output tape number on which to write a message if an error is detected in some lower-level subroutine; no message is written if $NU(2) \leq 0$. NU(3) is an error message limiter; if an error is detected, $NU(3) = (NU(3) - 1)$. Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.

Output: A = Array of M enriched percent lines, with "header" that contains a label, number of points, and starting location in A for each percent line. See Appendix D for format.

NA = Total number of points in array A. The total number of elements used in A is $3 * (M + NA)$.

NU = Error indicator array: $NU(1) = 0$ if no errors are detected. NU(3) may have been reduced by a lower-level subroutine if an error occurred.

SUBPROGRAMS

CALLED: NWEED
RICH3A

ERROR RETURNS: NU = -1 if NWEED detected an error; this could be caused by a very large value of EPS. For any other nonzero value of NU, see RICH3A.

RESTRICTIONS: $MAX \geq 3 * M * (N + 1)$

STORAGE: $400_{10} = 620_8$

SUBJECT: FORTRAN IV Subroutine RITE

PURPOSE: To output the x, y, and z components of velocity induced by the various singularities.

METHOD: If a printout of the velocity components is requested, the x, y, and z components of velocity are written on the output tape. The components are identified in the printout as the x component, AXIAL(U); the y component, TRANSVERSE(V); and the z component, VERTICAL(W). By an input code, the proper identification relating the velocity components to the singularity is also printed.

USAGE: Call RITE (NFMT, NTAPEO, NP, NROW, NCOL, THETA, U, V, W)

 DIMENSION NFMT(7), U(NP), W(NP)

Input: NFMT control code

 NFMT(I) = 0, output of velocity components not
 (I = 1, 7) requested.

 NFMT(1) = 1, velocity components on body panels
 resulting from body panel pressure
 singularities.

 NFMT(2) = 2, velocity components on body panels
 resulting from wing panel pressure
 singularities.

 NFMT(3) = 3, velocity components on body panels
 resulting from wing sources.

 NFMT(4) = 4, velocity components on wing panels
 resulting from wing panel pressure
 singularities.

 NFMT(5) = 5, velocity components on wing panels
 resulting from wing sources.

 NFMT(6) = 6, velocity components on wing panels
 resulting from body panel pressure
 singularities.

 NFMT(7) = 7, velocity components on wing panels
 body line sources and doublets.

 NTAPEO = Logical number of output tape.

 NP = Number of wing or body panels.

NROW = Number of rows of panels on wing
or body.
 NCOL = Number of chordwise columns of
panels on wing or number of longi-
tudinal columns of panels on body.
 THETA = If body case, the θ angles around the
body of the data output points.
 U = x component of velocity.
 V = y component of velocity.
 W = z component of velocity.

SUBPROGRAMS OUTB
 CALLED: OUTW

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $409_{10} = 631_8$

SUBJECT:

FORTRAN IV Subroutine RRAT

(See Subroutine QRAT)

SUBJECT: FORTRAN IV Subroutine SAVTAP

PURPOSE: To write the aerodynamic matrices for a given configuration and Mach number on a logical tape that can be saved and used for later computer runs.

METHOD: The aerodynamic matrices are read from several logical tapes as indicated below and written as one file on logical tape NTAPEC.

For wing-alone configurations, the matrices are written in the following order:

<u>Previous tape</u>	<u>Matrix</u>	<u>Description</u>
1. NTAPEA	$[A_{WW}]$	Aerodynamic influence coefficients due to wing sources.
2. NTAPEA	$[WW]$	Drag minimization.
3. NTAPEA	$[WW]^{-1}$	Inverse of drag minimization matrix constrained for wing lift.
4. NTAPEA	$[WW]^{-1}$	Inverse of drag minimization matrix constrained for wing lift and pitching moment.
5. NTAPEB	$[U_{WW}]$ $[V_{WW}]$ $[W_{WW}]$	Velocity components due to wing sources.
6. NTAPEB	$[U_{WW}]$ $[V_{WW}]$ $[W_{WW}]$	Velocity components due to wing surface vortices.
7. NTAPEE	$[A_{WW}]$	Aerodynamic influence coefficients due to wing surface vortices.
8. NTAPEE	$[A_{WW}]^{-1}$	Inverse of matrix of aerodynamic influence coefficients due to wing surface vortices.

For wing-body configurations, the matrices are written in the order:

<u>Previous tape</u>	<u>Matrix</u>	<u>Description</u>
1.-5. (same as wing-alone configurations)		
6. NTAPED	$\begin{bmatrix} U_{BB} \\ V_{BB} \\ W_{BB} \end{bmatrix}$	Velocity components on the body due to body surface vortices.
7. NTAPED	$\begin{bmatrix} U_{WB} \\ V_{WB} \\ W_{WB} \end{bmatrix}$	Velocity components on the wing due to body surface vortices.
8. NTAPED	$\begin{bmatrix} U_{BW} \\ V_{BW} \\ W_{BW} \end{bmatrix}$	Velocity components on the body due to wing surface vortices.
9. NTAPED	$\begin{bmatrix} U_{WW} \\ V_{WW} \\ W_{WW} \end{bmatrix}$	Velocity components on the wing due to wing surface vortices.
10. NTAPEE	$\begin{bmatrix} A_R \end{bmatrix}$	"Reduced" aerodynamic matrix.
11. NTAPEE	$\begin{bmatrix} A_R \end{bmatrix}^{-1}$	Inverse of "reduced" aerodynamic matrix.
12. NTAPEF	$\begin{bmatrix} A_{BB} \end{bmatrix}^{-1}$	Inverse of matrix of aerodynamic influence coefficients.
13. NTAPEF	$\begin{bmatrix} D \end{bmatrix}$	Product matrix, $\begin{bmatrix} D \end{bmatrix} = \begin{bmatrix} A_{WB} \end{bmatrix} \begin{bmatrix} A_{BB} \end{bmatrix}^{-1}$

<u>Previous tape</u>	<u>Matrix</u>	<u>Description</u>
--------------------------	---------------	--------------------

14. NTAPEF [E] Product matrix.

$$[E] = [A_{BB}] \cdot [A_{BW}]$$

This subroutine is not used for body-alone configurations.

USAGE:

CALL SAVTAP (ISAVET)

Input: ISAVET = Code that indicates if matrices are to be saved. If ISAVET > 0 matrices are written as one file on logical tape NTAPEC as indicated above. If ISAVET ≤ 0, a dummy file is written on logical tape NTAPEC.

NTAPEA	}	= Logical tape numbers from which aerodynamic matrices are read.
NTAPEB		
NTAPED		
NTAPEE		
NTAPEF		

NTAPEC = Logical tape number on which aerodynamic matrices are written and saved.

SUBPROGRAMS
CALLED:

TTAPE

FSF

ERROR RETURNS:

None

RESTRICTIONS:

This subroutine cannot be used for body-alone configurations.

STORAGE:

$1212_{10} = 2274_8$

SUBJECT:

FORTRAN IV Subroutine SCAMP4

PURPOSE:

Given a set of n points (x_i, y_i) whose abscissae form a strictly monotone sequence, a first or second derivative at x_1 , and a first or second derivative at x_n , to find the smoothest possible curve passing rigorously through the given points, satisfying the specified boundary conditions, and possessing continuous first and second derivatives. The criterion for smoothness is the minimization of the integral of the square of the second derivative, from x_1 to x_n , over all functions having the stated properties. Accordingly, the curve found is a chain of cubics, i.e., a separate cubic defined on each interval (x_i, x_{i+1}) . The coefficients of each such cubic are explicitly found in the form:

$$y = C_0 + C_1x + C_2x^2 + C_3x^3$$

METHOD:

The most economical (in time and space) and most accurate method of finding such a chain of cubics is to solve first for the n slopes y_i of the curve. This is done by the composite cubic subroutine COMCU, which solves an n th order linear system, the coefficient matrix of which is tridiagonal. Having found the slopes at each of the n given x_i , one can determine the coefficients of each cubic separately by using CUBIC2, which finds the cubic through two points, being given the slope at each. The coefficients of all the $n-1$ cubics can be obtained by using the subject routine (SCAMP4) which serves as a vehicle for calling COMCU (once) and CUBIC2 ($n-1$ times). SCAMP4 has an option to compute the required boundary conditions (first or second derivatives at the end points) if these are not known by the calling program; in this case, the computation of first derivatives at x_1 and x_n is recommended.

The cubic coefficients found by SCAMP4 are either stored in a 4 by $n-1$ array or are arranged in the composite curve format, i.e. in a single linear array where each segment is specified by a block of seven consecutive words: $x_i, x_{i+1}, 3., c_0, c_1, c_2, c_3$. The calling program should dimension the coefficient array as a doubly subscripted variable in the former case and singly subscripted in the latter case.

USAGE:

CALL SCAMP4 (X, Y, N, NDA, NDB, DA, DB, C, S, M)

DIMENSION X(N), Y(N), C(4, N-1) or C(7, K)

where $K = N - 1$

Input:	X	=	Array of x-abscissae.
	Y	=	Array of y-ordinates.
	N	=	Number of points.
	NDA	=	The order (1 or 2) of the derivative to be given at X(1). If derivative is to be computed by SCAMP4, $NDA < 0$.
	NDB	=	The order of the derivative to be given at X(N). Similar to NDA.
	DA	=	The value of the derivative at X(1). If derivative is to be computed by SCAMP4, leave blank.
	DB	=	The value of the derivative at X(N). Similar to NDA.
	M	=	Code.
		≠	12, if the cubic chain coefficients are to be stored in a doubly dimensioned 4 x (N - 1) array.
		=	12, if the cubic chain coefficients are to be stored in a singly dimensioned array.
Output:	C	=	Array of cubic chain coefficients.
	S	=	Array of first derivatives.
	M	=	Error return.
		=	0 — success
		≠	0 — error detected

SUBPROGRAMS
CALLED:

COMCU
CUBIC2
DERIV1
DERIV2

ERROR RETURNS: $M = -1$, indicates $N < 2$. $1 \leq M \leq 7$, indicates an error return from COMCU. M large indicates error return k on the j^{th} call to CUBIC2 ($M = 100 \cdot j + k$).

STORAGE: $288_{10} = 440_8$

SUBJECT: FORTRAN IV Subroutine SIMUN3

PURPOSE: Given a set of n points (x_i, y_i) , to numerically calculate using Simpson's (parabolic) rule the value of the integral:

$$\int_{x_1}^{x_n} y \, dx.$$

METHOD: Simpson's rule for a single interval containing three equally spaced points can be written:

$$\int_{x_1}^{x_3} y \, dx \sim \frac{\Delta x}{3} (y_1 + 4y_2 + y_3)$$

If, in fact, there are m successive subintervals each containing three points for a total of $2m + 1$ equally spaced points, this formula can be rewritten:

$$\int_{x_1}^{x_{2m+1}} y \, dx \sim \frac{\Delta x}{3} (y_1 + 4y_2 + 2y_3 \dots + 2y_{2m-1} + 4y_{2m} + y_{2m+1})$$

The set of input points (x_i, y_i) may or may not consist of some odd number of equally spaced points as required for Simpson's rule. Subroutine SCAMP4 is first used to compute the coefficients of a chain of cubics fit to these input points. A second set of $2m + 1$ equally spaced points (\bar{x}_i, \bar{y}_i) is then obtained by using the cubic chain coefficients provided by SCAMP4 and interpolating on the set of input points. If for some \bar{x}_i :

$$x_j < \bar{x}_i \leq x_{j+1}$$

then,

$$\bar{y}_i = c_{1,j} + c_{2,j} \bar{x}_i + c_{3,j} \bar{x}_i^2 + c_{4,j} \bar{x}_i^3$$

where $c_{1,j}$, $c_{2,j}$, $c_{3,j}$ and $c_{4,j}$ are the coefficients of the j^{th} cubic polynomial. A numerical value for the integral in question is then calculated by directly applying Simpson's rule:

$$\int_{x_1}^{x_{2m+1}} y \, dx \sim \frac{\Delta x}{3} (\bar{y}_1 + 4 \sum_{i \text{ odd}} \bar{y}_i + 2 \sum_{i \text{ even}} \bar{y}_i + \bar{y}_{2m+1})$$

USAGE:

CALL SIMUN3 (X, Y, M, A, K)

DIMENSION X (M), Y (M)

Input: X = Array of x-ordinates of input points.

Y = Array of y-ordinates of input points.

M = Number of input points.

Output: A = Value of integral.

K = Error return

= 0 — success

≠ 0 — error detected.

SUBPROGRAMS
CALLED:

SCAMP4

MOD } (Built-in functions)
FLOAT }

ERROR RETURNS: Three types of errors are detected and indicated. If fewer than three points are input, K = 1. If SCAMP4 detects an error in fitting a chain of cubics to the set of input points, K = 2. If an error occurs in calculating the integral, K = 3. Otherwise, K = 0.

RESTRICTIONS: $3 \leq M \leq 55$

STORAGE: $628_{10} = 1164_8$

SUBJECT: FORTRAN IV Subroutine SIZE

PURPOSE: To determine the number and sizes of the partitions of a matrix, given the size of the matrix and a maximum partition size.

METHOD: The subroutine uses the following sequence of FORTRAN instructions

```

      NPMIN   =  2
      NT      =  MM
      NPART   =  MAX 0 (NPMIN, (NT - 1)/NMAX + 1)
      N       =  NPART
10      NSIZE(N) =  NT/N
      NT      =  NT - NSIZE(N)
      N       =  N - 1
      IF(N) 20, 20, 10
20      RETURN

```

USAGE: CALL SIZE (MM, NMAX, NPART, NSIZE)

DIMENSION NSIZE (NPART)

Input: MM = Size of matrix.

NMAX = Maximum partition size.

Output: NPART = Number of partitions.

NSIZE = Array of partition sizes.

SUBPROGRAM CALLED: MAX0 (Built-in function)

ERROR RETURNS: None

RESTRICTIONS: None

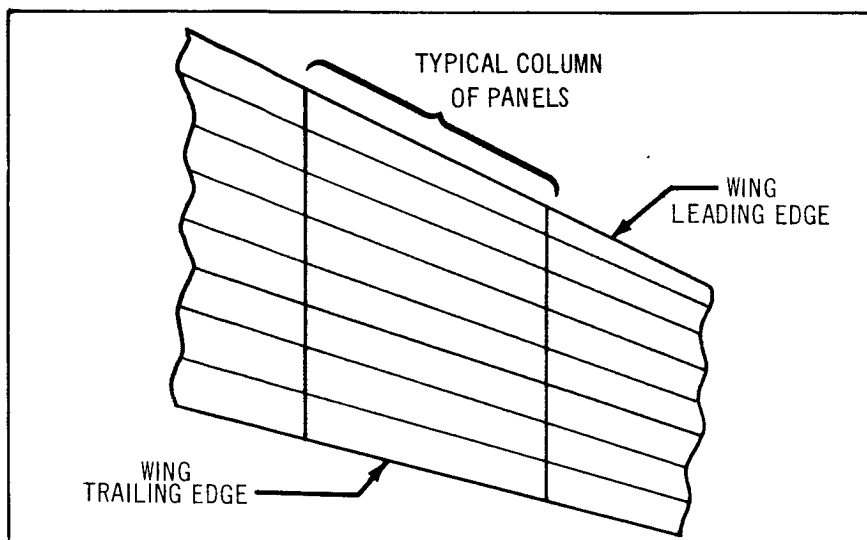
STORAGE: $74_{10} = 112_8$

SUBJECT: FORTRAN IV Subroutine SLOPEW

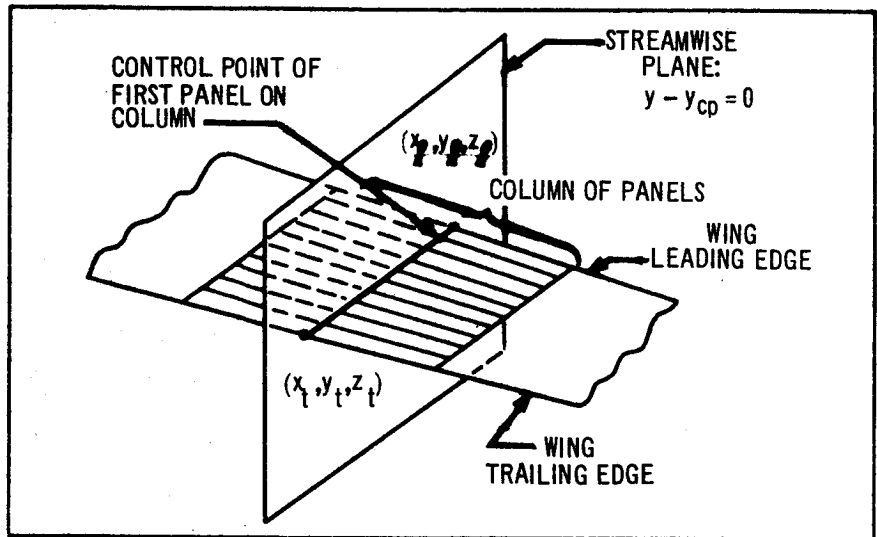
PURPOSE: To calculate camber and thickness ordinates and camber and thickness slopes for an airfoil.

METHOD: Program input can consist of single airfoil (or multiple airfoils) for which both an upper and lower surface are defined (see subroutine INPUTW). If a single airfoil is given, this airfoil is scaled accordingly and used to calculate camber and thickness for each column of panels on the wing. If multiple airfoils are given, each airfoil is reduced to a unit airfoil, scaled accordingly and used for camber and thickness calculations on but a single column of wing panels. Note that, for the latter case, as many airfoils as panel columns must be given on input cards.

For a given unit airfoil and the corresponding panel column, the program locates a local streamwise chord on the column, computes the chord length, and uses this value to scale the airfoil. For example, a typical panel column is represented below:



The program constructs a streamwise plane through the control point of the first panel on the column and intersects this plane with the wing leading and trailing edges. The panel side edges are streamwise; thus this construction is always possible and, because the control points for a given column of panels lie on the same streamwise chord, only one such construction is necessary. This is shown in the following sketch:



A chord length to be associated with this panel column is then calculated,

$$c = x_t - x_l$$

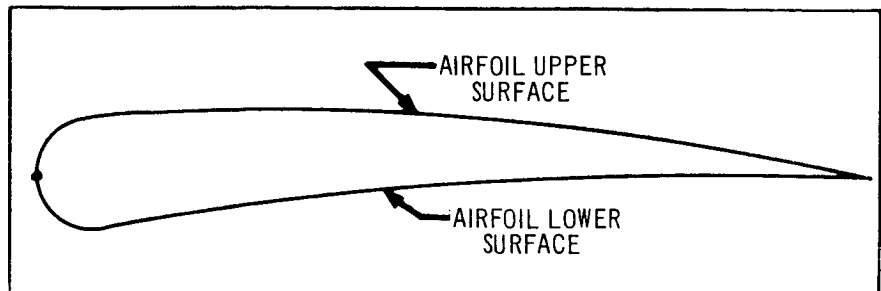
and this chord length is used to scale the airfoil so that,

$$x_k = x_{k_0} \cdot c$$

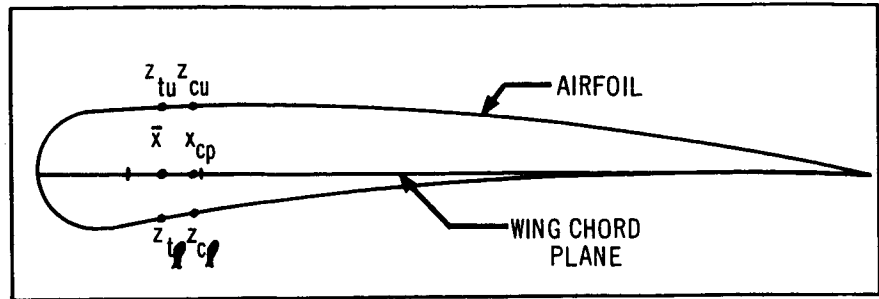
$$z_k = z_{k_0} \cdot c + \zeta$$

for which x_{k_0} , z_{k_0} are the x- and z-coordinates of the unscaled, unit airfoil, x_k , z_k are the coordinates of the scaled airfoil and ζ is the constant z-value for the wing.

Having scaled the airfoil to "fit" the wing for a particular column, the program then calculates camber and thickness ordinates for each panel of that column. To satisfy a condition of the program, the camber ordinate is computed at the panel control point and the thickness ordinate at the panel centroid. Because both the upper and lower surfaces of an airfoil are given as input (see sketch),



the program must interpolate on each surface for both the camber and thickness ordinate. As a result, four values are calculated



and used in camber and thickness calculations. For the camber ordinate,

$$z_{cam} = \frac{1}{2} (z_{cu} + z_{cl})$$

and for thickness,

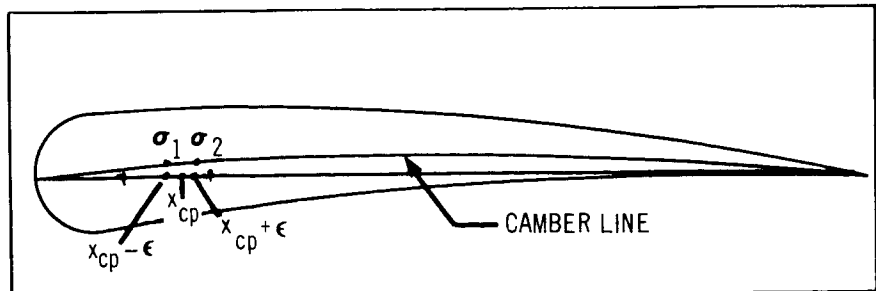
$$z_{thk} = \frac{1}{2} (z_{tu} - z_{tl}).$$

Using the camber and thickness ordinates that have been calculated, the program computes the camber and thickness slopes. As the camber is evaluated at the panel control point and the thickness at the centroid, the program constructs two distinct tables:

- 1) z_{cam} versus x_{cp}
- 2) z_{thk} versus \bar{x}

that are used for these calculations.

To obtain the camber slope at the x_{cp} for a given panel, the program evaluates the camber curve (1) at $x_{cp} - \epsilon$ and $x_{cp} + \epsilon$



for which

$$\epsilon = \frac{c}{10^5}$$

and c is the chord length.

The values σ_1 , σ_2 of the curve at these two points are used to compute the camber slope,

$$\alpha_{\text{cam}} = \tan^{-1} \left(\frac{\sigma_2 - \sigma_1}{2\epsilon} \right)$$

Similarly, to obtain the thickness slope at the \bar{x} of a given panel, the thickness curve (2) is evaluated at $\bar{x} - \epsilon$ and $\bar{x} + \epsilon$, and the values τ_1 and τ_2 of the curve at these two points are used,

$$\alpha_{\text{thk}} = \tan^{-1} \left(\frac{\tau_2 - \tau_1}{2\epsilon} \right)$$

As a last step the program smooths the camber and thickness slopes. The calculations of the slopes for a given column of panels result in two tables:

- 1) α_{cam} versus x_{cp}
- 2) α_{thk} versus \bar{x}

and each of these tables is smoothed through use of the subroutine MEAN.

The above calculations are used to obtain camber and thickness ordinates and camber and thickness slopes for panels of a column of the wing in all but two cases,

- 1) The inboard column on the wing for a body-wing case having a body contour in the intersection region;
- 2) The outboard wing column for wing having a nonstreamwise outboard wing edge.

For these two cases, the calculations are changed slightly because the edges of an arbitrary panel are not streamwise and the control points of all panels of the column do not lie on the same streamwise chord. A local streamwise chord must be constructed and a chord length determined for each panel in the column. The unit airfoil is scaled to "fit" the wing at the y_{cp} of each panel; then the camber and thickness are calculated.

USAGE: COMMON (See subroutine OPCAMI for unlabeled COMMON description)

COMMON /COM1/ (See subroutine PANEL)

Input: KOPTF
NUMS
KSTART
KEND
NPER
NPER1
NPLANE
NPLN1

COMMON /COM2/ (See subroutine WING)

Input: NPTS
X
Y
Z
SLOPE
XCEN
XCON
YCON
XFOIL
ZFOIL
XNUM

Output: ZCEN
ZCON
THETA
ALPHA

CALL SLOPEW

SUBPROGRAMS

CALLED: ATAN (Built-in function)
BITURP
MEAN
POLXN
CHECK

ERROR RETURNS: Error messages indicate whether error occurred in use of subroutine BITURP to interpolate on airfoil surfaces or on camber and thickness curves. An error message also indicates if the airfoil x-ordinates are not defined as a (strictly) monotonic increasing sequence.

STORAGE: $2272_{10} = 4340_8$

SUBJECT: FORTRAN IV Subroutine STRM1

PURPOSE: To integrate a three-dimensional streamline around a supersonic wing-body combination.

METHOD: LACKEY obtains velocities which are interpreted as derivatives of the streamline. The DEDIS package is used to perform an Adams-Moulton predictor-corrector variable stepsize integration. (See DEDIS)

USAGE: COMMON /INTGA/ DUM (3500)

CALL STRM1 (X, Y, Z, XMAX, XMIN, XDELTA, DXMAX, DXMIN, IND1, IND2)

Input:

- x = x-coordinate of starting point of streamline.
- y = y-coordinate of starting point of streamline.
- z = z-coordinate of starting point of streamline.
- XMAX = Maximum value which the x-coordinate of the streamline is allowed to attain.
- XMIN = Minimum value which the x-coordinates of the streamlines is allowed to attain.
- XDELTA = Initial stepsize.
- DXMAX = Maximum stepsize allowed.
- DXMIN = Minimum stepsize allowed.
- IND1 = 1. Negative running streamline.
= 2. Positive running streamline.
- IND2 = 1. Interpolated output (see output).
= 2. Actual points determined by integration.

Output: On user option, the streamlines are written on the output tape in step increments of XDELTA or the actual points are determined by the variable stepsize integration are written.

**SUBPROGRAMS
CALLED:**

DED
DES
DEI
BJTURP
LACKEY
SQRT (Built-in function)

ERROR RETURNS: None

RESTRICTIONS: If the number of points determined by the integration routine exceeds 200 before reaching one of the x-coordinate extrema (DXMAX, or DXMIN), the integration is terminated and results are output at that point.

STORAGE: $734_{10} = 1336_8$

SUBJECT:

FORTRAN IV Subroutine TAN

(See subroutine FTAN)

SUBJECT: FORTRAN IV Subroutine TDUMP

PURPOSE: To read the binary tape produced by the Geometry Definition section and to write its contents on an output tape.

METHOD: A given logical array, which contains tape record status information, is checked. If there are no valid records on the binary tape, control is returned to the calling program. Otherwise, each of the 18 records is processed. The tape format is given in Appendix D.

USAGE: LOGICAL LGDEF(3, 6)
 CALL TDUMP (LO, LTAPE, LGDEF)
 Input: LO = Output tape number.
 LTAPE = Binary tape number.
 LGDEF = See subroutine GEOMD.

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: Records must not contain more than 2000 words.

STORAGE: $2175_{10} = 4177_8$

SUBJECT: FORTRAN IV Subroutine TFLAT

PURPOSE: To transform body and wing to a new coordinate system, to flatten the wing, and to find the intersection of each wing percent line with the body surface.

METHOD: Three types of cases may be handled: body alone, wing alone, or wing-body combination. If a body surface is involved, it is assumed to be symmetrical about the X-Z plane; only half of it is given. Then a new x, y, z coordinate system is set up with origin at the centroid of forward end of the body and the x-axis passing through the aft-end centroid; the z-axis lies in the X-Z plane. In the new coordinate system, the body ends (unless of zero radius) are not necessarily parallel to the y-z plane; this is corrected by a linear adjustment of all x-coordinates of the body points. Also, the new body length (distance between body end centroids) may be different than the original length. The original set of body defining stations is converted to the new coordinate system by a transformation of the form $x = \alpha X + \beta$. The body radius and centroid are computed at each of these stations. In a body alone case, the radius and centroid are then found by interpolation at a given number of equally spaced stations; otherwise, this calculation is deferred.

In a wing-body combination, the wing is also transformed to the x, y, z coordinate system. Then the intersections of the wing leading and trailing edges with the body surface are computed; let z_A be the average of the z-coordinates of these two points. The wing is effectively flattened by changing each z-coordinate of the wing to z_A . The body is then intersected by each wing percent chord line of the flattened wing.

The body radius and centroid calculation can now be resumed. A set of equally spaced stations is chosen between the forward end of the body and the station at which the wing leading edge intersects the body; a similar set is selected from there on aft. The calculation of the interval between stations in each region is subject to the constraints that the total number of stations must agree with a given number and that the two intervals must be approximately the same in each region.

In a wing alone case, the transformation is omitted. However, the wing is flattened: z_A is taken

as the average of the z-coordinates of the first point in the leading- and trailing-edge percent lines.

The body and wing definitions are on a binary tape, LA, which has a format as described in Appendix D. The body is given by meridian lines, the wing by percent chord lines; meridian and percent lines are described by sets of three-dimensional points (see subroutine WBXUL). One data card is required; it is read with FORMAT (5F10.0) as follows:

<u>Columns</u>	<u>Symbol</u>	<u>Explanation</u>
1-10	XNRX	Number of body stations at which body radius and centroid are desired. If this number is less than 3 or greater than 50, it is set equal to 50.
11-20	CHD	A tolerance passed on to subroutine TFLAT1, and then to BODCR, for eventual use by subroutines ENRYCH and OPTIM3. CHD is used only to find body centroids, as follows: A section, normal to the x-axis, is taken through the body. The section has one point for each meridian line. If $CHD \leq 0$, the centroid is found assuming the section to be polygonal. If $CHD > 0$ and there are at least four meridian lines, additional section points are generated by ENRYCH on a smooth curve through the vertices of the polygon: a sufficient number of points will be generated so that the difference between the chord of the resultant polygon and the arc of the smooth curve is (approximately) less than CHD. A positive value of CHD should not be used unless there are at least eight meridian lines on a non-symmetrical (about a horizontal plane) body.

<u>Columns</u>	<u>Symbol</u>	<u>Explanation</u>
21-30	BCODE (1)	An interpolation code used by BITURP to find body radius and z_c , (z-coordinate of the body centroid) at values of x between defining stations. BCODE (1) = 1 for linear interpolations, = 2 for biquadratic interpolation.
31-40	BCODE (2)	An interpolation code used by BITURP to find the intersections of wing percent lines with the body surface (see subroutine WBXX). This process involves finding body sections at various values of x. If BCODE (2) = 1, linear interpolation is used to find y as a function of z; this is equivalent to saying that the body is polygonal in cross section. If BCODE (2) = 2 (and there are at least three meridian lines), biquadratic interpolation is used; this is equivalent to specifying a body of curved cross section (but see RESTRICTIONS, under BITURP).
41-50	EPRC	A tolerance applied to body radius and z_c (z-coordinate of the body any value of x) is less than EPRC, the corresponding radius or z_c is set to zero. EPRC is introduced to help offset round-off errors.

Two binary tapes are written by TFLAT; their formats are described in Appendix D.

USAGE:

COMMON /LGEOMD/LGDEF (3, 6)

LOGICAL LGDEF

DIMENSION DAT (2)

CALL TFLAT(DAT, LI, LO, LA, LB, LD, NBODY, IOK)

Input: DAT = Date (alphameric).
 LI = Input tape number.
 LO = Output tape number.
 LA = Binary tape number; this tape is read
 by TFLAT (see Appendix D).
 LB = Binary tape number; three records
 are to be written on this tape, unless
 a wing-only case is processed (see
 Appendix D, section 3).
 LD = Binary tape number; six records are
 to be written on this tape (see Appen-
 dix D, section 2).
 LGDEF = Logical array, in COMMON, which
 indicates body and wing status.
 LGDEF(1, 3) = .TRUE. if a body
 definition was requested; LGDEF(3, 3)
 = .TRUE. if the body definition was
 successfully written on tape LA.
 LGDEF(1, 1) = .TRUE. if a wing
 definition was requested; LGDEF(3, 1)
 = .TRUE. if the wing definition was
 successfully written on tape LA. The
 other elements of LGDEF are not used
 by TFLAT.
 Output: NBODY = Code to indicate a successful body-
 alone case; then NBODY = -1. Other-
 wise, NBODY = 0.
 IOK = Error indicator, which is zero if
 success.

SUBPROGRAMS
 CALLED:

WBXX
 TRAPCT
 BITURP
 TFLAT1
 TFLATM
 TFLATW
 TFLATX
 TRAV
 FSR

ERROR RETURNS:

If an error is detected, a message is written on the output tape. Then data cards on the input tape are skipped over until the next case, or end of data, is found. A new case is signaled by the word DEFINE or DEFINE in columns 1-6 of a data card; end of data is signaled by the word END OF. The input tape is then backspaced one record.

The argument IOK is set to one of the following values if an error is found:

<u>IOK</u>	<u>Explanation</u>
2	A body or wing definition failed in a previous link.
4	Error reading body stations from tape LA. Either the number of stations is less than 2 or greater than 51, or something is wrong with the tape.
6	Error reading body meridian lines from tape LA. Something is wrong with the tape or record 4 has more than 4368 words.
8	Error from subroutine TFLAT1.
10	Error reading wing percent lines from tape LA. Record 7 is not correct.
12	Record 7 on tape LA indicates that record 8 has more than 4368 words.
14	Error from subroutine WBXX in finding wing percent line intersections with the body (before transformation).
16	Either the leading or trailing edge of the wing does not intersect the body.
24	Error from subroutine WBXX in finding the intersections of the flattened wing with the transformed body.
26	Error from subroutine TFLATX. One or more of the flattened wing percent lines did not intersect the transformed body.
32	Error from subroutine BITURP in interpolating points on the radius versus station or z-centroid versus station curve.

If IOK = 2, the message "ERROR IN PREVIOUS LINK" is written. If IOK > 2, the message:

"TFLAT ERROR i, CODE j

IREC = i_1 i_2 i_3 i_4 "

is written, where i = IOK, j = error code from a subroutine (if IOK = 8, 14, 24, 26, or 32), and i_1, i_2, i_3, i_4 are the first four elements of the last odd-numbered record read from tape LA. If IOK = 14 or 16, the transformed wing percent lines are written by subroutine TFLATW to aid in diagnosing the error.

RESTRICTIONS:

Only a single wing surface can be processed. If tape LA is written by the geometry definition program, a lower-wing case cannot be handled since TFLAT only examines the upper-wing portion of tape LA. The number of words in records 4 and 8 cannot exceed 4368.

STORAGE:

$$11957_{10} = 27265_8$$

SUBJECT: FORTRAN IV Subroutine TFLAT1

PURPOSE: To transform body meridian lines to a new coordinate system, and to find the centroid and equivalent body radius at a set of body stations.

METHOD: This subroutine is used by subroutine TFLAT. The body centroid at each end of the body is found by subroutine BODCR. Then a new coordinate system is set up such that the origin is at the forward end centroid and the new x-axis passes through the aft-end centroid. After transforming the given body to the new coordinate system, the body radius and z-coordinate of the centroid is found at each given body station.

USAGE:

DIMENSION STA(51), B(2448), S(100, 2), E(2000),
RT(3, 4), ALFBET(2), RZ(51, 2) NU(3)

CALL TFLAT1 (CHD, NSTA, STA, NBPCT, B, S, E, RT,
ALFBET, RZ, EPRC, NU)

Input:

CHD	= A chord-arc tolerance, read from data card by subroutine TFLAT.
NSTA	= Number of body stations.
STA	= Array of original body stations (see Output, below).
NBPCT	= Number of body meridian lines.
B	= Array of points on original body meridian lines (see Output, below). This array (with a header) has a format as described in Appendix D,
EPRC	= A tolerance, read from data card by subroutine TFLAT.
NU	= Error indicator array. NU(1) is not used, on input. NU(2) is an output tape number on which to write a message if an error is detected; no message is written if $NU(2) \leq 0$. NU(3) is an error message limiter; if an error is detected, Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.

Output: STA = Array of transformed body stations.
 B = Array of points on transformed body meridian lines (with header).
 S = Scratch array.
 E = Scratch array.
 RT = Transformation matrix (see TROTPT).
 ALFBET = Transformation constants to convert original body stations to new stations (see TFLAT).
 RZ = Array of body radii and z-centroid corresponding to each body station.
 NU = Error indicator array (see Input)
 NU(1) = 0 for success.

SUBPROGRAMS CALLED:
 UVECN
 BSCALE
 BODCR
 VCROS
 TRAPCT
 TRAV

ERROR RETURNS: If an error is detected, the message "TFLAT ERROR i, CODE J," is written.

<u>i</u>	<u>j</u>	<u>Explanation</u>
1	k	Error k from BODCR at forward body end.
2	k	Error k from BODCR at aft body end.
3	0	The original body length is zero.
4	k	Error k from BSCALE.
5	0	The transformed body length is zero.
6	k	Error k from BODCR at some transformed body station (an additional comment will identify the station).

RESTRICTIONS: It is assumed that the given body meridian lines describe only half of a body that is symmetrical about a plane parallel to the xz plane.

STORAGE: $381_{10} \approx 575_8$

SUBJECT: FORTRAN IV Subroutine TFLATM

PURPOSE: To write body meridian line points on an output tape.

METHOD: This is primarily an output routine for TFLAT. The meridian lines are given in a single array with a format such as that described in Appendix D. The polar coordinates of each point are computed in a plane normal to the x-axis, with polar origin at the body axis.

USAGE: **DIMENSION** B(1), AXIS(2), TITLE(12), DAYT(2), STA(1)
CALL TFLATM (B, NB, AXIS, TITLE, DAYT, LO, STA)

Input: B = Array of meridian lines, with header.
 NB = Number of meridian lines.
 AXIS = y, z coordinates of main body axis.
 TITLE = Title (alphameric).
 DAYT = Date (alphameric).
 LO = Output tape number.
 STA = Not used.

Output: = Print-out on tape LO

SUBPROGRAMS ATN1
CALLED: SQRT (Built-in function)
 TRAV

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $346_{10} = 532_8$

SUBJECT: FORTRAN IV Subroutine TFLATW

PURPOSE: To write wing percent lines on an output tape.

METHOD: This is an output subroutine used by subroutine TFLAT.
 The percent lines are given in a single array with a format
 as described in Appendix D.

USAGE: DIMENSION B(1), TITLE(12), DAYT(2)
 CALL TFLATW (B, NB, TITLE, DAYT, LO)

Input: B = Array of percent lines, with header.
 NB = Number of percent lines.
 TITLE = Title (alphameric).
 DAYT = Date (alphameric).
 LO = Output tape number.

SUBPROGRAM
 CALLED: TRAV

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $312_{10} = 470_8$

SUBJECT: FORTRAN IV Subroutine TFLATX

PURPOSE: To write wing-body intersection points on an output tape.

METHOD: This is an output subroutine for subroutine TFLAT (see subroutine TFLAT). The polar coordinates of each point are computed and written on the output tape along with the x, y, z coordinates.

USAGE: DIMENSION DAT(2), W(1), WB(3, NW)
CALL TFLATX (LO, DAT, NW, W, WB, NU)

Input: LO = Output tape number.
DAT = Date (alphameric).
NW = Number of wing percent lines (also number of wing-body intersection points).
W = Array of wing percent lines, with header (see Appendix D).
WB = Array of points (x_i, y_i, z_i) that are the intersections of wing percent lines with body surface.

Output: NU = Error indicator, which is zero for success.

SUBPROGRAMS CALLED: ATN1
SQRT (Built-in function)
TRAV

ERROR RETURNS: NU = 1 if any intersection point is not valid (indicated by coordinates all 10^{30}).

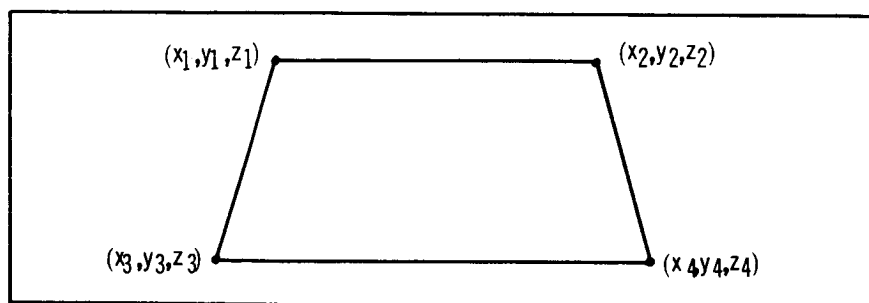
RESTRICTIONS: None

STORAGE: $240_{10} = 360_8$

SUBJECT: FORTRAN IV Subroutine THETAB

PURPOSE: To calculate body panel theta-inclination angles.

METHOD: The program calculates the panel theta-inclination angle by use of standard geometric formulae. The inclination angle θ is the angle of the panel in the x, y, z coordinate system of the body as viewed down the x-axis. A program check determines if the panel is "horizontal" by comparing the z-coordinates of the two trailing-edge panel corner points. If the panel is horizontal, theta is set equal to zero. For a nonhorizontal panel defined as follows,



theta is calculated from the formula,

$$\theta = \frac{|z_4 - z_3|}{(z_4 - z_3)} \cos^{-1} \left[\frac{A}{(A^2 + B^2)^{1/2}} \right]$$

for which,

$$A = \begin{vmatrix} x_1 & y_1 & 1 \\ x_3 & y_3 & 1 \\ x_4 & y_4 & 1 \end{vmatrix}$$

$$B = - \begin{vmatrix} x_1 & z_1 & 1 \\ x_3 & z_3 & 1 \\ x_4 & z_4 & 1 \end{vmatrix}$$

USAGE: COMMON (See subroutine OPCAMI for unlabeled COMMON description).

COMMON /COM1/ (See subroutine PANEL)

**Input: NPER1
 NPLN1**

COMMON /COM2/ (See subroutine BODY)

**Input: XCOR
 YCOR
 ZCOR**

Output: THETA

CALL THETAB

SUBPROGRAMS

CALLED:

ACOS

SQRT (Built-in function)

ERROR RETURNS:

None

STORAGE:

$244_{10} = 364_8$

SUBJECT: FORTRAN IV Subroutine TRAPCT

PURPOSE: To perform a coordinate transformation on a set of body meridian lines or wing percent lines.

METHOD: Subroutine TROTPT is applied to transform each point, using a given transformation matrix.

USAGE: DIMENSION B(1), RT(3, 4)
CALL TRAPCT (B, N, RT)

Input: B = Meridian or percent line array (see sub-
routines TFLAT and TFLAT1).
N = Number of meridian or percent lines.
RT = Transformation matrix (see subroutine
TROTPT).

Output: B = Transformed array.

**SUBPROGRAM
CALLED:** TROTPT

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $86_{10} = 126_8$

SUBJECT: FORTRAN Subroutine TRAV

PURPOSE: To move a block of N cells starting at location B to another region starting at location A.

METHOD:

```

DO 100 I = 1, N
100 A(I) = B(I)

```

USAGE

```

CALL TRAV (A, B, N)
DIMENSION A(N), B(N)

```

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: $N > 0$

STORAGE: $35_{10} = 43_8$

SUBJECT: FORTRAN IV Subroutine TROTPT

PURPOSE: Given the coordinates of a point (in 3-space) in one of two rectangular Cartesian coordinate systems and the rotation and translation matrices relating the systems, to compute the coordinates of the point in the other system.

METHOD: Let an arbitrary point have the coordinates $P = (X_1, Y_1, Z_1)$ in an $X_1 Y_1 Z_1$ coordinate system, and the coordinates $Q = (X_2, Y_2, Z_2)$ in an $X_2 Y_2 Z_2$ coordinate system. Let R be a 3-by-3 rotation matrix constructed as follows: the first column is a unit vector, in the $X_1 Y_1 Z_1$ system, along the $+X_2$ axis; similarly, the second column is a unit vector along the $+Y_2$ axis, and the third column is a unit vector along the $+Z_2$ axis. Let T be a 1-by-3 translation matrix that contains the $X_1 Y_1 Z_1$ coordinates of the origin of the $X_2 Y_2 Z_2$ system. Then, if P and Q are considered to be 1-by-3 matrices,

$$Q = (P - T)R$$

$$P = QR^{-1} + T$$

USAGE: DIMENSION R(3 3), T(3), P(3), Q(3)
CALL TROTPT (R, T, K, P, Q)

Input: R = Rotation matrix.
T = Translation matrix.
K = A code that is 1 if Q is input and P is output,
or 2 if P is input and Q is output.

P
or Q = Point coordinates.

Output: Q
or P = Point coordinates.

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: The rotation matrix must be orthogonal. The same array may be used for both P and Q; e.g., CALL TROTPT(R, T, 1, Q, Q).

STORAGE: $112_{10} \approx 160_8$

SUBJECT: FORTRAN IV Subroutine TTAPE

PURPOSE: To copy matrices from tape to tape.

METHOD: A single matrix (or multiple matrices) is read from one tape and written on a second tape under binary format.

USAGE: CALL TTAPE (KIND, IN, JN, NTIN, NTOUT, A, B, C)

DIMENSION A(IN), B(IN), C(IN)

Input: KIND = Code for number of matrices to be copied. If KIND = 0, one matrix (A) to be copied. If KIND \neq 0, three matrices (A, B, and C) to be copied.

IN = Number of rows.

JN = Number of columns.

NTIN = Tape from which matrices are read.

NTOUT = Tape on which matrices are written.

A } = Dummy arrays.

B }

C }

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $159_{10} = 237_8$

SUBJECT: FORTRAN IV Subroutine TVEL

PURPOSE: To compute the velocity components resulting from a specified wing thickness distribution from the velocity components resulting from a wing thickness distribution of unit incidence.

METHOD: The velocity components in the x, y, and z directions on panel i resulting from a specified wing thickness distribution of incidence α T_j are found by:

$$U_i = \sum_{j=1}^{NWING} U_{ij} \cdot \alpha T_j$$

$$V_i = \sum_{j=1}^{NWING} V_{ij} \cdot \alpha T_j$$

$$W_i = \sum_{j=1}^{NWING} W_{ij} \cdot \alpha T_j$$

where U_i , V_i and W_i = The i^{th} velocity components resulting from a wing thickness distribution of unit incidence.

NWING = The total number of wing panels.

The normal component of velocity on a body panel i resulting from wing thickness is given by

$$n_{B_i} = \sum_{j=1}^{NWING} A_{BWS_{ij}} \cdot \alpha T_j$$

where A_{BWS} = The normal velocity on the body resulting from wing thickness distribution of unit incidence.

USAGE: CALL TVEL (A, B, C, D, ALPHAT, UBWT, VBWT, WBWT, UWWT, VWWT, WWWT, AN, CHORD, THICK, NROW)

COMMON DATE(2), NTAPEA, NTAPEB, NTAPEC,
 NTAPEB, NTAPEE, NTAPEF, NTAPEI,
 NTAPEO, NBODY, NWIN, XMACH, SYM,
 KACE

DIMENSION A(210), B(210), C(210), D(210),

ALPHAT (110), UBWT (100), VBWT (100), WBWT (100),

UWWT (110), VWWT (110), WWWT (110), AN (100),

CHORD (210), NROW (2)

Input: A }
 B } = Dummy arrays
 C }
 D }

ALPHAT = Array of wing thickness slopes.

CHORD = Array of panel chord lengths.

NROW = Array of number of rows of panels.

For wing-alone configurations,
 NROW (1) = number of panel rows
 on wing and NROW (2) is dummy
 argument. For wing-body config-
 urations, NROW (1) = number of
 panel rows on body and NROW (2)
 = number of panel rows on wing.

THICK = Code. If THICK = 0, wing thickness
 effects to be ignored. If THICK =
 1, wing thickness effects to be
 included.

Output: UBWT } = Arrays of velocity components in x-,
 VBWT } y- and z-directions on the body due
 WBWT } to a given wing thickness distri-
 bution.

UWWT } = Arrays of velocity components in
 VWWT } x-, y- and z-directions on the
 WWWT } wing due to a given wing thickness
 distribution.

AN = Array of normal velocity components
on the body due to a given wing
thickness distribution.

SUBPROGRAM

CALLED: FSF

ERROR RETURNS: None

RESTRICTIONS: NBODY \leq 100

NWING \leq 110

STORAGE: $580_{10} = 1104_8$

SUBJECT: FORTRAN IV Subroutine UNLOAD

PURPOSE: To rewind and unload a logical tape unit. The unload operation prevents any further reading or writing on the specified unit until the unit is readied by an operator.

METHOD: The program delays until all I-O operations are finished, executes a rewind and unload command, then delays until the channel is again out of operation.

USAGE: CALL UNLOAD (NT)

Input: NT = logical tape number

SUBPROGRAMS CALLED: None

RESTRICTIONS: None

ERROR RETURNS: None

STORAGE: $43_{10} = 53_8$

SUBJECT: FORTRAN IV Subroutine USETAP

PURPOSE: To read the aerodynamic matrices for a given configuration and Mach number from a previously saved tape and to rewrite them on other logical tapes in the formats required for a computer run.

METHOD: The previously saved tape is mounted on logical tape NTAPEC and the aerodynamic matrices are read and rewritten on other logical tapes as indicated below.

For wing alone configurations, the matrices are written in the order:

	<u>New Tape</u>	<u>Matrix</u>	<u>Description</u>
1.	NTAPEA	$\begin{bmatrix} A_{WW} \end{bmatrix}$	Aerodynamic influence coefficients due to wing sources.
2.	NTAPEA	$\begin{bmatrix} WW \end{bmatrix}$	Drag minimization.
3.	NTAPEA	$\begin{bmatrix} WW \end{bmatrix}^{-1}$	Inverse of drag minimization matrix constrained for wing lift.
4.	NTAPEA	$\begin{bmatrix} WW \end{bmatrix}^{-1}$	Inverse of drag minimization matrix constrained for wing lift and pitching moment.
5.	NTAPEB	$\begin{bmatrix} U_{WW} \end{bmatrix}$	Velocity components due to wing sources.
		$\begin{bmatrix} V_{WW} \end{bmatrix}$	
		$\begin{bmatrix} W_{WW} \end{bmatrix}$	
6.	NTAPEB	$\begin{bmatrix} U_{WW} \end{bmatrix}$	Velocity components due to wing surface vortices.
		$\begin{bmatrix} V_{WW} \end{bmatrix}$	
		$\begin{bmatrix} W_{WW} \end{bmatrix}$	
7.	NTAPEE	$\begin{bmatrix} A_{WW} \end{bmatrix}$	Aerodynamic influence coefficients due to wing surface vortices.

- | | | |
|-----------|-----------------|---|
| 8. NTAPEE | $[A_{WW}]^{-1}$ | Inverse of matrix of aerodynamic influence coefficients due to wing surface vortices. |
|-----------|-----------------|---|

For wing-body configurations, the matrices are written in the following order:

<u>New Tape</u>	<u>Matrix</u>	<u>Description</u>
1. through 5.	(same as wing-alone configurations)	
6. NTAPED	$[U_{BB}]$ $[V_{BB}]$ $[W_{BB}]$	Velocity components on the body due to body surface vortices.
7. NTAPED	$[U_{WB}]$ $[V_{WB}]$ $[W_{WB}]$	Velocity components on the wing due to body surface vortices.
8. NTAPED	$[U_{BW}]$ $[V_{BW}]$ $[W_{BW}]$	Velocity components on the body due to wing surface vortices.
9. NTAPED	$[U_{WW}]$ $[V_{WW}]$ $[W_{WW}]$	Velocity components on the wing due to wing surface vortices.
10. NTAPEE	$[A_R]$	"Reduced" aerodynamic matrix.
11. NTAPEE	$[A_R]^{-1}$	Inverse of "reduced" aerodynamic matrix.
12. NTAPEF	$[A_{BB}]^{-1}$	Inverse of matrix of aerodynamic influence coefficients.

	New Tape	Matrix	Description
13.	NTAPEF	$[D]$	Product matrix.

$$[D] = [A_{WB}] \cdot [A_{BB}]^{-1}$$

14.	NTAPEF	$[E]$	Product matrix.
-----	--------	-------	-----------------

$$[E] = [A_{BB}] \cdot [A_{BW}]$$

This subroutine is not used for body-alone configurations.

USAGE:

CALL USETAP

Input:	NTAPEA	}	= Logical tape numbers on which aerodynamic matrices are rewritten.
	NTAPEB		
	NTAPED		
	NTAPEE		
	NTAPEF		
	NTAPEEC		
			= Logical tape number of save tape and from which aerodynamic matrices are read.

SUBPROGRAMS

CALLED:

TTAPE
FSF

ERROR RETURNS: None

RESTRICTIONS: This subroutine is not used for body-alone configurations.

STORAGE: $1309_{10} = 2435_8$

SUBJECT: FORTRAN Function UVECN

PURPOSE: Given two points A and B in N-space, to find components of vector (or unit vector) directed from A to B and distance between A and B.

METHOD: Vector $\bar{V} = \bar{B} - \bar{A}$ and sum $S = V_1^2 + V_2^2 + \dots + V_n^2$ are formed. If $S > 0$, then distance $D = \sqrt{S}$; if a given code indicates that a unit vector is required, then $\bar{V} = \bar{V}/D$. Function value UVECN is set to D before return. If $S = 0$, then $\bar{V} = \bar{0}$ and $D = 0$.

USAGE: $D = \text{UVECN}(A, B, V, K, N)$
DIMENSION A(N), B(N), V(N)

Input: A, B = Point coordinates
K = If K = 0, then a unit vector
 $V = (B - \bar{A}) / |\bar{B} - \bar{A}|$ is desired;
N = If K \neq 0, then $\bar{V} = \bar{B} - \bar{A}$.
Dimension of the space in which A and B are defined.

Output: V = Vector \bar{V}
D = Distance from A to B

SUBPROGRAM CALLED: SQRT (Built-in function)

ERROR RETURNS: None

RESTRICTIONS: $N > 0$

STORAGE: $80_{10} = 120_8$

SUBJECT: FORTRAN IV Subroutine VCROS

PURPOSE: To find cross-product of two vectors.

METHOD: Given vectors $\bar{A} = \begin{pmatrix} a_1 \\ a_2 \\ a_3 \end{pmatrix}$ and $\bar{B} = \begin{pmatrix} b_1 \\ b_2 \\ b_3 \end{pmatrix}$, then cross-product,
 $\bar{A} \times \bar{B}$, is vector

$$\bar{V} = \begin{pmatrix} a_2 b_3 - a_3 b_2 \\ a_3 b_1 - a_1 b_3 \\ a_1 b_2 - a_2 b_1 \end{pmatrix}$$

USAGE: DIMENSION A(3), B(3), V(3)
 CALL VCROS (A, B, V, D, K)

Input: A = \bar{A}
 B = \bar{B}
 K = 0 if \bar{V} is not to be normalized
 $\neq 0$ if \bar{V} is to be normalized

Output: V = $\bar{A} \times \bar{B}$ if K was 0
 = $(\bar{A} \times \bar{B})/D$ if K was not 0 and D > 0.
 D = Magnitude of V (before normalization)
 K = 0 if success
 = 1 if K $\neq 0$ on input and D = 0.

SUBPROGRAM
CALLED: VDOTP
 SQRT (Built-in function)

RESTRICTIONS: Note that K is both an input and an output.

STORAGE: 106₁₀ = 152₈

SUBJECT: FORTRAN Function VDOTN

PURPOSE: To find dot-product of two vectors in N-space.

METHOD: Standard

USAGE: DP = VDOTN (A, B, N)
 DIMENSION A(N), B(N)
 Input: A = Vector of dimension N
 B = Vector of dimension N
 Output: $DP = \bar{A} \cdot \bar{B} = \sum_{i=1}^N A_i B_i$

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: $N > 0$

STORAGE: $40_{10} = 50_8$

SUBJECT: FORTRAN IV Function VDOTP

PURPOSE: To find dot-product of two vectors.

METHOD: Given two vectors $\bar{A} = \begin{pmatrix} a_1 \\ a_2 \\ a_3 \end{pmatrix}$ and $\bar{B} = \begin{pmatrix} b_1 \\ b_2 \\ b_3 \end{pmatrix}$, dot-product is the scalar $P = a_1 b_1 + a_2 b_2 + a_3 b_3$.

USAGE: DIMENSION A(3), B(3)
P = VDOTP (A, B)
Input: A = Vector \bar{A}
B = Vector \bar{B}
Output: P = A · B

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $43_{10} = 53_8$

SUBJECT: FORTRAN IV Subroutine VEL1

PURPOSE: To compute velocity components and pressures induced at field points by sources and doublets on an isolated body (Refer to KARMOR).

METHOD: The equations used in this routine are given in Part I, section 4.4.

USAGE: COMMON/FLOV1/KACE, NPANEL, NBODY, NWING, NBODYS, NWINGS, NROW(2), XMACH, SYM

DIMENSION A(210, 3, 4), B(210, 3, 4), C(210, 3, 4), NPART(210)

DIMENSION ALPHAS (210), THETA(210)

DIMENSION XB(50), R(50), WT(120)

DIMENSION T(50), TC(50), SST(210), CHORD(210)

COMMON/FLOV2/A, B, C, NPART, ALPHAS, THETA, XB, R, WT, T, TC, SST, CHORD

COMMON/FLOV3/T11, TC11

COMMON/THICK/THKW, ARA

CALL VEL1 (X, Y, Z, UU, VV, WW)

Input: X = x-coordinate of field point.

Y = y-coordinate of field point.

Z = z-coordinate of field point.

XB = Array of x-coordinates of the body line source and doublet segments.

R = Array of body radii defined at the XB coordinates.

T = Array of line source strength.

TC = Array of doublet strengths.

T11 = Strength of linearly varying source.

TC11 = Strength of linearly varying doublet.

ARA = Angle of attack.

Output:	UU	= x-direction velocity component due to body.
	VV	= y-direction velocity component due to body.
	WW	= z-direction velocity component due to body.

SUBPROGRAMS
CALLED:

ALOG	}	(Built-in functions)
COS		
SQRT		
SIN		
ATN1		

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $400_{10} = 740_8$

SUBJECT: FORTRAN IV Subroutine WBX

PURPOSE: To find the intersections of a set of wing percent chord lines with a body surface and to delete the portions of percent chord lines inside the body.

METHOD: The body surface is defined by an array of NB meridian lines and a code that determines body shape between meridian lines (see subroutine WBXUL). Each wing percent chord line consists of a series of straight-line segments connecting three-dimensional points. The intersection of each wing percent chord line with the body surface is then calculated.

The body is cut (see subroutine WBXC) by a transverse plane that passes through the first wing percent chord point. The horizontal distance normal to the x-axis from the percent point to the body surface is found in this region. This calculation is repeated for successive percent chord line points until a change in sign of the distance is detected; this means that the last two wing points, W_1 and W_2 for example, are on opposite sides of the body surface. An iterative procedure is now used to locate the intersection point.

Let α be the distance along the line segment $\overline{W_1 W_2}$ from W_1 to some point W on the segment. Let $f(\alpha)$ be the horizontal distance from W to the body surface. If L is the length of $\overline{W_1 W_2}$, then $f(0)$ and $f(L)$ have opposite signs (because $f(0)$ corresponds to W_1 and $f(L)$ corresponds to W_2). Subroutine FROOTA is used to iterate on α until $f(\alpha)$ is as small as possible. The point W is then on or very near the body surface; the corresponding point on the body surface is taken as the intersection.

If the first wing percent chord line point is forward or aft of the body, the transverse plane through the point does not intersect the body; WBX then continues to process points until a body intersection is found. If all points so far processed are on the same side of the body surface, and the current point is forward or aft of the body, then the previous point is taken as W_1 ; W_2 is found by subroutine WBXD as the intersection of the percent chord line with a transverse plane through the appropriate body end. If all percent chord lines are processed without finding two adjacent points on opposite sides of the body surface, the intersection point is taken as $(10^{30}, 10^{30}, 10^{30})$ to indicate that no intersection point was found.

USAGE:

DIMENSION B(1), W(1), S(2, NB), BW(3, NW), NU(3)

CALL WBX (B, NB, W, NW, EPS, KODE, S, BW, NU)

Input: B = Array of body meridian lines (described in subroutine WBXUL).

NB = Number of meridian lines.

W = Array of wing percent chord lines (described in subroutine WBXUL).

NW = Number of percent chord lines.

EPS = Tolerance — a message will be written on the output tape (see NU) if the error in finding an intersection is greater than EPS.

KODE = A code that determines the shape of the body surface between meridian lines (see subroutine WBXUL).

NU = Error indicator array: NU(1) is not used on input. NU(2) is an output tape number on which to write a message if an error is detected; no message is written if $NU(2) \leq 0$. NU(3) is an error message limiter; if an error is detected, $NU(3) = (NU(3) - 1)$. Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.

Scratch: S = Storage for sections through the body.

Output: W = Array of wing percent chord lines, truncated at the body surface.

BW = Array of intersection points (x_i, y_i, z_i).

NU = Error indicator array: NU(1) is zero if no error is detected. NU(3) may have been changed (see INPUT, above).

SUBPROGRAMS

CALLED:

UVECN
FROOTA
TRAV
WBXA
WBXC
WBXD

ERROR RETURNS: The following message is written (see NU) if an error is detected: "ERROR i, CODE j IN SUBROUTINE WBX, WING PERCENT LINE m, POINT n."

<u>i</u>	<u>i</u>	<u>Explanation</u>
4	1	WBXA error; see note 1, below.
5	2	WBXD error; see message written by WBXD.
6	-3	WBXC error; first and last points in a body section (through a wing percent line point) have the same z-coordinate.
7	3	WBXC error; two points in body section, near the wing-body intersection, have the same z-coordinate
8	1 2	A wing percent chord line point is above or below the body section and has the same y-coordinate as the first or last section point.
9	-	See note 1.
10	k	WBXC error k in iteration loop.
11	k	FROOTA error; see note 1.
12	0	Iteration to find intersection did not converge; see note 1.

Note 1: Machine or program error.

RESTRICTIONS: If a wing percent chord line intersects the body surface more than once, only one intersection point will be found. Body sections in the wing-body intersection region must be single-valued in y as a function of z. Wing percent chord lines must have at least one point that lies between body station planes through the body ends. A percent chord line intersection will not be found, even though it exists, if all percent chord points except the last are forward (or aft) of the body.

STORAGE: $605_{10} = 1135_8$

SUBJECT: FORTRAN IV Subroutine WBXA

PURPOSE: To modify a wing percent chord line array so that the first part of a given percent chord line is removed.

METHOD: The format of the wing percent chord line array, B, is explained in Appendix D. K, the number of points to be removed, and P, the new first-point, are given. If K = 0, P is not used and the entire old percent chord line is moved to its new position. Otherwise, K points are removed and P, followed by the remaining points, is moved. The corresponding portion of the array header is adjusted to reflect the new location of the percent chord line in the array and the new number of points. The remaining percent chord lines are not disturbed.

USAGE: DIMENSION B(1), P(3)
CALL WBXA (B, I, K, P, NU)

Input: B = Percent chord line array.
I = The percent chord line to be modified.
K = Number of points to be removed.
P = New first-point.

Output: B = Modified percent chord line array.
NU = Error indicator, which is zero if successful.

SUBPROGRAM CALLED: None

ERROR RETURNS: NU = 1 if $K < 0$ or if $K \geq$ number of points in old percent chord line.

RESTRICTIONS: WBXA must be called successively with $I = 1, 2, \dots, N$ where N = number of percent chord lines.

STORAGE: $202_{10} = 312_8$

SUBJECT:

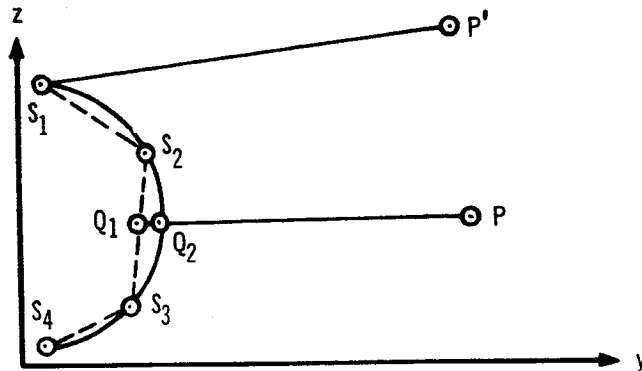
FORTRAN IV Subroutine WBXC

PURPOSE:

To find the distance from an arbitrary point to a body surface.

METHOD:

The body is described by NB meridian lines (see subroutine WBXUL). Let $P(x_P, y_P, z_P)$ be the given point. Subroutine BCUTX is used to find the intersection points (y_i, z_i) of the plane $x = x_P$ with the meridian lines. The points form a body section, S.



Let $Q(x_Q, y_Q, z_Q)$ be a point on the body so that $x_Q = x_P$, $z_Q = z_P$. The value of y_Q is found by interpolation at $z = z_Q$ from the table (z_i, y_i) , using subroutine BITURP. If a given code is 1, the interpolation is linear (Q_1 in figure); if the code is 2, the interpolation is biquadratic (Q_2 in figure). This code effectively determines the body shape between meridian lines. If P should be above the body (see P' in drawing), then Q is taken as the first meridian line point. Similarly, the last meridian line point is used for Q if P is below the body. The required distance from P to the body surface is $y_P - y_Q$.

USAGE:

DIMENSION B(1), P(3), S(2, NB), Q(3)

CALL WBXC (B, NB, EP, P, CODE, S, D, Q, NU)

Input: B = Array of body meridian line points, with header (see subroutine WBXUL).

NB = Number of body meridian lines.
 EP = Tolerance used by BCUTX in finding intersections of body meridian lines with the plane $x = P(1)$.
 P = x, y, z coordinates of given point.
 KODE = Code, used by BITURP, that determines the shape of the body between meridian lines. KOD = 1 if polygonal, 2 if not (see METHOD, above).
 Output: S = Section points (y_i, z_i) , $i = 1, 2, \dots, NS$, where $NS \leq NB$.
 D = Distance.
 Q = Point on body surface.
 NU = Error indicator array. NU = 0, 1 or 2 if successful; 0 if $Q(3) = P(3)$, 1 if S_1 was used for Q, 2 if S_{NB} was used for Q.

SUBPROGRAMS BITURP
 CALLED: BCUTX

ERROR RETURNS: NU = -5 if the number of section points is less than 2; this may be caused by $NB < 2$ or failure of the plane $x = x_P$ to cut some of the meridian lines. NU = -3 if S_1 and S_{NB} have the same z-coordinate.

RESTRICTIONS: The value of D returned is the horizontal distance between P and Q; if P is above or below the body, the true distance is greater than D. If all meridian lines do not have the same x-range, the number of section points (S) may possibly be less than NB; see BCUTX.

STORAGE: $139_{10} = 213_8$

SUBJECT: FORTRAN IV Subroutine WBXD

PURPOSE: To find a point on a wing percent chord line which lies in the first or last body station plane, and to determine the horizontal distance of that point from the body surface.

METHOD: Subroutine WBXD is called by subroutine WBX only if the following situation arises: At least one point, W_1 , for instance, on some wing percent chord line has been processed; but the next point, W_2 , is either forward or aft of the body. Let BXF and BXL be the extreme x-coordinates of body meridian line 1; let WXF and WXL be the x-coordinates of W_1 and W_2 , respectively. If BXF lies in the range (WXF, WXL), a plane $x = BXF$ is formed; otherwise BXL is assumed to be the range and the plane is taken as $x = BXL$. The line segment $\overline{W_1W_2}$ is intersected with the plane to obtain point P, which lies on the wing percent line. The horizontal distance from P to the body, and the corresponding point Q on the body are then found by subroutine WBXC.

USAGE: DIMENSION R(4), B(1), P(3), Q(3), S(2, NB), W(3, 2), NU(3)

Call WBXD (R, B, NB, KODE, P, Q, S, W, NU)

Input: B = Array of body meridian line points, with header (see subroutine WBXUL).

NB = Number of body meridian lines.

KODE = Body shape code (see WBXC).

W = Two adjacent points on a wing percent chord line (see W_1 and W_2 , METHOD, above).

NU = Error indicator array. NU(1) is not used, on input. NU(2) is an output tape number on which to write a message if an error is detected; no message is written if $NU(2) \leq 0$. NU(3) is an error message limiter; if an error is detected, $NU(3) = (NU(3) - 1)$. Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.

Output: S = Section points (Y_i, Z_i).

R = R(1) = x-coordinate of P; R(2) = horizontal distance = P(2) - Q(2); R(3) = R(1); R(4)

P = x, y, z coordinates of point on wing percent chord line.

Q = Corresponding point on body surface.

NU = Error indicator array. NU(1) is zero if success. NU(3) may have changed if an error was detected (see Input).

SUBPROGRAMS CALLED: POLXN
WBXC

ERROR RETURNS: A message "ERROR i, CODE j, IN SUBROUTINE WBXD" is written if an error is detected.

<u>i</u>	<u>j</u>	<u>Explanation</u>
1	0	Machine or program error.
2	k	Error k from WBXC. If k = 1 or 2, point P is above or below the body and P(2) = Q(2).

RESTRICTIONS: See WBXC

STORAGE: $219_{10} = 333_8$

SUBJECT: FORTRAN IV Subroutine WBXUL

PURPOSE: To find the intersections of upper and lower wing percent chord lines with a body surface, to delete the portions of percent chord lines that are inside the body, and to write results.

METHOD: A set of NB meridian lines defines the basic body surface. These lines may be visualized as stringers running lengthwise along the surface of the body. Each meridian line consists of a series of straight-line segments connecting three-dimensional points. The surface between meridian lines is determined by taking any section, normal to the X-axis, through the body; this yields the (Y, Z) coordinates of NB points on the surface. Under one option, the surface at this section is assumed to be polygonal (adjacent points connected by straight lines). In the other option, the surface between each pair of points is assumed to be represented by a cubic; points between meridian lines are interpolated by subroutine BITURP.

The wing surface (upper, lower, or both) is defined by NW wing percent chord lines, which are similar to meridian lines. The 0-percent line forms the leading edge of the wing, and the 100-percent line is the trailing edge. The wing surface is not defined between percent chord lines. The main function of WBXUL is to find the point of intersection of each wing percent chord line with the body surface.

All of the body meridian line points are stored in a single array. The first 3*NB cells form a "header" that is a key to the rest of the array. Cell 1 is a number that forms a label for the first meridian line. Cell 2 contains the number of points in the first meridian line. Cell 3 contains the cell number at which the x-coordinate of the first point in the first meridian line is located. Similarly, cells 4, 5, and 6 apply to the second meridian line, etc. This storage scheme, described in Appendix D, is also used for the upper wing percent lines and the lower percent lines.

The subroutine begins by a check that the body and at least one wing surface are defined. Then one card is read with FORMAT(2F10.0). The first field contains a code, later used by BITURP, that determines body shape between

meridian lines (1 if polygonal, 2 if not). The second field contains a tolerance, EPS, that is set to 10^{-5} if less than 10^{-5} ; subroutine WBX writes a message if the error in locating an intersection point is more than EPS. The following process is then carried out, for the upper wing surface and then the lower.

If the wing surface is defined, storage is reserved in the buffer for the intersection points (see Appendix A). Subroutine WBX is called to find the intersection points and remove that part of each wing percent chord line inside the body surface. Each wing percent chord line now starts at the body surface; this, of course, requires a new "header" for the array. The X, Y, Z and polar coordinates of each intersection point are written on the output tape. The polar coordinate system for each point lies in a plane through the point and normal to the X-axis, with origin at the known body axis; the angle is measured from the vertical (Z-axis). If any percent line fails to intersect the body surface, a message is written but the routine continues.

USAGE:

```
DIMENSION B(1), DAT(2), LOK(3, 9), BTITLE(12),
          WTITLE(12), BAXIS(2), NU(3)
```

```
LOGICAL LGDEF(3, 6)
```

```
CALL WBXUL(B, LI, LO, DAT, LGDEF, LOK, BTITLE,
          WTITLE, BAXIS, NU)
```

Input:	B	= Storage buffer for variable length arrays.
	LI	= Input tape number.
	LO	= Output tape number.
	DAT	= Date (alphameric).
	LGDEF(2, 1)	= .TRUE. if upper wing is defined.
	(2, 2)	= .TRUE. if lower wing is defined.
	(2, 3)	= .TRUE. if body is defined.
	LOK	= Array that tells where in B the wing percent chord line arrays and body meridian line array are located, and the length of each array. Consider LOK(1, j): The upper wing percent chord line corresponds to

LOK(i, 1), the lower to LOK(i, 2); the body corresponds to LOK(i, 3). An array starts in B(LOK(1, j)). LOK(2, j) = number of percent chord lines or meridian lines. LOK(3, j) = total number of elements in array.

BTITLE = Body title (alphameric).

WTITLE = Wing title (alphameric).

BAXIS = Y and Z coordinates of the body axis.

NU = Error indicator array: NU(1) is not used, on input. NU(2) is an output tape number on which to write a message if an error is detected; no message is written if $NU(2) \leq 0$. NU(3) is an error message limiter; if an error is detected, $NU(3) = (NU(3) - 1)$. Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.

Output: B = Storage buffer for variable-length arrays.

LGDEF(1, 5) = Set equal to LGDEF(1, 1) to indicate that a wing-body intersection was requested.

(1, 6) = Set equal to LGDEF(1, 2).

(2, 5) = Set to .TRUE. if intersections of the upper wing percent chord lines with the body were found.

(2, 6) = Set to .TRUE. if intersections of the lower wing percent chord lines with the body were found.

LOK = Array that tells where in B various arrays are stored (see Input). The truncated upper wing percent chord lines (part outside body) correspond to j = 3, the lower to j = 4; the upper intersection point array corresponds to j = 8, the lower to j = 9. An array starts in

= B(LOK(1, j)). LOK(3, j) = total number of elements in array. LOK(2, j) = number of percent lines if j = 3 or 4. LOK(2, j) is not used for j = 8 or 9.

NU = Error indicator array. NU(1) is zero if success. NU(3) may have been changed if an error was detected; see Input, above.

SUBPROGRAMS CALLED: ATN1
WBX
MERR
SQRT (Built-in function)
TRAV
IRSERV } (see Appendix A)
IPACK }

ERROR RETURNS: Function MERR is used to write a message "ERROR i, CODE j IN SUBROUTINE WBXUL DURING GEOMETRIC DEFINITION" if an error is detected.

<u>i</u>	<u>j</u>	<u>Explanation</u>
1	0	Either the body or wing was not successfully defined. However, if both upper and lower wing surfaces were requested but one surface failed, this error will not stop WBXUL (provided the body is defined).
2	0	} The storage buffer, B, is not large enough or, a storage error has been detected.
3	0	
4	k	Error k from WBX.

RESTRICTIONS: The storage buffer, B, must have been initialized by subroutine INIBFR (see Appendix A) or its equivalent. The original wing percent lines (stored starting in B(LOK(1, i)), i = 1 and 2) are destroyed.

STORAGE: $758_{10} = 1366_8$

SUBJECT: FORTRAN IV Subroutine WBXX

PURPOSE: To find the intersections of a set of wing percent chord lines with a body surface.

METHOD: The body surface is defined by an array of NB meridian lines and a code that determines body shape between meridian lines (see subroutine WBXUL). Each wing percent line consists of a series of straight-line segments connecting three-dimensional points. The intersection of each wing percent chord line with the body surface is found in turn.

The body is cut (see subroutine WBXC) by a transverse plane that passes through the first wing percent chord line point. In this section, normal to the X-axis, the horizontal distance (with sign) from the percent point to the body surface is found. This process is repeated for successive percent chord line points until a change in sign of the distance is detected; this means that the last two wing points, W_1 and W_2 , for example, are on opposite sides of the body surface. An iterative procedure is now used to locate the intersection point.

Let α be the distance along the line segment $\overline{W_1W_2}$ from W_1 to some point W on the segment. Let $f(\alpha)$ be the horizontal distance from W to the body surface. If L is the length of $\overline{W_1W_2}$, then $f(0)$ and $f(L)$ have opposite signs (because $f(0)$ corresponds to W_1 and $f(L)$ corresponds to W_2). Subroutine FROOTA is used to iterate on α until $f(\alpha)$ is as small as possible. The point W is then on or very near the body surface; the corresponding point on the body surface is taken as the intersection.

If the first wing percent chord line point is forward or aft of the body, the transverse plane through the point does not intersect the body; WBXX then continues to process points until a body intersection is found. If all points so far processed are on the same side of the body surface, and the current point is forward or aft of the body, then the previous point is taken as W_1 ; W_2 is found by subroutine WBXD as the intersection of the percent chord line with a body station plane through the appropriate body end. If all percent chord lines are processed without finding two adjacent points on opposite sides of the body surface, the intersection point is taken as $(10^{30}, 10^{30}, 10^{30})$ to indicate that no intersection point was found.

USAGE:

DIMENSION B(1), W(1), S(2, NB), BW(3, NW), NU(3)

CALL WBXX (B, NB, W, NW, EPS, KODE, S, BW, NU)

Input: B = Array of body meridian lines (described in subroutine WBXUL).

NB = Number of meridian lines.

W = Array of wing percent chord lines (described in subroutine WBXUL).

NW = Number of percent chord lines.

EPS = Tolerance; a message will be written on the output tape (see NU) if the error in finding an intersection is greater than EPS.

KODE = A code that determines the shape of the body surface between meridian lines (see subroutine WBXUL).

NU = Error indicator array. NU(1) is not used, on input. NU(2) is an output tape number on which to write a message if an error is detected; no message is written if $NU(2) \leq 0$. NU(3) is an error message limiter; if an error is detected, $NU(3) = (NU(3) - 1)$. Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.

Scratch: S = Storage for sections through the body.

Output: BW = Array of intersection points (x_i, y_i, z_i) .

NU = Error indicator array. NU(1) is zero if no error is detected. NU(3) may have been changed (see Input, above).

SUBPROGRAMS CALLED:

UVECN
FROOTA
TRAV
WBXC
WBXD

ERROR RETURNS:

The following message is written (see NU) if an error is detected: "ERROR i, CODE j IN SUBROUTINE WBXX, WING PERCENT LINE m, POINT n."

<u>i</u>	<u>j</u>	<u>Explanation</u>
5	2	WBXD error; see message written by WBXD.
6	-3	WBXC error; first and last points in a body section (through a wing percent line point) have the same z-coordinate.
7	3	WBXC error; two points in body section, near the wing-body intersection, have the same Z-coordinate
8	1 2	A wing percent line point is above or below the body section and has the same Y-coordinate as the first or last section point.
9	-	See note 1, below.
10	k	WBXC error k in iteration loop.
11	k	FROOTA error; see note 1.
12	0	Iteration to find intersection did not converge; see note 1.

Note 1: Machine error or program error.

RESTRICTIONS:

If a wing percent chord line intersects the body surface more than once, only one intersection point will be found. Body sections in the wing-body intersection region must be single-valued in y as a function of z. Wing percent chord lines must have at least one point that lies between body station planes through the body ends. A percent chord line intersection will not be found, even though it exists, if all percent points except the last are forward (or aft) of the body.

STORAGE:

$$584_{10} = 1110_8$$

SUBJECT: FORTRAN IV Subroutine WING

PURPOSE: To serve as control program for wing paneling subroutines.

METHOD: Program uses a series of FORTRAN IV language "CALL" instructions to call required wing paneling subroutines.

The program has the following labeled COMMON statement that is also in all lower level wing geometry paneling subroutines,

```
COMMON /COM2/ IJ, NPTS(16), X(90, 16), Y(90, 16),  
Z(90, 16), KPNT, VALUE(5), YCEPT(16), SLOPE,  
KPANEL(2, 15), XCOR(16, 16), YCOR(16, 16), ZCOR(16, 16)  
XINT(2, 15), YINT(2, 15), ZINT(2, 15), XCEN(15, 15),  
YCEN(15, 15), ZCEN(15, 15), XCON(15, 15), YCON(15, 15),  
ZCON(15, 15), AREA(15, 15), ARAT(15, 15), THETA(15, 15),  
ALPHA(15, 15), CHORD(15, 15), XFOIL(16, 25, 2),  
ZFOIL(16, 25, 2), XNUM(16, 2), XTAB1(25), ZTAB1(25),  
XTAB2(25), ZTAB2(25)
```

IJ = Code for internal program control.

NPTS = Number of points on the successive wing
percent chord lines that define the wing.

X } = x, y, z coordinates of points
Y } on wing percent chord lines.
Z }

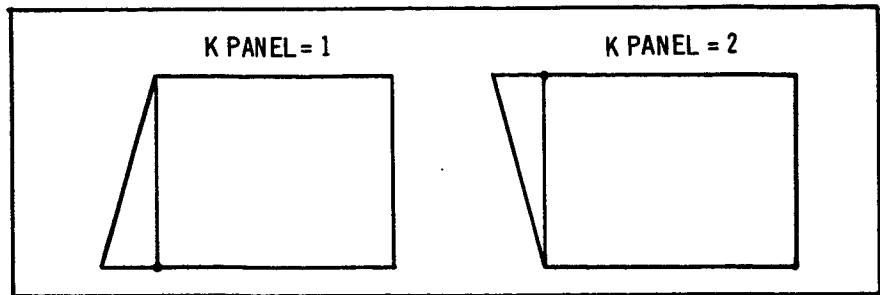
KPNT = Input constant

VALUE = Input array.

YCEPT = y-intercepts of wing cutting planes.

SLOPE = Slope (dx/dy) of outboard wing edge.

KPANEL = Code for wing panel type. If KPANEL
(I, J) = 1, additional subpanel corner
point is located on trailing edge. If
KPANEL(I, J) = 2, point is located on
leading edge. Note this code is deter-
mined only for panels on inboard column
if body and wing intersect in nonstream-
wise line, and for panels on outboard
edge if outboard edge is a nonstream-
wise line.



XCOR } YCOR } ZCOR }	= x, y, z coordinates of wing panel corner points.
XINT } YINT } ZINT }	= x, y, z coordinates of addi- tional wing panel point.
XCEN } YCEN }	= x and y coordinates of wing panel centroid.
ZCEN:	= Wing panel thickness ordinate.
XCON } YCON }	= x and y coordinates of wing panel control point.
ZCON	= Wing panel camber ordinate.
AREA	= Wing panel area.
ARAT	= Ratio of subpanel area to panel area.
THETA	= Wing panel thickness slope.
ALPHA	= Wing panel camber slope.
XFOIL } ZFOIL } XNUM }	= Input arrays.
XTAB1 } XTAB2 } ZTAB1 } ZTAB2 }	= Temporary storage arrays used in sub- routine slope.

USAGE:

COMMON (See subroutine OPCAMI for description of un-
labeled COMMON)

CALL WING

SUBPROGRAMS

CALLED:

INPUTW
CRNRW
AREAP
CENTRD
CNTRLW
CHORDW
SLOPEW
OUTPTW

ERROR RETURNS: Error message indicates whether error occurred in calculation of wing panel geometry.

STORAGE: $220_{10} = 334_8$

SUBJECT:

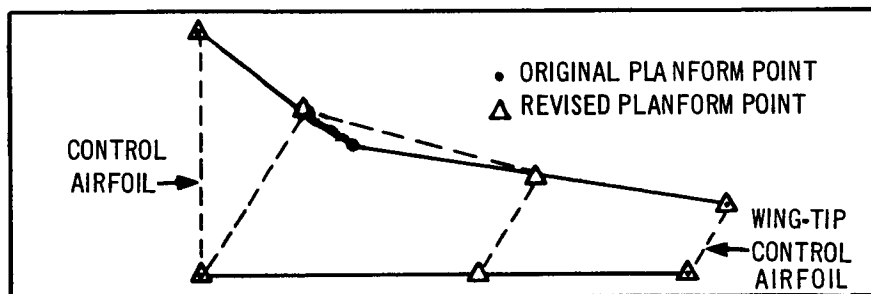
FORTRAN IV Subroutine WING1

PURPOSE:

To read data cards that describe a wing by a planform and a set of control airfoils, and put this data in a standard form suitable for other subroutines.

METHOD:

All of the data cards described in the attachment to subroutine WING1A are read. After the first three cards are read and checked, appropriate information is written on the output tape. Then storage is reserved in a buffer for variable length and scratch arrays (see Appendix A). Points describing the planform are read from cards 4 and 5. Subroutine WING1A is called to read cards 6, 7, and 8, scale the control airfoils to fit on the planform, and find the leading and trailing edge points corresponding to each airfoil. The original planform is assumed to be straight between given points; a new planform is constructed by joining the airfoil leading edge points and the trailing edge points. These planforms may differ as shown below.



After releasing scratch storage from the buffer, B, the percentages at which wing percent chord lines are to be constructed are read and checked. If an error is detected, a message is written.

USAGE:

```
DIMENSION  B(1), DAT(2), KOD(2), TITLE(12), NU(3)
```

```
LOGICAL  LOGUL(2)
```

```
CALL WING1 (B, LI, LO, DAT, LLETE, LOGUL, NAF,
            NPL, LAFN, LPCT, KOD, CHD, EPS,
            TITLE, NU)
```

Input: LI = Input tape number.

 LO = Output tape number.

DAT = Date (alphameric).
 NU = Error indicator array: NU(1) is not used on input. NU(2) is an output tape number on which to write a message if an error is detected; no message is written if $NU(2) \leq 0$. NU(3) is an error message limiter; if an error is detected, $NU(3) = (NU(3) - 1)$. Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.
 Output: B = Storage buffer for variable-length arrays.
 LLETE = Array containing the intersection points (X_i, Y_i) of the control airfoil with the wing leading and trailing edges is stored starting in B(LLETE). The point corresponding to the first airfoil, leading edge, is stored first, followed by the point for the trailing edge. The intersection points corresponding to the remaining airfoils are similarly stored. This array corresponds to the PT array in subroutine WING1A.
 LOGUL = LOGUL(1) = .TRUE. if the upper wing surface is defined; LOGUL(2) = .TRUE. if the lower wing surface is defined.
 NAF = Number of control airfoils.
 NPL = Number of wing percent chord lines.
 LAFN = An array, starting in B(LAFN) tells where, in B, the control airfoil points are stored and the number of elements (twice the number of points) in the airfoil upper or lower surface. This array is the same as array NAME in subroutine WING1A. The elements in this array are type INTERGER, although B is type REAL. The first four elements apply to the first airfoil, the second four elements to the second foil, etc.

LPCT = Array of percentages (to specify set of wing percent chord lines) is stored starting in B(LPCT).
 KOD = See ACODE and PCODE, card 3 (described in subroutine WINGA).
 CHD = See CHD, card 2.
 EPS = See EPS, card 3.
 TITLE = See TITLE, card 1.
 NU = Error indicator array. NU(1) is zero if no errors are detected. NU(3) may have been changed if an error was found (see Input, above).

**SUBPROGRAMS
CALLED:**

WING1A
 MERR
 IDLETE }
 IRSERV } (See Appendix A)
 IPACK }

ERROR RETURNS: Function MERR is used to write an error message "ERROR i, CODE j IN SUBROUTINE WING1 DURING GEOMETRIC DEFINITION" if an error is detected.

<u>i</u>	<u>j</u>	<u>Explanation</u>
1	0	WUL (see card 2) is not 0., 1., or 3.
2	0	PNLE, PNTE, AFN, or PLN (see card 2) is less than 2 or greater than 150. However, this is not considered a fatal error.
3	0	The storage buffer, B, is not large enough or a storage error has been detected.
5	0	
8	0	
9	0	
7	k	Error code k from subroutine WING1A.
10	0	A percentage (see card 9) is less than zero or greater than 100.

RESTRICTIONS: None

STORAGE: $802_{10} = 1442_8$

SUBJECT: FORTRAN IV Subroutine WING1A

PURPOSE: To read data cards that define a set of control airfoils, to compute points on the airfoils (scaled to fit planform), and to find the intersections of each airfoil with the planform.

METHOD: The wing planform is given by a set of points (X_i, Y_i) on the leading edge and another set on the trailing edge; adjacent points of each set are considered to be connected by straight lines. A card is read (card 6, see WINGA) that determines the placement of the airfoil on the planform and the number of points on the upper and lower surface of the airfoil. After these data are written, the intersections of the control airfoil and the planform leading and trailing edges are found. The airfoil chord length is the distance between these intersections.

A given code determines whether the upper wing, the lower wing, or both, are defined. Depending on this code, subroutine WING1B is called once or twice to read cards 7 and/or 8. These cards contain points (U_i, V_i) which determine shape of the control airfoil. The points are scaled so that the magnitude of the difference of the U-coordinates of the first and last point is equal to the chord length (as computed from the planform). The scaled points have coordinates (U', Z) where U' is distance along the airfoil and Z is in the wing coordinate system. WING1B also writes airfoil data on the output tape. A control airfoil is considered to be a single point if only a single point is given or if the first and last given points have the same abscissa; in either case no scaling takes place, and the ordinate of the first point will be taken as Z . If the set of given control airfoil points contain $n > 2$ points and has a nonzero chord length, but the true chord length (from the planform) is zero, then the scaled airfoil will have n points with all coordinates $(0, 0)$; this is an alternate way of specifying a point airfoil in the x,y plane.

USAGE: DIMENSION B(1), NAME(2, 2, 1), LPLF(2), NLTEP(3),
 PT(2, 2, 1), TITLE(12), DAT(2)

LOGICAL LOGUL(2)

CALL WING1A (B, NAME, LPLF, NLTEP, LOGUL, PT,
 LI, LO, TITLE, DAT, MU)

Input: B = Storage buffer for variable length arrays.

LPLF = The points (X_i, Y_i) that define the leading edge of the wing are stored starting in B(LPLF(1)); similarly, the points on the trailing edge start in B(LPLF(2)).

NLTEP(1) = Number of points on the leading edge.

NLTEP(2) = Number of points on the trailing edge.

NLTEP(3) = Number of control airfoils = NAF.

LOGUL = LOGUL(1) = .TRUE. if the upper wing surface is to be defined;
LOGUL(2) = .TRUE. if the lower wing surface is to be defined.

LI = Input tape number.

LO = Output tape number.

TITLE = Title (alphameric)

DAT = Date (alphameric)

Output: B = Storage buffer for variable length arrays.

NAME = Array that tells where in B the control airfoil points are stored, and the number of elements in each airfoil. The points (U_i, Z_i) for airfoil j are stored starting in B(NAME(1, i, j)), where i = 1 for upper surface of the airfoil, i = 2 for lower surface of the airfoil. The corresponding number of elements (twice the number of points) is stored in NAME(2, i, j).

PT = Array containing the intersections (X_i, Y_i) of the control airfoils with the leading and trailing edges of the wing. The X-coordinate of the intersection of control airfoil j with edge i is stored in PT(1, i, j), where i = 1 for leading edge, and i = 2 for trailing edge; similarly, the Y-coordinate is stored in PT(2, i, j).

MU = Error indicator, which is zero for success.

SUBPROGRAMS

CALLED:

DISPTA
WING1B
SIN (Built-in function)
POLXN
COS (Built-in function)
IRSERV (See Appendix A)

ERROR RETURNS: See WINGA, card 6, for explanation of symbols.

MU = 5 AFK is not 1., 2., or 3.
MU = 6, 7 YL (or YT) is outside the range of the leading edge (or trailing edge). If AFK = 1. or 2., MU = 6, if AFK = 3., MU = 7.
MU = 8 The control airfoil (defined by AFK, BETA, YL, YT) does not intersect the leading edge (or trailing edge) in exactly one point.
MU = 9 AFNU or AFNL is zero, indicating that this control airfoil has the same shape as the previous airfoil, but this is the first airfoil.
MU = 10 The storage buffer, B, is not large enough to store the control airfoil points.
MU = 11 This control airfoil has the same shape as the previous airfoil, but the previous one was a single-point airfoil.

RESTRICTIONS:

The given control airfoil points are not checked to see that they have reasonable values. The storage buffer, B, must have been initialized by subroutine INIBFR (Appendix A) or its equivalent.

STORAGE:

$719_{10} = 1317_8$

SUBJECT:

FORTRAN IV Subroutine WING1B

PURPOSE:

To read and write data points describing a control airfoil and to scale both coordinates of each point so that the airfoil has a given chord length.

METHOD:

After reading the control airfoil points (see NOTE, below), from an input tape, the point coordinates are written on an output tape. The chord length of a control airfoil is taken as the magnitude of the difference in X-coordinates of the first and last points. Then the airfoil is scaled by multiplying both coordinates of each point by the ratio of a given chord length to the computed chord length.

An option is provided so that instead of reading control airfoil points from cards, a given array of points is used; thereafter, the procedure is the same. This feature is useful when processing a series of airfoils which are similar to a preceding airfoil. Instead of writing out the (unscaled) points, the remark "THE GIVEN...AIRFOIL IS THE SAME AS PRECEDING ONE" is written.

An error code is returned if a control airfoil has less than two points or if the computed chord length is zero. Then the remark "THE AIRFOIL IS A POINT" is written. Since a single-point control airfoil may be legitimate, the calling program can take appropriate action.

USAGE:

DIMENSION B(1), A(1)

CALL WING1B (LI, LO, UL, CHORD, NB, B, NA, A, NI

Input: LI = Input tape number.
LO = Output tape number.
UL = Hollerith word "UPPER" or "LOWER."
CHORD = Chord length of the control airfoil.
NB = Number of elements (twice the number of points) in array B.
B = Array of points in a given control airfoil, stored $(x_1, z_1, x_2, z_2, \dots)$. B is not used unless $NA < 2$.
NA = If $NA < 2$, this control airfoil is similar to the given airfoil, B, but has a chord length = CHORD; the airfoil points in B will

be used instead of being read from cards. If $NA \geq 2$, NA is the number of elements (twice the number of points) in the control airfoil. NA elements will be read on tape LI.

Output: NA	Twice the number of points in A.
A	Array of $NA/2$ points in the control airfoil, scaled to chord length = CHORD, and stored $(x_1, z_1, x_2, z_2, \dots)$.
NU	Error indicator, which is zero for success.

SUBPROGRAM

CALLED: None

ERROR RETURNS: NU = -1 if the control airfoil has less than two points or if the first and last point have the same x-coordinate.
 NU = 1 if NA is less than 2 (on input), and NB is less than 4.

RESTRICTIONS: A warning message is printed if the points in A are not increasing in x, but this condition is not considered to be an error.

STORAGE: $332_{10} = 514_8$

NOTE: See cards 7 or 8, Wing Input Data Format (attachment to subroutine WINGA).

SUBJECT:

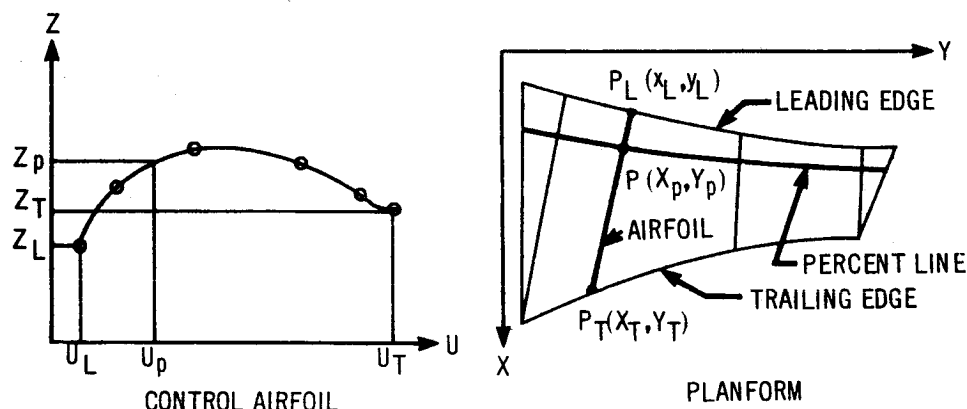
FORTRAN IV Subroutine WING2

PURPOSE:

To construct three-dimensional points on wing percent chord lines (corresponding to given control airfoils), and, if required, to interpolate additional points.

METHOD:

The input includes NAF control airfoils and NPL percent values. It is necessary to compute NAF points (X_i, Y_i, Z_i) on each of the NPL percent chord lines. A point corresponding to a particular control airfoil and a percent chord line is found thus:



A set of points (U_i, Z_i) which describe the control airfoil is illustrated in first figure above. The (X, Y) coordinates are given for points P_L and P_T , shown in second figure. The control airfoil is to be placed on the planform so that U_L corresponds to P_L , and U_T to P_T ; the U -coordinates of the airfoil may require scaling to do this, but the Z -coordinates are not to be scaled. Let p = percentage/100. Then

$$X_P = (1 - p) X_L + pX_T$$

$$Y_p = (1 - p) Y_L + pY_T$$

$$U_p = (1 - p) U_L + pU_T$$

The value of Z_P is found by interpolation (using subroutine BITURP) from the control airfoil points (U_i, Z_i) at $U = U_P$, if a control airfoil is described by only one point, $X_P = X_L, Y_P = Y_L$, and $Z_P = Z_L$.

After the basic percent chord lines are computed, they are written on the output tape by subroutine WING2P. Subroutine RICHNA is then called to remove any near-coincident points in each percent chord line, to interpolate additional points (if $CHD > 0.$), and to place a "header" (table of contents) in front of the array. If both upper and lower wing surfaces are defined, the entire process is repeated for the lower surface. Then the control airfoil point arrays and the NAME array are deleted from buffer B, since they are no longer needed.

USAGE:

```
DIMENSION B(1), LOK(3,2), KOD(2), PLT(2,2,NAF),
NAME(2,2,NAF), PCT(NPL), TITLE(12), DAYT(2), NU(3)

LOGICAL LGDEF(3,6), LOGUL(2)

CALL WING2 (B, LO, LGDEF, LOK, LOGUL, NAF,
NPL, LAFN, KOD, PLT, NAME, PCT, CHD, EP, TITLE,
DAYT, NU)
```

Input: B = Storage buffer for variable length arrays.

 LO = Output tape number.

 LOGUL = LOGUL(1) = .TRUE. if upper wing is defined;

 LOGUL(2) = .TRUE. if lower wing is defined.

 NAF = Number of control airfoils.

 NPL = Number of percent chord lines.

 LAFN = The array NAME starts in B(LAFN); that is, the location in core of NAME (1,1,1) is the same as the location of B(LAFN).

 KOD = Interpolation codes. KOD(1) is used by subroutine BITURP; KOD(2) is used by subroutine RICHNA. (See ACODE and PCODE, card 3, subroutine WINGA.)

 PLT = Array of coordinates (X_i, Y_i) of intersection points of control airfoils with the leading and trailing edges of the

wing. The intersection point of the k^{th} control airfoil with edge j is stored starting in PLT (1, j , k), where $j = 1$ for leading edge, $= 2$ for trailing edge. PLT corresponds to B(LLETE) in subroutine WING1.

NAME = An array that tells where in B the control airfoil points are stored, and the number of elements in each airfoil. The points (U'_i , Z_i) for control airfoil j are stored starting in B(NAME(1, i , j)), where $i = 1$ for upper surface of the airfoil, $i = 2$ for lower surface of the airfoil. The corresponding number of elements (twice the number of points) is stored in NAME(2, i , j). The NAME array is generated in subroutine WING1A.

PCT = Array of percentages associated with the wing percent chord lines.

CHD = Chord-arc tolerance. (See CHD, card 2, subroutine WINGA.)

EP = See EPS, card 3, subroutine WINGA.

TITLE = Title (alphameric).

DAYT = Date (alphameric).

NU = Error indicator array: NU(1) is not used, on input. NU(2) is an output tape number on which to write a message if an error is detected; no message is written if $NU(2) < 0$. NU(3) is an error message limiter; if an error is detected, $NU(3) = (NU(3) - 1)$. Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.

Output: B = Storage buffer for variable-length arrays.

LGDEF = LGDEF(2,1) is set to .TRUE. if upper wing percent lines are successfully generated; LGDEF(2,2) is set to .TRUE. if lower wing percent chord lines are successfully generated.

LOK = Array which tells where in B the percent chord line arrays are located, and the length of each percent chord line array. Consider LOK(i, j). The upper wing surface corresponds to j = 1, the lower to j = 2. The percent chord line array, consisting of a header followed by point coordinates (see Appendix D), starts in B(LOK(1, j)). The number of percent chord lines in the array is stored in LOK(2, j). The total number of elements in the array is stored in LOK(3, j).

NU = Error indicator array. NU(1) is zero if no errors are detected. NU(3) may have been changed (see Input).

SUBPROGRAMS
CALLED:

RICHNA
 WING2P
 BITURP
 MERR
 IDLETE
 IRLEAS
 IRSERV
 IPACK

(See Appendix A)

ERROR RETURNS: Function MERR is used to write a message "ERROR i, CODE j IN SUBROUTINE WING2 DURING GEOMETRIC DEFINITION" if an error is detected.

<u>i</u>	<u>i</u>	<u>Explanation</u>
1	0	The storage buffer, B, is not large enough or a storage error has been detected.
5	0	
6	0	
8	0	
2	0	No points are given for a control airfoil (this error should be detected in a previous subroutine).
3	k	Error k from BITURP in interpolation from a given control airfoil to get a percent chord line point. The control airfoil has invalid points.
7	k	Error k from RICHNA.

RESTRICTIONS:

The storage buffer, B, must have been initialized by subroutine INIFBR (Appendix A) or its equivalent.

STORAGE:

$$550_{10} = 1046_8$$

SUBJECT: FORTRAN IV Subroutine WING2P

PURPOSE: To write wing percent chord lines on an output tape.

METHOD: The basic wing percent chord lines, computed by subroutine WING2, consist of three-dimensional points on the surface of a wing. After title and headings are written on each page, the points are written, one point per line.

USAGE: **DIMENSION** W(3, NPT, NPCT), TITLE(12), DAYT(2),
PCT(NPCT)

CALL WING2P (LO, W, NPCT, NPT, TITLE, UPLO,
DAYT, PCT)

Input: LO = Output tape number.

W = Array on NPCT percent chord lines.
Each line contains NPT points (x_i, y_i, z_i) .

NPCT = Number of percent chord lines.

NPT = Number of points in each percent chord line.

TITLE = Title (alphameric).

UPLO = 6H UPPER or 6H LOWER.

DAYT = Date (alphameric).

PCT = Array of percentages, corresponding to the percent chord lines in W.

Output: Printout on tape LO.

SUBPROGRAM CALLED: None

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $205_{10} = 315_8$

SUBJECT: FORTRAN IV Subroutine WINGA

PURPOSE: To read data cards defining a wing and construct percent chord lines on its surface.

METHOD: Subroutine WING1 is called to read data cards (see attachment) that define the wing. Then subroutine WING2 constructs three-dimensional percent chord lines that lie on the wing surface.

USAGE:

```

DIMENSION  B(1), DAT(2), LOK(3, 9), TITLE(2), NU(3)
LOGICAL  LGDEF(3, 6)
CALL WINGA (B, LI, LO, DAT, LGDEF, LOK, LWPF,
            TITLE, NU)

```

Input:

- B** = Storage buffer for variable length arrays.
- LI** = Input tape number.
- LO** = Output tape number.
- DAT** = Date (alphameric).
- NU** = Error indicator array used by lower level routines: NU(1) is not used on input. NU(2) is an output tape number on which to write a message if an error is detected; no message is written if $NU(2) \leq 0$. NU(3) is an error message limiter; if an error is detected, $NU(3) = (NU(3) - 1)$. Then if $NU(3) > 0$ and $NU(2) > 0$, an error message is written.

Output:

- B** = Storage buffer for variable length arrays.
- LGDEF(1, 1)** . TRUE. if upper wing was requested.
- (1, 2)** . TRUE. if lower wing was requested.
- (1, 4)** . TRUE.
- (2, 1)** . TRUE. if upper wing successfully defined.
- (2, 2)** . TRUE. if lower wing successfully defined.

(2, 4) .TRUE. if WING1 was successful.

LOK = Array that tells where in B the wing percent chord line arrays and wing planform point array are located and the length of each array. Consider LOK(i, j). The upper wing percent chord line array corresponds to LOK(i, 1), the lower to LOK(i, 2); the planform point array corresponds to LOK(i, 7). An array starts in B(LOK(1, j)); the total number of elements in the array = LOK(3, j). LOK(2, 1) = number of upper percent chord lines, LOK(2, 2) = number of lower percent chord lines, and LOK(2, 7) = number of control airfoils = number of pairs of planform points (leading edge, trailing edge).

LWPF = The location of LWPF is the same as that of LOK(1, 7). (LWPF need not have been an argument.)

TITLE = Wing title (alphameric).

NU = Error indicator array. NU(1) is zero if no error is detected. NU(3) may have been changed (see INPUT, above).

SUBPROGRAMS

CALLED: WING1
WING2
IPACK (See Appendix A)

ERROR RETURNS: NU(1) \neq 0 if an error occurred in WING1 or WING2.
LGDEF(2, 4) will be .FALSE. if the error was in WING1,
.TRUE. if in WING2.

RESTRICTIONS: The storage buffer, B, must have been initialized by sub-routine INIBFR (Appendix A) or its equivalent. LGDEF(i, j), i = 1, 3; j = 1, 2, 4 must have been set to .FALSE.

STORAGE: $153_{10} = 231_8$

ATTACHMENT: Wing Input Data Format

	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Card 1</u>	1-72	TITLE	Any desired title.
<u>Card 2</u>	1-10	PNLE	Number of corner or break points defining the planform leading edge.
	11-20	PNTE	Number of corner or break points defining the planform trailing edge.
	21-30	AFN	Number of planform control airfoils. $AFN \geq 2$. including the wing tip airfoil.
	31-40	PLN	Number of constant percent chord lines. $PLN \geq 1$.
	41-50	WUL	= 1. only the upper wing surface is defined. = 2. only the lower wing surface is defined. = 0. both upper and lower wing surfaces are defined.
	51-60	CHD	Dimensional tolerance for the density of points interpolated (between control airfoils) on percent chord lines. If $CHD \leq 0.$, or if $AFN < 4.$, no additional points are generated. Do not specify $CHD > 0.$ unless <u>every</u> basic percent chord line has at least four <u>distinct</u> points.
<u>Card 3</u>	1-10	PCODE	Code that controls the type of three-dimensional interpolation to be used for generating additional points on percent chord lines. PCODE is not effectively used on any basic percent chord line of less than four distinct points or if $CHD \leq 0.,$ For a more detailed explanation of PCODE, see KD in subroutine RICH3A.

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
		<p>= 0., enriching (interpolation of additional points) is done on points projected into a plane which "best" fits the basic percent chord line points. Enriched percent lines can appear curved between control airfoils in the planview.</p> <p>= 1., enriching is done on points projected into a plane normal to the X-Y plane through the percent chord line ends. Resulting percent lines appear as straight lines between control airfoils in the planview.</p> <p>= 2., enriching is done as for PCODE = 1. but resultant percent lines can appear curved between control airfoils in the planview.</p>
		<p>NOTE: If PCODE = 1. or 2., and the percent chord line lies roughly in a horizontal plane (e.g., leading or trailing edge), enriching may not add points to the basic percent line.</p>
	11-20	ACODE
		<p>= 1., linear interpolation is used between points on control airfoils to find points on the basic percent chord lines.</p> <p>= 2., biquadratic interpolation is used.</p>
	21-30	EPS
		<p>A tolerance used to eliminate coincident percent chord line points. The basic percent chord lines consist only of intersections of percent chord lines with control airfoils. If two of these points are closer together than EPS, one is eliminated. If $EPS \leq 0.$, a value of 0.01 is used.</p>
<u>Cards 4</u>	1-10	X_1
	11-20	Y_1
	21-30	X_2
		<p>Array of points defining the planform leading edge, arranged in order from inboard to outboard. There must be PNLE point pairs, <u>three coordinate</u></p>

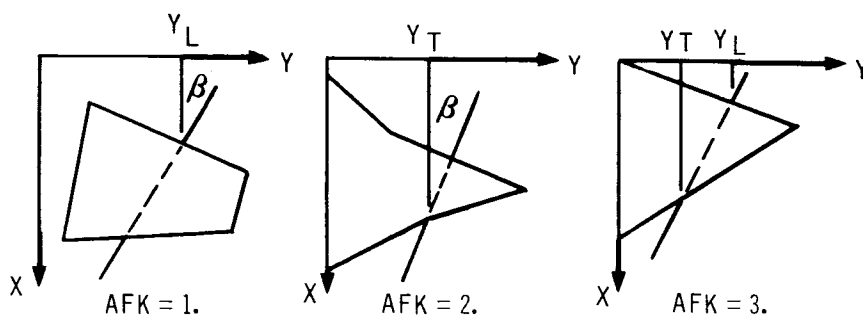
	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>Cards 5</u>	31-40	Y_2	pairs per card. Note that the leading edge may be modified by the program, depending on the placement of control airfoils on the planform.
	41-50	X_3	
	51-60	Y_3	
	1-10	X_1	Similar to cards 4, but for the trailing edge.
	11-20	Y_1	
	21-30	X_2	
	31-40	Y_2	
	41-50	X_3	
	51-60	Y_3	

Cards 6

These cards, one for each control airfoil, give the airfoil location on the planform and the number of points on the upper and lower parts of the control airfoil. Each card 6 is followed by one or more cards 7 and 8 (unless the previous airfoil is to be repeated).

Code to indicate how the control airfoil is oriented on the planform. See sketches below.

1-10 AFK



Two of the three quantities β , Y_L , Y_T must be given to specify the control airfoil location. AFK indicates which two quantities are to be used.

11-20 BETA

The angle β , positive if as shown on the sketches. BETA is ignored if $AFK = 3$.

21-30 Y_L

Y_L , Y-coordinate at which the control airfoil intersects the leading edge. Y_L is ignored if $AFK = 2$.

<u>Column</u>	<u>Code</u>	<u>Explanation</u>
31-40	Y_T	Y_T , Y-coordinate at which the control airfoil intersects the trailing edge. Y_T is ignored if $AFK = 1..$
41-50	AFNU	Number of points on the control airfoil upper surface. The coordinates of these points (cards 7) follow this card. However, if $AFNU = 0..$, then the previous airfoil upper surface points are used and a card 7 must <u>not</u> follow. If $WUL = 2.$ (upper wing not defined), then AFNU is ignored, and a card 7 must <u>not</u> follow.
51-60	AFNL	Number of points on the control airfoil lower surface. The coordinates of these points (cards 8) follow cards 7 (or card 6 if no card 7 is used). However, if $AFNL = 0..$, then the previous airfoil lower surface points are used and a card 8 must <u>not</u> follow. If $WUL = 1.$ (lower wing not defined), then AFNL is ignored, and a card 8 must <u>not</u> follow. Note that the leading and trailing edge points must be included, even if they repeat those of the airfoil upper surface.
<u>Cards 7</u>	1-10	Array of points (U_i, V_i) on the control airfoil upper surface, in increasing order from leading edge to trailing edge. The points will later be scaled to fit the planform. This card must not follow a card 6 if $WUL = 2.$ or if $AFNU = 0..$
	11-20	
	21-30	
	31-40	
	41-50	
	51-60	
<u>Cards 8</u>	1-10	Similar to card 7, but apply to the control airfoil lower surface points. Cards 8 follow cards 7 (or a card 6 if a card 7 is not used). A card 8 must not be used if $WUL = 1.$ or if $AFNL = 0..$
	11-20	
	21-30	
	31-40	
	41-50	
	51-60	

<u>Cards</u>	<u>Column</u>	<u>Code</u>	<u>Explanation</u>
<u>9</u>	1-10	P_1	Array of constant percent chord values corresponding to the spanwise panel edges. For example, if percent chord lines 0, 20, 50, 100 are desired, then $P_1 = 0.$, $P_2 = 20.$, $P_3 = 50.$, and $P_4 = 100.$
	11-20	P_2	
	.		
	.		
	51-60	P_6	

SUBJECT:

FORTRAN IV Subroutine WLDM

PURPOSE:

To compute the coefficients of lift, drag, and pitching moment of the wing and the spanwise distribution of the coefficients of lift and drag.

METHOD:

The force normal to a panel is given as the product of dynamic pressure, surface pressure coefficient, and panel area:

$$F_i = q \cdot C_{p_i} \cdot A_i$$

Resolving into the components normal and parallel to the free-stream direction yields

$$L_i = - F_i \cdot \cos \theta_i$$

$$D_i = F_i \cdot n_i$$

where n_i is the component of velocity normal to the x-axis and θ_i is the angle between the plane of the panel and a plane parallel to the x-y plane.

The moment of force with respect to a point (x, 0, z) gives the pitching moment.

$$M_i = - L_i (\bar{x}_i - x) + D_i (\bar{z}_i - z)$$

where \bar{x} and \bar{z} are the x and z coordinates of the panel centroids.

The coefficients of lift, drag, and moment for the entire wing are given by

$$C_L = \frac{1}{q \cdot S_W} \sum_{i=1}^{NM} L_i$$

$$C_D = \frac{1}{q \cdot S_W} \sum_{i=1}^{NM} D_i$$

$$C_M = \frac{1}{q \cdot S_W} \sum_{i=1}^{NM} M_i$$

where S_W is the wing reference area, and NM is the number of wing panels.

The spanwise distribution of the coefficients of lift and drag is given by

$$C_{L_j} = \frac{1}{q \cdot S_W} \sum_{i=1}^{NROW} L_i$$

$$C_{D_j} = \frac{1}{q \cdot S_W} \sum_{i=1}^{NROW} D_i \quad , j = 1, \dots, NCOL$$

where NROW is the number of panels in a chordwise column,
and NCOL is the number of chordwise columns.

USAGE:

CALL WLDM (NM, NROW, XP, ZP, RFAREA, AREA,
XBAR, ZBAR, ALPHAM, THETAM, CPM,
SCL, SCD, CL, CD, CM)

DIMENSION AREA(NM), XBAR(NM), ZBAR(NM),
ALPHAM(NM), THETAM(NM), CPM(NM),
SCL(NCOL), SCD(NCOL)

Input: NM = Number of wing panels.
NROW = Number of panels in a steamwise column.
XP = x-coordinate of the point about which
the pitching moments are to be calculated.
ZP = z-coordinate of the point about which
the pitching moments are to be calculated.
RFAREA = Wing reference area.
AREA = Array of wing panel areas.
XBAR = Array of wing panel centroid x-
coordinates.
ZBAR = Array of wing panel centroid z-
coordinates.
ALPHAM = Array of velocity components normal
to the x-axis.
THETAM = Array of angles between the plane of
the panel and a plane parallel to the
x-y plane.

Output: SCL = Array of spanwise lift coefficients.
SCD = Array of spanwise drag coefficients.
CL = Coefficient of lift.

CD = Coefficient of drag.
CM = Coefficient of pitching moment.

SUBPROGRAM

CALLED: COS

ERROR RETURNS: None

RESTRICTIONS: None

STORAGE: $187_{10} = 273_8$

The Boeing Company
Commercial Airplane Division
Renton, Washington
August 1967

5. APPENDIXES

5.1 Appendix A — Dynamic Storage Allocation Package

SUBJECT: Dynamic Storage Allocation in FORTRAN

PURPOSE: To provide a means for allocating, using, and releasing blocks of storage on a dynamic basis during execution of FORTRAN programs.

METHOD: The buffer format is illustrated in figure 1, page 421. Each buffer is divided into a (variable) number of arrays, some of which may be full while others are available to be filled. Initially the buffer contains only one array; this is empty. The first word of each buffer is a "header" which contains the total length of the buffer.

Each array is preceded by a "secret" header of two codes, illustrated in figure 1, which contains the following information:

- 1) Whether the array is full or empty
- 2) The length of the array
- 3) The relative address of the first word of the buffer
- 4) The absolute address of the array name (if the array is full).

In using the buffer, a programmer can ignore the headers, because the subroutines he uses will accommodate this bookkeeping. These routines will also indicate situations such as an overflowing buffer or reference to an array in the buffer that is not a legitimate array.

The subroutines involved in the scheme may be divided into three classes:

- 1) Basic subprograms
- 2) Primitive subprograms
- 3) User's subprograms

The first two of these classes are an integral part of the automatic storage scheme and are discussed in more detail below. Their structure is illustrated in figure 2, page 422. The user's subprograms are provided by the authors of the computing system and will call the basic subprograms into execution. The user should never have to call a primitive subprogram directly. When setting up an array in the buffer, either by use of the function IADARY or by reserving space with the function IRSERV, the user will obtain a "name" for that array stored as a FORTRAN integer in a cell that may be called NAME. This name is now uniquely

associated with the array. If the buffer is called BUFFER, the first word of the array will always be BUFFER(NAME) and the i^{th} word will be BUFFER(NAME + I - 1), regardless of any shuffling that may take place automatically in the buffer. However, because data shuffling may occur, the array must always be referred to by the same NAME, which will be kept updated automatically. Obviously, each array can have only one name.

USAGE:

Basic

Subprograms:

The following seven subprograms form the basic set which can be called directly by the user. With the exception of INIBFR and CLEAR they are coded in FORTRAN.

1) Subroutine CLEAR (BFRA, BFRB, ...)

To reinitialize and make available for reuse any number of buffers BFRA, BFRB, ..., etc.

2) Subroutine INIBFR (BFRA, NA, BFRB, NB, ...)

To initialize any number of buffers, BFRA, etc., of length NA, etc., words. This routine must be called before a buffer can be used.

3) Function IADARY (ARRAY, N, BFR, NAME)

To place an array, ARRAY, of length N words, into the buffer, BFR, and to assign to it the name, NAME. The function value will be the same as NAME unless some error or misuse is detected, in which case it will be negative. To circumvent the oddities of the FORTRAN subscripting, procedure IADARY should be used thus:

NAME = IADARY (ARRAY, N, BFR, NAME)

4) Function IDLETE (BFR(NAME))

To delete (i.e., make available for reuse) an array in the buffer, BFR, whose name is NAME. The function value will be zero unless some error is detected, when deletion will not occur.

5) Function IPACK (BFR)

The pack a buffer, BFR, by moving all full arrays to the beginning of the buffer and condensing all the empty arrays into one at the end. The function value will be equal to the length of the final empty array unless an error is detected, when it will be negative and packing will not occur.

6) Function IRLEAS (BFR(NAME), N)

To release all cells beyond cell N in an array in the buffer, BFR, whose name is NAME; i.e., BFR(NAME) - BFR(NAME + N-1) are retained but BFR(NAME + N) - the end of the array are made available for reuse. The function value will be zero unless some error is detected, when release will not occur.

7) Function IRSERV (N, BFR, NAME)

To reserve an array of N words in the buffer, BFR, and to assign to it the name, NAME. The comments under IADARY concerning function value apply also to IRSERV.

Primitive

Subprograms:

For completeness, the eight primitive subprograms of the scheme are briefly described here. They are all coded in assembly language.

1) Function ARFRE (NAME)

To set up the first code word of an empty array. FORTRAN IV version has deck name ARFREE.

2) Function ARFUL (NAME)

To set up the first code word of a full array.

3) Function ARSEC (N, NAME)

To set up the second code word of an array. FORTRAN IV version has deck name ARSECR.

4) Function FOOL(I)

To store a fixed point variable in a floating point location. The FORTRAN IV version has deck name UFOOL and two entry points, FOOL and IFOOL.

5) Function IBFR (A)

To locate the first word of a buffer relative to the first word of an array.

6) Function ICODE (A)

To determine whether an array is full or empty.

7) Function LENG (A)

To determine the length of an array

8) Subroutine UPDATE (A)

To update the contents of an array name following data shuffling in the buffer.

EXAMPLE:

An example is given in figure 3, page 423, of a program which reads in an ($l \times m$) and an ($m \times n$) matrix, multiplies them together and prints out the ($l \times n$) resultant. The input arrays are then deleted from the buffer.

FLOWCHARTS:

Flowcharts of all the primitive and basic subprograms of the dynamic storage package are included. These flowcharts are for the FORTRAN II versions. The FORTRAN IV subprograms differ slightly because of the forward storage of arrays and full word instead of decrement format of fixed-point variables.

**SUBPROGRAM
CALLED:**

None

EQUIPMENT:

IBM 7094 II

STORAGE:

<u>Subprogram</u>	<u>FORTRAN II</u>		<u>FORTRAN IV</u>	
	<u>Octal</u>	<u>Decimal</u>	<u>Octal</u>	<u>Decimal</u>
ARFREE	10	8	7	7
ARFUL	10	8	7	7
ARSECR	10	8	11	9
CLEAR	25	21	22	18
IADARY	273	187	255	173
IBFR	24	20	23	19
ICODE	23	19	22	18
IDLETE	65	53	62	50
INIBFR	33	27	33	27
IPACK	316	206	266	182
IRLEAS	173	123	165	117
IRSERV	42	34	45	37
LENG	4	4	5	5
UFOOL	2	2	2	2
UPDATE	<u>14</u>	<u>12</u>	<u>13</u>	<u>11</u>
TOTALS	1334	732	1252	682

BFR (1)
2
3
4
⋮
 $M_1 + K_1 - 1$

4	0	7	N
P_1	0	7	4
0	M_1	0	$ANAME_1$
Array #1			

$K_i - 2$
 $K_i - 1$
 K_i

P_i	0	7	K_i
0	M_i	0	$ANAME_i$
Array #i			

$K_j - 2$
 $K_j - 1$
 K_j
⋮
 $N = K_j + M_j - 1$

P_j	0	7	K_j
0	M_j	0	$ANAME_j$
Array #j (last)			

NOTES

For a full array:

$$P_i = 7$$

$ANAME_i$ is the absolute address of the array name, $NAME_i$. The word $NAME_i$ contains K_i as a decrement integer.

For an empty array:

$$P_i = 0$$

$ANAME_i$ is irrelevant.

In general:

M_i is the length of the i th array.

K_i is the first word of the array relative to the beginning of the buffer.

N is the total length of the buffer.

The first code word of the buffer and of the arrays are illegal both as FORTRAN integers and as floating point numbers.

FIGURE 1 BUFFER FORMAT

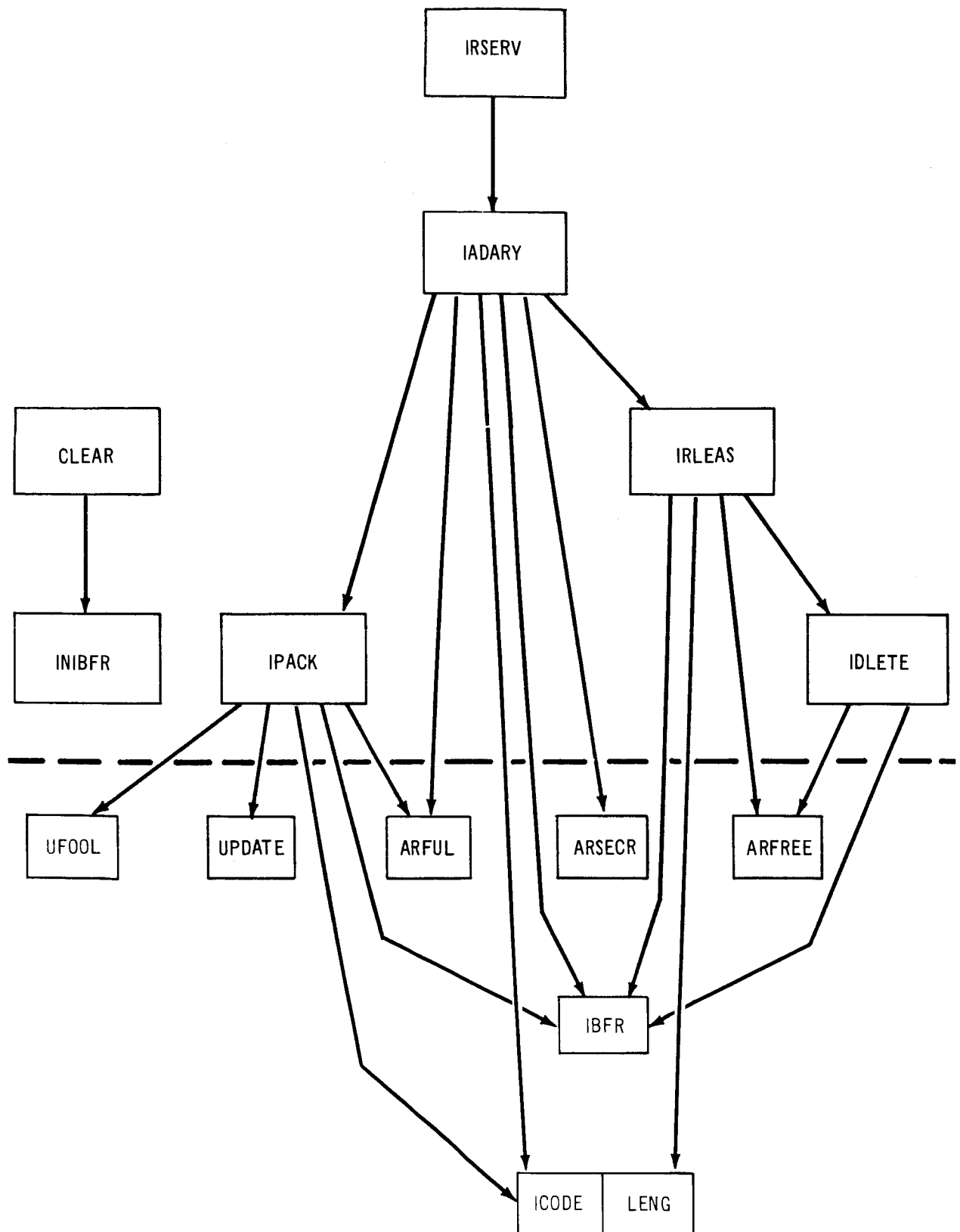


FIGURE 2 STRUCTURE OF THE DYNAMIC STORAGE SCHEME

```

        DIMENSION BFR(1000)
C
        CALL INIBFR (BFR,1000)
C
        READ INL
        READ INPUT TAPE 5,1,L,M,N
1      FORMAT (6G)

C
        NAM1=IRSERV(L*M,BFR,NAM1)
        NAM2=IRSERV(M*N,BFR,NAM2)
        IJ=IRSERV(L*N,BFR,NAM3)-1

C
        K=NAM1+L*M-1
        READ INPUT TAPE 5,1,(BFR(I),I=NAM1,K)
        K=NAM2+M*N-1
        READ INPUT TAPE 5,1,(BFR(I),I=NAM2,K)
C
        DO 20 J=1,N
        DO 20 I=1,L
        IK=NAM1+I-1
        KJ=NAM2+(J-1)*M

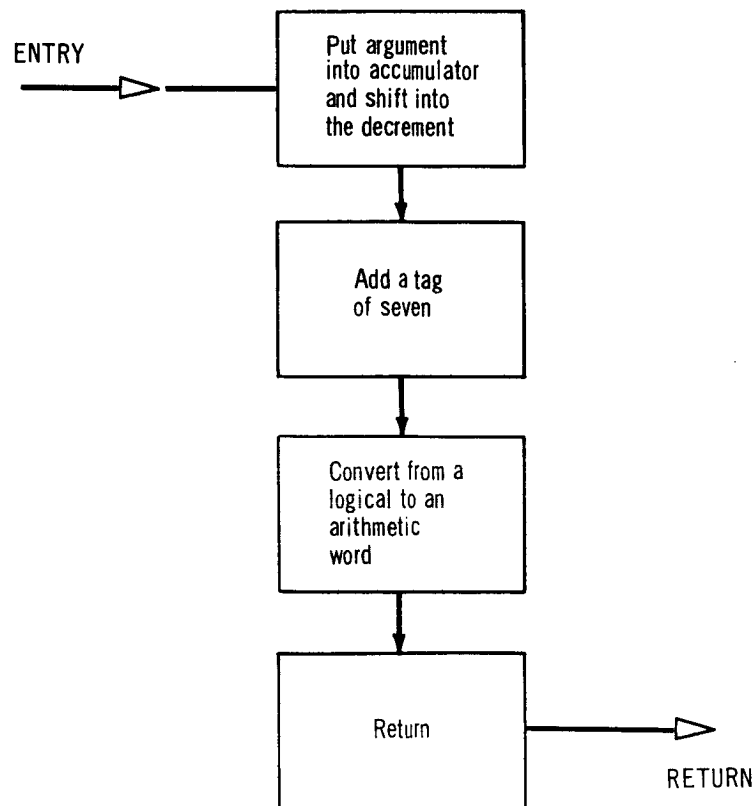
C
        DO 10 K=1,M
        B=B+BFR(IK)*BFR(KJ)
        IK=IK+L
10      KJ=KJ+1

C
        IJ=IJ+1
20      BFR(IJ)=B
C
        CALL IDLETE(BFR(NAM1))
        CALL IDLETE(BFR(NAM2))
C
        WRITE OUTPUT TAPE 6,2,(BFR(I),I=NAM3,IJ)
2      FORMAT (G20.6)
        STOP
        END(1,1,0,0,0,0,0,1,0,1,0,0,0,0,0)

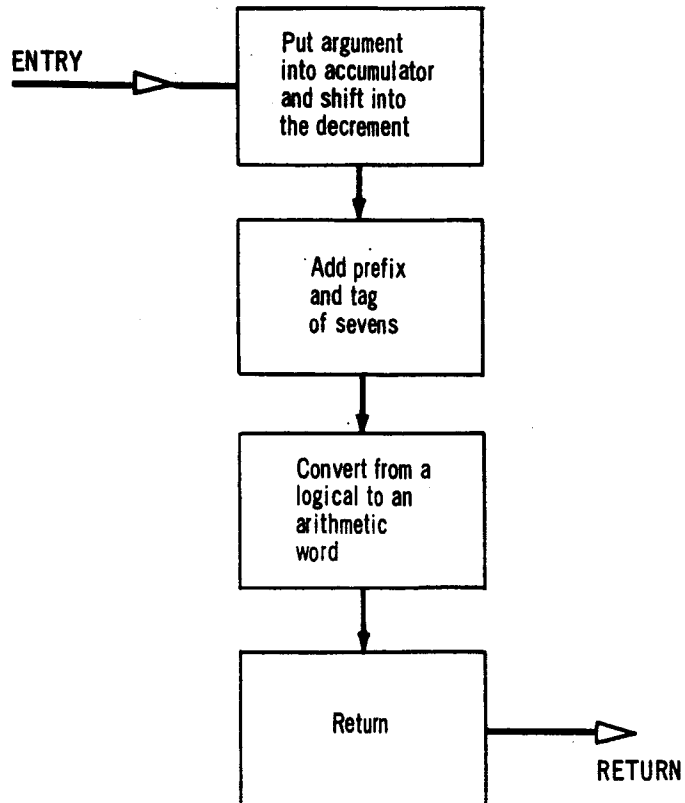
```

FIGURE 3 EXAMPLE FOR DYNAMIC STORAGE

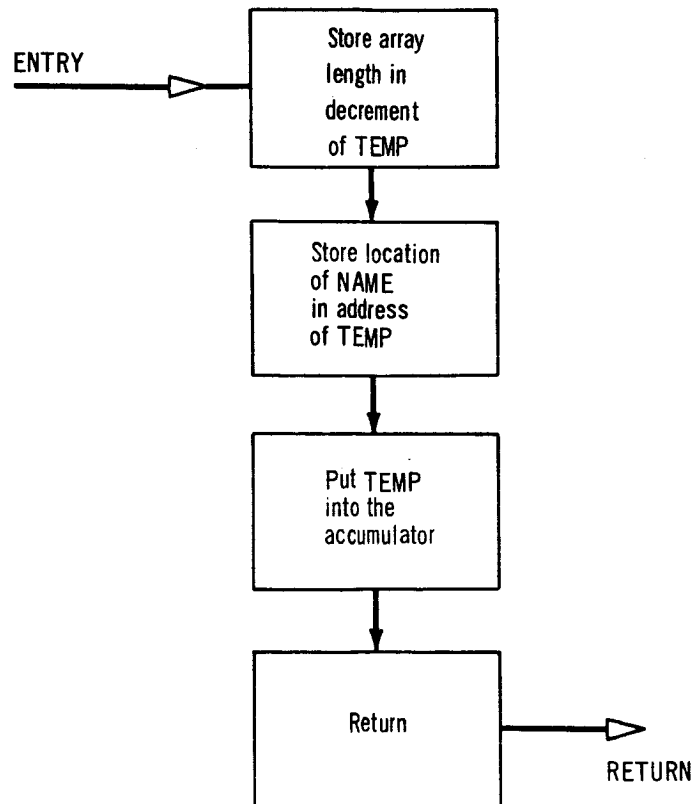
ARFREE



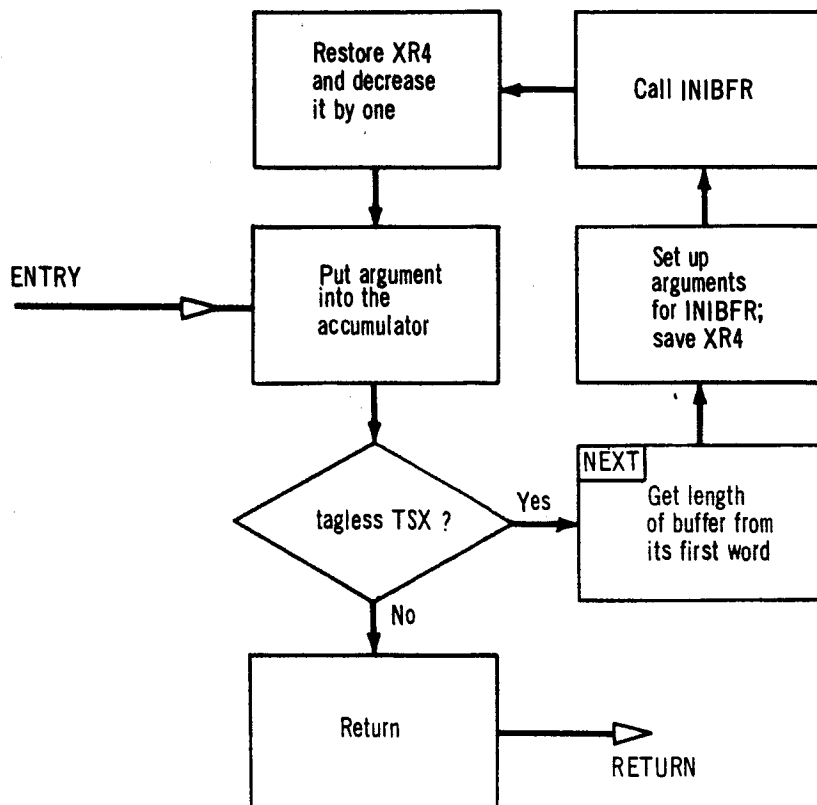
ARFUL

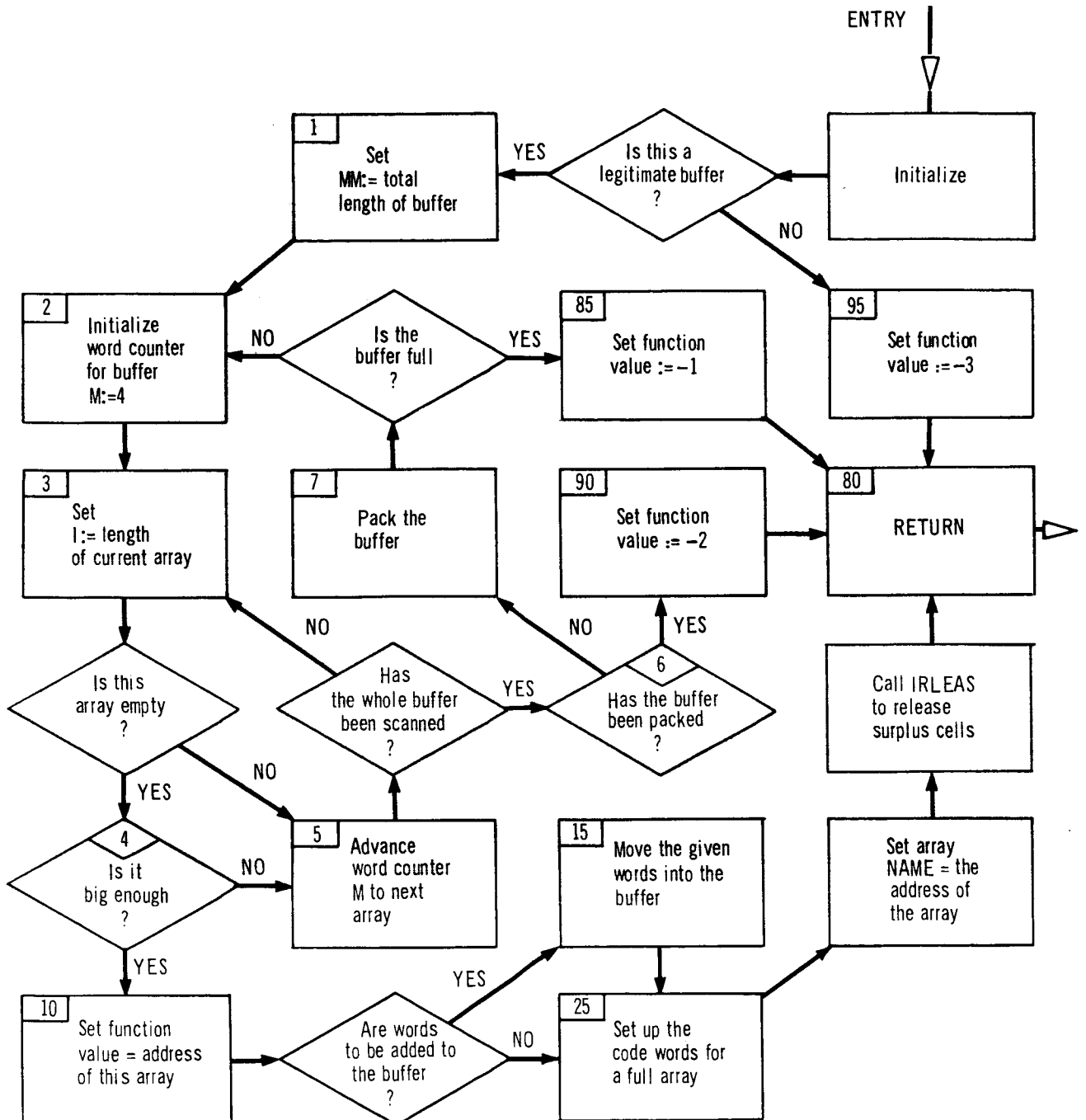


ARSECR

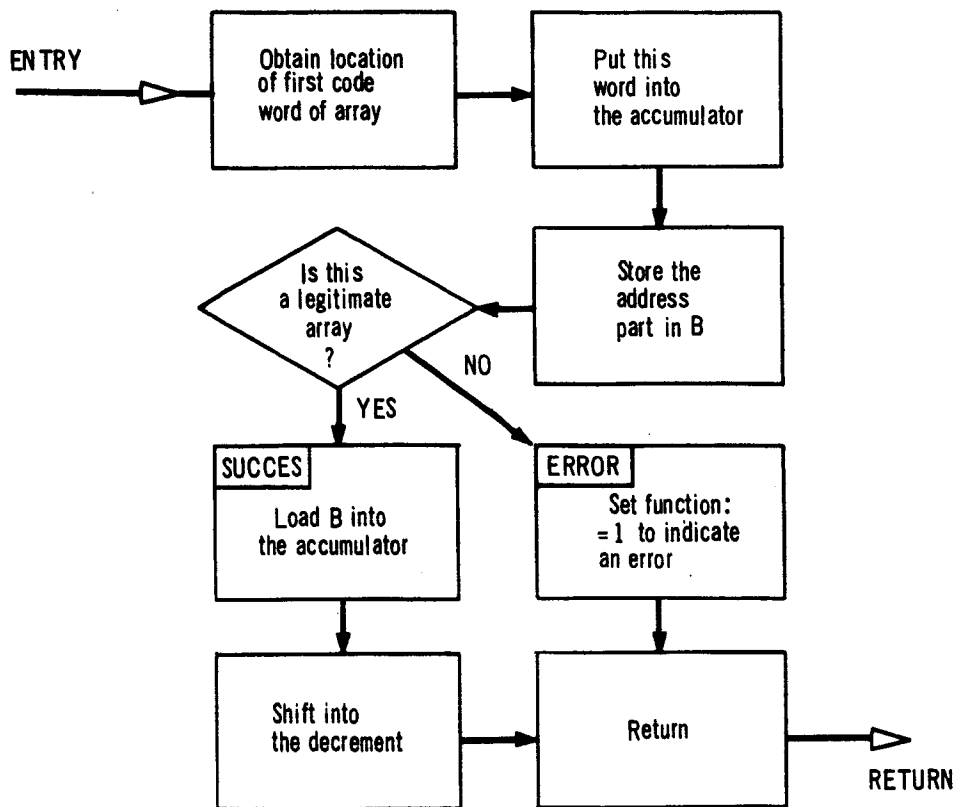


CLEAR

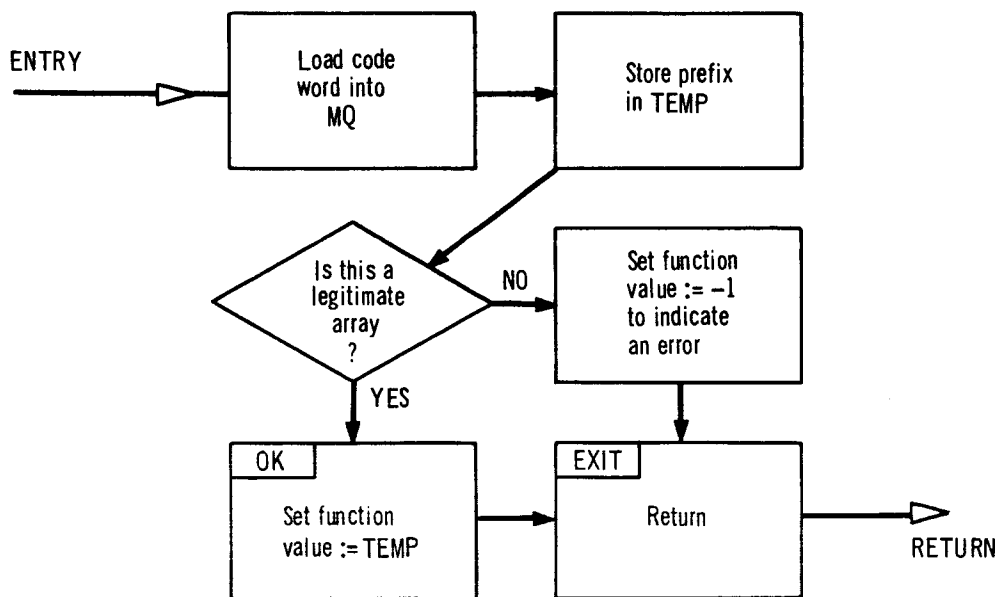




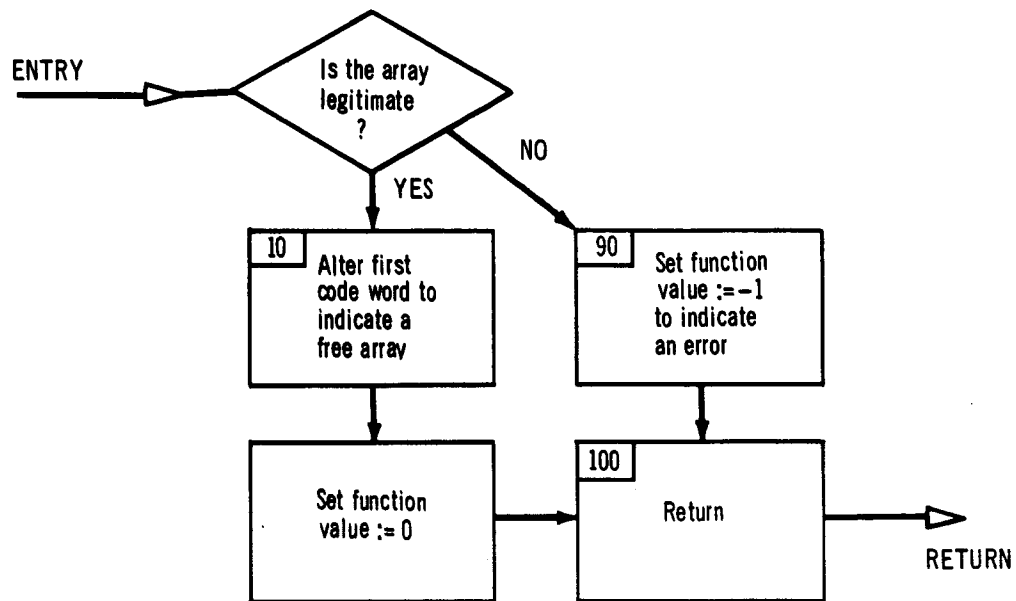
IBFR



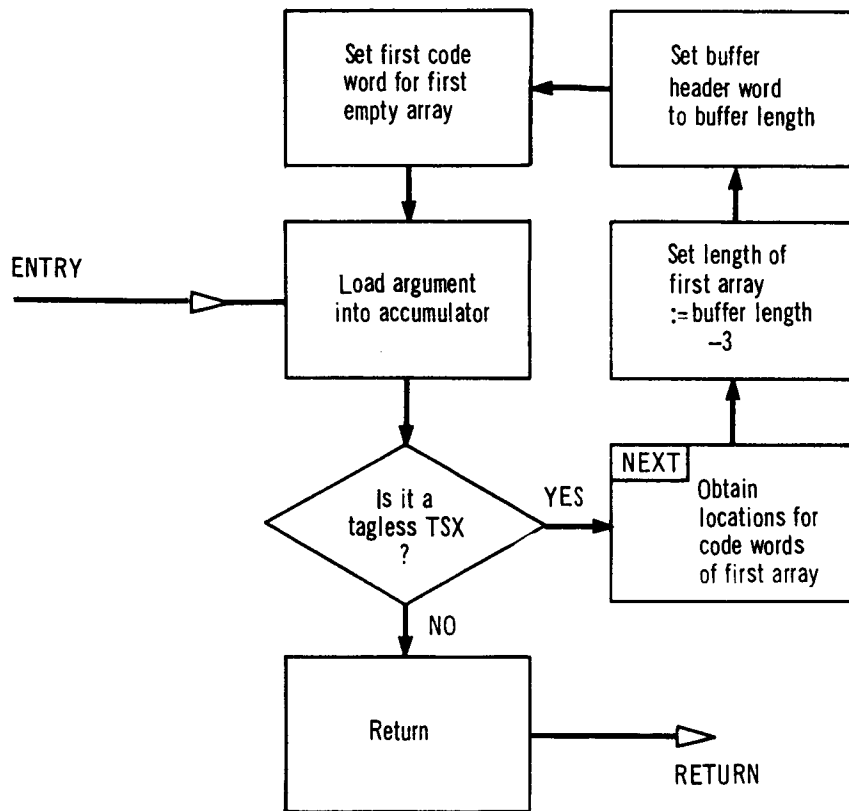
ICODE



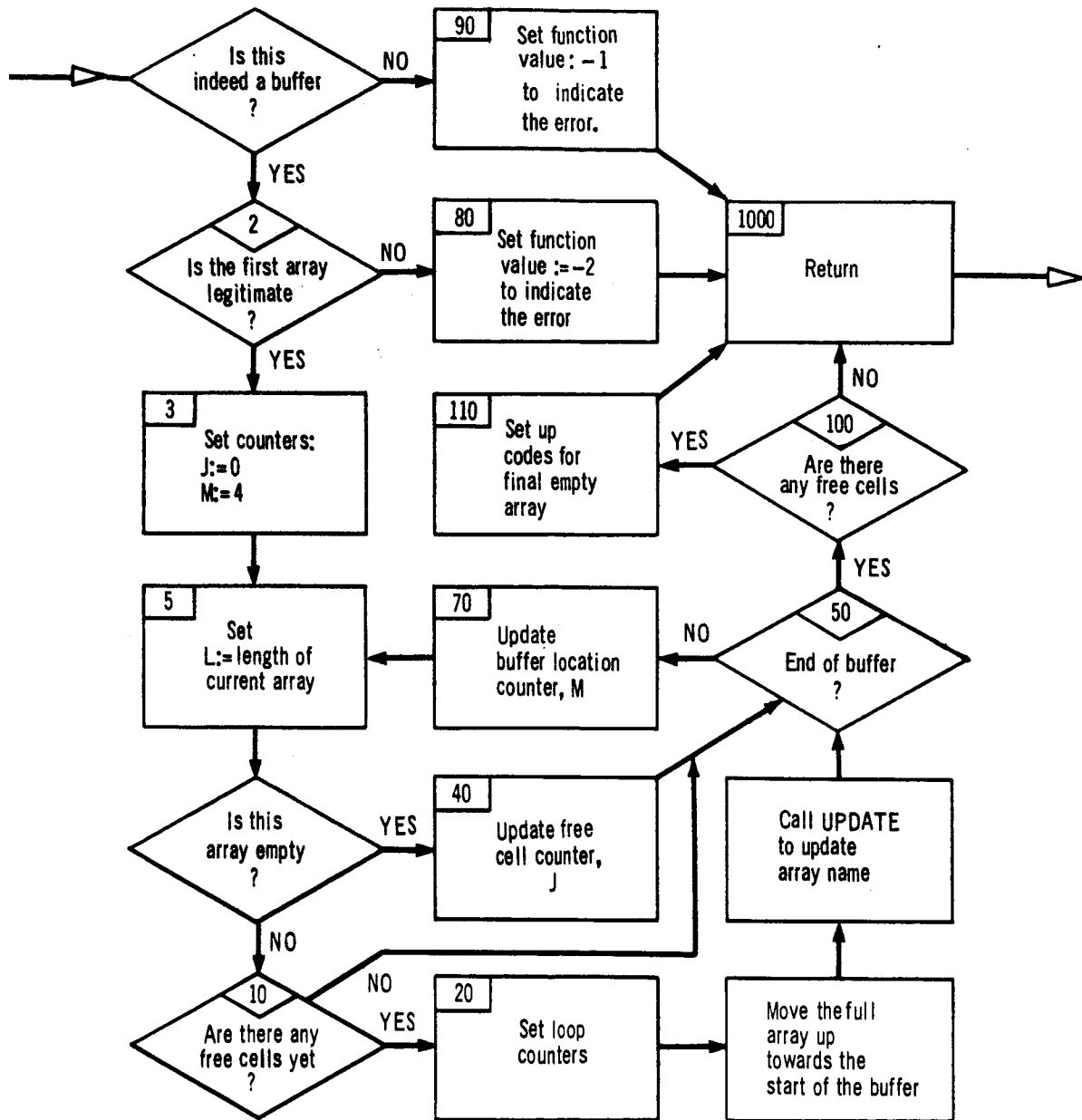
IDLETE



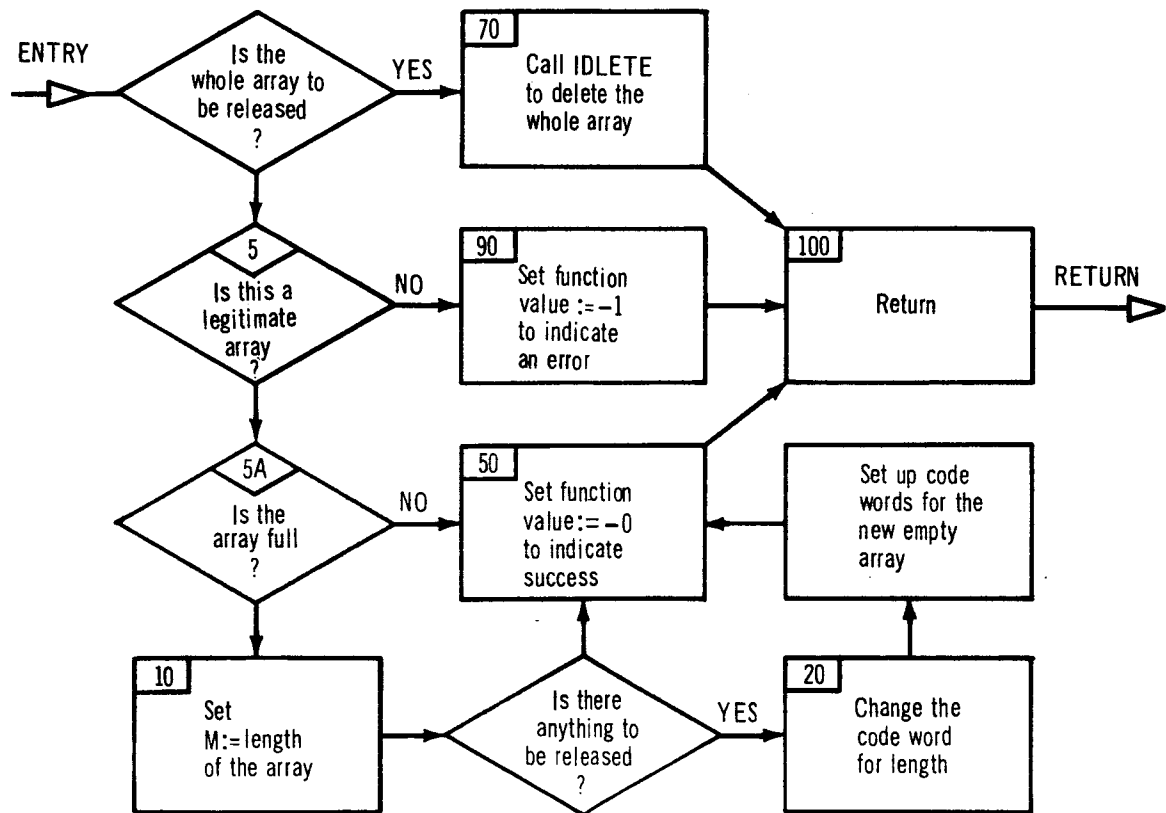
INI BFR



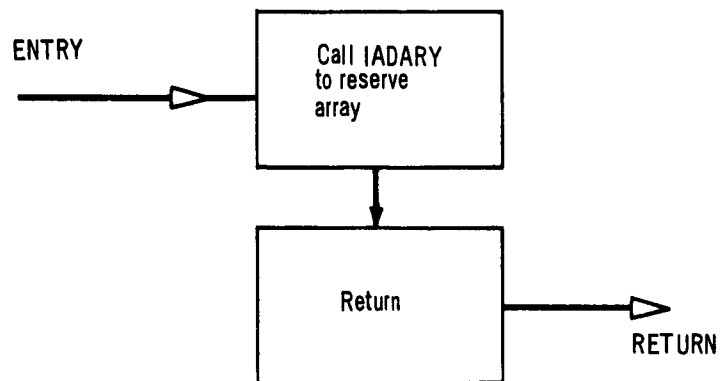
IPACK



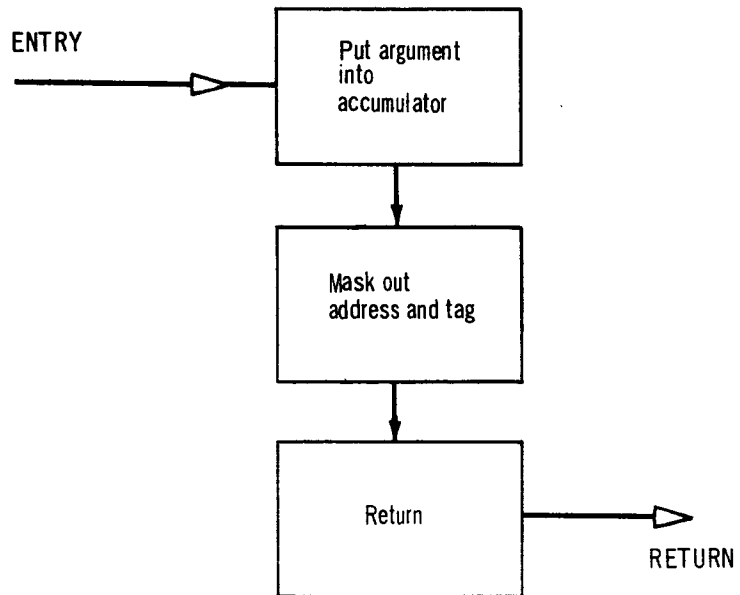
IRLEAS



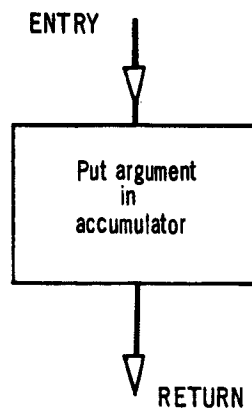
IRSERV



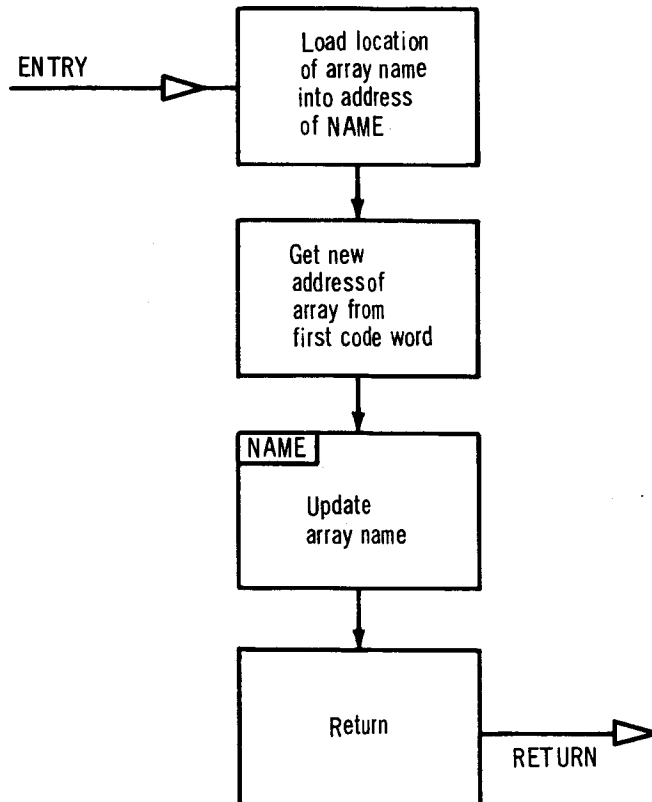
LENG



UFOOL



UPDATE



5.2 Appendix B — Matrix Inversion Package

SUBJECT: FORTRAN IV Subroutine SINVRT and MAP Subroutine INV4S

PURPOSE: To invert an n-by-n matrix and compute its determinant.

METHOD:

1. Before the inversion process starts, the matrix is scaled so that the element of largest magnitude is greater than or equal to $1/4$ and less than $1/2$. This is accomplished through fixed-point addition or subtraction in the characteristic, which avoids the introduction of round-off during scaling.
2. A theorem of matrix algebra states that for any non-singular matrix A , there exist elementary transformations R and S such that:

$$RAS = I \quad (1)$$

where I is the identity matrix. Because R and S are elementary transformations, they are necessarily non-singular which permits taking the inverse of both sides of equation (1).

$$S^{-1} A^{-1} R^{-1} = I$$

Then solving for A^{-1} gives,

$$A^{-1} = SIR = SR$$

The transformations S and R are determined by reducing A to the identity matrix. In INV4S R consists of row interchanges and arithmetic operations on rows, while S consists solely of column interchanges.

3. The inversion is performed in single precision, and it leaves a single-precision inverse and determinant. Normal 7094 single-precision floating-point restrictions apply.
4. The inversion of a sparse matrix is speeded up by a checking feature that can sense a zero reduction factor and bypass a row reduction.
5. At the start of each reduction stage, rows and columns are interchanged to select the element of largest magnitude from the remaining submatrix and place it in the pivotal position.

USAGE:

```
CALL SINVRT (A, K, N, IRR1, IRR2, SCALE, DET,  
             NDETXP)
```

A = Matrix to be inverted.

K = Row DIMENSION statement entry for A.

N = Number of rows (columns) in matrix (decrement integer).

IRR1 = Error code from INV4S (decrement integer).

IRR2 = Error code from INV4S (decrement integer).

SCALE = Error cell from INV4S.

DET = Mantissa part of determinant (single precision):

(1. $< |\text{DET}| < 10$.)

NDETXP = Exponent part of determinant (decrement integer):

$$-(2^{17} - 1) < \text{NDETXP} < (2^{17} - 1)$$
$$\text{determinant} = \text{DET} \times 10^{(\text{NDET} \times \text{P})}$$

CALL INV4S (A, N, IRR1, IRR2, SCALE, DET, NDETXP)

A = Location of (1, 1) matrix element.

N = Number of rows (columns) in matrix (address integer).

IRR1 = Error code 1 (address integer).

IRR2 = Error code 2 (address integer).

SCALE = Error cell.

DET = Mantissa part of determinant (single precision):

(1. $< |\text{DET}| < 10$.)

NDET_{XP} = Exponent part of determinant:

$$-(2^{35} - 1) < \text{NDET XP} < (2^{35} - 1)$$
$$\text{determinant} = \text{DET} \times 10^{(\text{NDETXP})}$$

SUBPROGRAMS

CALLED:

A. SINVRT calls INV4S

B. INV4S None

ERROR RETURNS: Error codes for both subroutines:

IRR1 = 0 inversion successful
= 1 overflow occurred
= 2 matrix is singular
= 3 scaled inverse cannot be rescaled
without causing overflow
= 4 rows and columns cannot be rearranged
= 10 + I error code 3 occurred subsequent to
error code 1
= 20 + I error code 4 occurred subsequent to
error code 1

IRR2 = Rank if IRR1 = 2
= Reduction stage during which overflow occurred
if IRR1 = 1
= 0 for all other values of IRR1

SCALE = Scale factor if IRR1 = 3
= 0 for all other values of IRR1

If IRR1 = 1 or 2, then the matrix will be rearranged and rescaled as though the inversion were successful, and the determinant will be set to zero.

RESTRICTIONS:

A. These must apply to the two routines:

1. They must be used on the IBM 7094 only.
2. The matrix is always destroyed during the inversion process, since the inverse is stored over the matrix.
3. Because of the internal scaling process, some matrix elements will be set to zero if the ratio of the largest to smallest magnitudes exceeds 10^{38} .
4. If underflow occurs, a normal zero is stored for the answer. Overflow always results in an error return.
5. The machine is left in single tag mode and floating point trap mode upon return to the calling program.

B. These apply to SINVRT only:

1. The inversion is performed by INV4S.
2. The matrix to be inverted must be stored in normal FORTRAN IV order and in single precision.

3. During the inversion process a total of $n^2 + 2n + 3$ locations must be available starting at the matrix (1, 1) element and ending at a lower core location.

C. This applies to INV4S only:

The total storage required is $n^2 + 2n + 3$.

STORAGE:

A. SINVRT $315_{10} = 473_8$

B. INV4S $489_{10} = 751_8$

TIMING:

For INV4S and SINVRT, the time in seconds to invert a matrix of order n is given by:

$$\text{Time} = 4.0 \times 10^{-5} \times n^3 \text{ seconds}$$

CHECKOUT:

All of the routines were tested on various-order Hilbert matrices and their inverses. Below is a table of the results.

Hilbert Matrix Order	Minimum Number of Signifi- cant Figures in Inverse (INV4S/SINVRT)
2	8
3	7
4	5
5	4
6	3

Also tested was the PEI matrix (Comm. A.C.M. V.5, 1962, page 508) with various diagonal terms and various orders. All input was single precision.

Order of PEI Matrix	Diagonal Term	Minimum Number of Signifi- cant Figures in Inverse (SINVRT)
40	1.001	5
60	1.001	6
65	1.00001	3
100	1.001	5
100	1.0001	4
100	1.00001	3
100	1.000001	2
100	1.0000001	2
100	1.5	7
100	1000.	7

<u>Order of PEI Matrix</u>	<u>Diagonal Term</u>	<u>Minimum Number of Signifi- cant Figures in Inverse (SINVRT)</u>
130	1000.	6
130	1000.	6

RECOMMENDED

USAGE:

Below is a portion of a FORTRAN IV program which uses SINVRT acceptably.

```

      DIMENSION  A(60, 60), B(123), D(3723)
      EQUIVALENCE (A, C), (B, C(3601))
      .
      .
      .
      READ (5, 8000) N, ((A(I, J), J=1, N), I=1, N)
      CALL SINVRT (A, 60, N, IRR1, IRR2, SCALE, DET,
                   NDETXP)
      IF (IRR1) 6000, 20, 6000
20
      .
      .
6000 WRITE (6, 9000) IRR1, IRR2, SCALE

      CALL EXIT

8000 FORMAT (I10/(7F10.0))
9000 FORMAT (1H1,5X, 18H ERROR CODE 1 = I5, 14H
             ERROR CODE 2=I5, 14H SCALE FACTOR =
             E16.8)

```

The array C has $N^2 + 2N + 3 = 3723$ cells to ensure sufficient core to invert A. An extra 123 locations are then available in B for use at other times.

5.3 Appendix C — Differential Equation Solver Package

SUBJECT: FORTRAN IV Subroutines DED, DEDIS, DEI, DES

PURPOSE: To solve a set of N first-order ordinary differential equations by the Adams-Moulton predictor-corrector method.

METHOD: The differential equations must be in the form:

$$y'_1 = f_1(t, y_1, y_2, \dots, y_n)$$

$$y'_2 = f_2(t, y_1, y_2, \dots, y_n)$$

$$y'_1 = f_1(t, y_1, y_2, \dots, y_1, \dots, y_n)$$

$$y'_n = f_n(t, y_1, y_2, \dots, y_n)$$

t is the independent variable and y_1, y_2, \dots, y_n are the dependent variables that must be determined for a given range of t .

A description of this method follows:

1. The initial conditions for t, y_1, y_2, \dots, y_n must be given as well as an initial dependent variable increment h . Backward integration may be performed by using a negative h .
2. Each differential equation requires four points before the predictor-corrector equations may be applied. The first three integrations are performed by the Runge-Kutta method, and the initial conditions give the required starting points for the predictor-corrector formulas. Each time the step size is altered, it is necessary to obtain new starting points using Runge-Kutta integration.
3. Once four points are determined, the integration is performed from point n to $n + 1$ along the curve using equation 3.a to predict and 3.b to correct. Let h be the independent variable increment:

$$\text{a. } y_{i,n+1}^{(p)} = y_{i,n} + \frac{h}{24} (55f_{i,n} - 59f_{i,n-1} + 37f_{i,n-2} - 9f_{i,n-3})$$

$$\text{b. } y_{i,n+1}^{(p)} = y_{i,n} + \frac{h}{24} (9f_{i,n+1} + 19f_{i,n} - 5f_{i,n-1} + f_{i,n-2})$$

(p) and (c) represent predicted and corrected values respectively. $y_{i,n+1}^{(p)}$ and $y_{i,n+1}^{(c)}$ are tested. If the test is satisfied so that it is not required to change h, the derivatives $y'_{i,n+1}$ are calculated from the differential equations.

USAGE:

More than one system of differential equations may be solved in a given FORTRAN program. Let N be the maximum number of differential equations required to solve in a FORTRAN program. The following must be considered in using the routines.

1. A FORTRAN floating array of $12A + 9$ storage cells must be reserved in a dimension statement. This block shall be referred to as T.
2. Dealing with a particular system of differential equations, the number of equations must be stored in two FORTRAN fixed variable locations. These locations will be referred to as NUM and NUM1.
3. An equivalence statement giving T(1) and NUM1 the same working location must be written.
4. There are certain parameters which are input to the differential equation routine. The following parameters are used:

β The fractional part to decrease the interval h if it needs to be reduced. Normally, set $= 0.5$ and it must be in the range $0 < \beta < 1$.

A A number used in determining the relative error between the predicted and corrected values. Normally, $A = 1$.

h_{\min} The minimum increment of the independent variable. This value must not be negative.

- h_{\max} The maximum allowable increment of the independent variable. This value must not be negative.
- M Ratio between upper bound and lower bound relative error. Normally, give it the value 1,000.
- E Allowable relative error between the predicted and corrected value. A representative value is 10^{-6} .

5. The following FORTRAN locations must be initialized with the indicated quantities prior to entering the differential equation solving routines.

FORTRAN location

NUM, NUM1	Number of differential equations that must be solved.
T(12*NUM)	Initial value of 1 st dependent variable.
T(12*NUM-1)	Initial value of 2 nd variable.
.	
.	
.	
T(12*NUM-NUM+1)	Initial value of last dependent variable.
T(12*NUM+1)	Initial increment of independent variable.
T(12*NUM+2)	Initial value of independent variable.
T(12*NUM+4)	β as defined in 4.
T(12*NUM+5)	h_{\min}
T(12*NUM+6)	h_{\max}
T(12*NUM+7)	A
T(12*NUM+8)	M
T(12*NUM+9)	E

6. A block in the program or a subprogram must be made to calculate the derivatives. These must be calculated in terms of T block locations since the differential equation subprogram links to this block to compute the derivatives when required. The coding of the derivative calculations may be simplified by equivalence statements if the number of differential equations is invariant.

FORTTRAN name

T(11*NUM)	First derivative	y'_1
T(11*NUM-1)	Second derivative	y'_2
T(11*NUM-NUM+1)	Last derivative	y'_n

7. There are three linkages to the differential equation-solving routine, DEDIS, by CALL statements. They are given the names DES, DEI, and DED.

a. DES Used once at the beginning to set up the routine for integration of a given set of differential equations. The statement is CALL DES(NUM1, IND, NTEST).

b. DEI Linked to the required number of times to integrate all y_i from t_{initial} to t_{final} . The CALL statement is CALL DEI(NUM, IND, NTEST).

c. DED The statement is CALL DED(NARG).

8. The following fixed point arguments are required for the CALL statements:

NUM }
NUM1 } = Number of equations in the system.

IND = 0, variable interval using Adams-Moulton predictor-corrector method.

NTEST = Used in the differential equation program in order to have the correct linkage to the differential equation routine. Its value is set in the differential equation routine. It must be the 3rd argument of DES and the argument of the IF statement as indicated below.

NARG = Calculated in the differential equation subprogram and tested in the calling sequence to determine whether an integration step is completed.

EXAMPLE CALLING SEQUENCE

```
CALL DES(NUM1, IND, NTEST)
7 IF(NTEST) 15, 15, 11
11 CALL DEI(NUM, IND, NTEST)
15 (Derivative Calculation)
CALL DED(NARG)
IF(NARG.EQ.O) GOTO 7
```

SUBPROGRAMS

CALLED: None

ERROR RETURNS: If an error is detected, a comment is printed and exit is made to the monitor. Checks are made for the following errors:

<u>Error</u>	<u>Error comment</u>
1. The number of differential equations $N = 0$.	Differential equation sub-routine DES input error $N = 0$.
2. N is floating or $n > 4096$	Differential equation sub-routine DES input error N FLT.
3. Step size $H = 0$	Differential equation sub-routine DES input error $H = 0$.
4. Integration mode indicator $\neq 0, 1$, or 2 .	Differential equation sub-routine DES input error IND.
5. Predictor-corrector tolerance $E = 0$	Differential equation sub-routine DES input error $E = 0$.

RESTRICTIONS: See above, ERROR RETURNS

STORAGE:

1. DED	$46_{10} = 56_8$
2. DEDIS	$1309_{10} = 2435_8$
3. DEI	$37_{10} = 45_8$
4. DES	$36_{10} = 44_8$

5.4 Appendix D — Tape Formats

Format 1 — Geometry definition tape format

This tape, written by the Geometry Definition section and read by the Transformation section, contains 18 binary records in the first file. Odd-numbered records have 10 fixed-point words; even-numbered records have a variable number of floating-point words. The tape symbol is LA in subroutine OPCAMI, LTAPE in subroutine DEFEN1 (which writes the tape), and LA in subroutine TFLAT (which reads the tape).

Record 1: Body Stations

Word 1 = 1
2 Number of words in record 2.
3 Code* (appears after record 18, at the end of this section).
4 - 10 Not used.

Record 2: Body Stations

Word 1 First body station.
2 Second body station.
.
.
.
n Last body station.

Record 3: Basic Body Meridian Lines

Word 1 = 3
2 Number of words in record 4.
3 Code*.
4 Number of meridian lines.
5 - 10 Not used.

Record 4: Basic Body Meridian Lines

Word 1 θ
2 Number of points in meridian line.
3 Word number of first point in meridian line. } First meridian line.
Repeat for each additional meridian line.
$$\left. \begin{array}{l} i \quad X_1 \\ i + 1 \quad Y_1 \\ i + 2 \quad Z_1 \end{array} \right\} \text{Coordinates of first point in first meridian line.}$$

Repeat for each additional point in first meridian line and continue this way for each additional meridian line.

Record 5: Wing Planform (Leading and Trailing Edge Points for Each Control Airfoil or Chord)

Word 1 = 5
2 Number of words in record 6.
3 Code*.
4 Number of control airfoils or chords.
5 - 10 Not used.

Record 6: Wing Planform (Leading and Trailing Edge Points for Each Control Airfoil or Chord).

Word 1 X_1 } Coordinates of leading-edge point of first control airfoil
2 Y_1 } or chord.
3 X_2 } Coordinates of trailing-edge point of first control airfoil
4 Y_2 } or chord.
Follow with leading- and trailing-edge points of remaining control airfoils or chords.

Record 7: Basic Upper Wing Percent Chord Lines

Word 1 = 7
2 Number of words in record 8.
3 Code*.
4 Number of percent chord lines.
5 - 10 Not used.

Record 8: Basic Upper Wing Percent Chord Lines

Word	1	Percent.	} First percent chord line.
	2	Number of points in percent chord line.	
	3	Word number of first point in percent chord line.	

Repeat for each additional percent chord line and follow with the coordinates of each point in each percent chord line.

NOTE: The format of record 8 is identical to that of record 4 except that words 1, 4, 7, ..., $3n - 2$ contain percent instead of θ , where n = number of percent chord lines.

Record 9: Basic Lower Wing Percent Chord Lines

Word 1 = 9

2 Number of words in record 10.

3 Code*.

4 Number of percent chord lines.

5 - 10 Not used.

Record 10: Basic Lower Wing Percent Chord Lines

Same format as record 8.

Record 11: Upper Wing-Body Intersection Points

Word 1 = 11

2 Number of words in record 12.

3 Code*.

4 Number of intersection points of upper wing percent chord lines with body.

5 - 10 Not used.

Record 12: Upper Wing-Body Intersection Points

Word	1	X_1	} Coordinates of the intersection of the first upper wing percent chord line with the body.
	2	Y_1	
	3	Z_1	

Repeat for each additional intersection point of the upper wing.

Record 13: Upper Wing Percent Chord Lines (Outside Body)

Word 1 = 13
2 Number of words in record 14.
3 Code*.
4 Number of percent chord lines.
5 - 10 Not used.

Record 14: Upper Wing Percent Chord Lines (Outside Body)

Same format as record 8.

Record 15: Lower Wing-Body Intersection Points

Word 1 = 15
2 Number of words in record 16.
3 Code*.
4 Number of intersection points of lower wing chord percent lines with body.
5 - 10 Not used.

Record 16: Lower Wing-Body Intersection Points

Word 1 X_1 }
2 Y_1 } Coordinates of the intersection of the first lower wing
3 Z_1 } percent chord line with the body.
Repeat for each additional intersection point of the lower wing.

Record 17: Lower Wing Percent Chord Lines (Outside Body)

Word 1 = 17
2 Number of words in record 18.
3 Code*.
4 Number of percent chord lines
5 - 10 Not used.

Record 18: Lower Wing Percent Chord Lines (Outside Body)

Same format as record 8.

* CODE = 0 If this and the next record have been successfully processed.
< 0 An error occurred and the next record is a dummy (all zeros).
> 0 This option was not requested; the next record is a dummy (all zeros).

Format 2 — Geometry transformation tape format

This tape, written by the Geometry Transformation section and read by the Geometry Paneling section of the program, contains 6 binary records in the first file. Odd-numbered records have 10 fixed-point words; even-numbered records have a variable number of floating-point words. The tape symbol is LD in subroutine OPCAMI, LD in subroutine TFLAT (which writes the tape), and ND4 in subroutines INPUTB and INPUTW (which read the tape).

Record 1: Body Meridian Lines

Word 1 = 1
2 Number of words in record 2.
3 Code* (appears after record 6, at the end of this section).
4 Number of meridian lines.
5 - 10 Not used.

Record 2: Body Meridian Lines

Word 1 θ
2 Number of points in meridian line.
3 Word number of first point in meridian line } First meridian line.
Repeat for each additional meridian line.
1 X_1 }
1 + 1 Y_1 } Coordinates of first point in first meridian line.
1 + 2 Z_1 }
Repeat for each additional point in first meridian line and continue this way for each additional meridian line.

Record 3: Wing Percent Chord Lines

Word 1 = 3
2 Number of words in record 4.
3 Code*.
4 Number of percent chord lines.
5 - 10 Not used.

Record 4: Wing Percent Chord Lines

Word	1	Percent.	}	First percent chord line.
	2	Number of points in percent chord line.		
	3	Word number of first point in percent chord line.		

Repeat for each additional percent chord line and follow with the coordinates of each point in each percent chord line.

NOTE: The format of record 4 is identical to that of record 2 except that words 1, 4, 7, ..., $3n - 2$ contain percent instead of θ , where n = number of percent chord lines.

Record 5: Wing-Body Intersection Points

Word	1	= 5
	2	Number of words in record 6.
	3	Code*.
	4	Number of intersection points of wing percent chord lines with body.
	5 - 10	Not used.

Record 6: Wing-Body Intersection Points

Word	1	X_1	}	Coordinates of the intersection of the first wing percent chord line with the body.
	2	Y_1		
	3	Z_1		

Repeat for each additional intersection point.

* CODE = 0	If this and the next record have been successfully processed.
< 0	An error occurred and the next record is a dummy (all zeros).
> 0	This option was not requested; the next record is a dummy (all zeros).

Format 3 — Transformation data tape format

This tape, containing three records in the first file, is written by the Geometry Transformation section of the program; both the Geometry Paneling and Aerodynamics sections read the tape. The tape symbol is LB in subroutine OPCAMI, LB in subroutine TFLAT (which writes the tape), ND1 in subroutine INPUTB (which reads only the first record), and NTAPEB in subroutine INTAPE (which reads all records).

Record 1

Word	1	x	} Components of a unit vector (in original coordinate system) along the x axis of the new coordinate system.
	2	y	
	3	z	
	4	z_A	z coordinate of the transformed and flattened wing.
	5	α	} An original body station X is related to the new body station x by $x = \alpha X + \beta$.
	6	β	

Record 2

Word	1	NRX	Number of triplets (x_i, r_i, z_i) in record 3.
	2	INDEX	For INDEX = j. The triplet (x_i, r_i, z_i) corresponds to the intersection of the leading edge of the wing with the body surface (see record 3).

Record 3

After the body has been transformed to a new coordinate system such that the new x axis passes through the centers of body ends, the body radius and centroid is found at a number of body stations. Let x = body station, r = body radius, and z = z-coordinate of body centroid.

Word	1	x	} x, r and z at first body station.
	2	r	
	3	z	

Repeat until the record contains NRX triplets.

Format 4 — Geometry Paneling tape format

This tape is written by the Geometry Paneling section for use in the Aerodynamics section. The tape symbol NTAPE2 is used in the Geometry Paneling section and NTAPEC is used in the Aerodynamic section. The sample format given below is that used for a case requiring both body and wing paneling. It should be noted that parts 1, 2, and 3 are deleted for a case that involves only wing paneling and that the tape is not written for a body-alone case. Body paneling data are written in parts 1, 2, and 3 and data for wing paneling in parts 4, 5, and 6; panel corner point coordinates are output in parts 1 and 4 and the additional geometry in parts 2 and 5. One-, two-, and three-records are written in parts 1 and 4 for panels of one, two, and three parts respectively. For these two tape parts, the initial record of each record set always has the format of record 1 as given below and the remaining records of the set have the format described for record 2. A single record is written per panel in parts 2 and 5.

Part 1

Record 1

Word	1	Body panel number.
	2	Number of body panel parts.
	3	Coordinates of inboard leading-edge corner point (first panel part).
	4	
	5	
	6	Coordinates of outboard leading-edge corner point (first panel part).
	7	
	8	
	9	Coordinates of inboard trailing-edge corner point (first panel part).
	10	
	11	

12	}	Coordinates of outboard trailing-edge corner point (first panel part).
13		
14		

Record 2

Word	1	}	Coordinates of inboard leading-edge corner point (second panel part).
	2		
	3		
	4	}	Coordinates of outboard leading-edge corner point (second panel part).
	5		
	6		
	7	}	Coordinates of inboard trailing-edge corner point (second panel part).
	8		
	9		
	10	}	Coordinates of outboard trailing-edge corner point (second panel part).
	11		
	12		

These records are repeated for additional body panels as indicated above.

Part 2

Record 1

Word	1	Body panel number.
	2	}
	3	
	4	
	5	}
	6	
	7	
	8	Body panel area.
	9	Body panel θ -inclination angle.

- 10 Body panel α -incidence angle.
- 11 Body panel (streamwise) chord length.
- This single record is repeated for each additional body panel.

Part 3

Record 1

- Word 1 Number of body panels per column.
- 2 Fractional value (XPER) used to calculate streamwise location
 of panel control point (see subroutine PANEL).

 This is the only record written for this part.

Part 4

Record 1

- Word 1 Wing panel number.
- 2 Number of wing panel parts.
- 3)
- 4) Coordinates of inboard leading-edge corner point (first panel
- 5) part).
- 6)
- 7) Coordinates of outboard leading-edge corner point (first panel
- 8) part).
- 9)
- 10) Coordinates of inboard trailing-edge corner point (first panel
- 11) part).
- 12)
- 13) Coordinates of outboard trailing-edge corner point (first panel
- 14) part).

Record 2

- Word 1)
- 2) Coordinates of inboard leading-edge corner point (second panel
- 3) part).

4	}	Coordinates of outboard leading-edge corner point (second panel part).
5		
6		
7	}	Coordinates of inboard trailing-edge corner point (second panel part).
8		
9		
10	}	Coordinates of outboard trailing-edge corner point (second panel part).
11		
12		

Record 1 or records 1 and 2 are repeated for additional one- or two-part wing panels as indicated above.

Part 5

Record 1

Word	1	Wing panel number.
	2	Coordinates of wing panel centroid.
	3	
	4	
	5	Coordinates of wing panel control point.
	6	
	7	
	8	Wing panel area.
	9	Wing panel thickness slope.
	10	Wing panel camber slope.
	11	Wing panel (streamwise) chord length.

This one record is repeated for each additional wing panel.

Part 6

Record 1

Word	1	Number of wing panels per column.
	2	Fractional value (XPER) used to calculate streamwise location of panel control point (see subroutine PANEL).

This is the only record written for this part.

Format 5 — Aerodynamics save tape format

This tape is written in the Aerodynamics section and can be saved for analysis of additional aerodynamic cases on later computer runs. The tape is also used in the Flow Visualization section. The geometrical data of parts 1-4 and the aerodynamic matrices of part 7 are used in the Aerodynamics section. Parts 5, 6, and 8-11 contain data for the Flow Visualization section. The tape symbol is NTAPEC in the Aerodynamics section and N8 in the Flow Visualization section. The sample format given below is that used for a wing-body configuration. Dummy files are written as necessary for wing-alone or body-alone configuration.

Part 1

Word 1	Panel number
2	} x -, y -, and z-coordinates of panel centroid.
3	
4	
5	} x -, y -, and z-coordinates of panel control point.
6	
7	
8	Panel area.
9	Panel Θ - inclination angle.
10	Panel α - incidence angle.
11	Panel chord length.

Words 1 through 11 are repeated for each panel.

N + 1	Code = 1, for wing-alone or body-alone configuration = 2, for wing-body configuration
N + 2	Number of panel rows on body if body-alone or wing-body configuration. Number of panel rows on wing if wing-alone configuration.
N + 3	Number of panel rows on wing if wing-body configuration. Otherwise, = 0.
N + 4	Fractional value for chordwise location of panel control point.

Part 2

Word 1	Wing panel α_T thickness slope.
--------	--

This word is repeated for each wing panel.

Part 3

Word 1 Wing panel α_C camber slope.

This word is repeated for each wing panel.

Part 4

Record 1

Word 1 Number of body meridian lines.
2 Angle of first body meridian line.

Word 2 is repeated for each body meridian line.

Record 2

Word 1 Body radius at first body station.

This word is repeated for each body station

Record 3

Word 1 Body camber at first body station.

This word is repeated for each body station.

Record 4

(Same as record 3)

Part 5

Word 1 Code = 1, if wing-alone configuration.
 = 2, if body-alone configuration.
 = 3, if wing-body configuration.

2 Total number of panels on configuration.

3 Number of body panels.

4 Number of wing panels.

5 Number of body stations.

6 Number of wing panels plus number of panel columns
 on wing.

7 Number of panel rows on body if body-alone or wing-body
 configuration.
 Number of panel rows on wing if wing-alone configuration.

8 Number of panel rows on wing if wing-body configuration.
 Otherwise, = 0.

9 Mach number.

10 Symmetry condition.

Part 6

Record 1

Word 1 Total number of panels on configuration.

Record 2

Word 1 Number of panel parts for first panel.

Record 3

Word 1	}	x- , y- and z-coordinates of inboard leading edge corner point of first panel part.
2		
3		
4	}	x- , y- and z-coordinates of outboard leading edge corner point of first panel part.
5		
6		
7	}	x- , y- and z-coordinates of inboard trailing edge corner point of first panel part.
8		
9		
10	}	x- , y- and z-coordinates of outboard trailing edge corner point of first panel part.
11		
12		

Record 3 is repeated for each panel part. Record 2 and Record(s) 3 are repeated as a set for each panel.

Record 4

Word 1	}	x- , y- and z-coordinates of panel centroid.
2		
3		

Words 1-3 are repeated for each panel.

Record 5

Word 1	}	x- , y- and z-coordinates of panel control point.
2		
3		

Words 1 through 3 are repeated for each panel.

Record 6

Word 1	}	Panel α - incidence angle.
2		Panel Θ - inclination angle.
3		Panel chord length.

Words 1 through 3 are repeated for each panel.

Part 7

Record 1	$[A_{WW}]$	Matrix of aerodynamic influence coefficients due to wing sources.
Record 2	$[WW]$	Drag minimization matrix.
Record 3	$[WW]^{-1}$	Inverse of drag minimization matrix constrained for wing lift.
Record 4	$[WW]^{-1}$	Inverse of drag minimization matrix constrained for wing lift and pitching moment.
Record 5	$[U_{WW}]$	Matrices of velocity components on the wing due to wing sources.
	$[V_{WW}]$	
	$[W_{WW}]$	
Record 6	$[U_{BB}]$	Matrices of velocity components on the body due to body surface vortices.
	$[V_{BB}]$	
	$[W_{BB}]$	
Record 7	$[U_{WB}]$	Matrices of velocity components on the wing due to body surface vortices.
	$[V_{WB}]$	
	$[W_{WB}]$	
Record 8	$[U_{BW}]$	Matrices of velocity components on the body due to wing surface vortices.
	$[V_{BW}]$	
	$[W_{BW}]$	
Record 9	$[U_{WW}]$	Matrices of velocity components on the wing due to wing surface vortices.
	$[V_{WW}]$	
	$[W_{WW}]$	

Record 10 $[A_R]$ "Reduced" aerodynamic matrix.

$$[A_R] = \left\{ [A_{WW}] - [A_{WB}][A_{BB}]^{-1}[A_{BW}] \right\}$$

Record 11 $[A_R]^{-1}$ Inverse of "reduced" aerodynamic matrix.

Record 12 $[A_{BB}]^{-1}$ Inverse of matrix of aerodynamic influence coefficients on the body due to body surface vortices.

Record 13 $[D]$ Product matrix.

$$[D] = [A_{WB}] \cdot [A_{BW}]^{-1}$$

Record 14 $[E]$ Product matrix.

$$[E] = [A_{BB}] \cdot [A_{BW}]$$

Part 8

Word 1 Code = 0., wing thickness effects not to be included.
 = 1., wing thickness effects to be included.
 2 Angle of attack of configuration.

Part 9

Record 1

Word 1 Number of wing panels plus number of panel columns on wing.

Record 2

Word 1 Wing panel α_T thickness slope.
 Record 2 is repeated for each wing column leading edge and wing panel trailing edge.

Part 10

Record 1

Word 1 Number of body stations.

Record 2

Word 1 x-coordinate at first body station.
 2 Body radius at first body station.

Words 1 and 2 are repeated for each body station.

Record 3

Word 1	Strength of quadratically varying source at first body station.
2	Strength of quadratically varying doublet at first body station.

Words 1 and 2 are repeated for each body station.

Record 4

Word 1	Strength of linearly varying source at body nose.
2	Strength of linearly varying doublet at body nose.

Part 11

Record 1

Word 1	Total number of panels on configuration.
--------	--

Record 2

Word 1	Strength of vortex on panel surface.
--------	--------------------------------------

Word 1 is repeated for each panel.

Appendix E — Subroutine Listings

Listings of the subroutines in the following index are given in this appendix.

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05/22/67

AERO - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE AERO

C CONTROL ROUTINE FOR AERODYNAMIC LINKS

COMMON DATE(2),NTAPEA,NTAPER,NTAPEE,NTAPEF,NTAPEI,
1,NTAPEO,NBODY,NWING,XMACH,SYM,KACE
DIMENSION DICT(5)

DATA DICT/6HUSE TA,6HSAVE T,6HCOMPUT,6HFLOW V,6HFLOW V/

REWIND NTAPEA
REWIND NTAPEE
REWIND NTAPEF
REWIND NTAPEE
REWIND NTAPEF

IGO=INTURP(DICT,3,NTAPEI,NTAPEO)

IGO=IGO+1

GO TO (900,50,80,100),IGO

50 REWIND NTAPEE

ISAVET=-1

READ (NTAPEI,5010) DUM

DC 60 I=4,5

60 IF (DUM.EQ.DICT(I)) GO TO 550

CALL USEYAP

GO TO 500

80 ISAVET=1

GO TO 150

100 ISAVET=0

150 CONTINUE

CALL AMATE

C KACE = 1 WING ALONE

C KACE = 2 BODY ALONE

C KACE = 3 WING-BODY COMBINATION

GO TO (200,450,300),KACE

200 CALL INVH

GO TO 400

300 CONTINUE

CALL INVBB

CALL REDUCE

CALL INVH

CALL PARTV

CALL MDMAE

450 CALL SAVTAP(1,ISAVET)

500 CALL FCES

IGO=INTURP(DICT(4),2,NTAPEI,NTAPEO)

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05/31/67

ALLIN - EFN SOURCE STATEMENT - IFNISI -

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SURROUTINE ALLIN(NTA)
  DIMENSION X(210,3,4),Y(210,3,4),Z(210,3,4),NRCH(2),NPART(210)
  DIMENSION ALPHAS(210),THETA(210)
  DIMENSION XBB(50),R(50),WT(120)
  DIMENSION T(50),TC(50),SST(210),CHORD(210)
  COMMON /FLOV1/KACE,NPANEL,NBODY,NWING,NBODYS,NWINGS,NRCW,XMACH,SYM
  COMMON /FLOV2/X,Y,Z,NPART,ALPHAS,THETA,XBB,R,WT,T,TC,SST,CHORD
  COMMON /BA/XR(210),YR(210),ZR(210)
  COMMON /BB/XC(210),YC(210),ZC(210)
  COMMON /FLOV3/ T11, TC11
  COMMON /THICK/THKW,ARA,CPCALC,CAMN
  NR=NTA
  REMIND NTA
  CALL FSE(4,NB,ER)
  READ(NR) KACE,NPANEL,NBODY,NWING,NBODYS,NWINGS,NRCW,XMACH,SYM
  CALL FSE(1,NB,ER)
  IF(NWING.EQ.0) GO TO 15
  READ(NB) NPANEL
  DO 5 J=1,NPANEL
    READ(NTA) NPART(J)
    APT=NPART(J)
    READ(NTA) (X(J,M,K),Y(J,M,K),Z(J,M,K),K=1,4),P=1,NPT)
  5 CONTINUE
  XC,YC,ZC ARE CENTROID POINTS
  XE,YE,ZB ARE BOUNDARY POINTS
  READ(NB) (X(J),Y(J),ZB(J),J=1,NPANEL)
  READ(NB) (XC(J),YC(J),ZC(J),J=1,NPANEL)
  READ(NB) (ALPHAS(J),THETA(J),CHORD(J),J=1,NPANEL)
  15 CONTINUE
  CALL FSE(2,NB,ER)
  READ(NR) THKW,ARA
  CALL FSE(1,NB,ER)
  IF(THKW.EQ.0) GO TO 25
  READ(NB) NWING
  DO 20 J=1,NWING
    READ(NB) WT(J)
  20 CONTINUE
  25 CONTINUE
  CALL FSE(1,NB,ER)
  IF(NBODYS.EQ.0) GO TO 35
  READ(NB) NBODYS
  READ(NB) (XPR(J),R(J),J=1,NBODYS)
  READ(NB) (T(J),TC(J),J=1,NBODYS)
  READ(NB) T11,TC11
  35 CONTINUE
  CALL FSE(1,NB,ER)
  IF(NWING.EQ.0) GO TO 30
  READ(NR) NPANEL
  READ(NB) (SST(J),J=1,NPANEL)
  30 CONTINUE
  REMIND NR
  RETURN
  ENB

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ALPHAB 09/14/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

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SUBROUTINE ALPHAB
COMMON DATE(2),NTAPE1,ND1,NTAPE2,ND2(3),NREAD,
INWRITE,NBODY,NMIG,KMACH,SYM,KACE
COMMON /COM1/ KODEB,KODEM,KODEWU,KODEI,KODEC,XPER,YPER,KOPTB,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPER1
2,NPLANE,NPLN1
COMMON /COM2/ NPLNB,NPLNW,JLEAD,JTRAIL,IMID,NPTS(16),X(16,90),Y(16
1,90),Z(16,90),XCEPT(21),XCEPT(16),XCEPT(16),ZCEPT(16
2),CODEBW(16),KPADEL(15,20),XCOR(16,21),YCOR(16,21),ZCOR(16,21),XIN
3T(15,20,2),YINT(15,20,2),ZINT(15,20,2),XCEN(15,20),YCEN(15,20),ZCE
4N(15,20),XCON(15,20),YCON(15,20),ZCON(15,20),AREA(15,20),ARAT(15,2
50),THETA(15,20),ALPHA(15,20),CHORD(15,20)
DIMENSION C(4),P(3,50),Q(3,5),LOC(3)

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C SUBROUTINE TO CALCULATE BODY PANEL ALPHA
C ANGLES

C DEFINE FUNCTION TO BE USED IN CALCULATIONS

C ANGL CALCULATES ALPHA INCIDENCE ANGLES USING

C ARCTANGENT ROUTINE

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ANGL(X1,X2,Y1,Y2,Z1,Z2,A)=ATAN(((Z2-Z1)*COS(A)-
1*(Y2-Y1)*SIN(A))/(X2-X1))

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C CALCULATE PANEL ALPHA ANGLES

80 DO 90 I=1,NPER1

DO 87 J=1,NPLN1

KGO=KPADEL(I,J)

GO TO (83,85,83,85),KGO

83 ALPHA(I,J)=ANGL(XCOR(I,J),XINT(I,J,1),YCOR(I,J),YINT(I,J,1),

ZCOR(I,J),ZINT(I,J,1),THETA(I,J))

GO TO 87

85 ALPHA(I,J)=ANGL(XINT(I,J,1),XCOR(I,J,1),YINT(I,J,1),YCOR(I,J,1),

ZINT(I,J,1),ZCOR(I,J,1),THETA(I,J))

87 CONTINUE

90 CONTINUE

100 RETURN

END

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05/22/67

AMATE - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE AMATE

C CONTROL ROUTINE FOR COMPUTING AERODYNAMIC INFLUENCE COEFFICIENTS
C MATRIX AND VELOCITY COMPONENTS

COMMON DATE(2),NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI
1,NTAPEO,NBODY,NWING,XMACH,SYM,KACE

COMMON /BLOCK/ALPHAS(210),AREA(210),A(210),ALPHAC(110),ALPHAT(110)
C,CHORD(210)

I,ISYM

N,NPART(210),NPANEL,NROW(2)

T,THETA(210),TAIL

U,UC(210)

V,V(210),VPM(210),VVE(210),VPM(210)

W,W(210),WPM(210),WVE(210),WPM(210)

X,X(210,3,4),XBAR(210),XC(210)

Y,Y(210,3,4),YBAR(210),YC(210)

Z,Z(210,3,4),ZBAR(210),ZC(210)

C READ IN GEOMETRICAL DATA
CALL INTAPE

KACE = 1 WING ALONE

KACE = 2 BODY ALONE

KACE = 3 WING-BODY COMBINATION

GO TO (200,300,200),KACE

C COMPUTE VELOCITY COMPONENTS DUE TO WING SOURCES

C THICKNESS CASE

NS=NBODY+1

CALL EVAL(NS,XBAR,1.)

C COMPUTE VELOCITY COMPONENTS TO WING PANEL SINGULARITIES

C LIFTING CASE

NS=1

CALL EVAL(NS,XC,0.)

300 REWIND NTAPEC

REWIND NTAPEA

REWIND NTAPEB

RETURN

END

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SUBROUTINE AREAP(X,Y,Z,S,R,NC,NR)
DIMENSION X(16,16),Y(16,16),Z(16,16),S(15,15),R(15,15)
DIMENSION A(3),B(3),V(3)

C SUBROUTINE TO CALCULATE BODY AND WING PANEL
C AREAS

C CALCULATE PANEL AREAS

DO 60 I=1,NC

DO 60 J=1,NR

A(1)=X(I,J)-X(I,J+1)

A(2)=Y(I,J)-Y(I,J+1)

A(3)=Z(I,J)-Z(I,J+1)

B(1)=X(I+1,J+1)-X(I,J+1)

B(2)=Y(I+1,J+1)-Y(I,J+1)

B(3)=Z(I+1,J+1)-Z(I,J+1)

CALL VCROSS(A,B,V,D,K)

S1=D/2.

A(1)=X(I,J)-X(I+1,J)

A(2)=Y(I,J)-Y(I+1,J)

A(3)=Z(I,J)-Z(I+1,J)

B(1)=X(I+1,J+1)-X(I+1,J)

B(2)=Y(I+1,J+1)-Y(I+1,J)

B(3)=Z(I+1,J+1)-Z(I+1,J)

CALL VCROSS(A,B,V,D,K)

S2=D/2.

S(I,J)=S1+S2

RT(I,J)=S1/S(I,J)

RETURN

END

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07/31/65

\$IBLDR ARFREE
ASSEMBLED TEXT.
\$TEXT ARFREE

ARFRONN

STEXT ARFREE

ARFP.0301

*ARFREE MICHAEL SYNGE 6-9247 ASSEMBLED 26 JAN 65
* TO FORM THE FIRST CODE WORD OF AN EMPTY ARRAY.

CALLING SEQUENCE

BUF(M-2)=ARFRE(M)

WHERE BUF(N) IS THE FIRST CELL OF THE ARRAY

ENTRY	ARFRE
IRFRE	ENTRY

BINARY CARD (NOT PUNCHED)	
00000	0500 60 4 00003
00001	0361 00 0 00006
00002	0602 00 0 00005
00003	0500 00 0 00005
00004	0020 00 4 00001
00005	0 00000 0 00000
00006	000000700000
	00000
	01111

CONTROL DICTIONARY

SCDICT AP.FREE

BINARY CARD (NOT PUNCHING)

START=0,LENGTH=7,TYPE=7094,CMPLEX=5

PREFACE

ARCREF DECK LOC=0,LENGTH=7

LOC=0,LENGTH=7

ARFQ RFAL LOC=0,LENGTH=0

LOC=0,LENGTH=0

IRFRE REAL LOC=0,LENGTH=0

LOC=0, LENGTH=0

\$0KEND ARE FREE

ARFR0303

NO MESSAGES FOR THIS ASSEMBLY

07/31/65

ARFRE
SYMBOL REFERENCE DATA

REFERENCES TO DEFINED SYMBOLS.

CLASS	SYMBOL	VALUE	REFERENCES
LCR	ARFRE	00000	
QUAL	BLCTR		
LCR	UNOS		
	//		
	TEMP	00005	2,3

07/31/65

ARFU0300

ARFU0301

*ARFUL MICHAEL SYNGE 6-9247 ASSEMBLED 21 AUG 64
* TO FORM THE FIRST CODE WORD OF A FULL ARRAY.

CALLING SEQUENCE

BUF(M-2)=ARFUL(M)

WHERE BUF(M) IS THE FIRST CELL OF THE ARRAY.

ENTRY ARFUL

BINARY CARD (NOT PUNCHED)	
00000	0500 60 4 00003
00001	0361 00 0 00006
00002	0602 00 0 00005
00003	0500 00 0 00005
00004	0020 00 4 00001
00005	0 00000 0 00000
00006	750000700000
	00000
	01111

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*LONG
END
TEMP
TRA 1.4
CLA
SLW TEMP
ACL 3.4
ARFUL -0700000700000

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CENTROL DICTIONARY

SCDICT ARFUL

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BINARY CARD (NOT PUNCHED)
000007000000
000004000005
215126644360
000007000000
215126644360
000000000000

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START=0,LENGTH=7,TYPE=7094,CMBLX=5
LOC=0,LENGTH=7
LOC=0,LENGTH=0
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SDKEND ARFUL

ARFUND03

NO MESSAGES FOR THIS ASSEMBLY

REFERENCES TO DEFINED SYMBOLS.

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ARFUL 00000

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LCTR //

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ARSECR
7C94 RELMOD ASSEMBLY.

07/31/65

ARSE0300
ARSE0301

ARSECR
\$IBLDR ARSECR
ASSEMBLED TEXT.

\$TEXT ARSECR

*ARSECR MICHAEL SYNGE 6-9247 ASSEMBLED 26 JAN 65
* TO FORM THE SECOND CODE WORD OF A FULL ARRAY.
*
* CALLING SEQUENCE
*
* RUF(M-1)=ARSEC(N,NAME)
*
* WHERE N = THE LENGTH OF THE ARRAY
* NAME = THE NAME OF THE ARRAY
*
* ENTRY ARSEC
* IRSEC ENTRY ARSEC
*

BINARY CARD (NOT PUNCHED)

00000	0500 60 4 00003	10000	ARSEC	CLA*	3,4
00001	0767 00 0 00022	10000	ALS		18
00002	0600 00 0 00010	10001	STZ		TEMP
00003	0622 00 0 00010	10001	STD		TEMP
00004	0500 00 4 00004	10000	CLA		4,4
00005	0621 00 0 00010	10001	STA		TEMP
00006	0500 00 0 00010	10001	CLA		TEMP
00007	0020 00 4 00001	10000	TRA		1,4

*
00010 0 00000 0 00000 10000 TEMP
00000 01111
CONTROL DICTIONARY

ARSE0302

BINARY CARD (NOT PUNCHED)

00001	10000000	PREFACE	START=0, LENGTH=9, TYPE=7094, CMPLX=5
000004000005		ARSEC DECK	LOC=0, LENGTH=9
215162252351		ARSEC REAL	LOC=0, LENGTH=0
000011000000		IRSEC REAL	LOC=0, LENGTH=0
215162252360			
000000000000			
315162252360			
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\$DKEND ARSECR

ARSE0303

NO MESSAGES FOR THIS ASSEMBLY

07/31/65

ARSCP
SYMBOL REFERENCE DATA

REFERENCES TO DEFINED SYMBOLS.

CLASS	SYMBOL	VALUE	REFERENCES
	ARSEC	00000	
LCTR	BLCTR		
QUAL	UNOS		
LCTR	//		
	TEMP	00010	2,3,5,6

05/22/67

BCAM - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE BCAM(NBODYS,NROWB,XB,ZDELTA,XC,DZDXB,ACB)
DIMENSION XB(1),ZDELTA(1),XC(1),DZDXB(1),ACB(1)

C COMPUTES BODY CAMBER SLOPES, GIVEN BODY CAMBER SHAPE

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NB=NBODYS-1
DO 100 I=1,NB
  DZDXB(I+1)=(ZDELTA(I+1)-ZDELTA(1))/(XB(I+1)-XB(1))
  DZDXB(1)=DZDXB(2)
DO 120 J=1,NROWB
  IF (XB(I)-XC(J)) 110,115,115
110 CONTINUE
115 ACB(J)=DZDXB(I-1)+(XC(J)-XB(I-1))/(XB(I)-XB(I-1))*(DZDXB(I)-DZDXB(
  11-1))
120 CONTINUE
      RETURN
      END

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C      SURRCUTINF RCUTX(3,N,X,EP,NA,A)
C      DIMENSION B(1),C(4),A(2,1),LQ(2),Q(3)
C      USED BY MBXC TO CUT THE BODY WITH A STATION PLANE
C      TO GET A 2-DIM. ARRAY OF PTS. (A) IN THE PLANE.
C      A = (Y1,Z1,Y2,Z2,.....)
C      NA = NO. PTS. IN A.
C      INPUTS ARE 3,N,X,EP.  OUTPUTS ARE NA,A
C      DATA C/-1.,3*0./

C      J=0
C      C(4)=X
C      DO 1000 K=1,N
C      K1=3*K
C      K2=9(K1-1)
C      K3=9(K1)
C      CALL PCLXN(C,9(K3),3,K2,EP,1,0,LQ,L)
C      IF (L.NE. 1) GO TO 1000
C      J=J+1
C      A(1,J)=Q(2)
C      A(2,J)=Q(3)

C      1000 CONTINUE
C      NA=J
C      9000 RETURN
C      END

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BITURP
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT

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SUBROUTINE BITURP(X,Y,IXY,NXY,KD,XI,YI,NU)
DIMENSION X(1),Y(1),NU(3),C(4),YIQ(2)

C GIVEN NXY POINTS AND X=XI, INTERPOLATE TO FIND Y=YI.
C X AND Y VALUES SPACED IXY APART. IXY=1 IF CONSECUTIVE.
C KD=1 IF LINEAR INTERPOLATION, KD=2 IF BIQUADRATIC.
C LOGICAL LINT,LIF,LIL

C NU=0
LINT=.FALSE.
LIF=.FALSE.
LIL=.FALSE.

C 100 IF (IXY)110,110,200
110 NU=-1
GO TO 5000
200 IF (NXY-2)210,220,300
210 NU=-2
GO TO 3200
C USE LINEAR INTERPOLATION IF ONLY 2 POINTS.
220 LINT=.TRUE.
C 300 IX=IXY*(NXY-1)+1
JXY=IXY
C 400 IF (X(IX)-XI)*420,410,430
410 NU=-3
GO TO 3200
C X-VALUES OF POINTS IN DECREASING ORDER.
C WE WILL SEARCH FROM RIGHT TO LEFT INSTEAD OF
C LEFT TO RIGHT.
420 IA=IX+IXY
JXY=-JXY
GO TO 500
C 430 IA=1-IXY
C SEARCH FOR INTERVAL CONTAINING XI
500 DO 600 I=1,NXY
IA=IA+JXY
510 IF (XI-X(I*IA))700,800,600
600 CONTINUE
610 NU=2
GO TO 800
C 700 IF (I-2)/10,900,1000
710 NU=1
C XI FALLS EXACTLY ON A POINT OR IS OUTSIDE THE TABLE.
800 YI=Y(IA)
GO TO 3100
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07/31/65

BITURP	EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
C	900	IF (LIF=.TRUE.)	,31
C	1000	IF (I-NX)1100,1010,1010	,32
C	1010	IF (I-NX)1100,1010,1010	,33
C	1100	IF (I-NX)1100,1010,1010	,34
C	1200	IF (KD-2)3000,1250,1250	,35
C	1250	IF (LINT) GO TO 3000	,36
C	1300	QUADRATIC OR BIQUADRATIC INTERPOLATION	
C	1400	DO 1800 IZ=1,2	,37 ,38 ,39
C	1500	IF (IIZ.EQ.1 .AND. LIL) .OR. (IIZ.EQ.2 .AND. LIF) GO TO 1800	
C	1600	CALL ORAT(X(JA),Y(JA),JXY,1,XI,YIQ(I2),C,MU)	,40 ,41 ,42 ,43 ,44 ,45
C	1700	IF (MU)1710,1800,1710	,46 ,47 ,48
C	1710	NU=I2+2	,49
C	1800	TWO POINTS MUST HAVE SAME X	,50
C	1900	GO TO 3000	
C	2000	CONTINUE	,51 ,52
C	2100	IF (LIF.OR.LIL) GO TO 9000	,53 ,54 ,55
C	2200	BIQUADRATIC INTERPOLATION	
C	2300	KXY=JXY+JXY	,56 ,57 ,58 ,59
C	2400	I4=IA+JXY	
C	2500	YI=((X(I4)-XI)*YIQ(I2))/(X(I4)-X(I2))	
C	2600	GO TO 9000	
C	2700	LINEAR INTERPOLATION	,60
C	2800	YI=Y(I2)+(XI-X(I2))*((Y(I4)-Y(I2))/(X(I4)-X(I2)))	,61
C	2900	IF (NU)3200,9000,3200	
C	3000	ERROR. REDUCE ERROR COUNTER AND WRITE MESSAGE	,62
C	3100	LTAPE=NU(2)	,63
C	3200	NU(3)=NU(3)-1	,64
C	3300	IF (NU(3).LE.0 .OR. LTAPE.LE.0) GO TO 9000	,65
C	3400	WRITE (LTAPE,3410)NU(1),XI,YI,NXY,(X(1),Y(1),I=1,IX,IXY)	,66 ,67 ,68 ,69 ,70 ,71 ,72 ,73
C	3410	FORMAT(13H0BITURP ERROR 13,8H FOR X = F14.6,1H.14H RETURNED Y = F14.6,16,17H POINTS (X,Y) ARE/(1H 8F14.6))	
C	9000	RETURN	,74
C		END	,75

06/02/67

BJTURP - EFN SOURCE STATEMENT - IFN(S) -

```

SUBROUTINE BJTURP(X,Y,IXY,NXY,KD,XI,YI,MU)
  DIMENSION X(1),Y(1),MU(3),C(4),YIQ(2)
  C
  C GIVEN NXY POINTS AND X-XI, INTERPOLATE TO FIND Y-YI.
  C X AND Y VALUES SPACED IXY APART. IXY-1 IF CONSECUTIVE.
  C KD-1 IF LINEAR INTERPOLATION, KD-2 IF BICUADRATIC.
  C
  C LOGICAL LINT,LIF,LIL
  C
  MU=0
  LINT=.FALSE.
  LIF=.FALSE.
  LIL=.FALSE.
  C
  100 IF (IXY)110,110,200
  110 MU=-1
  GO TO 9000
  200 IF (NXY-2)210,220,300
  210 MU=-2
  GO TO 3200
  C
  C USE LINEAR INTERPOLATION IF ONLY 2 POINTS.
  220 LINT=.TRUE.
  C
  300 IX=IXY*(NXY-1)+1
  JXY=IXY
  C
  400 IF (X(IX)-X)420,410,430
  410 MU=-3
  GO TO 3200
  C
  C X-VALUES OF POINTS IN DECREASING ORDER.
  C WE WILL SEARCH FROM RIGHT TO LEFT INSTEAD OF
  C LEFT TO RIGHT.
  420 IA=IX+IXY
  JXY=-JXY
  GO TO 500
  C
  430 IA=1-IXY
  C
  C SEARCH FOR INTERVAL CONTAINING XI
  500 DO 600 I=1,NXY
  IA=IA+JXY
  510 IF (XI-X(IA))700,600,600
  600 CONTINUE
  610 MU=2
  GO TO 800
  C
  700 IF (I-2)710,900,1000
  710 MU=1
  C
  C XI FALLS EXACTLY ON A POINT OR IS OUTSIDE THE TABLE.
  800 YI=Y(IA)
  GO TO 3100
  C

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06/02/67

BJTURP - EFM SOURCE STATEMENT - IFN(3) -

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C 900 XI IN 1ST INTERVAL (OR LAST IF GOING FROM RIGHT)
    LIF=.TRUE.
C 1000 IF (I-NXY)1100,1010,1010
C 1100 XI IN LAST INTERVAL (OR 1ST)
    LIL=.TRUE.
C 1200 IF (KD-2)3000,1250,1250
    IF (LINT) GO TO 3000
C 1300 QUADRATIC OR BQUADRATIC INTERPOLATION
    JA=IA
    DO 1800 IZ=1,2
    JA-JA-JXY
    1500 IF ((IZ-EQ.1 .AND. LIL) .OR. (IZ-EQ.2 .AND. LIF)) GO TO 1800
    1600 CALL GRAT(X(JA),Y(JA),JXY,1,XI,YIQ(IZ),C,MU)
    YI=YIQ(IZ)
    1700 IF (MU)1710,1800,1710
    1710 MU=IZ+2
C TWO POINTS MUST HAVE SAME X
    GO TO 3000
C 1800 CONTINUE
C 1900 IF (LIF.OR.LIL) GO TO 9000
C BQUADRATIC INTERPOLATION
    2000 KXY=JXY+JXY
    I1=IA-KXY
    I4=IA+JXY
    YI=((X(I1)-XI)*YIQ(I1)+YIQ(I2))/(X(I1)-X(I2))
    GO TO 9000
C LINEAR INTERPOLATION
    3000 YI=Y(I2)*(XI-X(I1))/(X(I1)-X(I2))+Y(I1)*(X(I1)-X(I2))/(X(I1)-X(I2))
C 3100 IF (MU)3200,9000,3200
C 3200 ERROR. REDUCE ERROR COUNTER AND WRITE MESSAGE
    LTAPE=MU(2)
    MU(3)=MU(3)-1
    3300 IF (MU(3)-LE.0 .OR. LTAPE-LE.0) GO TO 9000
    3400 WRITE (LTAPE,3410)MU(1),XI,YI,NXY,(X(I1),Y(I1),1-1,XI,IXY)
    3410 FORMAT(13HBITURP ERROR 13,OH FOR X = F14.6,1M,14M RETURNED Y =
        .F14.6,16,17M POINTS (X,Y) ARE/(11H 8F14.6))
C 9000 RETURN
    END

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62

100

B L D M
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

08/16/65

SUBROUTINE B L D M (NM,XP,ZP,RFAREA,AREA,XBAR,ZBAR,ALPHAM,THETAM
1,CPM,CL,CD,CM)

C COMPUTES COEFFICIENT OF LIFT, DRAG, AND MOMENT CN BODY

DIMENSION AREA(1),XBAR(1),ZBAR(1),ALPHAM(1),THETAM(1),CPM(1)

DRAG=0.
XLIFT=0.
XM=0.0

DO 100 J=1,NM
F=CPM(J)*AREA(J)
XL=-F*CGS(THETAM(J))
XD=F*ALPHAM(J)
XM=XM-XL*(XBAR(J)-XP)+XD*(ZBAR(J)-ZP)
XLIFT=XLIFT+XL
DRAG=DRAG+XD
100 CONTINUE

CL=XLIFT/RFAREA
CD=DRAG/RFAREA
CM=XM/RFAREA

RETURN
END

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05/31/67

BLUNDR - FEN SOURCE STATEMENT - IFN(S) -

```

FUNCTION BLUNDR (IX,IY,IZ,MODE,NMAX)
COMMON DUM(4),N4,DM(3),N5,N6
BLUNDR=0.
GO TO(1,2,3,4),MODE
1 IF(IZ*IV.GT.NMAX) GO TO 5
RETURN
2 IF(IZ*IX.GT.NMAX) GO TO 5
RETURN
3 IF((IX*IV).GT.NMAX) GO TO 5
RETURN
4 IF((IX*IV+IV*IZ+IZ*IX).GT.NMAX) GO TO 5
RETURN
5 BLUNDR=1.
WRITE(N6,100) NMAX
100 FORMAT(1H0,8(1H*),45HGOLOS INPUT ERROR PRODUCT OF INCREMENT PARAME
    $ITERS GREATER THAN,2X,14,40(1H*))
RETURN
END

```

16

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SUBROUTINE BODCR(B,N,X,EP,CHD,MAXE,S,E,NE,Y,Z,AREA,RAD,NU)
FINDS THE AREA,EQUIV. RADIUS, AND CENTROID OF A BODY SECTION.
DIMENSION B(1),EP(5),S(2,N),E(MAXE),NU(3),CG(2)
THE BODY IS GIVEN AS A SET OF MERIDIAN LINES (SEE BODY1).
THE BODY IS SYMMETRICAL ABOUT A PLANE PARALLEL TO THE XZ PLANE.
WE HAVE THE MERIDIAN LINES FOR HALF THE BODY.
THE BODY SECTION IS THE INTERSECTION OF A STATION PLANE WITH THE BODY.
INPUTS ARE
B = BODY MERIDIAN LINE POINTS (WITH HEADER)
N = NO. OF MERIDIAN LINES
X = BODY STATION
EP = ARRAY OF TOLERANCES
CHD = CHORD HEIGHT TOLERANCE USED BY ENRYCH TO DETERMINE
      SPACING OF INTERPOLATED POINTS BETWEEN MERIDIANS.
MAXE = LENGTH OF ARRAY E
NU(2) = TAPE NO. FOR ENRYCH ERROR MESSAGE
NU(3) = ERROR LIMITER AND COUNTER (ALSO OUTPUT)
OUTPUTS ARE
S = ARRAY OF N POINTS (Y,Z) IN SECTION
E = IS ESSENTIALLY A SCRATCH ARRAY FOR ENRICHED SECTION POINTS.
THE 1ST N CELLS ARE THE Y VALUES OF S.
THE NEXT N CELLS ARE THE Z VALUES OF S.
THE NEXT NE CELLS ARE THE DENSE ARRAY OF POINTS,
      STORED (Y,Z,Y,Z,...) ON THE SECTION.
E IS NOT USED FOR DEGENERATE SECTIONS.
E IS USED BUT NO ENRICHING TAKES PLACE IF N .LT. 4 OR
      IF CHD .LE. 0.
NE IS EXPLAINED UNDER E
Y = Y COORD. OF CENTROID OF WHOLE SECTION.
Z = Z COORD. OF CENTROID
AREA = AREA OF WHOLE SECTION
RAD = AVERAGE DISTANCE FROM CENTROID TO EACH MERIDIAN LINE.
NU = 0 IF SUCCESS
      1 IF CUT THRU BODY DOES NOT INTERSECT ALL MERIDIAN LINES
      2,3,4, OR 5 IF ENRYCH ERROR.
      6 IF 1ST AND LAST PTS IN SECTION DO NOT HAVE SAME Y WITHIN EP(2)
KEE = 0
NU=1
CUT BODY WITH PLANE X = X TO GET SECTION S OF NS POINTS
CALL BCUTX(B,N,X,EP(1),NS,S)
IF(NS .NE. N .OR. N .LT. 2) GO TO 8000
NU=6
CHECK THAT 1ST AND LAST PTS IN SECTION HAVE SAME Y VALUE
IF(ABS(S(1,1)-S(1,N)) .GT. EP(2)) GO TO 8000
Y=(S(1,1)+S(1,N))/2.
CHECK FOR SECTION WITH ZERO AREA
IF(ABS(S(2,1)-S(2,N)) .GT. EP(4) .AND. N .GT. 2) GO TO 500
AREA=0.

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GO TO 1500
C
C
C   PREPARE TO ENRICH SECTION. WE MUST HAVE Y,Z IN SEPARATE
C   ARRAY SO USE 1ST PART OF E ARRAY
500 DO 600 I=1,N
    E(I)=S(I,1)
    II=I+N
600 E(II)=S(2,I)
C
C   IE=II+1
C   THE ENRICHED SECTION POINTS WILL START IN E(IE)
C   NE=MAXE-II-2
C   NE=AVAILABLE STORAGE FOR ENRICHED POINTS. WE SUBTRACT 2 BECAUSE
C   CEGAR WILL LATER FILL IN 2 CELLS AT END OF ARRAY.
C   CALL ENRYCH(E,E(N+1),N,CHO,E(IE),NE,NU)
C   IF(NU .EQ. 0) GO TO 1000
C   KEE = 1
C   IF(NU .NE. 3) GO TO 8000
C   NOTE WE IGNORE ERROR 3 FROM ENRYCH, ASSUMING THAT CALLING PROGRAM
C   HAS SET NUI(2), NUI(3) SO THAT ENRYCH PRINTED ERROR MESSAGE.
C   IF ERROR FROM ENRYCH, EXPLANATORY MESSAGE WRITTEN AT END (KEE = 1)
C
C   FIND AREA, CENTROID OF ENRICHED SECTION
1000 CALL CEGAR(NE/2,E(IE), AREA,CG)
C   AREA=AREA*AREA
C   IF AREA TOO SMALL, CG MAY BE INACCURATE
C   IF (AREA .LE. EP(3)) GO TO 1500
C   Z=CG(2)
C   GO TO 2000
C
1500 CONTINUE
C   FOR Z OF CENTROID, USE AVERAGE OF 1ST AND LAST POINTS.
C   Z=(S(2,1)+S(2,N))/2.
C
C   IF (AREA)1600,1600C,2000
1600 RAD=0.
C   GO TO 3000
C
2000 CONTINUE
C
C   COMPUTE RADIUS OF SECTION
C   SUMRAD=0.
C   DO 2500 I=1,NS
    RR=(S(1,I)-Y)**2 + (S(2,I)-Z)**2
    R=SQRT(RR)
    SUMRAD = SUMRAD + R
    IF (I .EQ. 1 .OR. I .EQ. NS) GO TO 2500
    SUMRAD = SUMRAD + R
2500 CONTINUE
C   FNS=NS*NS-2
C   RAD=SUMRAD/FNS
3000 CONTINUE
C   NU=0
C

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09/14/65

EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
8000	CONTINUE	
	LTAPE=NU(2)	
	IF(L.NOT.(NU .EQ. 0 .AND. LTAPE .GT. 0)) GO TO 9000	
	WRITE(LTAPE,8100)NU(1),(J,(S(1,J),I=1,2),J=1,NS)	
8100	FORMAT(12H0B0DCR ERROR 13,5X	
	1 5TH FAILURE IN FINDING CENTROID AND RADIUS OF A BODY SECTION	
	2 /30H BODY SECTION POINTS (Y,Z) ARE/(1H 13,2F20.6))	
9000	CONTINUE	
	IF(KEE .EQ. 0 .OR. LTAPE .LE. 0) GO TO 9900	
	WRITE (LTAPE,9100)	
9100	FORMAT(50H THE FOUR PTS WRITTEN BY ENRYCH ARE (Y,Z) OR (Z,Y) /	
	163H COORD. OF BODY MERIDIAN LINES, BEFORE OR AFTER TRANSFORMATION,	
	2/59H AT A GIVEN STATION. IF CODE = 3, NO POINTS ARE	
	3 27H INTERPOLATED IN AN INTERVAL /	
	4 26H BUT THE PROGRAM CONTINUES)	
9900	CONTINUE	
	IF(ABS(Z)-EP(5)) 9910,9910,9920	
9910	Z=0.	
9920	IF (RAD-EP(5)) 9930,9930,9940	
9930	RAD=0.	
9940	CONTINUE	
	RETURN	
	END	

08/16/65
 BODY
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

SUBROUTINE BODY
COMMON DATE(2),NTAPE1,NP1,NTAPE2,ND2(3),NREAD,
INWRITE,NBODY,NMING,XMACH,SYM,KACE
COMMON /COM1/ KODEB,KODEW,KODEMU,KODEI,KODEC,XPER,YPER,KOPTB,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPER1
2,NPLANE,NPLN1
COMMON /COM2/ NPLNB,NPLNW,JLEAD,JTRAIL,IMID,NPTS(16),XI(16,90),YI(16
1,90),ZI(16,90),XCEPT(21),XCEPTW(16),YCEPTW(16),ZCEPTW(16
2),CODEBW(16),XPAW(16,21),XCOR(16,21),YCOR(16,21),ZCOR(16,21),XIN
3T(15,20,21),YINT(15,20,21),ZINT(15,20,21),XCEN(15,20),YCEN(15,20),ZCF
4N(15,20),XCON(15,20),YCON(15,20),ZCON(15,20),AREA(15,20),ARAT(15,2
50),THETA(15,20),ALPHA(15,20),CHORD(15,20)
DIMENSION ND3(10855)
EQUIVALENCE (ND3(1),NPLN9)

```

C CONTROL PROGRAM FOR BODY PANELING SUBROUTINES

DATA NAME/6HDEFINE/

DEFINE CONSTANTS

C NBODY IS NUMBER OF BODY PANELS

C KODEB,KODEI ARE SCRATCH TAPE ERROR CODES

C IF KODEB OR KODEI ARE SET = 1 IN INPUTB

C THEN TAPE ERROR ENCOUNTERED

C 10 NBODY=0

KODEB=0

KODEI=0

C INITIALIZE COMMON ARRAYS

DO 15 I=1,10855

ND3(I)=0.

C CALL SUBROUTINES

CALL INPUTB

IF (KODEB) 150,25,150

IF (KODEI) 150,30,150

CALL CRNRB

IF (KODEB) 150,40,80

CALL AREAPI(XCOR,YCOR,ZCOR,AREA,ARAT,NPER1,NPLN1)

CALL CENTRD (XCOR,YCOR,ZCOR,ARAT,XCEN,YCEN,ZCEN,

INPER1,NPLN1)

CALL THETAB

IF (KODEB) 150,50,80

CALL CNTRLB

IF (KODEB) 150,60,80

CALL ALPHAB

IF (KODEB) 150,90,80

WRITE (NWRITE,900)

CALL OUTPTB

IF (KODEB) 150,100,150

100 RETURN

150 READ (NREAD,890) KARD

IF (KARD=NAME) 150,160,150

160 BACKSPACE NREAD

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BODY	EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
	KODEB=-1		*30
	GO TO 100		*31
890	FORMAT (A6)		
900	FORMAT (1H1,9X,13HEPROR MESSAGE/10X,		
	149HPANELLING DATA NOT COMPLETED DUE TO PROGRAM ERROR/10X,		
	238HINCOMPLETE PANELLING DATA TO BE OUTPUT)		
	END		,32

09/14/65
 BODY1
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

C      CALLED BY GEOMD
C      READS A BODY DEFINITION IN THE FORM OF CROSS-SECTIONS AT VARIOUS
C      STATION PLANES, AND THEN COMPUTES BODY MERIDIAN LINES (ALSO CALLED
C      PERCENT LINES) EACH OF WHICH CONSISTS OF 3-DIMENSIONAL POINTS ON THE
C      BODY SURFACE.
C
C      SUBROUTINE BODY1(DAT,L1,L0,B,LSTA,NSTA,LBPL,MBPL,NBPL,NBPL,
C      1,LTHETS,AXIS,TITLE,LGDEF,NU)
C
C      DIMENSION DAT(2),B(1),TITLE(12),NU(3),AXIS(2)
C      DATA MAX,SR/150,5HBODY1/
C      LOGICAL LGDEF(3,4)
C
C      INPUTS ARE DAT,L1,L0,NU(2)
C      INPUT-OUTPUTS ARE B,NU(3)
C      OUTPUTS ARE LSTA,NSTA,LBPL,MBPL,NBPL,LTHETS,AXIS,TITLE,NU(1),LGDEF
C
C      DEFINING STATION ARRAY STARTS IN B(LSTA)
C      NSTA = NO. OF STATIONS
C
C      BODY MERIDIAN LINE ARRAY (WITH HEADER) STARTS IN B(LBPL)
C      MBPL = NO. OF BODY PERCENT LINES (MERIDIAN LINES)
C      NBPL = NO. OF CELLS IN ARRAY
C      A PERCENT LINE OF N POINTS HAS 3*N ELEMENTS
C      X1,Y1,Z1, X2,Y2,Z2, ..... XN,YN,ZN
C      THE FIRST 3*J CELLS OF AN ARRAY B OF J PERCENT LINES FORMS A TABLE OF
C      CONTENTS TO THE REST OF THE ARRAY. ELEMENTS 1,4,7,... OF B ARE LABELS
C      FOR PERCENT LINES 1,2,3,... ELEMENTS 2,5,8,... ARE THE NUMBER OF
C      3-DIMENSIONAL POINTS IN PERCENT LINES 1,2,3,... ELEMENTS 3,6,9,... ARE
C      THE STARTING LOCATIONS IN B OF PERCENT LINES 1,2,3,...
C      FOR EXAMPLE, IF B(7) = 30., B(8) = 12. AND B(9) = 49., THEN THE PERCENT
C      LINE WITH THE LABEL 30. CONTAINS 12 POINTS AND STARTS IN B(49).
C
C      THE STANDARD SET OF THETAS STARTS IN B(LTHETS).
C      THERE ARE MBPL OF THEM
C      AXIS = Y,Z COORD. OF MAIN BODY AXIS
C      TITLE = BODY TITLE
C      LGDEF(1,1) = .TRUE. TO INDICATE BODY DEF. CALLED FOR.
C      LGDEF(2,1) = .TRUE. IF BODY SUCCESSFULLY DEFINED.
C
C      NU IS AN ERROR ARRAY WHICH IS PASSED DOWN TO LOWER LEVEL SUBROUTINES.
C      NU(1), AN OUTPUT, IS ZERO FOR SUCCESS, NON-ZERO FOR FAILURE.
C      NU(2), AN INPUT, MAY BE INTERPRETED AS A TAPE NUMBER ON WHICH TO
C      WRITE AN ERROR MESSAGE, IF GREATER THAN ZERO.
C      NU(3), BOTH AN INPUT AND AN OUTPUT, IS AN ERROR COUNTER AND ERROR MESSAGE
C      LIMITER. SOME LOWER LEVEL SUBROUTINES MAY SUBTRACT 1 FROM NU(3) IF AN
C      ERROR OCCURS AND THEN WRITE AN ERROR MESSAGE IF NU(3) AND NU(2) ARE BOTH
C      GREATER THAN ZERO.
C
C      LGDEF(1,3) = .TRUE.
C      READ(I,100)TITLE
C      100 FORMAT(12A6)

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09/14/65

EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
BODY1		
110	WRITE(LO,110)DAT,TITLE	,5 ,6 ,7
200	FORMAT(16H1BODY DEFINITION 38X 2A6/1H012A6)	
	READ(1,200)BNS,BTHETA,AXIS,CHD	,8 ,9 ,10
	FORMAT(16F10.0)	
	NSTA=BNS	,11
	NTHETA=BTHETA	,12
300	WRITE(LO,300)NSTA,NTHETA,AXIS,CHD	,13 ,14 ,15
	FORMAT(10H0THERE ARE 13,13H STATIONS AND 13,	
	1 15H MERIDIAN LINES/	
	2 59H0THE MAIN BODY AXIS (PARALLEL TO THE X AXIS) IS LOCATED AT	
	3/8X,3HY = F9.4,4X,3HZ = F9.4/	
	4 26H0CHORD-HEIGHT TOLERANCE = F8.4//)	
C	C	
C	C	
	CHECK NSTA,NTHETA	
	IF(NSTA .LT. 2 .OR. NSTA .GT. MAX .OR. NTHETA .LT. 2 .OR.	
	1 NTHETA .GT. MAX)GO TO 8000	,16 ,17 ,18
C	C	,19
	RESERVE STORAGE	,20
	LSTA=IRSERV(NSTA,B,LSTA)	,21
	LTHETS=IRSERV(NTHETA,B,LTHETS)	,22
	LTHETA=IRSERV(NTHETA,B,LTHETA)	,23
	LRHO=IRSERV(NTHETA,B,LRHO)	
	NTHETS=3*NTHETA	
	LPTS=IRSERV(NTHETS,B,LPTS)	
C	C	
	THESE LAST 3 ARRAYS ARE SCRATCH STORAGE FOR BODY1R.	
C	C	
	LEAVE BALANCE OF STORAGE FOR MERIDIAN LINES.	
C	C	
	WE WILL RELEASE EXCESS LATER.	
	MBPL=NTHETA	,24
	NBPL=IPACK(8)	,25
	MU=2	,26
C	C	
	SEE IF ENOUGH ROOM	,27
	IF(NBPL-NTHETS*(NSTA+1))8000,600,600	,28
600	LBPL=IRSERV(NBPL,B,LBPL)	,29
	IF(LBPL)8000,8000,700	
C	C	
	READ STANDARD SET OF THETAS	,30
700	LTH=LTHETS+NTHETA-1	,31
	READ(1,200)(B1),I=LTHETS,LTH)	
C	C	
	READ EACH DEFINING SECTION. FIND X,Y,Z,RHO,THETA FOR EACH PT.	
C	C	
	WRITE DATA FOR EACH SECTION. STORE PTS. IN B(LBPL) IN	
C	C	
	MERIDIAN LINE ORDER.	
	MU=3	,32 ,33 ,34 ,35 ,36
	CALL BODY1R(1,L,NTHETA,NSTA,AXIS,TITLE,DAT,B(LTHETS),	,37
	1 B(LTHETA),B(LRHO),B(LPTS),B(LBPL),B(LSTA),NU)	,38
	IF(NU)8000,900,8000	
C	C	
	PERFORM 3D INTERPOLATION ON EACH MERIDIAN LINE.	
C	C	
	THE ENRICHED MERIDIAN LINES (PRECEDED BY HEADER) WILL BE	
C	C	
	STORED STARTING IN B(LBPL).	
	MAXP=NBPL/3	,39
900	MU=4	,40
	CALL RICHNA(B(LBPL),MAXP,NTHETA,NSTA,B(LTHETS),.001	,41

BODY1		09/14/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	-	INTERNAL FORMULA NUMBER(S)
1	CHD,0,NA,NU)		
C	NA = TOTAL NO OF PTS		
	IF(NU)8000,1000,8000		
	1000 NBPL=3*(NA+NTHETA)		
C			
C	RELEASE UNUSED STORAGE		
	NU=5		
	IF(IRLEAS(B(LBPL),NBPL))8000,2000,8000		
C			
C	DELETE SCRATCH ARRAYS		
	2000 IF(IDLETE(B(LTHETA)))8000,2100,8000		
	2100 IF(IDLETE(B(LRHO)))8000,2200,8000		
	2200 IF(IDLETE(B(LPTS)))8000,3000,8000		
C			
C	WRITE BODY MERIDIAN LINES		
	3000 CALL BODYIM(B(LBPL),NTHETA,AXIS,TITLE,DAT,LO,B(LSTA))		
C			
C	SUCCESS		
	4000 LGDEF(2,3)=.TRUE.		
	GO TO 9000		
C			
C	ERROR. WRITE MESSAGE.		
	8000 I=MERR(NU,NU+1,ML,SR)		
	NU=NU		
C	IF MU = 3 OR 4. RELEASE BULK OF LBPL STORAGE SO WING CAN BE PROCESSED		
	IF(NU .LT. 3 .OR. MU .GT. 4)GO TO 9000		
	I=IRLEAS(B(LBPL),1000)		
C			
	9000 RETURN		
	END		

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650 FORMAT(19H0BODY PERIDIAN LINE 14,14H (CONTINUED))
700 GO TO 800
700 WRITE(LO,750)K
750 FORMAT(19H0BODY MERIDIAN LINE 14)
NUM=0
800 WRITE(LO,850)
850 FORMAT(14X1HX10X1HY10X1HZ12X3HRH07X5HTHETA)
C
C READY TO WRITE PCINTS, COMPUTING RHO-THETA AS WE GO
DO 2000 L=1,NL
NUM=NUM+1
CALL TRAY(XYZ,B(LA),3)
DY=XYZ(2)-AXIS(1)
DZ=XYZ(3)-AXIS(2)
RHO=SQRT(DY*DY+DZ*DZ)
IF(RHO)1100,1100,1200
1100 THETA=0.
1200 GO TO 1300
1200 THETA = ATN1(ABS(DY),DZ)*DEGRAD
C
1300 PNTR=BLANK
C DOES THIS PT. LIE IN A DEFINING STATION PLANE
IF(ABS(XYZ-STA(ISTA))-1.E-4) 140C,1400,1500
C YES. PRINT *
1400 PNTR=STAR
ISTA=ISTA+1
C
1500 WRITE(LO,1550)NUM,XYZ,PNTR,RHO,THETA
1550 FORMAT(14,4X,3F11.4,A3,2F11.4)
LA=LA+3
2000 CONTINUE
C
NELREM=NELREM-3*NL
IF(LB-LDCEND)300C,4000,4000
3000 NEWPCT=-FALSE.
LA=LB+1
GO TO 200
C
4000 CONTINUE
C
RETURN
END

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C      USED BY BODY1 TO READ DEFINING SECTION DATA, PROCESS IT,
C      WRITE SECTION DATA, AND FORM MERIDIAN LINES.
C
C      SUBROUTINE BODYIR(LI,LO,NPT,NSTA,BAXIS,TITLE,DAT,THETS,
C      1 THETA,RHO,PT, BPL,STA,NU)
C
C      DIMENSION BAXIS(2),TITLE(12),DAT(12),THETS(NPT),THETA(NPT)
C      1,RHO(NPT), PT(13,NPT),BPL(3,NSTA,NPT),NU(3),SECAX(2),STA(NSTA)
C
C      LOGICAL NEWPAG,NEWSTA
C
C      INPUTS ARE
C      LI = INPUT TAPE, LO = OUTPUT TAPE
C      NPT = NO. OF POINTS PER SECTION
C      NSTA = NO. OF STATIONS (DEFINING SECTIONS)
C      BAXIS = Y,Z OF BODY AXIS (AXIS PARALLEL TO X-AXIS)
C      TITLE, DAT = DATE
C      THETS = SET OF STANDARD THETA-VALUES (DEGREES)
C
C      SCRATCH ARRAYS ARE THETA, RHO AND PT
C
C      OUTPUTS ARE
C      BPL = XYZ COORD. GF POINTS ON MERIDIAN LINES.
C      STA = ARRAY OF BODY STATIONS
C      NU(1) = 0 IF SUCCESS
C
C      DATA LINPAG /45/
C      CHANGE LINPAG IF 45 LINES/PAGE NOT OK
C      ASSUME 7 LINES HAVE BEEN WRITTEN ON PAGE (TITLE, ETC.)
C
C      MAXLIN=LINPAG-2
C      LINREM=MAXLIN-5
C      NEWPAG=.FALSE.
C
C      DO 2000 K=1,NSTA
C
C      NEWSTA=.TRUE.
C      READ BODY SECTION DATA CARDS, COMPUTE PTS. ON SECTION
C      CALL RGDYIS(LI,RAXIS,NPT,THETS,SECAX,SCODE,THETA,RHO,PT,NU)
C      SECAX = Y,Z COORD. GF SECTION AXIS
C      NU=1 IF SCODE NOT BETWEEN 0. AND 6.
C      NU=2 IF SCODE = 3. (ELLIPSE) AND MAJOR OR MINOR AXIS N.G.
C      IF(NU) 8000,100,8000
C      100 STA(K)=PT
C      LINES=NPT
C      NUM=0
C
C      200 LINREM=LINREM-5
C      IF(LINREM-6) 300,400,400
C      300 NEWPAG=.TRUE.
C      LINREM=MAXLIN
C      GO TO 500
C      400 NEWPAG=.FALSE.

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500 NL=MNO(LINES,LINREM)
   IF(.NOT. NEWPAG) GO TO 600
   WRITE(LO,550)TITLE,CAT
550 FORMAT(1H1 12A6/54X 2A6)
C
600 IF(NEWSTA) GO TO 700
   WRITE(LG,610)PT(1,1),SCODE
610 FORMAT(18H0BODY STATION X = F10.4,13H (CONTINUED)
   1 8X,8HSCODE = F4.0)
   GO TO 800
C
700 WRITE(LO,710)PT(1,1),SCODE
710 FORMAT(18H0BODY STATION X = F10.4,21X,8HSCODE = F4.0)
C
800 WRITE(LO,810)SECAX
810 FORMAT(41H RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = (
   1 F9.4,1H, F9.4, 1H)/13HMERIDIAN NO. 4X,3HRHO 7X
   2 5HTHETA 18X 1HY 10X 1HZ)
C
   DO 900 L=1,NL
   NUM=NUM+1
900 WRITE(LO,910)NUM,RHO(NUM),THETA(NUM),IPT(I,NUM),I=2,3)
910 FORMAT(19,F14.4,F11.4,F21.4,F11.4)
C
   LINES=LINES+NL
   LINREM=LINREM+NL
   I=(LINES)/100,1100,1000
1000 NEWSTA=.FALSE.
   GO TO 200
C
C   STORE SECTION POINTS AS MERIDIAN LINES
1100 DO 1200 J=1,NPT
   DC 1200 I=1,3
1200 BPL(I,K,J)=PT(I,J)
C
2000 CONTINUE
C
8000 RETURN
END

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C      USED BY RCDYIR TO READ BODY SECTION CARDS, COMPUTE PTS. ON SECTION
C
C      SUBROUTINE BODY1S(LI,BAXIS,NPT,THETS,SECAX,SCODE,THETA,RHO,PT,NU)
C
C      DIMENSION BAXIS(2),THETS(NPT),SECAX(2),THETA(NPT),RHO(NPT),PT(3,NP
C      1T),RAD(2),V(2),PTSEC(2),YZ(2)
C
C      INPUTS ARE
C      LI = INPUT TAPE NO.
C      BAXIS = Y,Z OF MAIN BODY AXIS
C      NPT = NO. OF PTS IN SECTION
C      THETS = STANDARD SET OF THETA-VALUES TO USE IF SCODE = 1,2 OR 3
C      OUTPUTS ARE
C      SECAX = Y,Z OF SECTION AXIS
C      SCODE = CODE FOR TYPE OF SECTION
C      THETA, RHO = POLAR COORD. OF PTS ON SECTION (ORIGIN AT SECAX)
C      PT = XYZ COORD. OF PTS ON SECTION
C      NU = 0 IF SUCCESS
C           1 IF SCODE .LT. 0 OR .GT. 6
C           2 IF SCODE = 3 (ELLIPSE) AND A SEMI-AXIS IS = 0.
C
C      DATA DEGRAD/0206712273406/
C
C      READ(LI,100)STA,YZ,SCODE,RAD
C      FORMAT(5F10.0)
C      MU=1
C      CHECK FOR VALID SCODE
C      IF(SCODE .LT. 0 .OR. SCODE .GT. 6.) GO TO 8000
C      ICORE=SCODE
C      DO 210 I=1,2
C      210 SECAX(I)=BAXIS(I)+YZ(I)
C
C      IF ICODE .LE. 0, SECTION SAME AS PREVIOUS EX. FOR STATION
C      IF(ICODE)5000,5000,300
C      IF(.NOT. (ICODE .EQ. 1 .OR. ICODE .EQ. 5))GO TO 400
C      ICODE = 1 OR 5. READ RHO
C      READ(LI,100)(RHO(I),I=1,NPT)
C      IF(ICODE .LT. 4 .OR. ICODE .GT. 5)GO TO 500
C      ICODE = 4 OR 5. READ THETA
C      READ(LI,100)(THETA(I),I=1,NPT)
C      GO TO 1000
C      IF(ICODE .GT. 3)GO TO 1000
C      ICODE = 1,2 OR 3. STORE THETAS IN THETA
C      CALL TRAV(THETA,THETS, NPT)
C
C      THE TABLE BELOW SHOWS WHETHER RHO AND THETA HAVE BEEN FOUND
C      FOR EACH POINT ON THE SECTION
C
C      ICODE RHO THETA
C      0 YES YES
C      1 YES YES
C      2 NO YES
C      3 NO YES
    
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180/PI

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BODY15

EXTERNAL FORMULA NUMBER - SOURCE STATEMENT

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C      4      NO      YES
C      5      YES      YES
C      6      NO      NO
C
C      1000 GO TO (2000,1100,1200,1100,2000,4000),ICODE
C
C      CIRCLE (ICODE=2 OR 4)
C      1100 DO 1110 I=1,NPT
C      1110 RHO(I)=RAD
C      GO TO 2000
C
C      ELLIPSE (ICODE=3)
C      1200 DO 1400 I=1,NPT
C      THET=THETA(I)/DEGRAD
C      CALL ELLIPR(RAD,RAD(2),SIN(THET),COS(THET),RHO(I),X,Y,NU)
C      MU=2
C      IF(NU)8000,1300,8000
C      1300 PT(2,I)=X+SECAX(1)
C      1400 PT(3,I)=Y+SECAX(2)
C      CONTINUE
C      GO TO 5000
C
C      ICODE = 1,2,4 OR 5.  FIND Y,Z FOR EACH PT.
C      2000 DO 2010 I=1,NPT
C      THET=THETA(I)/DEGRAD
C      PT(2,I)=RHO(I)*SIN(THET)+SECAX(1)
C      2010 PT(3,I)=RHO(I)*COS(THET)+SECAX(2)
C      GO TO 5000
C
C      Y,Z GIVEN (ICODE=6).  READ Y,Z AND FIND RHO,THETA
C      4000 READ(I,100)((PT(I,J),I=2,3),J=1,NPT)
C
C      DO 4400 I=1,NPT
C      PTSEC(1)=PT(2,I)
C      PTSEC(2)=PT(3,I)
C      RHO(1)=UVECN(SECAX,PTSEC,V,0,2)
C      IF(RHO(1))4200,4200,4300
C      4200 THETA(1)=THETSI(1)
C      GO TO 4400
C      4300 THETA(1)=ATN1(ABS(V),V(2))*DEGRAD
C      4400 CONTINUE
C
C      WE NOW HAVE RHO,THETA,Y,Z FOR EACH PT.  STORE STA AS X.
C      5000 DO 5010 I=1,NPT
C      5010 PT(1,I)=STA
C      MU=0
C
C      8000 NU=MU
C      RETURN
C      END

```

```

SUBROUTINE BSCALE(B,NR,XEND,NU)
  DIMENSION B(1)
  C
  C SCALF X-VALUES OF BODY MERIDIAN LINES SUCH THAT
  C EACH LINE STARTS AT X=0, AND ENDS WITH X=XEND.
  C
  C  $X = (X - XF) * XEND / (XL - XF)$ 
  C WHERE XF = X OF 1ST POINT OF A LINE, XL = X OF LAST POINT
  C
  C J=R(3)
  C 1ST PT OF 1ST LINE STARTS IN B(J)
  C
  C DO 1000 K=1,NB
  C
  C   XF=R(J)
  C   NP=R(3*K-1)
  C   L=J+3*(NP-1)
  C   XL=B(L)
  C   DEL=XL-XF
  C   IF(DEL)200,100,200
  C
  C   100 NU=K
  C   GO TO 2000
  C
  C   200 DO 300 I=1,NP
  C     B(J)=((R(I)-XF)/DEL)*XEND
  C     J=J+3
  C
  C   300 CONTINUE
  C   NU=0
  C   2000 RETURN
  C   END

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05/22/67

PTHICK - EFN SOURCE STATEMENT - IFN(S) -

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SURROUTINE BTHICK(NBODYS,NBODY,NROWB,XB,R,XC,ALPHA,THETA)
C   COMPUTES BODY THICKNESS SLOPES FOR GIVEN BODY NBDII DISTRIBUTION
  DIMENSION XB(1),R(1),XC(1),ALPHA(1),THETA(1)
  NB=NBODYS-1
  NCOLB=NBODY/NROWB
  DO 100 I=1,NB
    ALPHA(I+1)=(R(I+1)-R(I))/(XB(I+1)-XB(I))
    ALPHA(1)=ALPHA(2)
  DO 250 J=1,NROWB
    DO 150 I=1,NB
      IF (XB(I)-XC(J)) 150,200,200
    150 CONTINUE
    I=NBODYS
    200 THETA(J)=ALPHA(I-1)+(XC(J)-XB(I-1))/(XB(I)-XB(I-1))*(ALPHA(I)-
      ALPHA(I-1))
    250 CONTINUE
  DO 400 J=1,NROWB
    DO 400 I=2,NCOLB
      IJ=(I-1)*NROWB+J
      THETA(IJ)=THETA(J)
    400 CONTINUE
  RETURN
END

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05/22/67

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CAMBER      - EFN      SOURCE STATEMENT - IFN(S) -
SUBROUTINE CAMBER(NCOLM,NROWM,CHORD,ALPHAM,CSHAPE,CHORDL)
  DIMENSION CHORD(1),ALPHAM(1),CSHAPE(1),CHORDL(1)
C  COMPUTES SURFACE SHAPE, GIVEN SURFACE SLOPES
      DO 305 J=1,NCOLM
        CHORDL(J)=0.
      DO 392 I=1,NROWM
        K=(J-1)*NROWM+I
        CHORDL(J)=CHORDL(J)+CHORD(K)
      DO 395 I=1,NROWM
        SUM=0.
        IV=1
      DO 394 IJ=1,IV
        K=(J-1)*NROWM+IJ
        SUM=SUM+ALPHAM(K)*CHORD(K)/CHORDL(J)
      394 CSHAPE(K)=SUM
      395 CONTINUE
      RETURN
      END

```

CAMBW
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

SUBROUTINE CAMBW (NW,NTAPEX,A,CLW,ALPHAW)
DIMENSION A(1),ALPHAW(1),CLW(1)

C FOR WING ONLY CASE, COMPUTES NORMAL VELOCITY COMPONENTS ON WING

DO 100 J=1,NW
ALPHAW(J)=0.0

100 CONTINUE

DO 200 J=1,NW
READ (NTAPEX) (A(I),I=1,NW)

DO 200 I=1,NW
ALPHAW(I)=ALPHAW(I)+A(I)*CLW(J)
200 CONTINUE

RETURN
END

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CAMBWB 08/16/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

SUBROUTINE CAMBWB (NR,NW,NTAPEX,NTAPEY,A,CLW,ALPHAB,ALPHAW)

C FOR WING-BODY CASES, COMPUTES NORMAL VELOCITY COMPONENTS ON WING

DIMENSION A(1),ALPHAW(1),ALPHAB(1),CLW(1)

DO 100 J=1,NW
ALPHAW(J)=0.

100 CONTINUE

DO 200 J=1,NW
READ (NTAPEX) (A(I),I=1,NW)

DO 200 I=1,NW
ALPHAW(I)=ALPHAW(I)+A(I)*CLW(J)

200 CONTINUE

DO 300 J=1,NB
READ (NTAPEY) (A(I),I=1,NW)

DO 300 I=1,NW
ALPHAW(I)=ALPHAW(I)+A(I)*ALPHAB(J)

300 CONTINUE

RETURN
END

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SUBROUTINE CEGAR(N,P,AREA,CGRV)

FINDS AREA AND CENTROID OF AREA OF A POLYGON

DIMENSION P(2,1),CGRV(2)

DOUBLE PRECISION A,C(2)

A=0.00

CG(1)=A

CG(2)=A

P(1,N+1)=P(1,1)

P(2,N+1)=P(2,1)

DO 100 J=1,2

K=(J+1)/J

DO 80 I=1,N

80 CG(J)=CG(J)+P(J,I+1)**2+P(J,I)**2+P(J,I+1)*P(J,I))*(P(K,I+1)-P(K,I))

11)

100 CONTINUE

DO 120 L=1,N

120 A=A+(P(2,L+1)+P(2,L))*(P(1,L+1)-P(1,L))

IF (A) 160,140,160

140 CG(1)=0.

CG(2)=0.

GO TO 180

160 CG(1)=CG(1)/(-A*3.)

CG(2)=CG(2)/(-A*3.)

A=ABS (A)/2.

180 CONTINUE

AREA=A

CGRV(1)=CG(1)

CGRV(2)=CG(2)

RETURN

END

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SUBROUTINE CENTRE (X,Y,Z,R,XC,YC,ZC,NC,NR)
DIMENSION X(16,16),Y(16,16),Z(16,16),R(15,15),XC(15,15),
YC(15,15),ZC(15,15)

C SUBROUTINE TO CALCULATE BODY AND WING PANEL
C CENTROID COORDINATES

C DEFINE FUNCTION TO BE USED TO CALCULATE

C PANEL CENTROID COORDINATE

CENT(A-.A2,A3,P1,P2)=A1+P1*(A2+P2*(A3-A2)-A1)

C DEFINE CONSTANTS

P1=2./3.

P2=.5

C CALCULATE PANEL CENTROID COORDINATES

50 DO 60 I=1,NC

DO 60 J=1,NR

XC1=CENT(X(I,J+1),X(I,J),X(I+1,J+1),P1,P2)

YC1=CENT(Y(I,J+1),Y(I,J),Y(I+1,J+1),P1,P2)

ZC1=CENT(Z(I,J+1),Z(I,J),Z(I+1,J+1),P1,P2)

XC2=CENT(X(I+1,J),X(I,J),X(I+1,J+1),P1,P2)

YC2=CENT(Y(I+1,J),Y(I,J),Y(I+1,J+1),P1,P2)

ZC2=CENT(Z(I+1,J),Z(I,J),Z(I+1,J+1),P1,P2)

XC(I,J)=XC2+R(I,J)*(XC1-XC2)

YC(I,J)=YC2+R(I,J)*(YC1-YC2)

ZC(I,J)=ZC2+R(I,J)*(ZC1-ZC2)

60 RETURN

100 END

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08/09/65

SUBROUTINE CHECK (X,N,K,L,N6)
DIMENSION X(1)

SUBROUTINE TO CHECK IF SEQUENCE IS
MONOTONIC INCREASING OR DECREASING

10 IF (K.LT.-2.OR.K.EQ.0.OR.K.GT.2) GO TO 80

K1=(K+IABS(K))/(2*K)

K2=K1-1

N1=N-1

30 DO 50 I=1,N1

L1=K1*(I+1)+K2*(N-I)

L2=L1-K1+K2

IF (IABS(K)-1) 80,40,50

40 IF (X(L1)-X(L2)) 90,60,60

50 IF (X(L1)-X(L2)) 90,90,60

60 CONTINUE

L=0

GO TO 100

80 WRITE (N6,900)

WRITE (N6,910) K

L=1

GO TO 100

90 WRITE (N6,900)

WRITE (N6,920) (X(I),I=1,N)

L=1

GO TO 100

100 RETURN

900 FORMAT (1H,9X,32HERROR MESSAGE - SUBROUTINE CHECK)

910 FORMAT (1H,9X,28HINVALID VALUE FOR K K = ,I3)

920 FORMAT (1H,9X,25HSEQUENCE IS NOT MONOTONIC//

1(F20.5))

END

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CHORDM 09/14/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

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SUBROUTINE CHORDM
COMMON DATE(2),NTAPE1,ND1,NTAPE2,ND2(3),NREAD,
1NWRITE,NBODY,NWING,XMACH,SYM,KACE
COMMON /COM1/ KOLEB,KODEM,KODEMU,KODEI,KODEC,XPER,YPER,KOPTB,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPERI
2,NPLANE,NPLNI
COMMON /COM2/IJ,NPTS(16),X(90,16),Y(90,16),Z(90,16),XPNT,VALUE(5),
1XCEPT(16),SLOPE,KPANEL(2,15),XCOR(16,16),YCOR(16,16),ZCOR(16,16),X
2INT(2,15),YINT(2,15),ZINT(2,15),XCEN(15,15),YGEN(15,15),ZGEN(15,15
3),XCON(15,15),YCON(15,15),ZCON(15,15),AREA(15,15),ARAT(15,15),THET
4A(15,15),ALPHA(15,15),CHORD(15,15),XFOIL(16,25,2),ZFOIL(16,25,2),X
5NUM(16,2),XTAB1(25),XTAB2(25),XTAB2(25),ZTAB2(25)
DIMENSION C(4),P(3,50),Q(3,5),LOC(5)

```

C SUBROUTINE TO CALCULATE WING PANEL STREAMWISE

C CHORD LENGTHS

C DEFINE CONSTANTS

```

E=.000001
F=.001
M=3
MAX=2
N=4
C(1)=0.
C(2)=-1.
C(3)=0.

```

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C CALCULATE PANEL CHORD LENGTHS

```

DO 70 I=1,NPLNI
DO 60 J=1,NPERI

```

18
19

C SETUP ARRAY

```

P(1,1)=XCOR(I,J)
P(2,1)=YCOR(I,J)
P(3,1)=ZCOR(I,J)
P(1,2)=XCOR(I+1,J)
P(2,2)=YCOR(I+1,J)
P(3,2)=ZCOR(I+1,J)
P(1,3)=XCOR(I+1,J+1)
P(2,3)=YCOR(I+1,J+1)
P(3,3)=ZCOR(I+1,J+1)
P(1,4)=XCOR(I,J+1)
P(2,4)=YCOR(I,J+1)
P(3,4)=ZCOR(I,J+1)
C(4)=YCON(I,J)

```

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22

C ATTEMPT INTERSECTION

```

CALL POLXN (C,P,M,N,F,MAX,Q,LOC,NINT)
IF (NINT-2) 80,6C,90
CHORD(I,J)=ABS(Q(1,1)-Q(1,2))
70 CONTINUE
GO TO 100

```

23
24
25
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29

CHORDW		09/14/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)	
C	ERROR MESSAGES		
80	WRITE (NWRITE,90C)		,30
	GO TO 95		,31
90	WRITE (NWRITE,91C)		,32
	GO TO 95		,33
95	KODEW=1		,34
	GO TO 100		,35
100	RETURN		,36
900	FORMAT (1H1,9X,32HERROR MESSAGE - SUBROUTINE CHORD/10X, 124HSUBROUTINE POLYN FAILURE/10X, 133HPANEL CHORD LENGTH NOT CALCULATED/10X, 237HFEWER THAN TWO INTERSECTIONS COMPUTED)		,37
910	FORMAT (1H1,9X,32HERROR MESSAGE - SUBROUTINE CHORD/10X, 124HSUBROUTINE POLYN FAILURE/10X, 133HPANEL CHORD LENGTH NOT CALCULATED/10X, 236HMORE THAN TWO INTERSECTIONS COMPUTED)		,38
	END		,39
			,40

CLEAR
7094 RELMOD ASSEMBLY.

10/04/65

\$IBLDR CLEAR

CLEA0000

ASSEMBLED TEXT.

\$TEXT CLEAR

CLEA0001

ASSEMBLED 21 SEP 64

*CLEAR MICHAEL SYNGE 6-9247
* TO CLEAR ANY NUMBER OF STORAGE BUFFERS
*
* CALLING SEQUENCE -
*
* CALL CLEAR (BUFA,BUFB,.....)
*
* ENTRY CLEAR
*

BINARY CARD ID. CLEA0002

00000	0634 00 4 00004	10001	CLEAR SXA	EXIT,4
00001	0500 00 4 00003	10000	CLA	3,4
00002	4320 00 0 00021	10001	ANA	=0777777700000
00003	0100 00 0 00006	10001	TZE	NEXT
00004	0774 00 4 00000	10000	AXT	0,4
00005	0020 00 4 00001	10000	TRA	1,4
00006	0500 60 4 00003	10000	NEXT	3,4
00007	0621 00 0 00020	10001	STA	LENG
00010	0500 00 4 00003	10000	CLA	3,4
00011	0621 00 0 00016	10001	STA	BUF
00012	0634 00 4 00014	10001	SXA	XR,4
00013	0C74 00 4 03000	10011	TSX	\$INIBFR,4
00014	0774 00 4 00000	10000	XR	**4
00015	1 7777 4 02001	10011	AXT	CLEAR+1,4,-1
00016	0000 00 0 00000	10000	TXI	**
00017	0000 00 0 00020	10001	BUF	LENG
00020	0 00000 0 00000	10000	HTR	
00021	777777700000	10000	HTR	
	00000	01111	*LORG	
			END	

CONTROL DICTIONARY

\$CDICT CLEAR

CLEA0003

BINARY CARD ID. CLEA0004

000022000000	PREFACE	START=0,LENGTH=18,TYPE=7094,CMPLEX=5
000004000005	DECK	LOC=0,LENGTH=18
234325215160	CLEAR	LOC=0,LENGTH=0
000022000000	REAL	
234325215160	INIBFR	SECT. 3
000000000000	VIRTUAL	
314531222651		
000000000000		

SUKEND CLEAR

CLEA0005

NO MESSAGES FOR THIS ASSEMBLY

SYMBOL REFERENCE DATA

REFERENCES TO DEFINED SYMBOLS.

CLASS	SYMBOL	VALUE	REFERENCES
	BUF	00016	11
	CLEAR	00000	15
	EXIT	00004	0
	LENG	00020	7,17
	NEXT	00006	3
LCTR	BLCTR		
QUAL	UNQS		13
LCTR	//		
	xr	00014	12

REFERENCES TO VIRTUAL SYMBOLS.

INIBFR	3	13
--------	---	----

CLOCK
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - 08/16/55
 INTERNAL FORMULA NUMBER(S)

C SUBROUTINE CLOK(TIME,DATE)
 C DUMMY ROUTINE TO RETURN TIME, DATE AS BLANKS.
 C IT MAY BE REPLACED BY A ROUTINE WHICH RETURNS TWO
 C HOLLERITH WORDS CONTAINING THE TIME AND DATE.
 DATA T/1H /
 TIME = T
 DATE = T
 RETURN
 END

*1
 *2
 *3
 *4

CNTRL9 08/14/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

SUBROUTINE CNTRLB
COMMON DATE(2),NTAPE1,RD1,NTAPE2,ND2(3),VREAD,
INRITE,NBODY,NWING,XMACH,SYM,KACE
COMMON /COM1/ KODEB,KODEW,KODEU,KODEI,KODEC,YPER,YPER,KOPTA,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPERI
2,NPLANE,NPLNI
COMMON /COM2/ NPLNB,NPLNW,JLEAD,JTRAIL,IMIQ,NPTS(16),X(16,20),Y(16,
1,20),Z(16,20),XCEPT(21),XCEPTB(21),XCEPTW(16),YCEPTW(16),ZCEPTW(16
2),CODEBW(16),XPANEL(15,20),XCOR(16,21),YCOR(16,21),ZCOR(16,21),XIN
3T(15,20,2),YINT(15,20,2),ZINT(15,20,2),XCEN(15,20),YCEX(15,20),ZCE
4N(15,20),XCON(15,20),YCON(15,20),ZCON(15,20),AREA(15,20),ARAT(15,2
50),THETA(15,20),ALPHA(15,20),CHORD(15,20)
DIMENSION C(4),P(3,10),O(3,5),LOC(5)

```

C SUBROUTINE TO CALCULATE BODY PANEL
C CONTROL POINT COORDINATES AND PANEL CHORD LENGTHS

C DEFINE FUNCTIONS TO BE USED IN CALCULATIONS
C XLENG CALCULATE LENGTH OF STREAMWISE CHORD
C THROUGH PANEL CENTROID
C XLENG(X1,X2,Y1,Y2,Z1,Z2)=SORT((X2-X1)**2+(Y2-Y1)**2+
1(Z2-Z1)**2)

C DEFINE CONSTANTS
C 10 M=3
MAX=2
N4=4
N5=5
E=0.001
F=0.000001

.1
.2
.3
.4
5

C CALCULATE PANEL CONTROL POINT COORDINATES
C AND PANEL CHORD LENGTHS

50 DO 90 I=1,NPER1
DO 80 J=1,NPLNI
IF (KODEC) 153,53,57
VTEMP=YCEN(I,J)
ZTEMP=ZCEN(I,J)
GO TO 60
VTEMP=YCOR(I,J)+YPER*(YCOR(I+1,J+1)-YCOR(I,J))
ZTEMP=ZCOR(I,J)+YPER*(ZCOR(I+1,J+1)-ZCOR(I,J))

.6
.7
.8
.9
.10
.11
.12
13

C SETUP ARRAY

60 P(1,1)=XCOR(1,J+1)
P(2,1)=YCOR(1,J+1)
P(3,1)=ZCOR(1,J+1)
P(1,2)=XCOR(1,J)
P(2,2)=YCOR(1,J)
P(3,2)=ZCOR(1,J)
P(1,3)=XCOR(1+1,J)
P(2,3)=YCOR(1+1,J)
P(3,3)=ZCOR(1+1,J)
P(1,4)=XCOR(1+1,J+1)

.14
.15
.16
.17
.18
.19
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.21
.22
23
.24

CNTRL9 08/16/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

63      P(2,4)=YCOR(I+1,J+1)
        P(3,4)=ZCOR(I+1,J+1)
        P(1,5)=XCOR(I,J+1)
        P(2,5)=YCOR(I,J+1)
        P(3,5)=ZCOR(I,J+1)
        IF (ABS(ZCOR(I+1,J+1)-ZCOR(I,J+1))-F) 63,63,67
        C(1)=0.
        C(2)=-1.
        C(3)=0.
        C(4)=YTEMP
        GO TO 70
67      C(1)=0.
        C(2)=-1*(YCOR(I+1,J+1)-YCOR(I,J+1))/(ZCOR(I+1,J+1)-ZCOR(I,J+1))
        C(3)=-1.
        C(4)=ZTEMP-C(2)*YTEMP
        C
70      C
        CALL POLXN (C,P,M,N5,F,MAX,Q,LOC,NINT)
        IF (NINT-2) 143,73,145
73      CHORD(I,J)=XLEN*(Q(1,1),Q(1,2),Q(2,1),Q(2,2),Q(3,1),Q(3,2))
        IF (Q(1,1)-Q(1,2)) 75,150,77
75      XCON(I,J)=Q(1,1)+XPER*(Q(1,2)-Q(1,1))
        YCON(I,J)=Q(2,1)+XPER*(Q(2,2)-Q(2,1))
        ZCON(I,J)=Q(3,1)+XPER*(Q(3,2)-Q(3,1))
        GO TO 80
77      XCON(I,J)=Q(1,2)+XPER*(Q(1,1)-Q(1,2))
        YCON(I,J)=Q(2,2)+XPER*(Q(2,1)-Q(2,2))
        ZCON(I,J)=Q(3,2)+XPER*(Q(3,1)-Q(3,2))
80      CONTINUE
90      CONTINUE
        GO TO 150
C
143      ERRORS MESSAGES
        WRITE (NWRITE,900)
        GO TO 147
145      WRITE (NWRITE,910)
        GO TO 147
147      KODEB=1
        GO TO 150
150      RETURN
900      FORMAT (1H1,9X,33HERROR MESSAGE - SUBROUTINE CNTRLB/10X,
134HPANEL CONTROL POINT NOT CALCULATED/10X,
124HSUBROUTINE POLXN FAILURE/10X,
237HFEWER THAN TWO INTERSECTIONS COMPUTED)
910      FORMAT (1H1,9X,33HERROR MESSAGE - SUBROUTINE CNTRL9/10X,
134HPANEL CONTROL POINT NOT CALCULATED/10X,
124HSUBROUTINE POLXN FAILURE/10X,
236HMORE THAN TWO INTERSECTIONS COMPUTED)
        END

```


09/14/65

```

DO 90 J=1,NPERI
IF (KODEC) 150,72,77
YCON(I,J)=YCEN(I,J)
YPER=YCON(I,J)-YCOR(I,J)/(YCOR(I+1,J)-YCOR(I,J))
GO TO 80
73 YCON(I,J)=YCOR(I,J)+YPER*(YCOR(I+1,J)-YCOR(I,J))
XLEAD=XCON(I,J)+YPER*(XCON(I+1,J)-XCON(I,J))
80 XTRAIL=XCON(I,J+1)+YPER*(XCON(I+1,J+1)-XCON(I,J+1))
ZLEAD=ZCON(I,J)+YPER*(ZCON(I+1,J)-ZCON(I,J))
ZTRAIL=ZCON(I,J+1)+YPER*(ZCON(I+1,J+1)-ZCON(I,J+1))
XCON(I,J)=XLEAD+XPER*(XTRAIL-XLEAD)
90 ZCON(I,J)=ZLEAD+XPER*(ZTRAIL-ZLEAD)
IF (KEND-NPLN1) 100,150,150
100 I=NPLN1
DO 135 J=1,NPERI
IF (KODEC) 150,103,107
103 YCON(I,J)=YCEN(I,J)
GO TO 110
107 YCON(I,J)=YCON(I,J)+YPER*(AMINI(YCOR(I+1,J),
YCON(I+1,J+1))-YCOR(I,J))
110 IF (YCON(I,J)-YCOR(I+1,J)) 113,113,115
113 YPERL=(YCON(I,J)-YCOR(I,J))/(YCOR(I+1,J)-YCOR(I,J))
XLEAD=XCON(I,J)+YPERL*(XCON(I+1,J)-XCON(I,J))
ZLEAD=ZCON(I,J)+YPERL*(ZCON(I+1,J)-ZCON(I,J))
GO TO 120
115 IF (YCON(I,J)-YCOR(I+1,J)) 117,117,140
117 YPERL=(YCON(I,J)-YCOR(I+1,J))/(YCOR(I+1,J+1)-YCOR(I+1,J))
XLEAD=XCON(I+1,J)+YPERL*(XCON(I+1,J+1)-XCON(I+1,J))
ZLEAD=ZCON(I+1,J)+YPERL*(ZCON(I+1,J+1)-ZCON(I+1,J))
120 IF (YCON(I,J)-YCOR(I+1,J+1)) 123,123,125
123 YPERT=(YCON(I,J)-YCOR(I,J+1))/(YCOR(I+1,J+1)-YCOR(I,J+1))
XTRAIL=XCON(I,J+1)+YPERT*(XCON(I+1,J+1)-XCON(I,J+1))
ZTRAIL=ZCON(I,J+1)+YPERT*(ZCON(I+1,J+1)-ZCON(I,J+1))
GO TO 130
125 IF (YCON(I,J)-YCOR(I+1,J)) 127,127,140
127 YPERT=(YCON(I,J)-YCOR(I+1,J+1))/(YCOR(I+1,J)-YCOR(I+1,J+1))
XTRAIL=XCON(I+1,J+1)+YPERT*(XCON(I+1,J)-XCON(I+1,J+1))
ZTRAIL=ZCON(I+1,J+1)+YPERT*(ZCON(I+1,J)-ZCON(I+1,J+1))
130 XCON(I,J)=XLEAD+XPER*(XTRAIL-XLEAD)
135 ZCON(I,J)=ZLEAD+XPER*(ZTRAIL-ZLEAD)
GO TO 150
140 WRITE (NWRITE,90C)
GO TO 150
150 RETURN
900 FORMAT (1H1,9X,3HEXOR MESSAGE - SUBROUTINE CNTRLW/10X,
157HPANEL CONTROL POINT Y-COORDINATE NOT CORRECTLY CALCULATED)
END

```

05/22/67

COEFS - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE COEFS(XB,R,FD,THETAB,CP88,NFT,NLT,NTHETA,XP,ZP,C,IRROR)

C

SUBROUTINE TO COMPUTE CX (ENTRY POINT SCX), CM

(ENTRY POINT SCM) AND CM (ENTRY POINT SCM)

C

DIMENSION XB(1),R(1),FD(1),THETAB(1),CP88(10,1)

DIMENSION Y(55),YY(10),S(55),T(10)

ENTRY SCX(XB,R,FD,THETAB,CP88,NFT,NLT,NTHETA,XP,ZP,C,IRROR)

DO 100 I= NFT,NLT

100 S(I)=FD(I)

DO 200 I=1,NTHETA

200 T(I)=0.

CC= 1.

GO TO 1000

ENTRY SCM(XB,R,FD,THETAB,CP88,NFT,NLT,NTHETA,XP,ZP,C,IRROR)

DO 400 I= NFT,NLT

400 S(I)=1.

DO 500 I=1,NTHETA

500 T(I)= THETAB(I)

CC=-1.

GO TO 1000

ENTRY SCM(XB,R,FD,THETAB,CP88,NFT,NLT,NTHETA,XP,ZP,C,IRROR)

DO 700 I= NFT,NLT

700 S(I)=XB(I)-XP

DO 800 I=1,NTHETA

800 T(I)= THETAB(I)

CC=-1.

1000 DO 1100 I= NFT,NLT

DO 1050 J=1,NTHETA

1050 YY(J)=CC*CP88(J,I)*COS(T(I,J))

CALL SIMUN3(THETAB,YY,NTHETA,A,IRR)

IF (IRR .NE. 0) GO TO 2000

1100 Y(I)=R(I)*S(I)*A

NCT=NLT-NFT+1

CALL SIMUN3(XB,Y,NCT ,A,IRR)

IF (IRR .NE. 0) GO TO 2000

C=A

IRROR=0

1500 RETURN

2000 IRROR=IRR

GO TO 1500

END

60
64

76

05/22/67

COMCU - EFN SOURCE STATEMENT - IFN(S) -

```

C      SUBROUTINE COMCU(DA,DB,S,X,Y,L,M,N,ND,NDA,NDB)
C      (FOR CDC 6600, 7/10/66)
C      DIMENSION C(400), D(400), E(400), S(1), X(1), Y(1)
C      K=N-1
C      KUE=0
C      IF (N-2) 5,10,30
C      5 M=-1
C      GO TO 260
C      10 IF (NDA-1) 25,15,25
C      15 IF (NDB-1) 25,20,25
C      20 S(1)=DA
C      S(2)=DB
C      M=0
C      GO TO 260
C      25 KUE=1
C      30 M=0
C      40 E(1)=0.0
C      C(N)=0.0
C      IF (NDA-1) 50,50,60
C      50 D=1.0
C      C=0.0
C      S=DA
C      GO TO 70
C      60 D=4.0
C      C=2.0
C      S=6.0*(Y(2)-Y(1))/(X(2)-X(1))-DA*(X(2)-X(1))
C      70 IF (KUE) 85,75,85
C      75 DO 80 I=2,K
C      U = X(I)-X(I-1)
C      V = X(I+1)-X(I)
C      C(I)=U
C      D(I)=2.0*(U+V)
C      E(I)=V
C      80 S(I)=3.0/(U+V) * ( U*S*(Y(I+1)-Y(I)) + V*S*(Y(I)-Y(I-1)) )
C      85 IF (NDB-1) 90,90,100
C      90 E(N)=0.0
C      D(N)=1.0
C      S(N)=DB
C      GO TO 110
C      100 E(N)=2.0
C      D(N)=4.0
C      S(N)=6.0*(Y(N)-Y(N-1))/(X(N)-X(N-1))+DB*(X(N)-X(N-1))
C      110 C=C/D
C      S=S/D
C      DO 120 I=2,M
C      F = D(I) - C(I-1)*E(I)
C      C(I)=C(I)/F
C      120 S(I) = ( S(I)-S(I-1)*E(I) )/F
C      DO 130 J=1,K
C      I=N-J
C      130 S(I) = S(I) - S(I+1)*C(I)
C      260 RETURN
C      END

```

05/31/67

COMP - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE COMP(GP,VLS,IC)
DIMENSION GP(3,1),VLS(4,1)
DATA ISTR/0/

DO 10 I=1,IC

10 CALL LACKEY(ISTR,
\$1),VLS(3,1),VLS(4,1))
RETURN
END

GP(1,1),GP(2,1),GP(3,1),VLS(1,1),VLS(2,

13

06/22/67

CP - EFN SOURCE STATEMENT - IFN(S) -

```

SUBROUTINE CP(NP,XNACH,CPCALC,U,V,W,CPP)
C  SUBROUTINE TO COMPUTE SECOND ORDER OR EXACT
C  ISENTROPIC COEFFICIENT OF PRESSURE
    DIMENSION U(1),V(1),W(1),CPP(1)
    XN2=XNACH*XNACH
    IF (CPCALC-1.) 200,200,300
C  SECOND ORDER CP CALCULATIONS
200 CONTINUE
    DO 250 J=1,NP
        CPP(J)=-2.*U(J)+XN2*U(J)*U(J)
250 CONTINUE
    GO TO 999
C  EXACT ISENTROPIC CP CALCULATIONS
300 CONTINUE
    DO 350 J=1,NP
        UVW2=U(J)*U(J)+V(J)*V(J)+W(J)*W(J)
        CPP(J)=1.42857/XN2*(1.-.2*XN2*(2.*U(J)+UVW2))*3.5 -1.)
350 CONTINUE
999 RETURN
    END

```



```

SURROUTINE CRNRB
COMMON DATE(2),NTAPE1,ND1,NTAPE2,ND2(3),NREAD,
INWRITE,NBODY,NWING,XMACH,SYM,KACE
COMMON /COM1/ KODEB,KODEM,KODEG,KODEI,KODEC,XPER,YPER,KOPTB,KOPTM
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPERI
2,NPLANE,NPLNI
COMMON /COM2/ NPLNB,NPLNW,JLEAD,JTRAIL,IMID,NPTS(16),XI(16,90),YI(16
1,90),ZI(16,90),XCEPT(21),XCEPTB(21),XCEPTW(16),YCEPTW(16),ZCEPTW(16
2),CODEFW(16),KPADEL(15,20),XCOR(16,21),YCOR(15,21),ZCOR(16,21),XIN
3T(15,20,21),YINT(15,20,21),ZINT(15,20,21),XCEN(15,20),YCE(15,20),ZCE
4N(15,20),XCON(15,20),YCON(15,20),ZCON(15,20),AREA(15,20),ARAT(15,2
50),THETA(15,20),ALPHA(15,20),CHORD(15,20)
DIMENSION C(4),D(4),P(3,50),R(3,50),O(3,5),LOC(3)
DIMENSION ISAVE(21)

```

C SUBROUTINE TO CALCULATE BODY PANEL CORNER
C POINT COORDINATES

C DEFINE CONSTANTS
EPS=0.04
E=0.001
F=0.0001
M=3
MAX=1
N=2

1
2
3
4
5

C CALCULATE X-, Y- AND Z-COORDINATES OF PANEL
C CORNER POINTS PREVIOUSLY DETERMINED BODY
C PERCENT LINES ARE INTERSECTED WITH SERIES
C OF PLANES PARALLEL TO X-Z PLANE

6
7
8
9
10
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12

```

3 DO 10 I=1,NPER
  NPOINT=NPTS(I)
  DO 5 J=1,NPOINT
    P(1,J)=X(I,J)
    P(2,J)=Y(I,J)
    P(3,J)=Z(I,J)
  DO 10 J=1,NPLANE
    C(1)=1.
    C(2)=0.
    C(3)=0.
    C(4)=-XCEPT(J)
    CALL POLXN (C,P,M,NPOINT,E,MAX,Q,LOC,NINT)
    IF (NINT) 250,260,7
  7 XCOR(I,J)=Q(1,1)
    YCOR(I,J)=Q(2,1)
    ZCOR(I,J)=Q(3,1)
  10

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C DEFINE KSTART KSTART=1 INDICATES BODY HAS
C NO MORE CLOSING
13 KSTART=1

27 28 29

C DEFINE KEND KEND=NPLNI INDICATES BODY HAS

C	NO AFT CLOSING KEND=NPLN1		,30
C	REDEFINE X-, Y- AND Z-COORDINATES OF BODY PANEL		
C	CORNER POINTS FOR BODY PANELS IN BODY-WING		
C	INTERSECTION REGION		,31
	27 IF (KOPTA) 300,30,110		,32
	30 IF (NPLNW) 300,110,35		,33
	35 IF (KINT) 300,300,40		,34
	40 NPLNW=NPLNW-1		
C	CHECK IF BODY-WING INTERSECTION POINT IS		
C	COINCIDENT (WITHIN A TOLERANCE) WITH A		
C	BODY MERIDIAN LINE		,35
	DO 50 J=1,NPLNW		,36
	DO 47 I=1,NPER		,38
	K=JLEAD+J		,40
	IF (ZCOR(I,K)-(ZCEPTW(J)+EPS/2.)) 43,43,47		,41
	ISAVE(J)=I-1		,42
43	GO TO 50		,43
	CONTINUE		,44
47	GO TO 270		,45
	CONTINUE		,46
50	DO 55 J=1,NPLNW1		,47
	IF (ISAVE(J+1)-ISAVE(J)) 280,55,280		,48
	CONTINUE		,49
55	IMID=ISAVE(1)		,50
	CONTINUE		,51
	CONTINUE		,52
C	CHECK IF BODY-WING INTERSECTION LINE IS		
C	COINCIDENT (WITHIN A TOLERANCE) WITH A		
C	SINGLE BODY MERIDIAN LINE		
60	DO 65 J=1,NPLNW		,54
	K=JLEAD+J		,55
	IF (ABS(ZCOR(IMID+1,K)-ZCEPTW(J))-FPS) 65,65,70		,57
	CONTINUE		,58
65	CONTINUE		,59
	GO TO 110		,60
70	NPER=NPER+1		,61
	NPER=NPER-1		,62
	ISTART=IMID+2		,63
	DO 75 I=ISTART,NPER		,64
	DO 75 J=1,NPLANE		,65
	L=NPER-(I-ISTART)		,66
	K=L-1		,67
	XCOR(L,J)=XCOR(K,J)		,68
	YCOR(L,J)=YCOR(K,J)		,69
	ZCOR(L,J)=ZCOR(K,J)		,70
	I=IMID+1		,71
75	CONTINUE		,72
	CONTINUE		,73
	CONTINUE		,74
	CONTINUE		,75
C	DEFINE ADDITIONAL MERIDIAN LINE		
C	AVERAGE ADJACENT POINTS FORE AND AFT OF		
C	INTERSECTION REGION		
	DO 80 J=1,NPLANE		,76
	XCOR(I,J)=XCOR(I-1,J)+.5*(XCOR(I+1,J)-XCOR(I-1,J))		,77
	YCOR(I,J)=YCOR(I-1,J)+.5*(YCOR(I+1,J)-YCOR(I-1,J))		,78
	CONTINUE		,79
	CONTINUE		,80

```

80 ZCOR(I,J)=ZCOR(I-1,J)+.5*(ZCOR(I+1,J)-ZCOR(I-1,J))
C
C USE BODY-WING INTERSECTION POINTS IN BODY-
C WING INTERSECTION REGION
DO 90 J=1,NPLNW
K=JLEAD+J
XCOR(I,K)=XCEPTW(J)
YCOR(I,K)=YCEPTW(J)
90 ZCOR(I,K)=ZCEPTW(J)
100 GO TO 110

C CALCULATE ADDITIONAL PANEL POINTS XINT,YINT.
C ZINT ARE POINTS ON PANEL LEADING AND TRAILING
C EDGES USED TO DEFINE (STREAMWISE) PANEL PARTS
C KPADEL IS CODE DEFINING PANEL TYPE
110 DO 220 I=1,NPERI
DO 220 J=1,NPLNI
KPADEL(I,J)=1
P(1,1)=XCOR(I,J+1)
P(2,1)=YCOR(I,J+1)
P(3,1)=ZCOR(I,J+1)
P(1,2)=XCOR(I+1,J+1)
P(2,2)=YCOR(I+1,J+1)
P(3,2)=ZCOR(I+1,J+1)
R(1,1)=XCOR(I,J)
R(2,1)=YCOR(I,J)
R(3,1)=ZCOR(I,J)
R(1,2)=XCOR(I+1,J)
R(2,2)=YCOR(I+1,J)
R(3,2)=ZCOR(I+1,J)

C LOCATE INBOARD POINT
153 IF (ABS(ZCOR(I+1,J+1)-ZCOR(I,J+1))-F) 153,153,155
C(1)=0.
C(2)=-1.
C(3)=0.
C(4)=YCOR(I,J)
GO TO 157
155 C(1)=0.
C(2)=-1*YCOR(I+1,J+1)-YCOR(I,J+1)/(ZCOR(I+1,J+1)-ZCOR(I,J+1))
C(3)=-1.
C(4)=ZCOR(I,J)-C(2)*YCOR(I,J)

C ATTEMPT TRAILING-EDGE INTERSECTION
157 CALL POLXN (C,P,M,N,F,MAX,O,LOC,NINT)
IF (NINT) 250,170,160
160 XINT(I,J,1)=Q(1,1)
YINT(I,J,1)=Q(2,1)
ZINT(I,J,1)=Q(3,1)
GO TO 190
170 KPADEL(I,J)=KPADEL(I,J)+1
IF (ABS(ZCOR(I+1,J)-ZCOR(I,J))-F) 173,173,175
173 O(1)=0.
O(2)=-1.

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175
D(3)=0.
D(4)=VCOR(I,J+1)
GO TO 177
D(1)=0.
D(2)=-{(VCOR(I+1,J)-VCOR(I,J))/(ZCOR(I+1,J)-ZCOR(I,J))
D(3)=-1.
D(4)=ZCOR(I,J+1)-D(2)*VCOR(I,J+1)

C
177 ATTEMPT LEADING-EDGE INTERSECTION
CALL POLYN (O,R,M,N,F,MAX,Q,LOC,NINT)
IF (NINT) 250,260,180
180 XINT(I,J,1)=Q(1,1)
YINT(I,J,1)=Q(2,1)
ZINT(I,J,1)=Q(3,1)

C
190 LOCATE OUTBOARD POINT
IF (ABS(ZCOR(I+1,J+1)-ZCOR(I,J+1))-F) 193,193,195
193 C(1)=0.
C(2)=-1.
C(3)=0.
C(4)=VCOR(I+1,J)
GO TO 197

195
C(1)=0.
C(2)=-{(VCOR(I+1,J+1)-VCOR(I,J+1))/(ZCOR(I+1,J+1)-ZCOR(I,J+1))
C(3)=-1.
C(4)=ZCOR(I+1,J)-C(2)*VCOR(I+1,J)

C
197 ATTEMPT TRAILING-EDGE INTERSECTION
CALL POLYN (C,P,M,N,F,MAX,Q,LOC,NINT)
IF (NINT) 250,210,200
200 XINT(I,J,2)=Q(1,1)
YINT(I,J,2)=Q(2,1)
ZINT(I,J,2)=Q(3,1)
GO TO 220
210 KPANEL(I,J)=KPANEL(I,J)+2
IF (ABS(ZCOR(I+1,J)-ZCOR(I,J))-F) 213,213,215
213 D(1)=0.
D(2)=-1.
D(3)=0.
D(4)=VCOR(I+1,J+1)
GO TO 217

215
D(1)=0.
D(2)=-{(VCOR(I+1,J)-VCOR(I,J))/(ZCOR(I+1,J)-ZCOR(I,J))
D(3)=-1.
D(4)=ZCOR(I+1,J+1)-D(2)*VCOR(I+1,J+1)

C
217 ATTEMPT LEADING-EDGE INTERSECTION
CALL POLYN (O,R,M,N,F,MAX,Q,LOC,NINT)
IF (NINT) 250,260,218
218 XINT(I,J,2)=Q(1,1)
YINT(I,J,2)=Q(2,1)
ZINT(I,J,2)=Q(3,1)
220 CONTINUE
GO TO 300

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CRNRB		09/17/65
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERVAL FORMULA NUMBER(S)
C	ERROR MESSAGES	
250	WRITE (NWRITE,900)	.175
	GO TO 295	.176 .177
260	WRITE (NWRITE,910)	.178
	GO TO 295	.179 .180
270	WRITE (NWRITE,920)	.181
	GO TO 295	.182 .183
280	IMAX=ISAVE(1)	.184
	DO 285 J=2,NPLNW	.185
285	IMAX=MAX0(IMAX,ISAVE(J))	.186 .187
	WRITE (NWRITE,930) IMAX	.188 .189
	GO TO 295	.190 .191 .192
295	KODEB=1	.193
	GO TO 300	.194
300	RETURN	.195
900	FORMAT (1H1,9X,32HERROR MESSAGE - SUBROUTINE CRNRB/10X, 140HPANEL (PART) CORNER POINT NOT CALCULATED/10X, 124HSUBROUTINE POLYN FAILURE/10X, 152HINTERSECTION NOT CALCULATED DUE TO ZERO COEFFICIENTS) FORMAT (1H1,9X,32HERROR MESSAGE - SUBROUTINE CRNRB/10X, 140HPANEL (PART) CORNER POINT NOT CALCULATED/10X, 124HSUBROUTINE POLYN FAILURE/10X, 127HINTERSECTION DOES NOT EXIST) FORMAT (1H1,9X,32HERROR MESSAGE - SUBROUTINE CRNRB/10X, 150HBODY-(PLANAR) WING INTERSECTION NOT CORRECTLY CALCULATED) FORMAT (1H1,9X,32HERROR MESSAGE - SUBROUTINE CRNRB/10X, 140HBODY-(PLANAR) WING INTERSECTION CROSSES .12, 221H BODY MERIDIAN LINE) END	.196
		.197

```

SUBROUTINE CRNRW
COMMON DATE(2),NTAPE1,ND1,NTAPE2,ND2(3),NREAD,
1NWRITE,NBODY,NWING,XMACH,SYM,KACE
COMMON /COM1/ CODEB,KODEW,KODEU,KODEI,KODEC,XPER,YPER,KOPTB,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPER1
2,NPLANE,NPLN1
COMMON /COM2/ IJ,NPTS(16),XI(90,16),YI(90,16),ZI(90,16),KPNT,VALUE(5),
1YCEPT(16),SLOPE,KPANEL(2,15),XCOR(16,16),YCOR(16,16),ZCOR(16,16),X
2INT(2,15),YINT(2,15),ZINT(2,15),XCEN(15,15),YCEN(15,15),ZCEN(15,15
3),XCON(15,15),YCON(15,15),ZCON(15,15),AREA(15,15),ARAT(15,15),THET
4A(15,15),ALPHA(15,15),CHORD(15,15),XFOIL(16,25,2),ZFOIL(16,25,2),X
5NUM(16,2),XTAB1(25),ZTAB1(25),XTAB2(25),ZTAB2(25)
DIMENSION C(4),P(3,50),Q(3,5),LOC(3)

```

C SUBROUTINE TO CALCULATE WING PANEL CORNER
C POINT COORDINATES

C CALCULATE Y-AXIS INTERCEPT OF OUTBOARD CUTTING
C PLANE

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10 IF (KOPTW) 300,10,80
11 IF (IJ) 300,13,300
12 IF (SLOPE) 20,14,20
13 IF (KPNT) 17,17,18
14 YCEPT(NPLANE)=VALUE(2)
15 GO TO 27
16 YCEPT(NPLANE)=VALUE(4)
17 GO TO 27
18 IF (KPNT-1) 23+23,25
19 YCEPT(NPLANE)=VALUE(2)-VALUE(1)/SLOPE
20 GO TO 27
21 YCEPT(NPLANE)=VALUE(4)-VALUE(3)/SLOPE
22 GO TO 27
23 IF (KINT) 300,40,30

```

C DEFINE INBOARD EDGE PANEL CORNER POINTS FOR
C INBOARD COLUMN OF PANELS TO BE BODY-WING
C INTERSECTION POINTS IF BODY AND WING INTER-
C SECT OTHERWISE SKIP TO STATEMENT 40

```

30 DO 35 J=1,NPER
31 XCOR(1,J)=XI(J)
32 YCOR(1,J)=YI(J)
33 ZCOR(1,J)=ZI(J)

```

C CALCULATE X-, Y- AND Z-COORDINATES OF PANEL
C CORNER POINTS PREVIOUSLY DETERMINED
C WING PERCENT LINES ARE INTERSECTED WITH
C SERIES OF CUTTING PLANES

```

40 DO 70 J=1,NPER
41 NPOINT=NPTS(IJ)
42 DO 43 I=1,NPOINT
43 P(1,I)=X(I,J)
44 P(2,I)=Y(I,J)
45 P(3,I)=Z(I,J)
46 DO 50 I=1,NPLN1

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CRNRW 09/14/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

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K=I+KINT
C(1)=0.
C(2)=1.
C(3)=0.
C(4)=-YCEPT(I)
E=0.001
M=3
MAX=1
CALL PULXN (C,P,M,NPOINT,E,MAX,Q,LOC,NINT)
IF (NINT) 230,24C,47
47 XCOR(K,J)=Q(1,1)
   YCOR(K,J)=Q(2,1)
   ZCOR(K,J)=Q(3,1)
50 IF (SLOPE) 57,53,57
53 C(4)=-YCEPT(NPLANE)
   GO TO 60
57 C(1)=1.
   C(2)=-SLOPE
   C(3)=0.
   C(4)=SLOPE*YCEPT(NPLANE)
60 CALL PULXN (C,P,M,NPOINT,E,MAX,Q,LOC,NINT)
65 L=NPLANE+KINT
   XCOR(L,J)=Q(1,1)
   YCOR(L,J)=Q(2,1)
   ZCOR(L,J)=Q(3,1)
70 CONTINUE
75 NPLANE=NPLANE+KINT
   NPLNI=NPLANE-1

C   DEFINE KSTART IF KSTART = 1,WING-BODY
C   INTERSECTION IS STRAIGHT LINE IN STREAMWISE
C   DIRECTION IF KSTART = 2,OTHERWISE
80 DO 85 J=1,NPER1
85   IF (ABS(YCOR(L,J+1)-YCOR(L,J))-0.001) 85,85,87
   KSTART=1
   GO TO 100
87 KSTART=2

C   DEFINE KEND IF KEND EQUAL TO NPLNI
C   WING HAS STREAMWISE OUTBOARD EDGE IF
C   KEND EQUAL TO NPLNI OTHERWISE
100 DO 110 J=1,NPER1
110   IF (ABS(YCOR(NPLANE,J+1)-YCOR(NPLANE,J))-0.001) 110,110,120
   CONTINUE
   KEND=NPLNI
   GO TO 130
120 KEND=NPLNI-1

C   CALCULATE ADDITIONAL PANEL POINTS FOR
C   PANELS IN BODY-WING INTERSECTION
C   XINT,YINT,ZINT ARE POINTS ON PANEL LEADING AND
C   TRAILING EDGES USED TO DEFINE (STREAMWISE) PANEL

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SOURCE STATEMENT

EXTERNAL FORMULA NUMBER

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C
130 PARTS
140 IF (KSTART-1) 300,170,140
DO 160 J=1,NPER1
P(1,1)=XCOR(2,J+1)
P(2,1)=YCOR(2,J+1)
P(3,1)=ZCOR(2,J+1)
P(1,2)=XCOR(1,J+1)
P(2,2)=YCOR(1,J+1)
P(3,2)=ZCOR(1,J+1)
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C
LOCATE POINT
C(1)=0.
C(2)=-1.
C(3)=0.
C(4)=YCOR(1,J)
E=0.001
M=3
MAX=1
N=2
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C
ATTEMPT TRAILING-EDGE INTERSECTION
CALL POLXN (C,P,M,N,E,MAX,Q,LOC,NINT)
IF (NINT) 230,150,145
145 XINT(1,J)=Q(1,1)
YINT(1,J)=Q(2,1)
ZINT(1,J)=Q(3,1)
KPADEL(1,J)=1
GO TO 160
150 P(1,1)=XCOR(2,J)
P(2,1)=YCOR(2,J)
P(3,1)=ZCOR(2,J)
P(1,2)=XCOR(1,J)
P(2,2)=YCOR(1,J)
P(3,2)=ZCOR(1,J)
C(4)=YCOR(1,J+1)
CALL POLXN (C,P,M,N,E,MAX,Q,LOC,NINT)
IF (NINT) 230,240,155
155 XINT(1,J)=Q(1,1)
YINT(1,J)=Q(2,1)
ZINT(1,J)=Q(3,1)
KPADEL(1,J)=2
160 CONTINUE
DO 165 J=1,NPER1
IF (YINT(1,J)-YCOR(2,J)) 165,165,250
165 CONTINUE
170 IF (KEND-NPLN) 180,210,300
180 DO 200 J=1,NPER1
P(1,1)=XCOR(NPLN1,J)
P(2,1)=YCOR(NPLN1,J)
P(3,1)=ZCOR(NPLN1,J)
P(1,2)=XCOR(NPLANE,J)
P(2,2)=YCOR(NPLANE,J)
P(3,2)=ZCOR(NPLANE,J)
C(1)=0.
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09/14/65

CRNRW	EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
		C(2)=-1.	.123
		C(3)=0.	.124
		C(4)=YCOR(NPLANE,J+1)	.125
		E=0.001	.126
		M=3	.127
		MAX=1	.128
		N=2	.129
		CALL POLXN (C,P,M,N,E,MAX,Q,LOC,NINT)	.130
		IF (NINT) 230,190,185	.131
185		XINT(2,J)=Q(1,1)	.132
		YINT(2,J)=Q(2,1)	.133
		ZINT(2,J)=Q(3,1)	.134
		KPANEL(2,J)=1	.135
		GO TO 200	.136
190		P(1,1)=XCOR(NPLN1,J+1)	.137
		P(2,1)=YCOR(NPLN1,J+1)	.138
		P(3,1)=ZCOR(NPLN1,J+1)	.139
		P(1,2)=XCOR(NPLANE,J+1)	.140
		P(2,2)=YCOR(NPLANE,J+1)	.141
		P(3,2)=ZCOR(NPLANE,J+1)	.142
		C(4)=YCOR(NPLANE,J)	
C		ATTEMPT LEADING-EDGE INTERSECTION	.143
		CALL POLXN (C,P,M,N,E,MAX,Q,LOC,NINT)	.144
		IF (NINT) 230,240,195	.145
195		XINT(2,J)=Q(1,1)	.146
		YINT(2,J)=Q(2,1)	.147
		ZINT(2,J)=Q(3,1)	.148
		KPANEL(2,J)=2	.149
200		CONTINUE	.150
		DO 205 J=1,NPER1	.151
		IF (YINT(2,J)-YCOR(NPLN1,J)) 260,205,205	.152
205		CONTINUE	.153
210		IF (KUPTW) 300,300,270	.154
C		ERROR MESSAGES	.156
230		WRITE (NWRITE,900)	.157
		GO TO 265	.158
240		WRITE (NWRITE,910)	.159
		GO TO 265	.160
250		WRITE (NWRITE,920)	.161
		GO TO 265	.162
260		WRITE (NWRITE,930)	.163
		GO TO 265	.164
265		KODEW=1	.165
		GO TO 300	.166
270		IF (KEND-NPLN1) 280,290,300	.167
280		J=NPLANE	.168
		SLOPE=(XCOR(NPER,J)-XCOR(1,J))/(YCOR(NPER,J)-YCOR(1,J))	.169
		GO TO 300	.170
290		SLOPE=0.	.171
300		RETURN	.172
900		FORMAT (1H1,9X,32HERROR MESSAGE - SUBROUTINE CRNRW/10X, 14HPANEL (PART-) CORNER POINT NOT CALCULATED/10X,	.173 .174 .175 .176

CRNRW
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - IFN(S) - INTERNAL FORMULA NUMBER(S)

09/14/65

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124HSUBROUTINE POLYN FAILURE/10X,
152HINTERSECTION NOT CALCULATED DUE TO ZERO COEFFICIENTS)
910  FORMAT (1H1,9X,32HERROR MESSAGE - SUBROUTINE CRNRW/10X,
141HPANEL (PART-J) CORNER POINT NOT CALCULATED/10X,
124HSUBROUTINE POLYN FAILURE/10X,
127HINTERSECTION DOES NOT EXIST)
920  FORMAT (1H1,9X,1CHDATA ERROR/10X,
135HINCORRECT WING PANEL (FIRST COLUMN))
930  FORMAT (1H1,9X,1CHDATA ERROR/10X,
134HINCORRECT WING PANEL (LAST COLUMN))
END

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05/22/67

CUBIC2 - EFM SOURCE STATEMENT - IFN(S) -

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C
C
C
SUBROUTINE CUBIC2(X,Y,D,C,J)
DIMENSION X(1),Y(1),D(1),C(1)
K2=X(2)
B=X-X2
IF (B)10,5,10
5  J=3
10  CALL OVERFL(J)
A=(Y-Y(2))/B
E=X+X2
C(4)=(D+D(2)-A-A)/B/B
C(3)=(A-D(2))/B-C(4)*(E+X2)
C(2)=A-E+C(3)-C(4)*(E+X2+X*2)
C=Y(2)-X2*(C(2)+X2*(C(3)+X2*C(4)))
CALL OVERFL(J)
J=3-J
30  RETURN
END

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8

CVEL
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
08/16/65

SUBROUTINE CVEL(M,N,NTAPEX,A,B,C,CL,U,V,W)

C COMPUTES VELOCITY COMPONENTS FOR A GIVEN PANEL PRESSURE DIFFERENCE

DIMENSION A(1),B(1),C(1),U(1),V(1),W(1),CL(1)

DO 100 J=1,M

U(J)=0.0

V(J)=0.0

W(J)=0.0

100 CONTINUE

DO 200 J=1,N

READ (NTAPEX) (A(I),B(I),C(I),I=1,M)

DO 200 I=1,M

U(I)=U(I)+A(I)*CL(J)

V(I)=V(I)+B(I)*CL(J)

W(I)=W(I)+C(I)*CL(J)

200 CONTINUE

RETURN

END

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DCPD		08/16/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	-	INTERNAL FORMULA NUMBER(S)
SUBROUTINE DCPD(NM,NTAPEX,A,ALPHAP,CLM)			
C	COMPUTES WING PANEL PRESSURE DIFFERENCE		
	DIMENSION A(1),ALPHAP(1),CLM(1)		
	DO 100 J=1,NM		,1
	CLM(J)=0.0		,2
	100 CONTINUE		
	DO 200 J=1,NM		,3
	READ (NTAPEX) (A(I),I=1,NM)		,4
	DO 200 I=1,NM		,5
	CLM(I)=CLM(I)+A(I)*ALPHAP(J)		,6
	200 CONTINUE		,7
			,8
			,9
			,10
			,11
			,12
			,13
			,14
			,15
	RETURN		,16
	END		,17

SUBROUTINE DCPI (NB,NW,NTAPEX,A,ALPHAB,CLW,CLB)

C COMPUTES BODY PANEL PRESSURE DIFFERENCE

DIMENSION A(1),ALPHAB(1),CLW(1),CLB(1)

DO 100 J=1,NB

CLB(J)=0.

100 CONTINUE

DO 200 J=1,NB

READ (NTAPEX) (A(I),I=1,NB)

DO 200 I=1,NB

CLB(I)=CLB(I)+A(I)*ALPHAB(J)

200 CONTINUE

DO 300 J=1,NW

READ (NTAPEX) (A(I),I=1,NB)

DO 300 I=1,NB

CLB(I)=CLB(I)+A(I)*CLW(J)

300 CONTINUE

RETURN

END

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.25
.26
.27
.28

06/02/67

DED - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE DED(NARG)
COMMON /JDED/I
I=3
CALL DEDISUM,IND,NTEST,I)
NARG=0
IF (I.GT.3)NARG=1
RETURN
END

DEDIS009
DEDIS010
DEDIS011
DEDIS012
DEDIS013
DEDIS014
DEDIS015

3

```

SUBROUTINE DEDIS(NUM,IND,MTEST,IFROM)
DOUBLE PRECISION DP
INTEGER ALPHA,R,TSXJC5,TOTOT2
LOGICAL SW1,SW2,DECRM,INCRH
EQUIVALENCE (DP,D(1)),(TEMP,
DIMENSION T(1,0:2),PKA(7,4),IT(1)
DATA (IRKAL1,J),I=1,7),J=1,4)/0.,2.,-1.,3.,-5.,1.,0.,0.,2.,-5.,-1.,
1.,5.,-33333333.,0.,-5.,1.,0.,-1.,0.,1.,0.,2.,6.,1.,3.,-5.,-5.,0.,/
DATA ERN1/3HN=0/,ERN2/5HN FLT/,ERRH/3HH=0/,ERRE/3HE=0/,ERRI/
13HND/
GO TO (1000,2000,3000), IFROM
SW1=.TRUE.
SW2=.TRUE.
TOTOT2=2+*27
IADD = LOC(NUM)- LOC(IADD)+65537
INTEST = LOC(MTEST)- LOC(IADD)+65537
IIND = LOC(IIND)- LOC(IADD)+65537
JND = IT(IIND)
N=NUM
N1=IADD+N
N2=N1+N
N3=N2+N
N4=N3+N
N5=N4+N
N6=N5+N
N7=N6+N
N8=N7+N
N9=N8+N
N10=N9+N
N11=N10+N
N12=N11+N
TEST IF N = 0
IF (N.EQ.0) GO TO 32
TEST IF N IS REAL
IF (N.GT.4096) GO TO 33
TEST IF H=0
IF (ABS(T(M12))-LT.1.E-35) GO TO 34
ASSURE IND=0, 1, OR 2
IF ((IABS(IND).NE.0).AND.(IND.NE.1)).AND.(IND.NE.2)) GO TO 36
IND IS 0, 1, OR 2
IF(IND.NE.0)GO TO 27
TEST IF E=0
IF (ABS(T(M12+8))-LT.1.E-35) GO TO 35
IF (IND-1) 21,20,19
SW2=.FALSE.
GO TO 677
GO TO 677
SW1=.FALSE.
GO TO 677
IF (TIM12+31) 9001,9000,9001
BETA=-5
GO TO 9002
BETA=TIM12+31
EBAR=14.*TIM12+8)
9001
9002

```

06/02/67

DEBIS - EFM SOURCE STATEMENT - IFM(S) -

```

TSXJCS-2
GO TO 999
12 IF (ALPHA-1) 900,901,902
902 DO 905 I=1,N
    M201 = M2-I
    M101 = M1-I
    905 YIN201)=YIN11Q1)
    GO TO 2212
901 DO 904 I=1,N
    M301 = M3-I
    M101 = M1-I
    904 YIN301)=YIN11Q1)
    GO TO 2212
900 DO 903 I=1,N
    M401 = M4-I
    M101 = M1-I
    YIN401)=YIN11Q1)
    M601 = M6-I
    M1201 = M12-I
    YIN601)=YIN12Q1)
    M501 = M5-I
    M1001 = M10-I
    YIN501)=YIN10Q1)
    903 YIN501)=YIN10Q1)
    2212 ALPHA=ALPHA+1
    23 RKA(7,1)=YIN12)/2-
    RKA(7,3)=RKA(7,1)
    MPASS-1
    GO TO 7023
3000 GO TO (26,3,24,4008,6) , TSXJCS
26 DO 3026 I=1,N
    M1001 = M10-I
    YIN1001)=0.
    3026 ALPHA=0
    R=0
    YI(TIMTEST)=1
    RETURN
    EMP1=0.
    DO 3003 I=1,N
    M801 = M8-I
    B(1)=YIN8Q1)
    M1001 = M10-I
    B(2)=YIN10Q1)
    M301 = M3-I
    M201 = M2-I
    M101 = M1-I
    TEMP=YIN12)*((1./24.)*YIN301)-(5./24.)*YIN201)+(19./24.)*YIN1Q1)+(18091369
    15./8.)*YIN11Q1))
    DP=DP+TEMP
    YIN1001)=B(2)
    M1201 = M12-I
    YIN1201)=B(1)
    M901 = M9-I
    3003 EMP1=AMAX1(EMP1,(ABS(YIN901)-YIN1201)/AMAX1(A,ABS(YIN1201))))

```

DEBIS123
 DEBIS124
 DEBIS125
 DEBIS126
 DEBIS127
 DEBIS128
 DEBIS129
 DEBIS130
 DEBIS131
 DEBIS132
 DEBIS133
 DEBIS134
 DEBIS135
 DEBIS136
 DEBIS137
 DEBIS138
 DEBIS139
 DEBIS140
 DEBIS141
 DEBIS142
 DEBIS143
 DEBIS144
 DEBIS145
 DEBIS146
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 DEBIS161
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 DEBIS166
 DEBIS167
 DEBIS168
 DEBIS169
 DEBIS170
 DEBIS171
 DEBIS172
 DEBIS173
 DEBIS174
 DEBIS175
 DEBIS176

06/02/67

DEDIS - EFN SOURCE STATEMENT - (FNIS) -

```

4 IF (.NOT.SW2) GO TO 5
  IF (EBAR-ENP1) 9017,9017,9013
9017 IF (.NOT-DECRH) GO TO 7
  IF (ABS(T(N12))-LT.HMINDB) GO TO 14
7 TEMP=T(N12)
  T(N12)=T(N12)+BETA
  IF (ALPHA-EG.3) GO TO 8
  T(N12+1)=T(N12+1)-TEMP
  DO 3008 I=1,N
    N1Q1 = N1-I
    N1Q1 = N1-I
    T(N1Q1)=T(N1Q1)
    N1Q1 = N12-I
    N1Q1 = N12-I
    T(N1Q1)=T(N1Q1)
    N1Q1 = N10-I
    N1Q1 = N10-I
    T(N1Q1)=T(N1Q1)
    N1Q1 = N7-I
    T(N1Q1)=T(N1Q1)
3008 DO 5008 I=1,N
  4008 DO 5008 I=1,N
    N1Q1 = N10-I
    N1Q1 = N10-I
5008 T(N1Q1)=3.*T(N1Q1)
6008 ALPHA=Q
  R=0
C IF P-C MODE CHECK IF INTEGRATION IS GOOD POINT
6 IF (ABS(JND)-NE.0) GO TO 31
C IND=0 P-C MODE
C IF (ALPHA-NE.0) GO TO 30
C ALPHA = 0
C IF (ABS(T(N12))-GT.HINT) GO TO 31
C H DECREASED
C GO TO 900
C ALPHA NOT 0

30 IF (ALPHA-LE.3) GO TO 38
C SUCCESS FROM D.E. ALPHA GREATER THAN 3 FOR P-C MODE
31 IFROM = 4
  RETURN
38 IFROM=5
  RETURN
9013 IF (EBARDM-ENP1) 14,14,9018
9018 IF (.NOT-INCRH) GO TO 15
9 IF (ABS(T(N12))-GT.HMAXTB) GO TO 5
15 R=R+1
  IF (R-LT.3) GO TO 5
10 T(N12)=T(N12)/BETA
  TSXJCS=4
  GO TO 999
14 R=0
5 DO 3005 I=1,N

```

06/02/87

DEDIS - EFN SOURCE STATEMENT - IFN(S) -

```

N4Q1 = N4-I
N3Q1 = N3-I
N2Q1 = N2-I
N1Q1 = N1-I
T(N4Q1)=T(N3Q1)
T(N3Q1)=T(N2Q1)
T(N2Q1)=T(N1Q1)
3005 T(N2Q1)=T(N1Q1)
      ALPHA=ALPHA+1
      TSXJCS=5
999  ITTINTEST)=0
      RETURN
24  IF (NPASS-EQ.4) GO TO 6
7023 DO 4023 I=1,N
      N9Q1 = N9-I
      N11Q1 = N11-I
      T(N9Q1)=RKA(1,NPASS)*T(N9Q1)+T(N12)+T(N11Q1)
      N10Q1 = N10-I
      TEMP=T(N9Q1)/RKA(2,NPASS)+RKA(3,NPASS)*T(N10Q1)
      IF (TEMP) 9014,3023,9014
9014 JTEMP=IADD/TOTOT27
      N12Q1 = N12-I
      IF (T(N12Q1)) 9015,3023,9015
9015 JTEMP2=ABS(T(N12Q1))
      JTEMP=(KTEMP/TOTOT27)-IABS(JTEMP)
      IF (JTEMP) 3023,3023,9016
9016 IF (JTEMP-27) 9019, 9019, 9020
9020 TEMP = 0.
      GO TO 3023
9019 JTEMP = 2+JTEMP
      IADD=IADD/JTEMP
      IADD=JTEMP+IADD
3023 T(N12Q1)=T(N12Q1)+TEMP
4023 T(N10Q1)=T(N10Q1)+RKA(6,NPASS)+TEMP+RKA(4,NPASS)+T(N9Q1)+RKA(5,NPASS)
      155)
      T(N12+1)=T(N12+1)+RKA(7,NPASS)
      TSXJCS=3
      GO TO 999
8  T(N12+1)=T(N12+1)-4.*TEMP
      DO 1008 I=1,N
      N11Q1 = N11-I
      N4Q1 = N4-I
      T(N11Q1)=T(N4Q1)
      N12Q1 = N12-I
      N6Q1 = N6-I
      T(N12Q1)=T(N6Q1)
      N10Q1 = N10-I
      N5Q1 = N5-I
      1008 T(N10Q1)=T(N5Q1)
      GO TO 4008

```

361

```

32 ERROR = ERRN1
GO TO 37
33 ERROR = ERRN2
GO TO 37
34 ERROR = ERRN3
GO TO 37
35 ERROR = ERRE
GO TO 37
36 ERROR = ERRI
37 WRITE(6,8000) ERROR
STOP
8000 FORMAT(51HODIFFERENTIAL EQUATION SUBROUTINE DES INPUT ERROR A6)
END

```

430

```

DED1S279
DED1S280
DED1S281
DED1S282
DED1S283
DED1S284
DED1S285
DED1S286
DED1S287
DED1S288
DED1S289
DED1S290
DED1S291

```

OFFEN1
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

07/31/65

SUBROUTINE DEFENI(B,J,K,L,TAPE,IREC)
DIMENSION R(1),IREC(10),JREC(10),DUM(9)
DATA DUM/9*0./,JREC/0,9,8*0/

C USED BY DEFEND TO WRITE DEFINITION TAPE

C IF (IREC(3))10,20,10

C 10 JREC=IREC

C JREC(3)=IREC(3)

C WRITE(LTAPE)JREC

C WRITE(LTAPE)DUM

C GO TO 100

C 20 WRITE(LTAPE)IREC
C WRITE(LTAPE)(B(I),I=J,K)

C 100 RETURN

C END

1
2
3
4 5 6
7 8 9
10 11 12 13
14 15 16 17 18
19
20

09/14/65
DEFEND
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

SUBROUTINE DEFEND18,LK,LO,LTAPE,LGDEF,LGTAPE,INTWB)
DIMENSION B(1),LK(3,9),LOK(3,9),IREC(10),KR(6),LGDEF(3,6)
LOGICAL LGDEF,LGTAPE
EQUIVALENCE (LOK(1,1),LUNPL),(LOK(2,1),MUNPL),(LOK(3,1),NUMPL),
X(LOK(1,2),LLWPL),(LOK(2,2),MLWPL),(LOK(3,2),NLWPL),
X(LOK(1,3),LLWPLX),(LOK(2,3),MLWPLX),(LOK(3,3),NLWPLX),
X(LOK(1,4),LLWPLX),(LOK(2,4),MLWPLX),(LOK(3,4),NLWPLX),
X(LOK(1,5),LBPL),(LOK(2,5),MBPL),(LOK(3,5),NBPL),
X(LOK(1,6),LSTA),(LOK(3,6),NSTA),
X(LOK(1,7),LWPF),(LOK(2,7),MWPF),(LOK(3,7),NMPF),
X(LOK(1,8),LUMB),(LOK(3,8),NUMB),
X(LOK(1,9),LLWB),(LOK(3,9),NLWB)
DATA IREC/10*0/

```

```

C
C SPECIAL SUBROUTINE USED BY GEOMD
C
C WRITES DEFINITION TAPE FOR USE BY PANEL LINK
C

```

```

90 IF (LGTAPE) GO TO 200
WRITE (LO,110) LTAPE
110 FORMAT(50HIDID NOT WRITE DEFINITION TAPE. LOGICAL TAPE NO.
-3HMAS 110)
GO TO 9000

```

```

C
C WE ALWAYS WRITE 18 RECORDS ON TAPE LTAPE, BUT IT MAY TAKE 2 CALLS OF
C DEFEND TO DO IT. IF A WING-BODY INTERSECTION IS CALLED FOR, WE WRITE
C THE BODY AND WING RECORDS BEFORE FINDING THE INTERSECTIONS BECAUSE THE
C ORIGINAL WING STORAGE IS RE-USED. THE REMAINING RECORDS ARE WRITTEN
C LATER, ON A SECOND CALL. INTWB IS A CODE WHICH CONTROLS THIS.

```

```

C THE 3RD WORD OF GOD-NUMBERED RECORDS IS =0 IF OK, =1 IF NOT WANTED,
C =-1 IF WANTED BUT ERROR OCCURRED. WE WRITE DUMMY RECORDS IF NOT =0.
C SET UP THIS WORD IN KR ARRAY.

```

```

200 DO 500 I=1,6
IF (LGDEF(1,I).AND.LGDEF(2,I)) GO TO 400
300 IF (LGDEF(1,I)) GO TO 310
KR(I)=1
GO TO 500
310 KR(I)=-1
GO TO 500

```

```

C
400 KR(I)=0
LGDEF(3,I)=.TRUE.
500 CONTINUE

```

```

C
DO 600 J=1,9
DO 600 I=1,3
LOK(I,J)=LK(I,J)

```

```

C
IF (INTWB) 650,650,2000
REWIND LTAPE

```

```

C
C BODY STATIONS
C IREC(1)=1

```

,1 ,2 ,3
,4 ,5 ,6

,7 ,8 ,10 ,11
,9 ,12 ,13 ,14
,15 ,16 ,17

,18 ,19 ,20
,21 ,22
,23 ,24

,25 ,26 ,27
,28

,29 ,30

DEFEND		09/14/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)	
C	IREC(2)=NSTA	,31	
	IREC(3)=KR(3)	,32	
C	CALL DEFEN1(8,LSTA,LSTA+NSTA-1,LTAPE,IREC)		
C	BASIC BODY PERCENT LINES	,33	
	IREC(1)=3	,34	
	IREC(2)=NBPL	,35	
	IREC(3)=KR(3)	,36	
	IREC(4)=NBPL	,37	
C	CALL DEFEN1(8,LBPL,LBPL+NBPL-1,LTAPE,IREC)		
C	WING PLANFORM (RECORDS 5,6)	,38	
	IREC(1)=5	,39	
	IREC(2)=NMPP	,40	
	IREC(3)=KR(4)	,41	
	IREC(4)=NMPP	,42	
C	CALL DEFEN1(8,LWPF,LWPF+NMPP-1,LTAPE,IREC)		
C	BASIC WING PERCENT LINES (RECORDS 7,8,9,10)	,43	
	DO 1000 IA=1,2	,44	
	IREC(1)=IA+IA+5	,45	
	IREC(2)=LOK(3,IA)	,46	
	IREC(3)=KR(1A)	,47	
	IREC(4)=LOK(2,IA)	,48	
	1000 CALL DEFEN1(8,LOK(1,IA),LOK(1,IA)+LOK(3,IA)-1,LTAPE,IREC)	,49	,50
C	2000 IF (INT(8)9000,2100,2100		
C	UPPER WING-BODY INTERSECTION POINTS (RECORDS 11,12)	,51	
	IREC(1)=11	,52	
	IREC(2)=NUMB	,53	
	IREC(3)=KR(5)	,54	
	IREC(4)=NUMPLX	,55	
C	CALL DEFEN1 (8,LCWB,LUMB+NUMB-1,LTAPE,IREC)		
C	UPPER WING OUTSIDE BODY (RECORDS 13,14)	,56	
	IREC(1)=13	,57	
	IREC(2)=NUMPLX	,58	
C	CALL DEFEN1 (8,LLWPLX,LLWPLX+NUMPLX-1,LTAPE,IREC)		
C	LOWER WING-BODY INTERSECTION POINTS (RECORDS 15,16)	,59	
	IREC(1)=15	,60	
	IREC(2)=NLWB	,61	
	IREC(3)=KR(6)	,62	
	IREC(4)=MLWPLX	,63	
C	CALL DEFEN1 (8,LLWB,LLWB+NLWB-1,LTAPE,IREC)		
C	LOWER WING OUTSIDE BODY (RECORDS 17,18)	,64	
	IREC(1)=17	,65	
	IREC(2)=NLWPLX	,66	
C	CALL DEFEN1 (8,LLWPLX,LLWPLX+NLWPLX-1,LTAPE,IREC)	,67	
	END FILE LTAPE	,68	

DEFEND 09/14/65
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
 9000 RETURN '69
 END '70

DEI - EFN SOURCE STATEMENT - IFN(S) - 06/02/67
 SUBROUTINE DEI(NUM, IND, NTEST)
 CALL DEDIS(NUM, IND, NTEST, 2)
 RETURN
 END
 DEDIS005
 DEDIS006
 DEDIS007
 DEDIS008

DERIVI - EFN SOURCE STATEMENT - IFN(S) -

```

C
C
FUNCTION DERIV(X1,Y1,N)
C
C
DIMENSION X(3),Y(3),X1(3),Y1(3)
EQUIVALENCE (S,K)
C
C
DO 10 I=1,3
  X(I)=X1(I)
  Y(I)=Y1(I)
10 K=N
C
C
C FIND COEFFICIENTS OF THE X-SQUARED TERM
C AND THE X TERM. NO NEED TO FIND CONSTANT
C TERM, AS IT DISAPPEARS UNDER DIFFERENTIATION.
E=Y-Y(2)
H=Y-Y(3)
A=X-X(2)
B=X-X(3)
C=X**2-X(2)**2
C=A*(X-X(2))
DT=X**2-X(3)**2
DY=B*(X+X(3))
C3=(B*(C-A*H))/(B*C-A*DT)
C2=(E-C*A*H)/(B*C-A)
C2=1E-C3*C1/A
C1=1ABS(K)
C
C
C TEST TO SEE WHETHER DERIVATIVE IS WANTED AT ONE
C OF THE INPUT POINTS OR ELSEWHERE.
DO 20 I=1,3
  IF(K1-I) 20,50,20
20 CONTINUE
GO TO 60
50 S=X(K1)
60 DERIV=C2+2.0*C3*S
RETURN
END

```

DER10030
DER10020
DER10040
DER10060
DER10140
DER10100
DER10110
DER10120
DER10130
DER10150
DER10160
DER10170
DER10180
DER10190
DER10200
DER10210
DER10220
DER10230
DER10240
DER10250
DER10260
DER10270
DER10280
DER10290
DER10300
DER10310
DER10320
DER10330
DER10340
DER10350
DER10360
DER10370
DER10380
DER10390

05/22/67

DERIV2 - EFN SOURCE STATEMENT - IFN(S) -

```

C
C
C
FUNCTION DERIV2(X,Y,XX)
  DIMENSION X(4),Y(4)
  DERIV2=0.0
  IF (X(4)-X(3)) 1,7,1
  1 IF (X(4)-X(2)) 2,7,2
  2 IF (X(4)-X(1)) 3,7,3
  3 IF (X(3)-X(2)) 4,7,4
  4 IF (X(3)-X(1)) 5,7,5
  5 IF (X(2)-X(1)) 6,7,6
  6 Q41=(Y(4)-Y(1))/(X(4)-X(1))
  Q31=(Y(3)-Y(1))/(X(3)-X(1))
  Q21=(Y(2)-Y(1))/(X(2)-X(1))
  E=(Q41-Q21)/(X(3)-X(2))
  D=((Q41-Q21)/(X(4)-X(2))-E)/(X(4)-X(3))
  C=E-D*(X(3)-X(2))*XX
  DERIV2=2.0*(C+3.0*D*XX)
  7 RETURN
END
DERIV2030
DERIV2020
DERIV2040
DERIV2050
DERIV2070
DERIV2080
DERIV2090
DERIV2100
DERIV2110
DERIV2120
DERIV2130
DERIV2140
DERIV2150
DERIV2160
DERIV2170
DERIV2180
DERIV2190
DERIV2200
DERIV2210
DERIV2220
DERIV2230

```

```

SUBROUTINE DERIV4(XB,R,NBODYS,FD,SD)
  DIMENSION XB(1),R(1),FD(1),SD(1),C(4,50)
  SURROUTINE TO OBTAIN FIRST AND SECOND
  DERIVATIVES SUBROUTINE USES SCAMP4 TO FIT
  A CHAIN OF CUBICS THROUGH AN ARRAY OF POINTS
  AND TO CALCULATE FIRST DERIVATIVES AT EACH OF
  THE POINTS SUBROUTINE THEN CALCULATES
  SECOND DERIVATIVES
  C
  C FIT CUBIC CHAIN AND GET FIRST DERIVATIVES
  CALL SCAMP4(XB,R,NBODYS,-1,-1,0.0,C,FD,0)
  C
  C CALCULATE SECOND DERIVATIVES
  NB1=NBODYS-1
  DO 100 I=1,NB1
  100 SD(I)=2.*C(3,I) +6.*C(4,I) *XS(I)
  SD(NBODYS)=2.*C(3,NB1)+6.*C(4,NB1)*XB(NBODYS)
  RETURN
END

```

C	DES	-	EFN	SOURCE STATEMENT	-	IFN(S)	-	06/02/67	2
				7094(FORTRAN IV) SUBPROGRAM IBSYS VERSION 9				DEDIS000	
				SUBROUTINE DES (NUM,IND,NTEST)				DEDIS001	
				CALL DEDIS(NUM,IND,NTEST,1)				DEDIS002	
				RETURN				DEDIS003	
				END				DEDIS004	

1
2
3
4
5
6
7
8

1
2
3
4
5
6
7
8

```

SUBROUTINE DMAXL(P,N,DIST,J,U,NU)
DIMENSION P(3,1),U(3),V(3),UC(3)

C GIVEN AN ARRAY P OF N POINTS IN 3-SPACE.
C FIND WHICH POINT IN P IS FARTHEST FROM THE LINE THRU END POINTS,
C AND ITS DISTANCE FROM THE LINE. IF MORE THAN ONE POINTS ARE
C EQUALLY FAR, CHOOSE 1ST SUCH POINT IN P.
C THE DESIRED POINT IS P(I,J)
C NU=0 IF SUCCESS, = -1 IF N.LT. 2, =-2 IF END POINTS OF P
C ARE COINCIDENT, =1 IF N=2.
C INPUTS ARE P,N. OUTPUTS ARE DIST,J,U,NU
C
NU=0
DP=0.
J=0
I=(N-2)/100,200,300
100 NU=-1
GO TO 2000

C
200 NU=1
GO TO 2000

C
300 NH=N-1
IF(UVECN(P,P(1,N),U,0,3))1400,400,500
U IS A UNIT VECTOR FROM P(1,1) TO P(1,N)
NU=-2
GO TO 2000

C
500 DO 1000 K=2,NM
DO 600 I=1,3
V(I)=P(I,K)-P(1,1)
V IS A VECTOR FROM P(1,1) TO THE K-TH POINT
KE=0
CALL VCRDS(U,V,UC,D,KE)
UC IS A VECTOR, THE CROSS-PRODUCT U X V.
D IS THE MAGNITUDE OF UC AND IS DISTANCE FROM LINE TO POINT
IF(D-DP)1000,1000,700
J=K
DP=D

C
1000 CONTINUE
2000 DIST=DP
3000 RETURN
END
    
```

,1
 ,2
 ,3
 ,4
 ,5
 ,6
 ,7
 ,8
 ,9
 ,10
 ,11
 ,12
 ,13
 ,14
 ,15 ,16
 ,17
 ,18
 ,19
 ,20
 ,21 ,23
 ,22
 ,24
 ,25
 ,26

ELLIPR 09/14/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

SUBROUTINE ELLIPR(A,B,SIN,COS,RHO,X,Y,NU)
C
C   GIVEN A RECTANGULAR ELLIPSE WITH MAJOR, MINOR SEMI-AXES A,B
C   AND CENTER AT THE ORIGIN.
C   GIVEN THE SIN AND COS OF AN ANGLE THETA MEASURED
C   CLOCKWISE FROM THE +Y AXIS.
C
C   FIND RHO, THE LENGTH OF A RADIUS VECTOR FROM ORIGIN ALONG THETA
C   TO THE ELLIPSE.
C   FIND (X,Y), THE CORRESPONDING POINT ON THE ELLIPSE.
C
  IF(A*B)200,100,200
  100 NU=1
  GO TO 9000
  200 U=(SIN/A)**2+(COS/B)**2
  IF(U)300,300,400
  300 NU=2
  GO TO 9000
  400 RHO=1./SQRT(U)
  X=RHO*SIN
  Y=RHO*COS
  NU=0
  9000 RETURN
  END

```

,1
,2
,3
,4
,5
,6
,7
,8
,9
,10
,11
,12
,13

SUBROUTINE ENRYCH(A,B,NI,EPS,C,NO,NU)
DIMENSION A(500),B(500), C(1000),D(4),E(4),F(4),G(4),H(200),Z(200)ENR10150
1),NU(3)

ENR10110

J. E. BROWN

ASSEMBLED 12-15-64

USES OPTIM3 TO CONVERT SPARSE ARRAY A, B
TO DENSE ARRAY C.
ENR10120
ENR10130
ENR10140

A = ARRAY OF X VALUES
B = ARRAY OF Y VALUES
NI = NUMBER OF INPUT POINTS
EPS = CHORD HEIGHT TOLERANCE
C = (X,Y,X,Y,....)
NO (INPUT) = LENGTH OF C
NO (OUTPUT) = NUMBER OF ELEMENTS PLACED IN C
NU = 0 IF SUCCESS
NU = 1 IF OPTIM3 ERROR WAS = 0 (NOT POSSIBLE)
NU = 2 IF 4 CONSEC. POINTS NOT MONOTONIC IN EITHER X OR Y
NU = 3 IF OPTIM3 GENERATED 199 POINTS BETWEEN 2 GIVEN PTS AND NOT DONE.
NU = 4 IF LENGTH OF C (=NO) WAS TOO SMALL
NU = 5 IF NO LESS THAN 2*NI

NU(2), AN INPUT, IS THE LOGICAL NUMBER OF AN OUTPUT TAPE ON WHICH TO WRITE
ERROR COMMENTS, IF ANY. NU(3), BOTH AN INPUT AND OUTPUT, IS AN ERROR
MESSAGE LIMITER AND COUNTER. IF AN ERROR OCCURS FOR WHICH A MESSAGE IS
NORMALLY WRITTEN, NU(3) IS FIRST REDUCED BY ONE. THE MESSAGE IS THEN
WRITTEN ONLY IF BOTH NU(2) AND NU(3) ARE GREATER THAN ZERO.
ENR10190

NU=0
NOM=NO
NO=0
NI=NI+NI
1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19

IF (NI-NOM)1,1,3
1 IF (NI-4)500,2,2
2 IF (EPS)500,500,10
3 NU=5
GO TO 1000

10 I1=1
12=1
13=1
KK=1

ENR10260
ENR10270
ENR10280
ENR10290

20 DO 320 I=1,12

13

30 DO 35 J=1,4
I4=I+J-1
D(IJ)=A(I4)
35 E(IJ)=B(I4)

14
15
16
17
18
19

07/31/65
INTERNAL FORMULA NUMBER(S)

SOURCE STATEMENT

EXTERNAL FORMULA NUMBER

ENRYCH

```

L1=0
40 IF (ABS(D(4)-D(1))-ABS(E(4)-E(1)))100,50,50
50 IF (D(2)-D(1))180,95,60
50 IF (D(3)-D(2))95,95,70
70 IF (D(4)-D(3))95,95,200
80 IF (D(3)-D(2))90,95,95
90 IF (D(4)-D(3))210,95,95
95 IF (L1)160,97,160
97 L1=1
100 IF (E(2)-E(1))130,150,110
110 IF (E(3)-E(2))150,150,120
120 IF (E(4)-E(3))150,150,220
130 IF (E(3)-E(2))140,150,150
140 IF (E(4)-E(3))230,150,150
150 IF (L1)160,152,160
152 L1=1
GO TO 50
C NOT MONOTONIC IN EITHER X OR Y
160 NU=2
L=1
GO TO 316
C
200 DO 205 J=1,4
F(J)=D(J)
205 G(J)=E(J)
MX=1
GO TO 240
210 DO 215 J=1,4
F(J)=-D(J)
215 G(J)=E(J)
MX=2
GO TO 240
220 DO 225 J=1,4
F(J)=E(J)
225 G(J)=D(J)
MX=3
GO TO 240
230 DO 235 J=1,4
F(J)=-E(J)
235 G(J)=D(J)
MX=4
240 CONTINUE

CALL OPTIM3 (F,G,EPS,M,Z,KK,L,MU)
MU = 0 IF F(1)=F(4) (NOT POSSIBLE)
MU = 1 IF SUCCESS
MU = 2 IF 199 PTS. GENERATED AND NOT DONE
250 IF (MU-1)251,260,251
251 NU=MU+1
GO TO 316

260 IF (L-1)275,275,265
265 IF ((F(13+1)-W(L))/(W(L)-W(L-1))-.2) 270,270,275
270 L=L-1

```

ENR10350 ,20
ENR10360 ,21
ENR10370 ,22
ENR10380 ,23
ENR10390 ,24
ENR10400 ,25
ENR10410 ,26
ENR10420 ,27
ENR10430 ,28
ENR10440 ,29
ENR10450 ,30
ENR10460 ,31
ENR10470 ,32
ENR10480 ,33
ENR10490 ,34
ENR10500 ,35
ENR10510 ,36
ENR10520 ,37
ENR10530 ,38
ENR10540 ,39
ENR10550 ,40
ENR10560 ,41
ENR10570 ,42
ENR10580 ,43
ENR10590 ,44
ENR10600 ,45
ENR10610 ,46
ENR10620 ,47
ENR10630 ,48
ENR10640 ,49
ENR10650 ,50
ENR10660 ,51
ENR10670 ,52
ENR10680 ,53
ENR10690 ,54
ENR10700 ,55
ENR10710 ,56
ENR10720 ,57
ENR10730 ,58
ENR10740 ,59
ENR10750 ,60
ENR10760 ,61
ENR10770 ,62
ENR10780 ,63
ENR10790 ,64
ENR10800 ,65
ENR10810 ,66
ENR10820 ,67
ENR10830 ,68
ENR10840 ,69
ENR10850 ,70

ENRYCH
07/31/65

EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
275	TA=L.0	ENR10840 ,71
	IF(MX-3)280,285,285	ENR10850 ,72
280	NA=1	ENR10860 ,73
	NB=0	ENR10870 ,74
	IF(MX-2)300,290,300	ENR10880 ,75
285	NA=0	ENR10890 ,76
	NB=1	ENR10900 ,77
	IF(MX-4)300,290,300	ENR10910 ,78
290	TA=-1	ENR10920 ,79
	NOM=NOM-L-L	ENR10930 ,80
300	IF (NOM)365,305,305	ENR10940 ,81
	DO 315 J=L,L	ENR10950 ,82
	NO=NO+2	ENR10960 ,83
	JA=NO-NA	ENR10970 ,84
	JB=NO-NB	ENR10980 ,85
	C(JA)=W(J)*TA	ENR10990 ,86
315	C(JB)=Z(J)	ENR10990 ,87
	GO TO 320	ENR10990 ,88
C	ERROR AT 160 OR 250. WRITE AND GO ON, WITHOUT ADDING NEW POINTS.	ENR11000 ,89
316	NU(3)=NU(3)-1	ENR11010 ,90
	IF (NU(3))321,321,317	ENR11020 ,91
317	LTAPE=NU(2)	ENR11030 ,92
	IF (LTAPE)321,321,318	ENR11040 ,93
318	WRITE (LTAPE,319)NU(1),EPS,NI,D,E	ENR11050 ,94
319	FORMAT(18H0ENRYCH ERROR CODE 12,34H FOR THE FOUR POINTS BELOW. EP	ENR11060 ,95
	15 = E12.4, 6H, NI = 14/4H X =4F20.9/4H Y =4F20.9)	ENR11070 ,96
321	NOM=NOM-2	ENR11080 ,97
	IF (NOM)365,323,323	ENR11090 ,98
323	NO=NO+1	ENR11100 ,99
	C(NO)=D(I3)	ENR11110 ,100
	NO=NO+1	ENR11120 ,101
	C(NO)=E(I3)	ENR11130 ,102
320	CONTINUE	ENR11140 ,103
330	IF (I3-2)340,350,360	ENR11150 ,104
340	I2=NI-3	ENR11160 ,105
	KK=2	ENR11170 ,106
	I3=2	ENR11180 ,107
	GO TO 20	ENR11190 ,108
350	I1=I2	ENR11200 ,109
	KK=3	ENR11210 ,110
	I3=3	ENR11220 ,111
	GO TO 20	ENR11230 ,112
360	IF (NOM-2)365,37C,370	ENR11240 ,113
365	NU=4	ENR11250 ,114
	GO TO 1000	ENR11260 ,115
370	C(NO+1)=A(NI)	ENR11270 ,116
		ENR11280 ,117

07/31/65
INTERNAL FORMULA NUMBER(S)

06/02/67

EVAL - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE EVAL (NI,XCPT,THKW)

C COMPUTES AERODYNAMIC INFLUENCE COEFFICIENTS MATRIX AND VELOCITY
C COMPONENTS MATRIX

ACOSH(U)=2.*ALOG(SORT(ABS((U-1.)/2.))+SORT(ABS((U+1.)/2.)))

COMMON DATE(2),NTAPEA,NTAPEB,NTAPEE,NTAPED,NTAPEE,NTAPEF,NTAPEI
1,NTAPEO,NBODY,NWING,XMACH,SYM,KACE

COMMON /BLOCK/ALPHAS(210),AREA(210),A(210),ALPHAC(110),ALPHAT(110)
C,CHORD(210)

I,ISYM

N,NPART(210),NPANEL,NROW(2)

T,THETA(210),TAIL

U,U(210)

V,V(210),VPM(210),VV(210),VPM(210)

W,W(210),WPM(210),WW(210),WPM(210)

X,X(210,3,4),XBAR(210),XC(210)

Y,Y(210,3,4),YBAR(210),YC(210)

Z,Z(210,3,4),ZBAR(210),ZC(210)

DIMENSION ASI(210),BBETAM(4),C(4),CPM(4),CPMM(4),Q(4)
1,PI(4),RPM(4),RPM(4),UU(210),US(210),VS(210),WS(210)
2,XCPT(210)

EPS=0.0001

BETA=SQRT(ABS(XMACH**2-1.))

PI=3.1415926

CONSTA=BETA/4.0

CONSTB=CONSTA/PI

CCNSTD=BETA/PI

IT=1

C INFLUENCING PANEL I

GO TO (1,980,3),KACE

1 NC=NPANEL/NROW(1)

NR=NROW(1)

GO TO 4

3 NC=NWING/NROW(2)

NR=NROW(2)

IF (THKW.NE.1.) GO TO 4

DC 34 I=1,NBODY

34 XCPT(I)=XC(I)

4 N=1

NCT=NI-1

DC 900 I=NI,NPANEL

5 IF(THKW)10,40,10

10 SL=1.0

```

1Y=1+I-NI-NR*(N-1)
I=(I+1)30,30,25

```

```

25 N=N+1

```

```

THKW=1.0

```

```

GO TO 40

```

```

30 THKW=-1.0

```

```

NCT=NCT+1

```

```

GO TO 40

```

```

35 SL=-1.0

```

```

THKW=1.0

```

```

40 COST=COS(THETA(I))

```

```

SINT=SIN(THETA(I))

```

```

TANA= TAN(ALPHA(I))

```

```

APR=BETA*TANA

```

```

IF(ABR-1.0)50,950,950

```

```

50 IF(ABS(ABR)-EPS)180,90,85

```

```

80 ABR=0.0

```

```

SA=1.0

```

```

GO TO 90

```

```

P5 SA=SIGN(1.,ABR)

```

```

on APR2=ABR*ABR

```

```

NPT=NPART(I)

```

```

C INFLUENCED PANEL J

```

```

DO 950 J=1,NPANEL

```

```

U(J)=0.0

```

```

V(J)=0.0

```

```

W(J)=0.0

```

```

VPM(J)=0.

```

```

WPM(J)=0.

```

```

VPMW(J)=0.

```

```

SINA=SIN(ALPHA(J))

```

```

COSA=COS(ALPHA(J))

```

```

DO 950N=1,NPT

```

```

BBETAM(1)=(X(I,M,2)-X(I,M,1))/(BETA*((Y(I,M,2)-Y(I,M,1))*COST

```

```

1+(Z(I,M,2)-Z(I,M,1))*SINT))

```

```

BBETAM(3)=(X(I,M,4)-X(I,M,3))/(BETA*((Y(I,M,4)-Y(I,M,3))*COST

```

```

1+(Z(I,M,4)-Z(I,M,3))*SINT))

```

```

BBETAM(2)=BBETAM(1)

```

```

BBETAM(4)=BBETAM(3)

```

```

C CORNER POINTS K OF INFLUENCING PANEL I

```

```

DO 910K=1,4

```

```

Q(K)=0.0

```

```

C(K)=0.0

```

```

Q(K)=0.0

```

```

RPM(K)=0.

```

```

CPM(K)=0.

```

```

RPMW(K)=0.

```

```

CPMW(K)=0.

```

```

RPM=BBETAM(K)

```

```

T=(THKW)99,99,91

```

45
47
49

69
71

```

91 IF(SL)2,99,93
92 IF(K-2)810,810,99
93 IF(K-2)99,99,810
99 IF(ABS(BPM)-EPS)105,105,100
100 SM=SIGN(1.0,BPM)
    GO TO 110
105 SM=1.0
    BPM=0.0
110 IF (ABS(ABS(BPM)-1.0)-EPS) 115,115,120
115 BPM=SM
120 BPM=SM*BPM
    BPM2=BPM*BPM
    CONSTC=1.+APM2*BPM2

```

C CONFIGURATION SYMMETRY CONDITION

```

DC ROOSIDE=1,ISYM
SM=(-1.0)*SIDE
DELTAT=THETA(I)*THETA(J)*SM
SINDT=SIN(DELTAT)
COSDT=COS(DELTAT)
DELTAY=SM*(-YC(J))-Y(I,M,K)
DELTAZ=ZC(J)-Z(I,M,K)
XPM=XCP(I,J)-X(I,M,K)
YPM=(DELTAY*COST+DELTAZ*SINT)*SM
ZPM=(DELTAY*SINT-DELTAZ*COST)*SINT
IF (ABS(ZPM)-EPS) 140,140,145
    ZPM=0.0
140 ZPM=0.0
145 SZ=SIGN(1.,ZPM)
    ZPM2=ZPM*ZPM
    IF (ABS(YPM)-EPS) 150,150,155
        YPM=0.0
150 YPM=0.0
155 SY=SIGN(1.,YPM)
    XIPM=XPM/BETA
    XIPM2=XIPM*XIPM
    YPM2=YPM*YPM
    IF (IPKM) 700,190,700
190 CONTINUE
    IF (ABR) 195,499,198

```

C VELOCITY COMPONENTS INDUCED BY PANELS NON-PARALLEL TO X- AXIS

```

195 APM=-AER
    ZPM=-ZBR
    GC TO 199
198 APM=ARR
    ZPM=ZBR
199 CONTINUE
    IF (XIPM-SQRT(YPM2+ZPM2)-EPS) 200,200,250
200 IF (BPM-1./SQRT(1.-APM2)) 205,205,550
205 TERMA=SQRT(1.-BPM2*(1.-APM2))
    TERMB=ZPM-APM*BPM*YPM
    TERPC=YPM+APM*BPM*ZPM

```

114
117
118

138
141
144

324	FTR1=ACOS(FTR1)*STERMC	198
325	IF (BPM-1./SQRT(TERMD))335,330,330	200
330	FTR2=ACOSH((BPM*XIPM-TERMF)/SQRT(TERME))	203
	GO TO 340	206
335	FTR2=(BPM*XIPM-TERMF)/SQRT(TERME)	211
	IF (FTR2<1.0) 339,339,336	
336	IF (FTR2-1.0) 337,338,338	
337	FTR2=-ACOS(FTR2)	
	GO TO 340	
338	FTR2=0.0	
	GO TO 340	
339	FTR2=-PI	
340	IF (YPM) 370,345,370	
345	IF (TERMC) 355,350,350	
350	FTR3=FTR1	
	GO TO 365	
355	IF (ZPM) 350,350,360	
360	FTR3=PI+FTR1	
365	FTR5=-APM2*8PM2*FTR3	
	GO TO 415	
370	IF (TERMB) 400,375,400	
375	IF (TERMA) 380,390,385	
380	IF (YPM) 385,390,395	
385	FTR3=0.0	
	GO TO 415	
390	FTR3=PI/2.0	
	GO TO 415	
395	FTR3=PI*STERMB	240
	GO TO 415	
400	FTR3=((1-XIPM*TERMF*8PM*(YPM2+ZPM2))/SQRT((YPM2+ZPM2)*TERME))	245
	IF (FTR3<1.0) 395,395,405	
405	IF (FTR3-1.0) 410,385,385	247
410	FTR1=ACOS (FTR3)*STERMB	
415	FTR3=FTR3*SIGN(1.-APM)	
	FTR4=SQRT(ABS(BPM2*TERMD-1.))	
	IF (YPM) 420,430,420	
420	FTR5=FTR3-FTR1*CONSTC	
	IF (YPM) 430,430,422	
422	IF (TERMC) 424,430,430	
424	IF (TERMB) 426,428,430	
426	FTR5=FTR5-2.*PI*CONSTC	
	GO TO 430	
428	FTR5=FTR5-PI*(2.+ABR2*8PM2)	
430	IF (YPM2+ZPM2) 435,440,435	261
435	FTR6=ACOSH(XIPM/SQRT(YPM2+ZPM2))	
	GO TO 445	
440	FTR6=1000.	
445	IF (TERMC) 455,450,455	
450	IF (YPM) 455,460,455	
455	FTR7=ACOSH(XIPM-APM*ZPM)/SQRT(TERMC2+TERMD*YPM2)*SQRT(TERMD)	269
	GO TO 465	270
460	FTR7=1000.	
465	FTR6=FTR6-CONSTC*FTR7	
	S=CONSTB/CONSTC*(APM*8PM*FTR4+FTR2+8PM*FTR3+FTR6/APM)	

```

D=CONSTB/CONSTC*(FTR4+FTR2-8PM+FTR6+FTR5/APH)*(-SA)
P=CONSTB*FTR1
IF (TERM) 795,470,795
470 P=PSA
GO TO 795

```

C VELOCITY COMPONENTS INDUCED BY PANELS PARALLEL TO X- AXIS

```

499 CONTINUE
ZPM=ZOR
TERMA=(XIPM-8PM*YPM)*2
TERMB=YPM*ZPM2
TERMC=SQRT(TERMB)
TERMD=8PM2-1.0
TERME=-TERMD
IF (RPM2-1.0) 500,560,560
500 IF (XIPM-TERMC)520,535,510
510 D=CONSTB*(SQRT(TERME)*ACOS((8PM*XIPM-YPM)/SQRT
1(TERMA+TERMD*ZPM2))+8PM*ACOSH(XIPM/TERMC)+
2YPM/TERMB*SQRT(XIPM2-TERMB))
GO TO 575
520 IF (YPM) 550,550,530
530 IF (XIPM-(8PM*YPM+SQRT(TERME)*ABS(ZPM))) 550,537,535
535 IF (YPM-8PM*XIPM)550,537,540
537 CT=.5
GO TO 545
540 CT=1.0
545 D=CONSTA*SQRT(TERME)*CT
S=CONSTA*8PM*SZ*CT
P=CONSTA*SZ*CT
GO TO 795
550 D=0.0
S=0.0
P=0.0
GO TO 795
560 IF (XIPM-TERMC) 550,550,570
570 D=CONSTB*(-SQRT(TERMD)*ACOSH((8PM*XIPM-YPM)
1/SQRT(TERMA+TERMD*ZPM2))+8PM*ACOSH(XIPM/TERMC)
2+YPM/TERMB*SQRT(XIPM2-TERMB))
575 IF (ZPM) 580,585,580
580 FACTOR= (-XIPM*YPM+8PM*TERMB)/SQRT(TERMB*
1(TERMA+TERMD*ZPM2))
IF (FACTOR+1.) 600,600,582
582 IF (FACTOR-1.) 584,590,590
584 FACTOR=ACOS(FACTOR)*SZ
GO TO 625
585 IF (YPM) 590,597,595
590 FACTOR=0.0
GO TO 625
595 IF (XIPM-8PM*YPM) 590,597,600
597 FACTOR=PI/2.
GO TO 625
600 FACTOR=PI*SZ
625 S=CONSTB*(8PM*FACTOR-ZPM/TERMB*SQRT(XIPM2-TERMB))
P=CONSTB*FACTOR
GO TO 795
700 CONTINUE

```

C VELOCITY COMPONENTS INDUCED BY WING SOURCES

```

ZPM=ZBR
TERMA=XIPM-BPM*YPM
TERMA=(XIPM-BPM*YPM)**2
TERMB=YPM**2+ZPM2
TERMC=SQRT(TERMB)
TERMD=BPM2-1.0
TERME=-TERMD
IF (XIPM-TERMC) 704,704,708
704 IF(TERMD)753,550,550
708 FTR1=ACOSH(XIPM/TERMC)
712 FTR2=ACOS((BPM*XIPM-YPM)/SQRT(TERMA+TERMD*ZPM2))/SQRT(TERME)
GO TO 724
716 FTR2=SQRT(XIPM2-TERMD)/(XIPM-YPM)
GO TO 724
720 FTR2=ACOSH(BPM*XIPM-YPM)/SQRT(TERMA+TERMD*ZPM2)/SQRT(TERMD)
724 IF (ZPM) 728,732,728
728 FTR3= (-XIPM*YPM+BPM*TERMD)/SQRT(TERMB*(TERMA+TERMD*ZPM2))
730 IF (FTR3+1.0) 748,748,730
730 IF (FTR3-1.0) 731,736,736
731 FTR3=ACOS(FTR3)*SZ
GO TO 750
732 IF (YPM) 736,736,740
736 FTR3=0.
GO TO 750
740 IF (XIPM-BPM*YPM) 736,744,748
744 FTR3=0.1/2.
GO TO 750
748 FTR3=PI*SZ
750 IF(ITHK)751,190,752
751 P= CONSTD*(TERMA*(FTR2+YPM*FTR1-ZPM*FTR3)/CHORDINCT)
S= CONSTD*(TERMA*(FTR1-BPM*FTR2)+BPM*ZPM*FTR3)
1-SORT(XIPM2-TERMD)/CHORDINCT)
D=CONSTD*(ZPM*(BPM*FTR1-TERMD*FTR2)-TERMA*FTR3)
1/CHORDINCT)
GO TO 795
752 P=FTR2/PI
S=-(FTR1-BPM*FTR2)/PI
D=FTR3/PI
GO TO 795
753 IF(YPM)550,550,756
756 IF (XIPM-TERMC) 760,764,708
760 IF (XIPM-BPM*YPM+SQRT(TERME)*ABS(ZPM)) 550,768,764
764 IF (YPM-BPM*XIPM) 550,768,772
768 CT=.5
GO TO 776
772 CT=1.

```

332

339 340 341

344

347 348

352

357

372

383

```

776 IF(THKW)777,190,778
777 P=((TERMAA/SQRT(ITERME))-ZPM*CT*SZ)*BETA/CHORD(NCT)
      S=BPMP
      D=BETA*(-ZPM*SQRT(ITERME)+TERMAA*CT*SZ)/CHORD(NCT)
      GO TO 795
778 P=CT/SQRT(ITERME)
      S=BPMP
      D=CT*SZ
393
395
399

795 CONTINUE
      SIM=1.
      R(K)=R(K)+S*SINDT*SIM
      C(K)=C(K)+D*CDSDT*SM*SIM
      Q(K)=Q(K)-P*SM*SIM
      RPH(K)=RPH(K)+S*SIM
      CPM(K)=CPM(K)+D*SM*SIM
      RPHM(K)=RPHM(K)-S*SM*SIM
      CPM(K)=CPM(K)-D*SM*SM*SIM
      GO TO 800
800 CONTINUE
810 CONTINUE
      U(J)=U(J)+(Q(1)-Q(2)-Q(3)+Q(4))/BETA
      V(J)=V(J)+(R(1)-R(2)-R(3)+R(4))
      W(J)=W(J)+(C(1)-C(2)-C(3)+C(4))
      VPM(J)=VPM(J)+(RPH(1)-RPH(2)-RPH(3)+RPH(4))
      WPM(J)=WPM(J)+(CPM(1)-CPM(2)-CPM(3)+CPM(4))
      VPMH(J)=VPMH(J)+(RPHM(1)-RPHM(2)-RPHM(3)+RPHM(4))
      WPMH(J)=WPMH(J)+(CPMH(1)-CPMH(2)-CPMH(3)+CPMH(4))
850 CONTINUE
      IF(THKW)865,855,865
855 DO 860 J=1,NPANEL
      U(J)=U(J)
      V(J)=VPMH(J)*COST-WPMH(J)*SINT
      W(J)=WPMH(J)*COST+VPMH(J)*SINT
860 A(J)=V(J)+W(J)
      GO TO 890
865 IF(ITT)880,880,870
870 DO 875 J=1,NPANEL
      US(J)=U(J)
      VS(J)=VPMH(J)*COST-WPMH(J)*SINT
      WS(J)=WPMH(J)*COST+VPMH(J)*SINT
875 AS(J)=V(J)+W(J)
      IF(ITT)890,890,5
880 DO 885 J=1,NPANEL
      U(J)=US(J)-U(J)*SL
      V(J)=VS(J)-(VPMH(J)*COST-WPMH(J)*SINT)*SL
      W(J)=WS(J)-(WPMH(J)*COST+VPMH(J)*SINT)*SL
885 AJ(J)=AS(J)-(V(J)+W(J))*SL
      IF(THKW)870,855,890

```


494
499

```
890 WRITE(NTAPEA)((AL(J),J=1,NPANEL)
  WRITE(NTAPEB)((UU(J),VV(J),WW(J),J=1,NPANEL)
  IF(I)900,895,900
895 IF(THRW)35.855,900
900 CONTINUE
```

513

```
GC TO 980
950 WRITE(NTAPEO,960)
960 FORMAT(1H0,41HERROR RETURN. WING LIES OUTSIDE MACH CONE)
GC TO 980
980 END FILE NTAPEA
END FILE NTAPEB
```

515

516

```
RETURN
END
```

08/08/67

EVAL1 - EFN SOURCE STATEMENT - IFN(S) -

EVAL1

SUBROUTINE EVAL1(NI, THKW, XC, YC, ZC, UF, VF, WF, NSTCP)
C COMPUTES AERODYNAMIC INFLUENCE COEFFICIENTS MATRIX AND VELOCITY
C COMPONENTS MATRIX
ACOSH(U)=2.*ALOG(SQRT(ABS((U+1.)/2.))+SQRT(ABS((U-1.)/2.)))
XCPT=XC

DIMENSION X(210,3,4), Y(210,3,4), Z(210,3,4), NROW(21), NPART(210)
DIMENSIONALPHAS(210), THETA(210)
DIMENSION XBB(50), R(50), WT(120),
COMMON /FLOV1/KACE, NPANEL, NBODY, NWING, NBODYS, NWINGS, NROW, XMACH, SYM
COMMON /FLOV2/X,Y,Z, NPART, ALPHAS, THETA, XBB, R, WT, T, TC, SST, CHORD
DIMENSION Y(50), TC(50), SST(210), CHORD(210)
DIMENSION C(4), Q(4), CPM(4), RPM(4), RPHM(4), CPMW(4), RBETAM(4)
EPS=0.0001
BETA=SQRT(ABS(XMACH**2-1.))
PI=3.1415926
CONSTA=BETA/4.0
CONSTB=CONSTA/PI
CONSTD=BETA/PI
IT=1
ISYM=1
IF(SYM.NE.0.) ISYM=2

JEL=1

C INFLUENCING PANEL I

UF=0.
VF=0.
WF=0.
GO TO (1,980,3), KACE
1 NC=NPANEL/NROW(1)
NR=NROW(1)
GO TO 4
3 NC=NWING/NROW(2)
NR=NROW(2)
4 N=1
NCT=NI-1
DO 900 I=NI, NSTOP
5 IF(THKW)10,40,10
10 SL=1.0
IT=1+1-NI-NR*(N-1)
IF(IT)30,30,25
25 N=N+1
THKW=1.0
GO TO 40
30 THKW=-1.0
NCT=NCT+1
GO TO 40
35 SL=-1.0

EVAL1

08/08/67

EVAL1 - FPN SOURCE STATEMENT - IFN(S) -

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```

THKW=1.0
40 COST=CCS(THETA(I))
   SINT=SIN(THETA(I))
   TANA=TAN(ALPHAS(I))
   ABR=BETA*TANA
   IF(ABR-1.0)50,95C,95C
50 IF(ABS(ABR)-EPS)80,9C,85
90 ABR=0.0
   SA=1.0
   GO TO 90
95 SA=SIGN(1.,ABR)
90 APM2=ABR*ABR
   NOT=NPART(I)

U=0.
V=0.
W=0.
VPM=0.
WPM=0.
VPMW=0.
WPMW=0.

```

C INFLUENCED PANEL J

```

ON RSDM=1,NPT
BETAM(1)=(X(I,M,2)-X(I,M,1))/(BETA*((Y(I,M,2)-Y(I,M,1))*COST
1*(Z(I,M,2)-Z(I,M,1))*SINT))
BETAM(3)=(X(I,M,4)-X(I,M,3))/(BETA*((Y(I,M,4)-Y(I,M,3))*COST
1*(Z(I,M,4)-Z(I,M,3))*SINT))
BETAM(2)=BETAM(1)
BETAM(4)=BETAM(3)

```

C CORNER POINTS K OF INFLUENCING PANEL I

```

ON RLOK=1,4
C(K)=0.0
Q(K)=0.0
RPM(K)=0.
CPM(K)=0.
RPMW(K)=0.
CPMW(K)=0.
BPM=BETAM(K)
IF(THKW)99,99,91
91 IF(SL)92,99,93
92 IF(K-2)90,91C,99
93 IF(K-2)99,95,910
99 IF(ABS(RPM)-EPS)105,105,10C
100 SW=SIGN(1.0,BPM)
   GO TO 110
105 SW=1.0
   BPM=0.0
110 IF(ABS(ABS(RPM)-1.0)-EPS) 115,115,12C
115 BPM=SW
120 BPM=SW*BPM

```

09/08/67

EVALI - EFN SOURCE STATEMENT - IFN(S) -

8PM2=8PM*8PM
CONSTC=1.+APM2*8PM2

C CONFIGURATION SYMMETRY CONDITION

DO 8)ISIDE=1,ISYM
SN=(-1,0)*ISIDE
DELTA1=THETA(I)
SINC1=SIN(DELTA1)
COS1=COS(DELTA1)
XPM=XCO1-X(1,M,K)
DELTA1=SN*(-YC)-Y(1,M,K)
DELTA2=ZC-Z(1,M,K)
YPM=(DELTA1+COS1+DELTA2*SINC1)*SM
ZBQ=DELTA2+COS1-DELTA1*SINC1
IF (ABS(ZBQ)-EPS) 140,140,145

140 ZBQ=0.0

145 SZ=SIGN(1.,ZBQ)

ZPM2=ZBQ*ZBQ

IF (ABS(YPM)-EPS) 150,150,155

150 YPM=0.0

155 SY=SIGN(1.,YPM)

XIPM=XPM/BETA

XIPM2=XIPM*XIPM

YPM2=YPM*YPM

IF (THKW) 700,150,700

190 CONTINUE

IF (ABR) 195,499,198

C VELOCITY COMPONENTS INDUCED BY PANELS NON-PARALLEL TO X- AXIS

195 APM=-APR

ZPM=-ZBR

GO TO 199

198 APM=ABR

ZPM=ZBR

199 CONTINUE

IF (XIPM-SQRT(YPM2+ZPM2)-EPS) 200,200,250

200 IF (3PM-1./SQRT(1.-APM2)) 205,550,550

205 TERMA=SQRT(1.-BPM2*(1.-APM2))

TERMB=ZPM-APM*8PM*YPM

TERMC=YPM+APM*8PM*ZPM

TERMD=1.+APM2*8PM2

IF ((18PM*TERMC+ABS(TERMB)+TERMA)/TERMD)-XIPM)210,210,550

210 IF (ZPM-APM*XIPM+EPS) 225,215,215

215 IF (YPM-8PM*XIPM*(1.-APM*TERMA)/TERMD)550,550,220

220 P=CONSTA

IF (ABS(ZPM-APM*XIPM)-EPS) 221,221,222

221 P=P*SA

222 D=CONSTA/CONSTC*(APM*8PM+TERMA)*SA

223 S=CONSTA/CONSTC*8PM*(1.-APM*TERMA)

GO TO 795

225 IF (YPM-8PM*XIPM*(1.+APM*TERMA)/TERMD)550,550,230

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05/08/67

EVAL1 - EFN SOURCE STATEMENT - IFN(S) -

```

339 FTR2=-PI
340 IF (YPM) 370,345,37C
345 IF (TERM) 355,35C,350
350 FTR3=FTR1
GO TO 365
355 IF (ZPM) 350,35C,36C
360 FTR3=PI+FTR1
365 FTR5=-APM2*BP2+FTR3
GO TO 415
370 IF (TERM) 400,375,40C
375 IF (TERMA) 380,38C,385
380 IF (YPM) 385,39C,395
385 FTR3=0.0
GO TO 415
390 FTR3=PI/2.0
GO TO 415
395 FTR3=PI*STERM
GO TO 415
400 FTR3=((-XIPM*TERM+BP2*(YPM2+ZPM2))/SQRT((YPM2+ZPM2)*TERM))
IF (FTR3+1.0) 395,395,405
IF (FTR3-1.0) 41C,385,385
405 FTR3=ACOS (FTR3)*STERM
410 FTR3=FTR3*SIGN(1.,APM)
415 FTR4=SQRT(ABS(BP2*TERM-1.))
IF (YPM) 420,430,42C
FTR5=FTR3-FTR1*CONSTC
IF (YPM) 430,430,422
422 IF (TERM) 424,43C,43C
424 IF (TERM) 426,428,42C
426 FTR5=FTR5-2.*PI*CONSTC
GO TO 430
FTR5=FTR5-PI*(2.+AP2*BP2)
430 IF (YPM2+ZPM2) 435,44C,435
435 FTR6=ACOSH(XIPM/SQRT(YPM2+ZPM2))
GO TO 445
440 FTR6=1000.
445 IF (TERM) 455,45C,455
450 IF (YPM) 455,46C,455
455 FTR7=ACOSH((XIPM-APM*ZPM)/SQRT((TERM2+TERM*YPM2))*SQRT(TERM))
GO TO 465
460 FTR7=1000.
465 FTR8=FTR6-CONSTC*FTR7
S=CONSTB/CONSTC*(APM*BP2*FTR2+BP2*FTR3+FTR4/APM)
D=CONST9/CONSTC*(FTR4*FTR2-BP2*FTR6*FTR5/APM)*(1.-SA)
P=CONST8*FTR1
IF (TERM) 795,47C,795
470 P=0.5A
GO TO 795

```

C VELOCITY COMPONENTS INDUCED BY PANELS PARALLEL TO X- AXIS

```

499 CONTINUE
ZPM=ZER
TERMA=(XIPM-BPM*YPM)**2

```

08/08/67

EVAL1 - EFN SOURCE STATEMENT - IFN(S) -

```

230 P=-CONSTA
    IF (TERMB) 235,240,235
235 S=-CONSTA/CONSTC*BPM*(1.+APM*TERMA)
    D=CONSTA/CONSTC*(1.-APM*BPM2+TERMA)*SA
    GO TO 795
240 S=-CONSTA/CONSTC*APM*TERMA*BPM
    D=CONSTA/CONSTC*TERMA*SA
    GO TO 795
250 TERMA=BPM*YPM-XIPM
    IF (ABS(TERMA)-EPS) 255,255,260
255 TERMA=0.0
260 TERMA2=TERMA*TERMA
    TERMB=APM*BPM*YPM-ZPM
    IF (ABS(TERMB)-EPS) 262,262,265
262 TERMB=0.0
    STERMB=1.0
    GO TO 270
265 STERMB=SIGN(1.0,-TERMB)
270 TERMB2=TERMB*TERMB
    TERMC=ZPM-APM*XIPM
    IF (ABS(TERMC)-EPS) 275,275,280
275 TERMC=0.0
    STERMC=1.0
    GO TO 285
280 STERMC=SIGN(1.0,TERMC)
285 TERMC2=TERMC*TERMC
    TERMD=1.-APM2
    TERME=TERPA2+BPM2+TERMC2-TERME2
    TERMF=YPM*APM*BPM*ZPM
    IF (XIPM-SORT(YPM2+ZPM2)) 550,550,298
298 IF (TERMC) 320,290,320
290 IF (TERMA) 300,305,310
300 IF (YPM) 310,305,315
305 FTR1=PI/2.
    GO TO 325
310 FTR1=0.0
    GO TO 325
315 FTR1=PI*STERMC
    GO TO 325
320 FTR1=(YPM*(TERMA-APM*TERMB)+BPM*TERMC2)/SORT
    1((TERMC2+TERMD*YPM2)*TERME)
    IF (FTR1+1.0) 315,315,322
322 IF (FTR1-1.0) 324,310,310
324 FTR1=ACOS(FTR1)*STERMC
325 IF (BPM-1./SORT(TERMC2)) 335,330,330
330 FTR2=ACOSH((BPM*XIPM-TERMF)/SORT(TERME))
    GO TO 340
335 FTR2=(BPM*XIPM-TERMF)/SORT(TERME)
    IF (FTR2+1.0) 339,339,336
336 IF (FTR2-1.0) 337,337,336
337 FTR2=-ACOS(FTR2)
    GO TO 340
338 FTR2=0.0
    GO TO 340

```

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08/08/67

EVAL1 - EFN SOURCE STATEMENT - IFN(S) -

```

TERPB=YPM2+ZPM2
TERMC=SQRT(TERMB)
TERPD=BPm2-1.0
TERPE=-TERMD
IF (BPm2-1.0) 500,560,560
500 IF (XIPM-TERMC) 520,535,510
510 D=CONSTB*(SQRT(TERME)*ACOS((BPm*XIPM-YPM)/SQRT
1(TERMA+TERMD+ZPM2))+BPm*ACOSH(XIPM/TERMC)+
2YPM/TERMB*SQRT(XIPM2-TERMB))
GO TO 575
520 IF (YPM) 550,550,530
530 IF (XIPM-(BPm*YPM+SQRT(TERME)*ABS(ZPM))) 550,537,535
535 IF (YPM-BPm*XIPM) 550,537,540
537 CT=5
GO TO 545
540 CT=1.0
545 D=CONSTA*SQRT(TERME)*CT
S=CONSTA*BPm*SZ*CT
P=CONSTA*SZ*CT
GO TO 795
550 C=0.0
S=0.0
P=0.0
GO TO 795
560 IF (XIPM-TERMC) 550,550,570
570 D=CONSTB*(-SQRT(TERMD)*ACOSH((BPm*XIPM-YPM)
1/SQRT(TERMA+TERMD+ZPM2))+BPm*ACOSH(XIPM/TERMC)
2+YPM/TERMB*SQRT(XIPM2-TERMB))
575 IF (ZPM) 580,585,580
580 FACTOR= (-XIPM*YPM+BPm*TERMB)/SQRT(TERMB*
1(TERMA+TERMD+ZPM2))
IF (FACTOR+1.) 600,600,582
IF (FACTOR-1.) 584,590,590
584 FACTOR=ACOS(FACTOR)*SZ
GO TO 625
585 IF (YPM) 590,597,555
590 FACTOR=0.0
GO TO 625
595 IF (XIPM-BPm*YPM) 590,597,600
597 FACTOR=PI/2.
GO TO 625
600 FACTOR=PI*SZ
625 S=CONSTB*(BPm*FACTOR-ZPM/TERMB*SQRT(XIPM2-TERMB))
P=CONSTB*FACTOR
GO TO 795
700 CONTINUE

```

C VELOCITY COMPONENTS INDUCED BY WING SOURCES

```

ZPM=ZBR
TERMA=XIPM-BPm*YPM
TERMB=(XIPM-BPm*YPM)**2
TERMB=YPM2+ZPM2

```

08/08/67

EVAL1 - EFN SOURCE STATEMENT - IFN(S) -

```

TERMC=SQRT(TERMB)
TERMD=PPM2-1.0
TERME=-TERMC
IF (XIPM-TERMC) 704,704,708
704 IF(ITERMD)753,550,550
708 FTR1=ACOSH(XIPM/TERMC)
IF (ITERMD) 712,716,720
712 FTR2=ACOSH((BPM*XIPM-YPM)/SQRT((TERMA+TERMD*ZPM2)))/SQRT(TERME)
GO TO 724
716 FTR2=SQRT(XIPM2-TERMB)/(XIPM-YPM)
GO TO 724
720 FTR2=ACOSH((BPM*XIPM-YPM)/SQRT((TERMA+TERMD*ZPM2)))/SQRT(TERMD)
724 IF (ZPM) 728,732,728
728 FTR3= (-XIPM*YPM+8PM*TERMP)/SQRT(TERMB*(TERMA+TERMD*ZPM2))
IF (FTR3+1.0) 748,748,730
730 IF (FTR3-1.0) 731,736,736
731 FTR3=ACOS(FTR3)*SZ
GO TO 750
732 IF (YPM) 736,736,740
736 FTR3=0.
GO TO 750
740 IF (XIPM-8PM*YPM) 736,744,748
744 FTR3=PI/2.
GO TO 750
748 FTR3=PI*SZ
750 IF (THKW)751,190,752
751 P= CONSTD*(TERMAA+FTR2+YPM*FTR1-ZPM*FTR3)/CHORD(NCT)
S=-CONSTD*(TERMAA*(FTR1-8PM*FTR2)+8PM*ZPM*FTR3
1-SQRT(XIPM2-TERMB))/CHORD(NCT)
D=-CONSTD*(ZPM*(8PM*FTR1-TERMD*FTR2)-TERMAA*FTR3)
1/CHORD(NCT)
GO TO 795
752 P=FTR2/PI
S=-(FTR1-8PM*FTR2)/PI
D=FTR3/PI
GO TO 795
753 IF (YPM)550,550,756
756 IF (XIPM-TERMC) 760,764,709
760 IF (XIPM-(8PM*YPM+SQRT(TERME)*ABS(ZPM))) 550,768,764
764 IF (YPM-8PM*XIPM) 550,768,772
768 CT=.5
GO TO 776
772 CT=1.
776 IF (THKW)777,190,778
777 P=(TERMAA/SQRT(TERME)-ZPM*CT*SZ)*BETA/CHORD(NCT)
D=BETA*(-ZPM*SQRT(TERME)+TERMAA*CT*SZ)/CHORD(NCT)
GO TO 795
778 P=CT/SQRT(TERME)
S=8PM*P
D=CT*SZ

```

795 CONTINUE

09/08/67

EVAL1 - EFN SOURCE STATEMENT - IFN(S) -

```

796 IF (ISIDE-1) 796,796,797
    SIM=1.
    GO TO 799
797 IF (THKW) 796,798,796
798 SIM=SYM
799 CONTINUE

Q(K)=Q(K)-P*SM*SIM
RPM(K)=RPM(K)+S*SIM
CPM(K)=CPM(K)+D*S*SIM
RPM(K)=RPM(K)-S*SN*SIM
CPM(K)=CPM(K)-D*S*SN*SIM
900 CONTINUE
910 CONTINUE

U=U+(Q(1)-Q(2)-Q(3)+Q(4))/BETA
VPM=VPM+(RPM(1)-RPM(2)-RPM(3)+RPM(4))
WPM=WPM+(CPM(1)-CPM(2)-CPM(3)+CPM(4))
VPM=VPM+(RPM(1)-RPM(2)-RPM(3)+RPM(4))
WPM=WPM+(CPM(1)-CPM(2)-CPM(3)+CPM(4))
850 CONTINUE

IF (THKW) 865,855,865
855 CONTINUE
UU=U
VV=VPM*CCST-WPM*SINT
WW=WPM*CCST+VPM*SINT
GO TO 890

965 IF (IT) 880,880,87C
870 CONTINUE
US=U
VS=VPM*CCST-WPM*SINT
WS=WPM*CCST+VPM*SINT
IF (IT) 890,890,5
890 CONTINUE
UU=US-U*SL
VV=VS-(VPM*CCST-WPM*SINT)*SL
WW=WS-(WPM*CCST+VPM*SINT)*SL
IF (THKW) 870,855,850
890 CONTINUE
IF (THKW,NE,0.) GO TC 8591
UF=UF+UU*SST(1)
VF=VF+VV*SST(1)
WF=WF+WW*SST(1)
GO TO 8992
8991 UF=UF+UU*WT(JEL)
VF=VF+VV*WT(JEL)
WF=WF+WW*WT(JEL)
JEL=JEL+1
8992 CONTINUE
IF (IT) 899,895,899
895 IF (THKW) 35,855,859

```

08/08/67

EVAL1 - EFN SOURCE STATEMENT - IFN(S) -

899 CONTINUE
900 CONTINUE

GO TO 980

950 WRITE(NTAPE,960)
960 FORMAT(1H0,41HERROR RETURN. WING LIES OUTSIDE MACH CONE)

429

980 CONTINUE
RETURN
END

\$TEXT FASNCS

FASNOOD

```
*ASMCS      I8JOB LIBRARY / ASIN AND ACOS  
ADAPTED FROM SHARE SUBROUTINE B1 CL ASCI  
CONVERTED TO IBMPL / 1-9-63 / E. WRIGHT - BOEING  
METHODS MEMO 7090-49
```

A-SIN (B)
A-ACOS (B)

ENTRY ASIN
ENTRY ACOS

```
ASIN0010  
ASIN0020  
ASIN0030  
ASIN0040  
ASIN0050  
ASIN0060  
ASIN0070  
ASIN0080  
ASIN0090  
ASIN0100  
ASIN0110  
ASIN0120  
ASIN0130  
ASIN0140  
ASIN0150  
ASIN0160  
ASIN0170  
ASIN0180
```

PRIMARY CARD (NOT PUNCHED)

00000	0600	00	0	04013	10011
00001	0020	00	C	00003	10001
00002	4625	00	0	04013	10011
00003	1	0000	C	00006	10001
00004	0774	00	4	00000	10000
00005	0020	00	4	00001	10000
00006	0634	00	4	07000	10011
00007	0634	00	4	00004	10001
00010	0634	00	4	00121	10001
00011	0500	60	4	00003	10000
00012	0601	00	C	04015	10011
00013	0500	00	C	00123	10001
00014	0306	00	0	04015	10011
00015	0601	00	0	04014	10011
00016	4120	00	C	00073	10001
00017	0500	00	C	04015	10011
00020	0520	00	C	04013	10011
00021	0020	00	0	00034	10001
00022	0560	00	0	00124	10001

PRIMARY CARD (NOT PUNCHED)

Card	Unit	Punched
000023	0760	000003
000024	0040	000015
000025	0500	000027
000026	0000	000026
000027	0500	000405
000030	0560	000125
000031	0765	000000
000032	0760	000002
000033	0020	000037
000034	0560	000126
000035	0120	000037
000036	0000	000001

ASIN0190
ASIN0200
ASIN0210
ASIN0220

ASIN0230
ASIN0240
ASIN0250
ASIN0260
ASIN0270
ASIN0280
ASIN0290
ASIN0300
ASIN0310
ASIN0320
ASIN0330

ASIN0340
ASIN0350
ASIN0360
ASIN0370
ASIN0380
ASIN0390
ASIN0400
ASIN0410
ASIN0420
ASIN0430
ASIN0440

ASIN	STZ	BEANIE	ASIN ENTRY
ACOS	TRA	PETUN	ACOS ENTRY
PETUN	STL	BEANIE	
	SAVEN		

SXA	LK.DR.4
CLA*	3.4
STO	X
ASIN3	
CL A	=1.0
X	
FSM	X
STD	TEMP
TMI	Error
CL A	
ZET	BEANIE
TRA	ACOSI
CSN6	-0.7171400000000
GET ARGUMENT X	
STORE X	
1 - ABS X	
WAS ENTRY ASIN OR ACOS	
2(-8) = -.00390625	

SPP		ASINIO	X EQUALS ARCSIN X
TLO		X	
CLA		PETUN	
RETURN		X	
ASINIO	CLA	=1.57079633	P I / 2
LQO		O	+ OR -- P I / 2
LRS			-X
CMS		ASIN23	ZERO
TRA		=O	
ACOSI	LQO	ASIN23	
TPL			

FASNC'S
ASSEMBLED TEXT.

00036	0560	00	0	00127	10001	LDQ	-3.14159265	PI	ASIN0490
00037	4600	00	C	04012	10011	ASIN23 STQ	A	A	ASIN0460
00040	0601	00	0	04013	10011	STQ	BEANIE	PLUS OR MINUS (8)	ASIN0470
00041	000C0000C000	00010				CALL	SQRT(TEMP)	SQUARE ROOT (1-ABS X)	ASIN0480
00041	0074	00	4	06000	10011				
00042	1	00001	C	01003	10011				
00043	0	00121	0	00072	10100				
00044	0	00000	0	04014	10011				

BINARY CARD (NOT PUNCHED)

00045	0560	00	0	04013	10011	LDQ	BEANIE		ASIN0490
00046	0763	00	C	00000	10000	LLS	0		ASIN0500
00047	0601	00	0	04013	10011	STQ	BEANIE	PLUS OR MINUS 8 SQRT (1-ABS X)	ASIN0510
00050	0560	00	0	04015	10011	LDQ	X	X	ASIN0520
00051	0763	00	C	00010	10000	LLS	8	GET CHARACTERISTIC	ASIN0530
00052	0734	00	4	00000	10000	PAX	0.4	PLACE IN TR4	ASIN0540
00053	4754	0C	C	00000	10000	ZAC			ASIN0550
00054	0765	00	4	00200	10000	LRS	128.4	SHIFT(128 - POWER)MODULO 256	ASIN0560
00055	4600	00	0	04015	10011	STQ	X	X IN FIXED POINT	ASIN0570
00056	0500	00	C	00101	10001	CLA	A8	A8	ASIN0580
00057	0774	00	4	00010	10000	AXT	8.4		ASIN0590
00060	0131	00	C	00000	10000	ASIN41 XCA			ASIN0600
00061	4200	00	0	04015	10011	MPR	X	TIMES X	ASIN0610
00062	0400	00	4	00112	10001	ADD	A0+1.4	PLUS A(1)	ASIN0620
00063	2	00001	4	00060	10001	TIX	ASIN41.4.1		ASIN0630
00064	0765	00	C	00010	10000	LRS	8		ASIN0640
00065	0760	00	C	00010	10000	RND			ASIN0650
00066	0400	00	C	00130	10001	ADD	-12988	FLOAT	ASIN0660
00067	0131	00	C	00000	10000	XCA			ASIN0670

BINARY CARD (NOT PUNCHED)

00070	0260	00	C	04013	10011	FMP	BEANIE	TIMES 8 SQRT (1-ABS X)	ASIN0680
00071	0300	00	C	04012	10011	FAD	A	PLUS A	ASIN0690
				00072		RETURN	PETUN	EXIT	ASIN0700

00073	000000000000	00010				ERROR CALL	.FXEM.(8AIL)	CALL ERROR EXECUTION MONITOR	ASIN0710
00073	0074	00	4	05000	10011				ASIN0720
00074	1	00001	C	01003	10011				ASIN0730
00075	0	00121	C	00136	10100				ASIN0740
00076	0	00000	C	00112	10001				
00077	0500	00	C	00123	10001				
00100	0020	00	0	00012	10001				

00101	000076257520	10000				CLA	-1.0	SET ARGUMENT TO ONE	ASIN0750
00102	400507371460	10000				TRA	ASIN3		ASIN0760
00103	0	01472	4	40066	10000				ASIN0770
00104	402641537160	10000							ASIN0780
00105	004173275020	10000							ASIN0790
00106	406374356540	10000							ASIN0800
00107	013313544557	10000							ASIN0810
									ASIN0820
									ASIN0830
									ASIN0840
									ASIN0850
									ASIN0860

FASACS
ASSEMBLED TEXT.

```

00110 433360112561 10000 OCT -033360112561 A1 ASIN0870
00111 311037552421 10000 OCT 311037552421 A0 ASIN0880

BINARY CARD (NOT PUNCHED)
00112 000000000101 10000 BAIL DEC 65 ASIN0881
00113 0 00002 C 00115 10001 PZE MESA,,2 ASIN0882
00114 0 00002 C 00117 10001 PZE MESB,,2 ASIN0883
00115 002151276027 10000 MESA 8CI 2.0ARG GT ONE ASIN0884
00116 636046452560 10000 MESB 8CI 2.0ARG = 1 ASIN0885
00117 002151276013 10000 * ASIN0890
00120 600160606060 10000 * ASIN0900
* ASIN0910
* ASIN0920
* ASIN0930

00121 000000000000 10000 LK-DR LDIR
00122 262162452362 10000 LONG
00123 201400000000 10000
00124 171400000000 10000
00125 201622071325 10000
00126 000000000000 10000
00127 202622071325 10000
00130 201000000000 10000

* ASIN0940
* ASIN0950
* ASIN0960
* ASIN0970
* ASIN0980
* ASIN0990
* ASIN1000
* ASIN1010

00131 100000000001 00001 ERASE CONTRL ER
00131 200000000001 00001 USE ER
00143 200000000001 00001 BSS 10
00144 200000000001 00001 A BSS 1
BEANIE BSS 1 RESERVE FOR SORT

BINARY CARD (NOT PUNCHED)
00145 200000000001 00001 TEMP BSS 1
00146 200000000001 00001 X BSS 1
00147 200000000001 00001 BSS 6

* ASIN1020
* ASIN1030
* ASIN1040
* ASIN1050
* ASIN1060
* ASIN1070
* ASIN1080

```

00000 01111

END

FASNC
CONTROL DICTIONARY

SCDXT FASNC.

FASN0002

BINARY CARD (NOT PUNCHED)	PREFACE	START=0,LENGTH=109,TYPE=7094,CPLX=5
000155000000	FASNC S DECK	LOC=0,LENGTH=109
000004000005	ASIN REAL	LOC=0,LENGTH=0
262162452362	ACOS REAL	LOC=2,LENGTH=0
000155000000	ERASE REAL	LOC=131,LENGTH=20
216231456060	-FXEM. VIRTUAL	SECT. 5,CALL
000000000000	SORT VIRTUAL	SECT. 6,CALL
212346626060	SYSLOC VIRTUAL	SECT. 7
000000000002		
255121622560		
000024000131		
332667254433		
200000100000		
625031636060		
200000100000		
627042434623		
200000000000		

FASN0003

SDKEND FASNC

NO MESSAGES FOR THIS ASSEMBLY

EXAMPLES
TEXT.

TEXT FATN1

```
* SINGLE-VALUED ARCTANGENT FUNCTION / ATN1
* SHARE SUBROUTINE BI GM ATN1
* METHODS MEMO 7090-45
```

ENTRY ATN1

[illegible]

STRT SAVEN 2, I

	ATN10190
SXA	LNKG,4
CLA*	4,4
XCA	
CLA*	3,4
STO	COMMON
TRA	BGN
TNA	SIRT
ATN10200	
ATN10210	
ATN10220	
ATN10230	
ATN10240	
ATN10250	

	BINARY	CARD (NOT PUNCHED)	BGN	STJ	COMMON-1 ATN1+19 27	STORE X	ATN10261
		00023 4500 00 0 03022	10011	STJ			ATN10270
		00024 0100 00 0 02023	10011	TZE			ATN10280
		00025 0771 00 0 00033	10000	ARS	CHAR. IN ACC EQUALS P		ATN10290
		00026 0760 00 0 00033	10000	SSP			ATN10300
		00027 0501 00 0 03020	10011	STD	CHAR. OF Y		ATN10310
		00030 0500 00 0 03022	10011	CLA			ATN10320
		00031 0100 00 0 02025	10011	TZE			ATN10330
		00032 3771 00 0 00033	10000	SPP	CHAR. OF X IN ACC EQUALS Q		ATN10340
		00033 0750 00 0 00003	10000	SSP	Q-P		ATN10350
		00034 0402 00 0 04020	10011	SU3	Q-P-1		ATN10360
		00035 0402 00 0 07147	10011	SUB			ATN10370
		00036 0801 00 0 03017	10011	STD			ATN10380
		00037 0760 00 0 00003	10000	SSP	ARS VALUE OF ABOVE		ATN10390
		00040 0402 00 0 02164	10011	SU3	I Q-P-1 I-128		ATN10400
		00041 4120 00 0 02027	10011	TMI	XFER IF IN RANGE		

STRE X

CHAR. IN ACC. EQUALS P.

CHAR. OF Y

CHAR. OF X IN ACC EQUALS Q

Q-Q

Q-P-1

ABS VALUE OF ABOVE

I Q-9-1 I-128

XFER. IF IN RANGE

FATNI
ASSEMBLED TEXT.

07/31/65

00042	0500	00	0	03020	10011	CLA	COMMON-3	Q-P	ATN10410
00043	0402	00	0	02164	10011	SUB	ATN1+115	Q-P-128	ATN10420
00044	0120	00	0	02025	10011	TPL	ATN1+21	XFER IF Y/X WOULD O-LOW	ATN10430
00045	4754	00	0	00000	10000	PXD	0,0	ZERO ACC, IF Y/X IS ZERO	ATN10440
BINARY CARD (NOT PUNCHED)									
00046	0020	00	0	02122	10011	TRA	ATN1+82	SET Z EQUALS ZERO	ATN10450
00047	0500	00	0	02146	10011	CLA	ATN1+102	PI/2, IF Y/X IS INF.,	ATN10460
00050	0020	00	0	02122	10011	TRA	ATN1+82	SET Z EQUALS PI/2	ATN10470
00051	0500	00	0	03022	10011	CLA	COMMON-1	X	ATN10480
00052	0300	00	0	02145	10011	FAD	ATN1+101	NORMALIZE	ATN10490
00053	0601	00	0	03021	10011	STD	COMMON-2	Y	ATN10500
00054	0500	00	0	03023	10011	CLA	COMMON	Y/X	ATN10510
00055	0241	00	0	03021	10011	FDP	COMMON-2		ATN10520
00056	4600	00	0	03021	10011	STD	COMMON-2		ATN10530
00057	0500	00	0	03021	10011	CLA	COMMON-2	ABS VAL OF Y/X	ATN10540
00060	0760	00	0	00003	10000	SSP	COMMON-2	EQUALS W	ATN10550
00061	0601	00	0	03021	10011	STD	COMMON-2		ATN10560
00062	0760	00	0	00000	10000	CLM	COMMON-8	SET SW1 TO ZERO	ATN10570
00063	0601	00	0	03013	10011	STD	COMMON-4	Q-P-1	ATN10580
00064	0500	00	0	03017	10011	CLA	COMMON-4	ABS VALUE	ATN10590
00065	0760	00	0	00003	10000	SSP	ATN1+118	I Q-P-1 I-10	ATN10600
00066	0402	00	0	02166	10011	SUB	ATN1+43	XFER IF W BETWEEN 2*-10+2**10	ATN10610
00067	4120	00	0	02053	10011	TMI	ATN1+103	1	ATN10620
00070	0500	00	0	02147	10011	CLA	ATN1+103		ATN10630
BINARY CARD (NOT PUNCHED)									
00071	0601	00	0	03013	10011	STD	COMMON-8	RESET SW1 TO 1	ATN10640
00072	0500	00	0	03017	10011	CLA	COMMON-4	Q-P-1	ATN10650
00073	0120	00	0	02064	10011	TPL	ATN1+52	XFER IF W GTR THAN 2**10	ATN10660
00074	0020	00	0	02056	10011	TRA	ATN1+46	XFER IF W LS THAN 2*-10	ATN10670
00075	0500	00	0	03021	10011	CLA	COMMON-2	W	ATN10680
00076	0302	00	0	02150	10011	FSB	ATN1+104	W-1	ATN10690
00077	0120	00	0	02064	10011	TPL	ATN1+52	XFER IF W GTR THAN 1	ATN10700
00100	0500	00	0	02146	10011	CLA	ATN1+102	PI/2	ATN10710
00101	0601	00	0	03014	10011	STD	COMMON-7	SET SW2 TO PI/2	ATN10720
00102	0500	00	0	02150	10011	CLA	ATN1+104	1. IF W LS THAN 1, USE 1/W,	ATN10730
00103	0241	00	0	03021	10011	FDP	COMMON-2	1/W + SUBT VALUE FROM PI/2	ATN10740
00104	4600	00	0	03021	10011	STD	COMMON-2	XFER TO POLYNOM	ATN10750
00105	0020	00	0	02066	10011	TRA	ATN1+54	ZERO ACC	ATN10760
00106	4754	00	0	00000	10000	PXD	0,0	SET SW2 TO ZERO	ATN10770
00107	0601	00	0	03014	10011	STD	COMMON-7	SW1	ATN10780
00110	0500	00	0	03013	10011	CLA	COMMON-8	IF NOT ZERO, BYPASS POLYNOM.	ATN10790
00111	4100	00	0	02117	10011	TNZ	ATN1+79	W	ATN10800
00112	0500	00	0	03021	10011	CLA	COMMON-2	W+1	ATN10810
00113	0300	00	0	02150	10011	FAD	ATN1+104		ATN10820
BINARY CARD (NOT PUNCHED)									
00114	0601	00	0	03017	10011	STD	COMMON-4	W-1	ATN10830
00115	0302	00	0	02151	10011	FSB	ATN1+105	IF ZERO, Z EQUALS PI/4	ATN10840
00116	0100	00	0	02115	10011	TZE	ATN1+77	W-1/W+1 EQUALS P	ATN10850
00117	0241	00	0	03017	10011	FDP	COMMON-4		ATN10860
00120	4600	00	0	03020	10011	STD	COMMON-3	R#R	ATN10870
00121	0260	00	0	03020	10011	FMP	COMMON-3		ATN10880

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FATNI
ASSEMBLED TEXT.

00122	9601	00	0	03017	10011	STO	COMMON-4	ATN10890
00123	0761	00	0	00000	10000	NOP		ATN10900
00124	0534	00	2	02152	10011	LXA	ATN1+106,2	ATN10910
00125	0500	00	0	02153	10011	CLA	ATN1+107	ATN10920
00126	0601	00	0	03015	10011	STO	COMMON-6	ATN10930
00127	0560	00	0	03015	10011	LDQ	COMMON-6	ATN10940
00128	0269	00	0	03017	10011	FMP	COMMON-4	ATN10950
00129	0300	00	2	02163	10011	FAD	ATN1+115,2	ATN10960
00130	0300	00	2	02163	10011	TIX	ATN1+68,2,1	ATN10970
00131	0761	00	0	00000	10000	NOP	COMMON-5	ATN10980
00132	0601	00	0	03016	10011	STO	COMMON-5	ATN10990
00133	0560	00	0	03016	10011	LDQ	COMMON-5	ATN11000
00134	0260	00	0	03020	10011	FMP	COMMON-3	ATN11010

BINARY CARD (NOT PUNCHED)

00137	0300	00	0	02163	10011	FAD	ATN1+115	T*PI/4	ATN11020
00140	0601	00	0	03021	10011	STO	COMMON-2	EQUALS Z	ATN11030
00141	0500	00	0	03014	10011	CLA	COMMON-7	TEST SM2 EQU. 0 OR PI/2	ATN11040
00142	0100	00	0	02123	10011	TZE	ATN1+83	XFER IF Z=0	ATN11050
00143	0302	00	0	03021	10011	FSB	COMMON-2	PI/2-Z	ATN11060
00144	0601	00	0	03021	10011	STO	COMMON-2	PORPER 1ST QUAD Z NOW IV CMW+2	ATN11070
00145	0567	00	0	03023	10011	LDQ	COMMON	Y INST 83-100 ADJUST Z TO	ATN11080
00146	0260	00	0	03022	10011	FMP	COMMON-1	Y*X	ATN11090
00147	0120	00	0	02136	10011	TPL	ATN1+94	XFER IF SAME SIGN	ATN11100
00150	0500	00	0	03022	10011	CLA	COMMON-1	X	ATN11110
00151	0120	00	0	02132	10011	TPL	ATN1+90	XFER IF X+,Y-4TH QUAD.	ATN11120
00152	0500	00	0	02165	10011	CLA	ATN1+117	PI	ATN11130
00153	0020	00	0	02134	10011	TRA	ATN1+92	PI	ATN11140
00154	0500	00	0	02165	10011	CLA	ATN1+117	4TH QUAD	ATN11150
00155	0300	00	0	02165	10011	FAD	ATN1+117	2*PI	ATN11160
00156	0302	00	0	03021	10011	FSB	COMMON-2	-Z	ATN11170
				00157		RETURN	STRT	X	ATN11180
00160	0500	00	0	03022	10011	CLA	COMMON-1	XFER IF X+,Y+,1ST QJAD	ATN11190
00161	0120	00	0	02143	10011	TPL	ATN1+99		ATN11200

BINARY CARD (NOT PUNCHED)

00162	0500	00	0	02165	10011	CLA	ATN1+117	PI	ATN11210
00163	0300	00	0	03021	10011	FAD	COMMON-2	+Z	ATN11220
				00164		RETURN	STRT		ATN11230
00165	0500	00	0	03021	10011	CLA	COMMON-2	Z	ATN11240
				00166		RETURN	STRT		ATN11250

* * * * *

00167	0000	00	0	00000	10000	HTR	0	FIRST PROGRAM CONSTANT	ATN11260
00170	201622077325				10000	DEC	1.57079633,1,1.2,7,-.004054058,.0218612288		ATN11270
00171	000000000001				10000				ATN11280
00172	201400000000				10000				ATN11290
00173	202400000000				10000				ATN11300
00174	000000000007				10000				
00175	571411537472				10000				
00176	173546131217				10000				
00177	574712007036				10000				
00200	175617737372				10000				ATN11310

FATNI
ASSEMBLED TEXT.

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FATN1
CONTROL DICTIONARY

07/31/65

SCDICT FATN1

FATN0302

BINARY CARD (NOT PUNCHED)
000235000000
00000400005
262163450160
000235000000
216345016060
000000000022
255121622560
000024000211
627062434623
200000000000

PREFACE
FATN1 DECK
ATN1 REAL
ERASE REAL
SYSLOC VIRTUAL
START=0,LENGTH=157,TYPE=7094,CPLX=5
LOC=0,LENGTH=157
LOC=22,LENGTH=0
LOC=211,LENGTH=20
SECT. 4

\$DKEND FATN1

FATN0303

NO MESSAGES FOR THIS ASSEMBLY

05/22/67

FCALC - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE FCALC

```

C
C
C      CONTR'L SUBROUTINE FOR CALCULATION OF FORCES, MOMENTS
C      AND PRESSURES
      COMMON DATE(2),NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI
      1,NTAPEQ,NBODY,NWING,XNACH,SYM,KACE

      COMMON /AVAR/  A(210),AC9(21),ABX(100),AWX(110),AREA(210),ARM(2),A
      RMT(20),ALPHA(210),ALPHAB(210),ALPHAS(210),ALPHAT(1
      10),ALPHAW(110),ALPHAX(110),AWS(110)
      A      .ALPHA,ALPHAD,ARA,ARADEG,ARB,ARW,ARAS,AT,AAA
      COMMON /BVAR/  B(210)
      B      .BCL,BCC,BCCM
      COMMON /CVAR/  C(210),CHORD(210),CL(210),CPBB(55,10),CPHN(55,10,2)
      C      .CLS(210)
      C      .CDR,CASE,CPCALC,CBAR,CONSNT,CLBAR,CLX,CLP,COM
      COMMON /DVAR/  D(210),DZDX(55)
      D      .DADFG,DARAD
      COMMON /IVAR/  IPOLAR
      COMMON /KVAR/  KASE,KONEIG,KPOLAR
      COMMON /NVAR/  NFHY(9),NRDM(2)
      N      .NS,NPANEL,NACEL,NROWS,NROWN,NCOLM,NRODYS,NTHETA,NT
      N      .HEIS,MXLE,NRG,NPOLAR,NCLX
      COMMON /PVAR/  POLAR
      COMMON /RVAR/  R(55),RM(55,2)
      R      .RATIOX,RFAREA
      COMMON /SVAR/  SERIS,SLC
      COMMON /TVAR/  TITLE(12),THETA(210),THETAR(10),THETAS(9),THETAN(10
      T      .2),TCL(110),TCD(10),TCM(10)
      T      .THICK,TWIST
      COMMON /UVAR/  UBMT(100),UBMT(110),UBMT(110),UNCL(210,2)
      COMMON /VVAR/  VBMT(100),VBMT(110),VBMT(110),VNCL(210,2)
      V      .VOUT
      COMMON /WVAR/  WBMT(100),WBMT(110),WBMT(110),WNCL(210,2)
      COMMON /XVAR/  XBAR(210),XC(210),XNI(2),XNKN(2),XNTH(2),XA(55),XN(
      X      55,2),XNDC(2),XNCL(2),XNCL(2),XNCLM(2),XYZ(3),XCL(10),XCD
      X      (10)
      X      .XNACEL,XP,XCPBAR
      COMMON /YVAR/  YBAR(210),YC(210),YNI(2)
      COMMON /ZVAR/  ZBAR(210),ZC(210),ZNI(2),ZDELTA(55),ZDN(55,2)
      Z      .ZP,ZA

      DIMENSION ALPHA(110),ALPHAUI(110)
      DIMENSION CHORD(20),CLAR(100),CLWM(110),CPB(100),CPL(110),CPU(110
      C      ),CSHAPE(110)
      DIMENSION U(110),URB(100),URW(100),URW(100),URB(110),UWN(110),UWM(
      U      110)
      DIMENSION V(110),VRB(100),VRW(100),VRW(100),VRB(110),VMW(110),VMW(
      V      110)

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      DIMENSION W(110),WRR(100),WRN(100),WRM(100),WRG(110),WRN(110),WRW(
      W 110),WSCLL(20),WSCUL(20),WSCDL(20),WSCDU(20),WSCUL(20),WSCDL(20),WSC
      W CD(20)
      C KONFIG = 1 WING ALONE CONFIGURATION
      C KONFIG = 2 BODY ALONE CONFIGURATION
      C KONFIG = 3 WING-BODY CONFIGURATION
      C
      BETA=SQRT(CABS(XMACM**XMACM-1.))
      BETA2=BETA*BETA
      BETAM=2.4/1.414214*XMACM**4/BETA**75
      RATIO0=.75
      C
      C ANY CONFIGURATION
      IF (KONFIG-2) 105, 90,95
      C
      C BODY-ALONE CONFIGURATION
      90 CONTINUE
      CALL FSF(10,NTAPEC,IRR)
      END FILE NTAPEC
      REWIND NTAPEC
      GO TO 550
      C
      C WING-BODY CONFIGURATION
      95 CONTINUE
      DO 100 J=1,NBODY
      UBN(J)=0.
      VBN(J)=0.
      WBN(J)=0.
      100 CONTINUE
      C
      C WING ALONE OR WING-BODY CONFIGURATION
      105 CONTINUE
      DO 110 J=1,NWING
      UWB(J)=0.
      VWB(J)=0.
      WWB(J)=0.
      UWN(J)=0.
      VWN(J)=0.
      WWN(J)=0.
      110 CONTINUE
      XWNCUT=0.
      XWNCOT=0.
      XWNCMT=0.
      C
      160 CONTINUE
      IF (IPOLAR .NE. 0) GO TO 210
      GC TO (170,210,260),KASE
      C
      C CALCULATE WING ALPHA, GIVEN WING CL KASE = 1
      170 CONTINUE
      IF (KONFIG-2) 180,190,190

```

2

3

6

7

8

C	WING ALONE CONFIGURATION	
180	CONTINUE	41
	CALL CAMBW (NWMG,NTAPEE,A,CL,ALPHAW)	42
	REWIND NTAPEE	
	GO TO 360	
C	WING-BODY CONFIGURATION	
190	CONTINUE	45
	CALL FSF (1,NTAPEE,IRR)	48
	CALL DCPI (NBDY,NWMG,NTAPEE,A,ABX,CL(NS),CL)	49
	REWIND NTAPEE	51
	CALL CAMBW (NBDY,NWMG,NTAPEE,NTAPEE,A,CL(NS),ABX,ABX)	52
	REWIND NTAPEE	53
	REWIND NTAPEE	
	DO 200 J=1,NWMG	
200	ALPHAW(J)=ABX(J)+ALPHAX(J)	
	GO TO 360	
C	CALCULATE WING CL. GIVEN WING ALPHA KASE = 2	
210	CONTINUE	
	IF (KONFIG-2) 220,230,230	
C	WING ALONE CONFIGURATION	
220	CONTINUE	67
	CALL FSF (1,NTAPEE,IRR)	69
	CALL DCPI (NWMG,NTAPEE,A,ALPHAW,CL)	70
	REWIND NTAPEE	
	GO TO 360	
C	WING-BODY CONFIGURATION	
230	CONTINUE	84
	DO 240 J=1,NWMG	
240	ABX(J)=ALPHAW(J)-ALPHAX(J)	99
	DO 250 J=1,NBDY	102
	READ (NTAPEE) (A(I),I=1,NWMG)	103
	DO 250 I=1,NWMG	104
250	ABX(I)=ABX(I)-A(I)+ABX(J)	107
	CALL FSF (1,NTAPEE,IRR)	108
	CALL DCPI (NWMG,NTAPEE,A,ABX,CL(NS))	
	REWIND NTAPEE	
	CALL FSF (1,NTAPEE,IRR)	
	CALL DCPI (NBDY,NWMG,NTAPEE,A,ABX,CL(NS),CL)	
	REWIND NTAPEE	
	GO TO 360	
C	OPTIMIZE CAMBER FOR GIVEN CL. OR FOR GIVEN CL AND CM KASE = 3	
260	CONTINUE	
	IF (CONSNT) 280,270,280	113
270	CALL FSF(2,NTAPEE,IRR)	
	GO TO 290	
280	CALL FSF(3,NTAPEE,IRR)	116
290	CONTINUE	

```

IF (KONFIG-2) 300,310,310
C
WING ALONE CONFIGURATION
300 CONTINUE
CALL OPTIM (NWIN,NTAPE,A,B,CONSNT,CLBAR,XCPBAR,RFAREA,AREA,CL)
REWIND NTAPE
CALL CAMB (NWIN,NTAPE,A,CL,ALPHA)
REWIND NTAPE
GO TO 360
120
121
122
123

C
WING-BODY CONFIGURATION
310 CONTINUE
CALL OPTIMB (NWIN,NBODY,NTAPE,NTAPE,THICK,A,B,ALPHA,ABX,ALPHA,
1 AREAINS),CONSNT,CLBAR,XCPBAR,RFAREA,CL(NS))
REWIND NTAPE
CALL FSF (1,NTAPE,IRR)
CALL DCPI (NBODY,NWIN,NTAPE,A,ABX,CL(NS),CL)
REWIND NTAPE
CALL CAMB (NBODY,NWIN,NTAPE,NTAPE,A,CL(NS),ABX,ABX)
REWIND NTAPE
REWIND NTAPE
DO 350 J=1,NWIN
350 ALPHA(J)=ABX(J)+ALPHA(J)
128
129
130
131
132
133
134
135
136
137
138

C
WING ALONE OR WING-BODY CONFIGURATION
360 CONTINUE
IF (KONFIG-2) 370,360,360
C
WING ALONE CONFIGURATION
370 CONTINUE
CALL FSF (1,NTAPE,IRR)
CALL CVEL (NWIN,NWIN,NTAPE,A,B,C,CL,UWM,VWM,WWM)
REWIND NTAPE
GO TO 390
151
153
154

C
WING-BODY CONFIGURATION
380 CONTINUE
CALL FSF (1,NTAPE,IRR)
CALL CVEL (NWIN,NBODY,NTAPE,A,B,C,CL,UWB,VWB,WWB)
CALL FSF (2,NTAPE,IRR)
CALL CVEL (NWIN,NWIN,NTAPE,A,B,C,CL(NS),UWM,VWM,WWM)
REWIND NTAPE
CALL RITE (INFT(6),NTAPE,NWIN,NBOW,NCOLM,DUMMY,UWB,VWB,WWB)
CALL RITE (INFT(7),NTAPE,NWIN,NROW,NCOLM,DUMMY,UWB,VWB,WWB)
157
159
161
164
165
166

C
WING ALONE OR WING-BODY CONFIGURATION
390 CONTINUE
CALL FSF (10,NTAPE,IRR)
WRITE (NTAPE) NPANEL
WRITE (NTAPE) (CL(J),J=1,NPANEL)
END FILE NTAPE
168
170
171
172
179

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160

REVIEW NTAPED
CALL RTE (NFT(4),NTAPED,NWING,NROW,NCOL,N,DUMMY,UWV,VWV,WNV)

181

C COMPUTE COEFFICIENT OF PRESSURE ON WING WITH OR WITHOUT WING
C THICKNESS

IF (THICK) 400,440,400

185

C WING ALONE OR WING-BODY CONFIGURATION
C WITH WING THICKNESS
400 CONTINUE

CALL RTE (NFT(5),NTAPED,NWING,NROW,NCOL,N,DUMMY,UWV,VWV,WNV)

DO 410 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

W(J)=WMB(J)+WMW(J)+WMBT(J)+WMNT(J)+WMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPU)

DO 420 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPL)

DO 430 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPL)

DO 440 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPL)

DO 460 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPL)

DO 470 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPL)

DO 480 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPL)

DO 490 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPL)

DO 500 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPL)

DO 510 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPL)

DO 520 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPL)

DO 530 J=1,NWING

U(J)=UMB(J)+UMW(J)+UMBT(J)+UMNT(J)+UMN(J)

V(J)=VMB(J)+VMW(J)+VMBT(J)+VMNT(J)+VMN(J)

CALL CP(O,NWING,XMACH,CPCALC,U,V,W,CPL)


```

DC 400 J=1,NCOLM
JN=(J-1)*NROWM+(NROWM+1)/2
JN=NBODY+JN
DY=AREA(JN)/CHORD(JN)
WSCD(J)=(WSCD(J)-WSCD(J))/DY*SEMI
WSCD(J)=(WSCD(J)-WSCD(J))/DY*SEMI
400 CONTINUE

WCL=WCLU-WCLL
WCD=WCDU-WCDL
WCM=(WCMU-WCML)/CBAR

IF (KONFIG.EQ. 1) GO TO 600

C WING-BODY CONFIGURATION
CALL CVEL (NBODY,NBODY,NTAPED,A,B,C,CL,UBB,VBR,WBR)
CALL FSF (2,NTAPED,TRR)
CALL CVEL (NBODY,NBODY,NTAPED,A,B,C,CL(NS),UBW,VBW,WBW)
REWINC NTAPED

CALL RTE (NFRT(1),NTAPED,NBODY,NROWB,NTHETA,THETAB,UBB,VBB,WBB)
CALL RTE (NFRT(2),NTAPED,NBODY,NROWB,NTHETA,THETAB,UBW,VBW,WBW)
337
339
342

C COMPUTE COEFFICIENT OF PRESSURE ON BODY WITH OR WITHOUT THE
EFFECT OF WING THICKNESS
IF (THICK) 500,520,500
343
344

500 CONTINUE
CALL RTE (NFRT(3),NTAPED,NBODY,NROWB,NTHETA,THETAB,UBWT,VBWT,WBWT)
1)
346
350

DC 510 J=1,NBODY
U(J)=UBB(J)+UBW(J)+UBN(J)
V(J)=VBB(J)+VBW(J)+VBN(J)
W(J)=WBB(J)+WBW(J)+WBN(J)
GO TO 540

520 CONTINUE
DC 530 J=1,NBODY
U(J)=UBB(J)+UBW(J)+UBN(J)
V(J)=VBB(J)+VBW(J)+VBN(J)
W(J)=WBB(J)+WBW(J)+WBN(J)
530
540 CONTINUE
CALL CP11,NBODY,XMACH,CPCALC,U,V,W,CPR)

C COMPUTE COEFFICIENTS OF LIFT, DRAG, MOMENT ON BODY PANELS
CALL INTPOL (NBODY,NROWB,RATIOX,RATIOY,CHORD,ALPHA,ALPHA)
CALL SLOM (NBODY,XP,ZP,FAREA,AREA,XBAR,ZBAR,ALPHA,THETA,CPR)
1,BWCL,BWCD,BWCM)
394
396

C BODY ALONE OR WING-BODY CONFIGURATION
550 CONTINUE
BCL=BCL/FAREA
BCD=BCD/FAREA
BCM=BCM/(FAREA*CBAR)
398

```

IF (KONFIG .EQ. 2) GO TO 600

C WING-BODY CONFIGURATION

BWCM=BWCM/CBAR

BCL=BWCL+BBCL

BCD=BWCD+BBGD

BCM=BWCM+BBGM

WBCL=BCL+WCL+XWNCLY

WBCD=BCD+WCD+XWNCDT

WBCM=BCM+WCM+XWNCWT

C ANY CONFIGURATION

C WRITE OUTPUT

600 CONTINUE

IF (KONFIG-2) 660,620,610

C WING-BODY CONFIGURATION

610 CONTINUE

WRITE (INTAPEO,6010)

GO TO 630

405

C BODY ALONE CONFIGURATION

620 CONTINUE

WRITE (INTAPEO,6020)

C BODY ALONE OR WING-BODY CONFIGURATION

630 CONTINUE

WRITE (INTAPEO,6080) BCCO,BBCL,BBCM

WRITE (INTAPEO,6030)

WRITE (INTAPEO,6036) (THETAS(I),I=1,NTHETS)

WRITE (INTAPEO,6038)

DC 640 I=1,NRODYS

640 WRITE (INTAPEO,6040) XR(I),ICPB(I,J),J=1,NTHETS)

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IF (KONFIG .EQ. 2) GO TO 999

C WING-BODY CONFIGURATION

650 CONTINUE

WRITE (INTAPEO,6014)

WRITE (INTAPEO,6080) BWCD,BWCL,BWCM

WRITE (INTAPEO,6032)

CALL OUTB (INTAPEO,NBODY,NTHETA,NROWB,THETAB,CPB)

WRITE (INTAPEO,6034)

CALL OUTB (INTAPEO,NBODY,NTHETA,NROWB,THETAB,ALPHAB)

432

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436

C WING ALONE OR WING-BODY CONFIGURATION

660 CONTINUE

437

IF (NACEL .EQ. 0) GO TO 690

C WING ALONE OR WING-BODY CONFIGURATION WITH NACELLE(S)

DO 680 J=1,NACEL

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NTN=XTNTN(J)
NXN=NXN(J)
WRITE (INTAPE,6042) J
WRITE (INTAPE,6080) XNMC(J),XNCL(J),XNMC(J)
WRITE (INTAPE,6044)
WRITE (INTAPE,6036) (THETA(I,J),I=1,NTN)
WRITE (INTAPE,6038)
DO 670 I=1,NXN
670 WRITE (INTAPE,6040) XN(I,J),(CPNN(I,K,J),K=1,NTN)
680 CONTINUE

690 CONTINUE
DO 700 J=NS,MPANEL
700 CL(J)=-CL(J)

IF (KONFIG-2) 710,720,720

C WING ALONE CONFIGURATION
710 CONTINUE
WRITE (INTAPE,6018)
GO TO 730

C WING-BODY CONFIGURATION
720 CONTINUE
WRITE (INTAPE,6012)

C WING ALONE OR WING-BODY CONFIGURATION
730 CONTINUE
WRITE (INTAPE,6080) WCD,WCL,WCM
WRITE (INTAPE,6060)
WRITE (INTAPE,6064) (I,I=1,NCOLW)
WRITE (INTAPE,6000) (WSCD(I),I=1,NCOLW)
WRITE (INTAPE,6062)
WRITE (INTAPE,6064) (I,I=1,NCOLW)
WRITE (INTAPE,6000) (WSCD(I),I=1,NCOLW)
WRITE (INTAPE,6050)
CALL OUTW (INTAPE,MWING,NCOLW,NROWW,CPU)
WRITE (INTAPE,6052)
CALL OUTW (INTAPE,MWING,NCOLW,NROWW,CPL)
WRITE (INTAPE,6054)
CALL OUTW (INTAPE,MWING,NCOLW,NROWW,CL(NS))
IF (THICK) 740,750,740
740 WRITE (INTAPE,6056)
CALL OUTW (INTAPE,MWING,NCOLW,NROWW,ALPHAU)
WRITE (INTAPE,6057)
CALL OUTW (INTAPE,MWING,NCOLW,NROWW,ALPHA)
750 WRITE (INTAPE,6058)
CALL OUTW (INTAPE,MWING,NCOLW,NROWW,ALPHA)
WRITE (INTAPE,6055)
WRITE (INTAPE,6000) (CHORD(I),I=1,NCOLW)

IF (KONFIG-50) 1) GO TO 999

C WING-BODY CONFIGURATION

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540

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WRITE (NTAPEO,6016)
WRITE (NTAPEO,6080) WBCD,WBCL,WBCM

C 999 ANY CONFIGURATION
CONTINUE
RETURN

C 6000 FORMAT(1H, 'F29.5,9F10.5)
6010 FORMAT(1H, 40H PRESSURES, FORCES, AND MOMENTS ON ISOLATED BODY)
6012 FORMAT(1H, 60H PRESSURES, FORCES, AND MOMENTS ON WING PANELS IN P
1RESENCE OF BODY)
6014 FORMAT(1H, 70H INCREMENTAL PRESSURES, FORCES, AND MOMENTS ON BODY
1 PANELS DUE TO WING)
6016 FORMAT(1H, 44H FORCES AND MOMENTS ON WING-BODY COMBINATION)
6018 FORMAT(1H, 38H PRESSURES, FORCES AND MOMENTS ON WING)
6020 FORMAT(1H, 38H PRESSURES, FORCES AND MOMENTS ON BODY)
6030 FORMAT(1H0/32H BODY PRESSURE COEFFICIENTS(CP))
6032 FORMAT(1H0/37H BODY PANEL PRESSURE COEFFICIENT(CP))
6034 FORMAT(1H0/25H BODY PANEL SLOPE(DR/DX))
6036 FORMAT(1H0,4X,11HTHETA(DEG.),F14.4,9F10.4,/(F29.4,9F10.4))
6038 FORMAT(1H, 9X,1HX)
6040 FORMAT(1H, 'F14.4,F15.5,9F10.5,/(F29.5,9F10.5))
6042 FORMAT(1H, 57H PRESSURES, FORCES, AND MOMENTS ON ISOLATED NACELLE
1 PAIR, 12)
6044 FORMAT(1H0/34H NACELLE PRESSURE COEFFICIENTS(CP))
6050 FORMAT(1H0/52H UPPER SURFACE WING PANEL PRESSURE COEFFICIENTS(CP)
1)
6052 FORMAT(1H0/52H LOWER SURFACE WING PANEL PRESSURE COEFFICIENTS(CP)
1)
6054 FORMAT(1H0/36H WING PANEL PRESSURE DIFFERENCE(CLI))
6056 FORMAT(1H0/23H WING CHORD LENGTH(SC))
6058 FORMAT(1H0/39H UPPER SURFACE WING PANEL SLOPE(DZ/DX))
6060 FORMAT(1H0/39H LOWER SURFACE WING PANEL SLOPE(DZ/DX))
6062 FORMAT(1H0/26H WING CAMBER SLOPE(DZ/DX))
6064 FORMAT(1H0/40H SPANWISE CD DISTRIBUTION(8/20 * DO/DY))
6066 FORMAT(1H0/40H SPANWISE CL DISTRIBUTION(8/20 * DL/DY))
6068 FORMAT(1H0,2X,16HSPANWISE STATION,18.9110,/(18X,18.9110))
6080 FORMAT(1H0/6H CD -,F10.5,10X,4HCL -,F10.5,10X,4HCM -,F10.5)
END

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FD
ASSEMBLED TEXT.

FD	ASSEMBLED TEXT.	TOV TRA	DATE+1 DATE+1	TURN OFF OVERFLOW LIGHT	DATE0440 DATE0450 DATE0460 DATE0470 DATE0480 DATE0490 DATE0500
00031	0140 00 0 02001	10011			
00032	0020 00 0 02001	10011			
00033	0 00000 0 00000	10000	0		
00034	000041214560	10000	4.00 JAN 00FEB 00MAR 00APR		
00035	000026252260	10000			
00036	000044213160	10000			
00037	000021473160	10000			
00040	000044217060	10000	4.00 MAY 00JUN 00JUL 00AUG		
00041	000041644360	10000			
00042	000041644360	10000			
00043	000021642760	10000			
00044	000062254760	10000	4.00 SEP 00OCT 00NOV 00DEC		
00045	000046236360	10000			
BINARY CARD (NOT PUNCHED)					
00046	000045466560	10000			
00047	000024252360	10000			
00050	000073670111	10000			
	00000	01111			

FDATE
CONTROL NICTICNARY

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FDAT0302

SCDICT FDATE

BINARY CARD (NOT PUNCHED)
000051000000
000004000005
252421632560
000051000000
242163256060
000000000002
627062434623
200000000000

PREFACE
FDATE DECK
DATE REAL
SYSLOC VIRTUAL

START=0, LENGTH=41, TYPE=7094, CMPLX=5
LOC=0, LENGTH=41
LOC=2, LENGTH=0
SECT. 3

FDAT0303

SDKEND FDATE

NO MESSAGES FOR THIS ASSEMBLY

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FFSF901

FFSF0020
FFSF0030
FFSF0040
FFSF0050
FFSF0060
FFSF0070
FFSF0080
FFSF0090
FFSF0100
FFSF0110
FFSF0120
FFSF0130
FFSF0140
FFSF0150
FFSF0160
FFSF0170
FFSF0180
FFSF0190

LOIR

FFSF0200
FFSF0210
FFSF0220
FFSF0230
FFSF0240

```
CALL FVID.(TEMP,TEMP+1)
```

FFSF0250
FFSF0260
FFSF0270
FFSF0280

FFSF030C
FFSF031C

FFSF
ASSEMBLED TEXT.

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00032	0500	00	0	03001	10011	CLA	TEMP+1	FFSF0320
00033	0621	00	0	00042	10001	STA	SETA	FFSF0330
00034	0621	00	0	00040	10001	STA	SETX	FFSF0340
00035	4054	00	0	040000	10000	LFT	040000	FFSF0350
00036	0020	00	0	00041	10001	TRA	LOOP	FFSF0360
00037	0074	00	4	04000	10011	TSX	-OPEN,4	FFSF0370
00040	5	00000	0	00000	10000	MON	**	FFSF0380
00041	0074	00	4	07000	10011	TSX	-READ,4	FFSF0390
00042	0	00000	0	00000	10000	PZE	***,0	FFSF0400
00043	0	00046	0	00053	10101	PZE	EOF,ERR	FFSF0410
00044	4	00002	0	03002	10011	IOCP	SKIM,0,2	FFSF0420

READ TO EOF

BINARY CARD (NOT PUNCHED)

00045	3	77777	2	00000	10000	IOPTN	**0,-1	FFSF0430
00046	4500	00	0	03003	10011	CAL	SKIM+1	FFSF0440
00047	4340	00	0	00063	10001	LAS	CODE	FFSF0450
00050	0020	00	0	00041	10001	TRA	LOOP	FFSF0460
00051	0020	00	0	00057	10001	TRA	ERRA	FFSF0470
00052	0020	00	0	00041	10001	TRA	LOOP	FFSF0480
00053	2	00001	1	00041	10001	TTX	LOOP,1,1	FFSF0490
00054	0534	00	4	00005	10001	LXA	-00001,4	FFSF0500
00055	0600	60	4	00005	10000	STZ*	5,4	FFSF0510
				00056		RETURN	FSF	FFSF0520
00057	0754	00	1	00000	10000	PXA	0,1	FFSF0530
00060	0534	00	4	00005	10001	LXA	-00001,4	FFSF0540
00061	0601	60	4	00005	10000	STD*	5,4	FFSF0550
00062	0020	00	0	00056	10001	TRA	ERRA-1	FFSF0570
00063	632147254524			00064	10000	BCI	1,TAPEND	FFSF0590
						LOGC		FFSF0590
00064	100000000064				00001	ERASE	CONTRAL	FFSF0600
00064	200000000002				00001	USE	ER	FFSF0610
00066	200000000002				00001	TEMP	BSS	FFSF0620
00070	2000000000020				00001	SKIM	BSS	FFSF0630
						ASS	16	

IF TAPEND

SET N=0

SET N TO CTR OF
UNSKIPPED FILES

BINARY CARD (NOT PUNCHED)

00000	01111	FND	FFSF0640
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FFSF02

SCDICT FFSF

BINARY CARD (NOT PUNCHF7)	PREFACE	START=0,LENGTH=72,TYPE=7094,CMLX=5
000110700000	DECK	LOC=0,LENGTH=72
000004000005	FFSF	LOC=2,LENGTH=0
262662265060	FSF	LOC=64,LENGTH=20
070110000000	REAL	SECT. 4,CALL
266226606060	REAL	SECT. 5
000003000002	ERASE	SECT. 6
255121622560	.FVIO.	SECT. 7
000024000064	VIRTUAL	
332665314633	SYSLOC	
200000100000	.OPEN	
627062434623	VIRTUAL	
2000000300000	.READ	
336647254560		
200000000000		
335125212460		
200003000000		

FFSF0303

SDXEND FFSF

NO MESSAGES FOR THIS ASSEMBLY

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FFSF
SYMBOL REFERENCE DATA

REFERENCES TO DEFINED SYMBOLS.

CLASS	SYMBOL	VALUE	REFERENCES
CODE	CODE	00053	47
	EDF	00053	43
	ERRA	00057	51,62
	ERR	00046	43
LCTR	ER		
	FSF	00002	56
	--0001	00005	14,15,16,54,60
	--0002	00007	6,11
LCTR	--0003	00011	2
	LOOP	00041	36,50,52,53
	RLCTR		
	UNOS		
LCTR	SETA	00042	33
	SETX	00040	34
	SKIN	00066	44,46
	TEMP	00064	20,25,27,30,32

REFERENCES TO VIRTUAL SYMBOLS.

-FVIO.	4	23
-OPEN	6	37
-READ	7	41
SYSLOC	5	12

FFSR
ASSEMBLED TEXT.

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STEXT FFSR

FFSR0001

```

* FORWARD SPACE RECORD / FSR
* JIM STOKER TRANSPORT - 4/61
* CONVERTED TO IBM MAP BY DOT TYLER - 10/63
* METHODS MEMO 7090-24
*
* * * * *
* CALL FSR (NREC,LTAPE,LError)
*
* NREC - NUMBER OF FORTRAN LOGICAL RECORDS TO SPACE FORWARD.
* LTAPE - LOGICAL TAPE NUMBER.
* LERROR - LOCATION IN WHICH THE ERROR CODE IS STORED.
* 0 INDICATES SUCCESS.
* N INDICATES NUMBER OF UNSPACED RECORDS WHEN AN
* END-OF-FILE MARK WAS FOUND. TAPE LEFT SPACED IN
* FRONT OF EOF.
*
* CALL FSPR(NPREC,LTAPE,LError)
*
* NPREC - NUMBER PHYSICAL RECORDS TO SPACE FORWARD.
*
* * * * *
* ENTRY FSR
* ENTRY FSPR
*
* * * * *

```

```

BINARY CARD (NOT PUNCHED)
00000 00000000000 10000
00001 262662516060 10000
00002 0600 00 0 04004 10011
00003 0020 00 0 01002 10011
00004 4625 00 0 04004 10011
00005 1 00000 0 00014 10001
00006 0774 00 2 00000 10000
00007 0774 00 1 00000 10000
00010 3774 00 4 00000 10000
00011 0441 00 0 00013 10001
00012 0020 00 4 00001 10000
00013 0 00000 0 00000 10000
00014 0604 00 0 00013 10001
00015 0634 00 4 06000 10011
00016 0634 00 4 00010 10001
00017 0634 00 1 00007 10001
00020 0634 00 2 00006 10001
00021 0500 60 4 00004 10000
00022 0601 00 0 04000 10011

```

```

BINARY CARD (NOT PUNCHED)
00023 0500 60 4 00003 10000

```

```

LDIR
FSR STZ CODE
TRA **2
FSR STL CODE
TURN SAVEN 4+2,1,I

```

FFSR00300
FFSR00310
FFSR00320
FFSR00330
FFSR00340

FFSR00350
FFSR00360

FFSR00370

07/31/65

FFSR
ASSEMBLED TEXT.

FSR00390
FSR00390
FSR00400

PAX 0,1
TZE WIND
CALL .FVIO.(TEMP,TEMP+1)

00024 0734 00 1 00000 10000
00025 0100 00 0 00063 10001
00026 000000000000 00010
00027 0074 00 4 05000 10011
00028 1 00002 0 01004 10011
00029 0 00000 0 00047 10100
00030 0 00000 0 04000 10011
00031 0 00000 0 04001 10011
00032 0535 00 2 04001 10011
00033 0636 00 2 00044 10001
00034 0636 00 2 00042 10001
00035 0441 00 2 00001 10000
00036 4054 00 0 00043 10001
00037 0020 00 0 07000 10011
00038 0074 00 4 07000 10000
00039 5 00000 0 00000 10000
00040 0074 00 4 10000 10011
00041 0 00000 0 00000 10000

FSR00410
FSR00420
FSR00430
FSR00440
FSR00450
FSR00460
FSR00470
FSR00480
FSR00490
FSR00500

LAC TEMP+1,2
SCA SETA,2
SCA SETB,2
LJI 1,2
LFT 040000
TRA READL
TSX .OPEN,4
MON **
READL TSX .READ,4
PZE SETA **,,0

BINARY CARD (NOT PUNCHED)

00045 0 00050 0 00060 10101
00046 4 00002 0 04002 10011
00047 3 77777 2 00000 10000
00048 0534 00 4 04002 10011
00049 0529 00 0 04004 10011
00050 7 00000 0 00043 10001
00051 2 00001 1 00043 10001
00052 4754 00 0 00000 10000
00053 0534 00 4 00010 10001
00054 0601 60 4 00005 10000
00055 0074 00 4 11000 10011
00056 0 00005 2 00000 10000
00057 0761 00 0 07000 10000
00058 0754 00 1 00000 10000
00059 0020 00 0 00055 10001

FSR00510
FSR00520
FSR00530
FSR00540
FSR00550
FSR00560
FSR00570
FSR00580
FSR00590
FSR00600
FSR00610
FSR00620
FSR00630
FSR00640
FSR00650
FSR00660
FSR00670
FSR00680
FSR00690
FSR00700
FSR00710
FSR00720
FSR00730

PZE EOF,,ERR
IOCP SKIM,0,2
IORIN **,,0,-1
LXA SKIM,4
ZET CODE
TXL READL,4,0
TIX READL,1,1
PXD 0,0
LXA .,0001,4
STG* 5,4
RETURN TURN
TSX .NDESEL,4
PZE 0,2,5
NOP
WIND PXA 0,1
TRA DONE

* * * * *
* * * * *
* * * * *

ERASE CONTRL ER
USE ER
TEMP RSS 2
SKIM BSS 2

00065 1000000000065 00001
00066 2000000000002 00001
00067 2000000000002 00001

BINARY CARD (NOT PUNCHED)

00071 2000000000001 00001
00072 2000000000017 00001
00000 01111
END

FSR00740
FSR00750
FSR00760
FSR00770
FSR00780
FSR00790

FFSR
CONTROL DICTIONARY

07/31/65

FFSR0002

\$CDICT FFSR

BINARY CARD (NOT PUNCHED)	PREFACE	START=0,LENGTH=73,TYPE=7094,CPLX=5
000111000000	FFSR DECK	LOC=0,LENGTH=73
000004000005	FSPR REAL	LOC=2,LENGTH=0
262662516060	FSR REAL	LOC=4,LENGTH=0
000111000000	ERASE REAL	LOC=65,LENGTH=20
266247516060	.FVIO. VIRTUAL	SECT. 5,CALL
000000000002	SYSLOC VIRTUAL	SECT. 6
266251606060	.OPEN VIRTUAL	SECT. 7
000000000004	.READ VIRTUAL	SECT. 8
255121622560	.NDSL VIRTUAL	SECT. 9
000000000005		
332665314633		
200000100000		
627062434623		
200000000000		
334647254560		
200000000000		
335125212460		
200000000000		
334524622543		
200000000000		

FFSR0003

\$DKEND FFSR

NO MESSAGES FOR THIS ASSEMBLY

08/08/67

FLOUT - EFM SOURCE STATEMENT - IFNIS -

```

100 CONTINUE
  WRITE(N6,1005)
  DO 110 J=1,IC
    U=VLS(1,J)
    V=VLS(2,J)
    W=VLS(3,J)
    IF (CPCALC-1.) 320,320,335
320 CONTINUE
  C      LINEAR CP FORMULA
    CP = -2.*U
    GO TO 340
330 CONTINUE
  C      NON-LINEAR CP FORMULA
    CP = -2.*U+8T2*U*U-V*V-W*W
    GO TO 340
  C      **EXACT** ISENTROPIC CP FORMULA
335 Q2=(U+COSARA)**2+V*V+(W+SINARA)**2
    CP = 1.42857/XMAC+2*(1.+2*XMAC**2*(1.-Q2))**3.5-1.)
340 CONTINUE
110 VLS(4,J)=CP
  WRITE(N6,1006)((CP(1,J),I=1,3),(VLS(I,J),I=1,4),J=1,IC)
  REMIND N1
  REMIND N2
  REMIND N3
  REMIND N4
  GO TO(15,21,31,120),NP
120 RETURN
  END

```

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87

92
106
107
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109

604

08/08/67

FLOVIZ - EFM SOURCE STATEMENT - IFN(S) -

```

N4=DM(2)
REWIND N1
REWIND N2
REWIND N3
REWIND N4
CALL ALLIN(N8)
COSARA=COS(ARA)
SINARA=SIN(ARA)
XMACH2=XMACH*XMACH
BT2=XMACH2-1.
READIN5,1006) CPCALC,CAMN,POP
IF(POP.EQ.0.) GO TO 50
IF(CAMN.EQ.0.) WRITE(N6,1020)
IF(CAMN.EQ.1.) WRITE(N6,1021)
IF(CAMN.EQ.2.) WRITE(N6,1022)
50 CONTINUE
IF(CPCALC-1.) 5,10,15
5 WRITE(N6,1016)
GO TO 20
10 WRITE(N6,1017)
GO TO 20
15 WRITE(N6,1018)
20 CONTINUE
1 CONTINUE
READIN5,1001) CUENRD
IF(CUENRD.EQ.GRID) GO TO 200
IF(CUENRD.EQ.STREAM) GO TO 300
IF(CUENRD.EQ.POINT) GO TO 400
100 WRITE(N6,1002) CUENRD
200 RETURN
200 WRITE(N6,1003) CUENRD
READIN5,1004) XNG
NGR=XNG
WRITE(N6,1005) NGR
DO 215 JJ=1,NGR
READIN5,1004) XO,YO,ZO,XA,YA,ZA,LIT
READIN5,1006) DX,DY,DZ,XM,YM,ZM,AMO
IX=XN
IY=YN
IZ=ZN
MODE=AMO
CALL GRID5
215 CONTINUE
GO TO 1
300 CONTINUE
WRITE(N6,1019)
WRITE(N6,1007)
READIN5,1006) DXMAX,DXMIN,PRINT
READIN5,1004) XNS
NS=XNS
DO 315 JJ=1,NS
READIN5,1006) XS,YS,ZS,XMAX,XMIN,XDELY
WRITE(N6,1013) XS,YS,ZS

```

08/08/67

FLOVIZ - EFN SOURCE STATEMENT - IFN(S) -

```

WRITE(N6,1014) XDDEL
CALL STRMI(XS,YS,ZS,XMAX,XMIN,XDEL,1)
CALL STRMI(XS,YS,ZS,XMAX,XMIN,XDEL,2)
315 CONTINUE
GO TO 1
400 CONTINUE
C POINTS COMPUTATION
REWIND N1
REWIND N2
REWIND N3
REWIND N4
WRITE(N6,1015)
WRITE(N6,1009)
WRITE(N6,1010)
READ(N5,1004) XP
ISTR=0
NP=XP
DO 415 JJ=1,NP
READ(N5,1004) XF,YF,ZF
CALL LACKEY(ISTR,
              XF,YF,ZF,U,V,W,CPL)
COSA=U-COSARA
COSB=V
COSC=W-SINARA
WRITE(N6,1011) XF,YF,ZF,COSA,COSB,COSC,U,V,W,CPL
415 CONTINUE
CALL FLOUT(NP)
GO TO 1
END

```

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05/22/67

FORCES - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE FORCES

C CONTROL ROUTINE FOR FORCES LINK

COMMON DATE(2),NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI
1,NTAPEO,NBODY,NWING,XMACH,SYM,KACE

COMMON /AVAR/ A(210),ACB(21),ABX(100),AWX(110),AREA(210),ARN(2),A
RWT(20),ALPHA(210),ALPHAB(210),ALPHAS(210),ALPHAT(1
10),ALPHAN(110),ALPHA(110),AWS(110)

A ALPHA,ALPHAD,ARA,ARADEG,ARB,ARH,ARAS,AT,AAA
B(210)

COMMON /BVAR/ BBCL,BBCD,BBCM
C(210),CHORD(210),CL(210),CPBB(55,10),CPNN(55,10,2)
CLST(210)

C CDR,CASE,CPCALC,CBAR,CONSNT,CLBAR,CLX,CLM,CDM
D(210),DZDX(55)

COMMON /DVAR/ DADEG,DARAD

COMMON /IVAR/ IPOLAR

COMMON /KVAR/ KASE,KONFIG,KPOLAR

COMMON /NVAR/ NFRT(9),NRNM(2)

N NS,NPANEL,NACEL,NROMB,NROMV,NCCLW,NBODYS,NTHETA,NT
HETS,NXLE,NRG,NPOLAR,NCLX

COMMON /PVAR/ POLAR

COMMON /RVAR/ R(55),RN(55,2)

R RATIOX,RFAREA

COMMON /SVAR/ SEMIS,SLC

COMMON /TVAR/ TITLE(12),THETA(210),THETAB(10),THETAS(9),THETAN(10
2),TCL(10),TED(10),TCM(10)

T THICK,TWIST

COMMON /UVAR/ UBWT(100),UMBT(110),UMWT(110),UMCL(210,2)

COMMON /VVAR/ VBWT(100),VMBT(110),VMWT(110),VMCL(210,2)

V VOUT

COMMON /WVAR/ WBWT(100),WMBT(110),WMWT(110),WMCL(210,2)

COMMON /XVAR/ XBAR(210),XC(210),XNI(2),XNKM(2),XNTN(2),XB(55),XN(55,2),XNCLD(2),XNCL(2),XNMC(2),XNMC(2),XVZ(3),XCL(10),XCD(10)

X XNACEL,XP,XCPBAR

COMMON /YVAR/ YBAR(210),YC(210),YNI(2)

COMMON /ZVAR/ ZBAR(210),ZC(210),ZNI(2),ZDELTA(55),ZDN(55,2)

Z ZP,ZA

C DEFINE CONSTANTS AND READ INPUT DATA

C KONFIG = 1 WING ALONE CONFIGURATION

C KONFIG = 2 BODY ALONE CONFIGURATION

C KONFIG = 3 WING-BODY CONFIGURATION

C CASE = 1. CALCULATE ALPHA, GIVEN CL

C CASE = 2. CALCULATE CL, GIVEN ALPHA

C CASE = 3. OPTIMIZE WING

C	CPCALC =0.	LINEAR CP	6
C	CPCALC =1.	NON-LINEAR CP	
C	CPCALC =2.	EXACT CP	
C	POLAR = 0.	POLARS NOT REQUESTED,OMIT DELTA ALPHA CARDS	
C	POLAR = 1.	POLARS REQUESTED,INSERT DELTA ALPHA CARDS	
C	THICK =0.	WING THICKNESS PRESSURES NOT TO BE ADDED	
C	THICK =1.	WING THICKNESS PRESSURES TO BE ADDED	
C	THICK =2.	WING THICKNESS PRESSURES TO BE ADDED USING	
C		RIEGELS CORRECTION RULE	
C	VOUT = 0.	VELOCITY COMPONENTS NOT TO BE PRINTED	
C	VOUT = 1.	VELOCITY COMPONENTS TO BE PRINTED	
C	XNACEL =0.	EFFECTS OF NACELS NOT INCLUDED	
C	XNACEL =X.	EFFECTS OF X PAIRS OF NACELLES, GEOMETRY EXPECTED	
C	XNACEL =-X.	EFFECTS OF X PAIRS OF NACELLES, GEOMETRY SAME AS	
C		PREVIOUS CASE	
C	RFAREA =0.	WING REFERENCE AREA TO BE CALCULATED	
C	RFAREA =X.	WING REFERENCE AREA TO BE SPECIFIED	
C	XP,ZP	X AND Z COORDINATES OF POINT ABOUT WHICH MOMENTS	
C		ARE TO BE COMPUTED	
C	CBAR	REFERENCE CHORD LENGTH USED IN PITCHING	
C		MOMENT CALCULATIONS	
C		CBAR =1. IF NOT SPECIFIED	
C	SEMTS	WING SEMI-SPAN USED IN SPANWISE CD AND CL	
C		CALCULATIONS	
C		SEMTS =1. IF NOT SPECIFIED	
C	KONFIG=KACE		
C	NPANEL=NWING+NBODY		
C	NS=NBODY+1		
C	CDR=57.2957795		
C	IF (KONFIG-2) 5,10,5		
C	5	READ CONFIGURATION GEOMETRY	
C		CONTINUE	
C		READ (NTAPEC) NBODY,NWING,NMACH,SYM,KACE	
C		READ (NTAPEC) (1,XBAR(1),YBAR(1),ZBAR(1),XC(1),YC(1),ZC(1),AREA(1	
C		1),THETA(1),ALPHA(1),CHORD(1),I=1,NPANEL),NRG,(NRCM(1),I=1,NRC),RA	
C		ZTINX	
C		REWIND NTAPEC	
C	10	CONTINUE	
C		READ CASE DATA	
C		READ (NTAPE1,5000) TITLE	

37

```

READ (NTAPE1,5010) CASE,CPCALC,POLAR,THICK,VOUT
IPOLAR=0

```

```

MACEL=0

```

```

IF (CASE) 20,999,20

```

20

```

CONTINUE

```

```

READ (NTAPE1,5010) RFAREA,XP,ZP,CBAR,SEMS

```

41

```

NTHETS=9

```

```

THETAS(1)=0.

```

```

DO 50 I=2,NTHETS

```

```

  THETAS(I)=THETAS(I-1)+22.5

```

50

```

CONTINUE

```

```

IF (CBAR .EQ. 0.) CBAR=1.

```

```

IF (SEMS .EQ. 0.) SEMS=1.

```

```

IF (VOUT) 75,85,75

```

75

```

CONTINUE

```

```

DO 80 J=1,9

```

80

```

  NMT(J)=J

```

```

  GO TO 100

```

85

```

CONTINUE

```

```

DC 90 J=1,9

```

90

```

  NMT(J)=0

```

100

```

CONTINUE

```

```

KASE=CASE

```

```

IF (RFAREA) 120,120,140

```

120

```

IF (KONFIG-2) 130,125,130

```

125

```

RFAREA=1.0

```

```

GO TO 140

```

130

```

RFAREA=0.0

```

```

DO 135 J=NS,MPANEL

```

135

```

  RFAREA=RFAREA+AREA(J)

```

140

```

CONTINUE

```

C

```

WRITE CASE DATA

```

```

WRITE (NTAPE2,6002) TITLE,DATE

```

```

CALL INOUT(NTAPE2,CASE,CPCALC,POLAR,THICK,VOUT,XMACH,SEMS,

```

```

  1XP,ZP,CBAR,RFAREA,SYM)

```

88

200

```

CONTINUE

```

C

```

ANY CONFIGURATION

```

```

IF (KONFIG .EQ. 1) GO TO 240

```

C

```

BODY ALONE OR WING-BODY CONFIGURATION

```

```

NROW=NROW(1)

```

```

IF (KONFIG-2) 210,210,220

```

C

```

BODY ALONE CONFIGURATION

```

210

```

READ (NTAPE2) NBODY,NWING,XMACH,SYM,KASE

```

```

GO TO 230

```

98

C	WING-BODY CONFIGURATION	
220	CALL FSF(3,NTAPEC,IRR)	104
230	CONTINUE	
	READ (NTAPEC) ALPHA	105
	READ (NTAPEC) NBODYS,NXLE,ZA,(XB(1),I=1,NBODYS)	106
	READ (NTAPEC) NTHETA,(THETAB(1),I=1,NTHETA)	
C	INPUT BODY VARIABLES	115
	READ (NTAPEI,5010) ARB	123
	CALL READ (NTAPEI,NTAPEO,NTAPEC,NBODYS,R)	124
	READ (NTAPEC) (ZDELTA(1),I=1,NBODYS)	125
	CALL READ (NTAPEI,NTAPEO,NTAPEC,NBODYS,ZDELTA)	132
	REWIND NTAPEC	133
	ARA=-ALPHA+ARB/CDR	
	WRITE (NTAPEO,6094) ZA	134
	IF (KONFIG .EQ. 2) GO TO 250	
C	WING-BODY CONFIGURATION	138
	CALL 9CAME(NBODYS,NROWB,XB,ZDELTA,XC,DZDXB,ACB)	
	CALL ETHICK(NBODYS,NBODY,NROWB,XB,R,XC,ALPHA,ALPHAS)	
C	WING ALONE OR WING-BODY CONFIGURATION	140
240	CONTINUE	
	NROWM=NROW(NRG)	
	NCOLW=NWING/NROWM	
	IF (KONFIG .EQ. 3) GO TO 250	
C	WING ALONE CONFIGURATION	
	ALPHA=0.	
	ARA=0.	
C	ANY CONFIGURATION	149
250	CONTINUE	150
	CALL FSF(7,NTAPEC,IRR)	151
	WRITE (NTAPEC) THICK,ARA	152
	END FILE NTAPEC	
	REWIND NTAPEC	
	ALPHAD=ALPHA+CDR	
	ARADEG=ARA+CDR	
	WRITE (NTAPEO,6090) ALPHAD	153
	WRITE (NTAPEO,6092) ARADEG	154
	IF (KONFIG.EQ.2) GO TO 420	
C	WING ALONE OR WING-BODY CONFIGURATION	
C	INPUT WING VARIABLES	
	GO TO (401,404,409),KASE	
401	CALL READ (NTAPEI,NTAPEO,NTAPEC,NWING,CL(NS))	161
	DO 402 J=NS,NPANEL	
	402 CL(J)=-CL(J)	

GO TO 411	172
404 READ (NTAPEI,5010) ARM,TWIST	
IF (TWIST -NE. 0.) GO TO 406	
DO 405 J=1,NCOLW	
405 ARWT(J)=0.0	
GO TO 407	
406 READ (NTAPEI,5010) (ARWT(I),I=1,NCOLW)	184
407 CONTINUE	
CALL PSF (2,NTAPEC,IRR)	192
CALL READ (NTAPEI,NTAPEQ,NTAPEC,NWING,ALPHA)	194
REWIND NTAPEC	195
DO 408 J=1,NWING	
JJ=(J-1)/NRONW+1	
408 ALPHA(I,J)=ALPHA(J)-ARA-(ARM+ARWT(JJ))/CDR	
GO TO 411	206
409 READ (NTAPEI,5010) CONSNT,CLBAR,XCPBAR	
IF (CONSNT -NE. 0.) GO TO 410	209
WRITE (NTAPEQ,6082) CLBAR	
GO TO 411	211
410 WRITE (NTAPEQ,6082) CLBAR	212
411 WRITE (NTAPEQ,6084) XCPBAR	
411 CONTINUE	
C WING ALONE OR WING-BODY CONFIGURATION	
IF (THICK) 440,420,440	
420 CONTINUE	216
CALL PSF(8,NTAPEC,IRR)	217
END FILE NTAPEC	218
REWIND NTAPEC	
IF (KONFIG-2) 470,425,472	
C WING-BODY CONFIGURATION WITHOUT WING THICKNESS	
425 CONTINUE	
DO 430 J=1,NBODY	
430 ALPHA(J)=0.	
GO TO 450	
C WING ALONE OR WING-BODY CONFIGURATION	
440 CONTINUE	
CALL TVEL(A,B,C,D,ALPHA,UNWT,VBWT,UNWT,VWWT,UNWT,	230
ALPHA,CHORD,THICK,NROW)	231
REWIND NTAPEC	232
REWIND NTAPEC	
IF (KONFIG .EQ. 1) GO TO 470	
C WING-BODY CONFIGURATION	
450 DO 460 J=1,NBODY	
JJ=J-((J-1)/NRONW)+NRONW	
ALPHA(J)=ALPHA(JJ)-(ARA	243
ABX(J)-ALPHA(J)	
460 CONTINUE	

C	ANY CONFIGURATION	
470	CONTINUE	
DO 471	J=1,MWING	
UMBT(J)=0.		
VMBT(J)=0.		
WMBT(J)=0.		
471	ALPHA(J)=0.	
IF (KONFIG.NE.1)	GO TO 472	265
CALL F5F(9,NTAPEC,IRR)		266
END FILE NTAPEC		267
REWIND NTAPEC		
GO TO 480		
472	CONTINUE	
BODY ALONE OR WING-BODY CONFIGURATION		
CALL KARMOR(NBODY5,NTHETS, 0.0,0.0,CPCALC,VOUT,ARA		
1,XP,ZP,RFAREA,XB,R,THETAS,ZDELTA,XC,YC,ZC,THETA,UMBT,VMBT,WMBT		
2,ALPHA,CPBB,BBCL,BBCL,BBCL,BBCL)		
480	CONTINUE	270
C	ANY CONFIGURATION	
500	CONTINUE	
CALL FCALC		
C	ANY CONFIGURATION	
READ ADDITIONAL POLARS		
IF (POLAR) 510,10,510		273
510	CONTINUE	
READ (NTAPE1,5010) DADEG		
IF (DADEG) 520,10,520		276
520	CONTINUE	
IPOLAR=1		
DARAD=DADEG/CDR		
ARA=ARA+DARAD		
ARADEG=ARA*CDR		
WRITE (NTAPE0,6002) TITLE		280
WRITE (NTAPE0,6008) DADEG		282
WRITE (NTAPE0,6092) ARADEG		283
IF (KONFIG.EQ. 2) GO TO 550		
C	WING ALONE OR WING-BODY CONFIGURATION	
DO 530	I=1,MWING	
530	ALPHA(I)=ALPHA(I)-DARAD	
IF (KONFIG.EQ. 1) GO TO 550		
C	WING-BODY CONFIGURATION	

```

DD 540 I=1,NBODY
540 ALPHAB(I)=ALPHAB(I)-DARAD*COS(THETA(I))
C ANY CONFIGURATION
550 CONTINUE
IF (KONFIG-2) 470,472,470
999 CONTINUE
RETURN
5000 FORMAT(12A6)
5010 FORMAT(7F10.0)
6002 FORMAT(1H1,12A6,30X,2A6)
6008 FORMAT(1H0,23HDELTA ANGLE OF ATTACK =,F10.4,2X,4HDEG.)
6082 FORMAT(1H0,27HHING OPTIMIZED FOR CL BAR =,F10.4)
6084 FORMAT(1H , 18X,9HXCP BAR =,F10.4)
6090 FORMAT(1H0,56HINCLINATION OF BODY AXIS WITH RESPECT TO DEFINING AX
IIS =,F10.4,2X,4HDEG.)
6092 FORMAT(1H0,43HANGLE OF ATTACK WITH RESPECT TO BODY AXIS =,F10.4,
12X,4HDEG.)
6094 FORMAT(1H0,38HHEIGHT OF WING PLANE ABOVE BODY AXIS =,F10.4)
END

```

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```

C      SUBROUTINE FROOTA(R,J)
C
C      DIMENSION R(10),F(10)
C
C      FROOTA IS A ROOT FINDER, DESIGNED TO BE CALLED REPEATEDLY
C      UNTIL CODE J INDICATES THAT A ROOT HAS BEEN FOUND.
C
C      ASSUME A SINGLE-VALUED FUNCTION F(X) WHICH THE CALLING PROGRAM
C      CAN EVALUATE FOR ANY X. FURTHER, THE PROGRAM KNOWS THAT THE
C      ROOT LIES BETWEEN XA AND XB.
C
C      ON THE FIRST CALL FOR A CASE, THE PROGRAM STORES
C      XA,F(XA),XB,F(XB) IN R(1),R(2),R(3),R(4), 0. IN R(9),
C      AND A TOLERANCE IN R(10).
C
C      FROOTA THEN COMPUTES TWO VALUES OF X, SAY XC AND XD,WHICH IT
C      STORES IN P(1) AND R(3), AND SETS J=1 WHICH INDICATES THAT
C      IT WANTS TO BE CALLED AGAIN. THE CALLING PROGRAM
C      RESPONDS BY STORING F(XC) IN R(2) AND F(XD) IN R(4), AND
C      THEN CALLING FROOTA. THIS PROCESS CONTINUES UNTIL FROOTA
C      SIGNALS THAT THE ROOT HAS BEEN FOUND BY SETTING J=0.
C
C      FROOTA KEEPS THE POINTS WHICH BRACKET THE ROOT IN R(5)-R(8).
C      THE ROOT IS CONSIDERED TO BE FOUND WHEN
C      (1) AN EXACT ROOT IS FOUND.
C      OR (2) THE DIFFERENCE IN X-VALUES OF THE BRACKETING POINTS IS
C           SMALLER THAN THE GIVEN TOLERANCE IN R(10)
C      OR (3) THE ROOT HAS BEEN LOCATED TO THE NEAREST 1-BIT CHANGE IN X.
C
C      FROOTA ESTIMATES ONE VALUE OF X AS HALF-WAY BETWEEN THE X,S OF
C      THE BRACKETING POINTS, AND THE OTHER BY ASSUMING THE
C      FUNCTION IS LINEAR BETWEEN THE BRACKETING POINTS.
C
C      J IS SET TO -2 OR -3 IF IT DETECTS AN ERROR.
C      J = -2 IF R(9) IS .LT. 0.
C      J = -3 IF (ON THE 1ST CALL ONLY) THE POINTS IN R(1)-R(4)
C      DO NOT BRACKET THE ROOT (I.E., IF F(A)*F(B) .GT. 0.)
C
C      R(9) IS A COUNTER (INCREASED BY 1. AT EACH CALL).
C
C      J=1
C      DO 100 I=1,10
C      F(I)=R(I)
C      F(9)=F(9)+1.
C
C      IF(F(9))-1.1200,300,1000
C      J=-2
C      GO TO 8000
C
C      IF(F(2)*F(4))500,1300,400
C      J=-3
C      GO TO 8000
C      THE BRACKETING POINT WITH THE SMALLER X IS STORED IN R(5),R(6)
C      IF(F(1) .LT. F(3)) GO TO 1800

```

1
 2
 3
 4
 5
 6
 7
 8
 9
 10
 11
 12
 13
 14

FRODTA		07/31/65
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
600	F(5)=F(3)	.15
	F(6)=F(4)	.16
	GO TO 1700	
C		.17
1000	IF(F(1) .LE. F(3)) GO TO 1200	.18
C	REVERSE THE 2 NEW POINTS SO ONE WITH SMALLER X WILL BE FIRST	.19
1100	F(1)=F(3)	.21
	F(2)=F(4)	.22
	F(3)=R(1)	.23
	F(4)=R(2)	
C		.24
1200	CONTINUE	.25
	IF(F(2)*F(4)) 1800,1300,1500	
C		.26
1300	CONTINUE	.27
	IF(F(2)) 1400,3000,1400	.28
1400	F(1)=F(3)	.29
	GO TO 3000	
C		.30
1500	IF(F(2)*F(6)) 1700,1700,1600	.31
1600	F(5)=F(3)	.32
	F(6)=F(4)	.33
	GO TO 2000	
C		.34
1700	CONTINUE	.35
	F(7)=F(1)	.36
	F(8)=F(2)	.37
	GO TO 2000	
C		.38
1800	CONTINUE	.39
	F(5)=F(1)	.40
	F(6)=F(2)	.41
	F(7)=F(3)	.42
	F(7)=F(3)	.43
	F(8)=F(4)	.44
	IF(F(1) .EQ. F(7)) GO TO 3000	
C		.45
2000	CONTINUE	.46
	FIND NEW TRIAL VALUES OF X	.47
C		.48
	F(3)=.5*(F(5)+F(7))	.49
	U=F(7)-F(5)	.50
	V=F(8)-F(6)	
C	WE COMPUTE F(1) IN TWO WAYS TO IMPROVE ACCURACY	.51
	IF(ABS(F(6))-ABS(F(8))) 2100,2100,2300	.52
2100	F(1)=F(5)-(F(6)/V)*U	.53
	IF(F(1) .EQ. F(5)) GO TO 3000	.54
	GO TO 2500	.55
2300	F(1)=F(7)-(F(8)/V)*U	.56
C		.57
2500	CONTINUE	.58
	IF(U .GT. ABS(F(10))) GO TO 8000	.59
C		.60
3000	CONTINUE	.61
	J=0	.62
		.63

EDCOTA		07/31/65	
EXTERNAL FORMULA NUMMER	SOURCE STATEMENT	-	INTERNAL FORMULA NUMBER(S)
C	8000 CONTINUE		,64
	20 3100 I=1,10		,65
	8100 R(I)=F(I)		,66
	9000 RETURN		,67 ,68
	END		,69
			,70

05/22/67

FRUNDOO I

**FROM
ASSEMBLED TEXT.**

STEXT FROM

BINARY	CARD ID.	FRUN0002	
00000	000000000000	10000	
00001	265164456040	10000	
00002	1 000000 0 00007	10001	
00003	0774 00 4 00000	10000	
00004	0441 00 0 00006	10001	
00005	0020 00 4 00001	10000	
00006	0 00000 0 00000	10000	
00007	0604 00 0 00006	10001	
00010	0634 00 4 05000	10011	
00011	0634 00 4 00000	10001	
00012	0634 00 4 00003	10001	
00013	0500 60 4 00003	10000	
00014	0401 00 0 03000	10011	
00015	000000000000	00010	
00015	0074 00 4 04000	10011	
00016	1 00002 0 10004	10011	
00017	0 00000 0 00005	10100	
00020	0 00000 0 03000	10011	
00021	0 00000 0 03001	10011	

LDIR
UNLOAD SAVE

```
CLA# 3,4  
STO TEMP  
CALL .FVIO.(TEMP,TEMP+1)
```

BINARY	CARD ID.	FRUN0003	
00022	0535 00 4	03001	10011
00023	0636 00 4	00025	10001
00024	0074 00 4	06000	10011
00025	0 00000 0	00000	10000
		00026	
		00027	
00027	100000000027		00001
00027	200000000002		00001
00031	2000000000022		00001
		00000	01111

```

LAC      TEMP+1,4
SCA      SETB,4
TSX      .CLOSE,4
PZE      **
RETURN   UNLOAD
LONG
CONTROL  ER
USE      ER
BSS      2
BSS      10
END

```

05/22/67

FRUN
CONTROL DICTIONARY
\$CDICT FRUN

FRUN0004

BINARY CARD ID. FRUN0005
000053000000
000004000005
265164456060
000053000000
644543462124
000000000002
255121622560
000024000027
332665314633
200000100000
627062434623
200000000000
332343462225
200000000000

START=0,LENGTH=43,TYPE=7094,CNPLX=5
LOC=0,LENGTH=43
LOC=2,LENGTH=0
LOC=27,LENGTH=20
SECT. 4,CALL
SECT. 5
SECT. 6

PREFACE
FRUN DECK
UNLOAD REAL
ERASE REAL
.FVIO. VIRTUAL
SYSLOC VIRTUAL
.CLOSE VIRTUAL

FRUN0006

\$DKEND FRUN

NO MESSAGES FOR THIS ASSEMBLY

07/31/65

FTAN
IFJ33 LIBRARY / TANGENT FUNCTION

```

00035 0771 00 0 00001 10000
00037 0100 00 0 00124 10001
*
* IF X GREATER THAN PI/2, PLACE IN PROPER QUADRANT
*
00040 0500 00 0 03000 10011
00041 4130 00 0 00000 10000
00042 0500 00 0 00172 10001
00043 0040 00 0 00053 10001
00044 0500 00 0 03000 10011
00045 4120 00 0 00051 10001

```

BINARY CARD (NOT PUNCHED)

```

00046 0302 00 0 00165 10001
00047 0601 00 0 03000 10011
00050 0020 00 0 00054 10001
00051 0300 00 0 00165 10001
00052 0601 00 0 03000 10011
*
00053 0500 00 0 03000 10011
00054 0760 00 0 00003 10000
00055 0560 00 0 00173 10001
00056 0040 00 0 00061 10001
*
* TAN X = CONTINUED FRACTION
*
00057 0074 00 4 00076 10001
00058 0020 00 0 00074 10001
*
* TAN X = 1/TAN(PI/2-ABS X)
*
00061 0500 00 0 03000 10011
00062 4120 00 0 00065 10001
00063 0302 00 0 00172 10001
00064 0760 00 0 00002 10000
00065 0020 00 0 00070 10001
00066 0300 00 0 00172 10001
00067 0760 00 0 00002 10000
00070 0601 00 0 03000 10011

```

BINARY CARD (NOT PUNCHED)

```

00071 0074 00 4 00076 10001
00072 0500 00 0 00161 10001
00073 0241 00 0 03002 10011
*
00074 0131 00 0 00000 10000
00075

```

```

FTAN0440
FTAN0450
FTAN0460
FTAN0470
FTAN0480
FTAN0490
FTAN0500
FTAN0510
FTAN0520
FTAN0530
FTAN0540
FTAN0550

FTAN0550
FTAN0560
FTAN0570
FTAN0580
FTAN0590
FTAN0600
FTAN0610
FTAN0620
FTAN0630
FTAN0640
FTAN0650
FTAN0660
FTAN0670
FTAN0680
FTAN0690
FTAN0700
FTAN0710
FTAN0720
FTAN0730
FTAN0740
FTAN0750
FTAN0760
FTAN0770
FTAN0780
FTAN0790
FTAN0800
FTAN0810

FTAN0820
FTAN0830
FTAN0840
FTAN0850
FTAN0860
FTAN0870
FTAN0880
FTAN0890
FTAN0900
FTAN0910
FTAN0920
FTAN0930

```

```

ALLOW 1 BIT RANGE
ERROR, X=PI/2

COMMON
X
ABS X
TEST IF X GREATER THAN PI/2
NO, X OK
YES, PLACE IN PROPER QUADRANT

QUADRANT 2
X REPLACED BY X-PI

QUADRANT 3
X REPLACED BY -X+PI

ABS X
TEST IF X GREATER THAN PI/4
YES

CONTR,4
TAN9

IS X NEGATIVE
YES
NO
REPLACE X BY PI/2-X

PEPLACE X BY -(PI/2-ABS X)

TAN(PI/2-ABS X)
1.0
TAN X = 1/TAN(PI/2-ABS X)

ANSWER IN ACCUMULATOR
RETURN

X

5,1
COMMON
COMMON

```

07/31/65

FTAN
IRJOR LIBRARY / TANGENT FUNCTION

00101	0601	00	0	03001	10011	STO	COMMON+1	X**2	FTAN0940
00102	0500	00	0	00154	10001	CLA	A6	A(6)=11.	FTAN0950
00103	0601	00	0	03002	10011	STO	COMMON+2	-X**2	FTAN0960
00104	0502	00	0	03001	10011	TAN12	COMMON+1		FTAN0970
00105	0241	00	0	03002	10011	FDP	COMMON+2		FTAN0980
00106	0131	00	0	00000	10000	XCA			FTAN0990
00107	0300	00	1	00162	10001	FAD	A1+1,1	A(1)	FTAN1000
00110	0601	00	0	03002	10011	STO	COMMON+2		FTAN1010
00111	2	00001	1	00104	10001	TIX	TAN12,1,1	5 TIMES	FTAN1020
00112	0500	00	0	03000	10011	CLA	COMMON	X	FTAN1030
00113	0241	00	0	03002	10011	FDP	COMMON+2		FTAN1040

BINARY CARD (NOT PUNCHED)

00114	4600	00	0	03002	10011	STO	COMMON+2		FTAN1050
00115	0020	00	4	00001	10000	TRA	1,4		FTAN1060
00116	00000000000000				00010	ERROR1 CALL	.5XEM.(BAIL)	ABS X TOD LARGE	FTAN1070
00117	0074	00	4	04000	10011				FTAN1080
00118	1	00001	0	01003	10011				FTAN1090
00119	0	00162	0	00202	10100				FTAN1100
00120	0	00000	0	00134	10001				
00121	4754	00	0	00000	10000	ZAC		SET RESULT TO ZERO	
00122	00000000000000				00010	RETURN	TAN		
00123	0074	00	4	04000	10011	ERROR2 CALL	.5XEM.(GIVE)	X ODD MULTIPLE	
00124	1	00001	0	01003	10011				
00125	0	00162	0	00217	10100				
00126	0	00000	0	00144	10001				
00127	0500	00	0	03000	10011	CLA	COMMON		
00128	0760	00	0	00000	10000	CLM		SET RESULT TO LARGEST NUMBER	
00129	00000000000000				00000	COM		WITH CORRECT SIGN.	
00130	00000000000000				00000	RETURN	TAN		
00131	00000000000000				00000	DEC	67		
00132	00000000000000				00000	BAIL			
00133	00000000000000				00000				

BINARY CARD (NOT PUNCHED)

00135	0	00003	0	00137	10001	PZE	MESA,3		FTAN1172
00136	0	00002	0	00142	10001	PZE	MESB,2		FTAN1173
00137	002122626067				10000	MESA	3,0ABS X TOD LARGE		FTAN1174
00138	606345466043				10000	MESB			
00139	215127256060				10000		2,0ANS = 0		FTAN1175
00140	00000000000000				10000	GIVE			
00141	00000000000000				10000	DEC	66		FTAN1176
00142	00000000000000				10001	PZE	MESC,3		FTAN1177
00143	0	00003	0	00147	10001	PZE	MESD,2		FTAN1178
00144	000002	0	00152	10000	10000	MESC	3,0X ODD MULTIPLE		FTAN1179
00145	006760462424				10000				
00146	604464436331				10000	MESD			FTAN117A
00147	474325606060				10000		2,0ANS=.17E39		
00148	002145621333				10000				FTAN1180
00149	010725031160				10000				FTAN1190

07/31/65

FTAN
18JOB LIBRARY / TANGENT FUNCTION

FTAN1200
FTAN1210

11..9..7..5..3.

DEC

* A6

00154 204540000000
00155 204440000000
00156 203700000000
00157 203500000000

LIBRARY CARD (NOT PUNCHED)

00160 202600000000
00161 201400000000

1.

DEC

* AI

10000
10000

FTAN1220
FTAN1230
FTAN1240
FTAN1250
FTAN1260
FTAN1270

* LK-DR LDIR

LOG

00162 000000000000
00163 266321456060
00164 234622077325
00165 202622077325
00166 163643334273
00167 233400000000
00170 177505746033
00171 200000000000
00172 201622077325
00173 200622077325

FTAN1280
FTAN1290
FTAN1300
FTAN1310
FTAN1320
FTAN1330
FTAN1340
FTAN1350
FTAN1360
FTAN1370
FTAN1380

* FRASE CONTRL ER
USE ER
COMMON BSS 3
BSS 17

00001 100000000174
00001 200000000003
00001 200000000021

END

00000 01111

FVID
FVID - FORTRAN VARIABLE I/O LOGICAL UNIT
08/16/65

CALLING SEQUENCE IS CALL .FVID.(LN,ERAS) WHERE LN IS
LOCATION OF VARIABLE LOGICAL UNIT AND ERAS WILL CONTAIN
CONTENTS OF APPROPRIATE .UNXX. (.UNXX. CONTAINS
PZE UNITXX WHERE XX CORRESPONDS TO LOGICAL UNIT N).
FVID IS CALLED FOR ANY I/O STATEMENT SPECIFYING
A VARIABLE LOGICAL UNIT.

BINARY CARD (NOT PUNCHED)		.FVID. SAVE (2)		PICK UP LOGICAL UNIT NUMBER		IS UNIT ZERO, OR TOO LARGE		SAVE ADDRESS OF FILE CONTROL BLOCK		LOGICAL UNIT IN ERAS		DEFINED FOR THIS UNIT VALUE. CONVERT THIS ILLEGAL VALUE TO DECIMAL FOR ERROR MESSAGE.	
00000	1 00000 0 00004	10001		CLA*	3,4								
00001	0774 00 2 00000	10000		PAC	2								
00002	0774 00 4 00000	10000		TXL	ERROR,2,-NUNITS-1								
00003	0020 00 4 00001	10000											
00004	0634 00 4 04000	10011											
00005	0634 00 4 06102	10001											
00006	0634 00 4 00002	10001											
00007	0634 00 2 00001	10001											
00010	0500 60 4 00003	10000											
00011	0737 00 2 00000	10000											
00012	7 00000 2 00016	11101											
	1 00070 0 00102	10101											
	1 00001 0 00000	10011											
	1 00000 0 00000	11100											
	1 00001 7 00000	10011											
00013	0500 60 2 00070	10001											
00014	0601 60 4 00004	10000											
		00015											
00016	0500 60 4 00003	10000											
BINARY CARD (NOT PUNCHED)		ANA		ADMSK									
00017	4320 00 0 00064	10001											
00020	0131 00 C 00000	10000											
00021	0774 00 4 00000	10000											
00022	0600 00 0 00065	10001											
00023	0754 00 0 00000	10000											
00024	0221 00 0 00066	10001											
00025	0767 00 4 00000	10000											
00026	4602 00 0 00065	10001											
00027	0500 00 0 00104	10001											
00030	0040 00 0 01002	10011											
00031	1 77772 4 00023	10001											
00032	4500 00 C 00067	10001											
00033	0767 00 4 00006	10000											
00034	4501 00 0 00065	10001											
00035	0602 00 0 00054	10001											
00036	000000000000	00010											
00037	0074 00 4 03000	10011											
00040	0 00102 0 00053	10100											
BINARY CARD (NOT PUNCHED)		UNERR		CALL									
00041	0 00000 0 00043	10001											


```

C SUBROUTINE GEOMD(DAT,LI,LC,LERR,LTAPE)
  GEOMETRIC DEFINITION LINK
  DIMENSION BUF(10000),DICT(9),NU(3),LOK(3,9),DAT(2)
  1  .RAXIS(2).BTITLE(12).WTITLE(12)
  COMMON /LGEOMD/LGDEF(3,6)
  LOGICAL LGDEF,LGTAPE,LTDUMP
  EQUIVALENCE (LOK(1,1),LWPL),(LOK(2,1),MWPPL),(LOK(3,1),NUMPL),
X(LOK(1,2),LLWPL),(LOK(2,2),MLWPL),(LOK(3,2),NLWPL),
X(LOK(1,3),LWPLX),(LOK(2,3),MWPLX),(LOK(3,3),NUMPLX),
X(LOK(1,4),LLWPLX),(LOK(2,4),MLWPLX),(LOK(3,4),NLWPLX),
X(LOK(1,5),LBPL),(LOK(2,5),MBPL),(LOK(3,5),NBPL),
X(LOK(1,6),LSTA),(LOK(2,6),NSTA),
X(LOK(1,7),LWPF),(LOK(2,7),MWPF),(LOK(3,7),NMWPF),
X(LOK(1,8),LWUB),(LOK(2,8),MWUB),
X(LOK(1,9),LLWB),(LOK(3,9),NLWB)
  DATA DICT/4HBODY,4HBODY,4HWING,4HWING,6HDEFEND,3HWBX,
1 6HNOTAPE,6HNOTAPE,5HTDUMP/,LGTAPE/T/,
1  NBUF,NDICT,NU(3),LOK/10000, 9,50,27*0/

C INTWB IS USED BY DEFEND
C INTWB=0
C LTDUMP=.FALSE.

C THE LGDEF ARRAY (LOGICAL) TELLS THE STATUS OF DEFINITION.
C LGDEF(I,J) HAS FOLLOWING FORMAT.
C J=1, UPPER WING. J=2, LOWER WING. J=3, BODY. J=4, WING
C PLANFORM. J=5, UPPER WING INTERSECTION. J=6, LOWER WING.
C I=1, REQUESTED. I=2, SUCCESSFULLY DEFINED.
C I=3, DEFINITION ON TAPE (LTAPE).

C DO 100 J=1,6
C DO 100 I=1,3
100 LGDEF(I,J)=.FALSE.

C CHECK LTAPE
C IF (LTAPE*(LTAPE-40))430,420,420
420 LGTAPE=.FALSE.
C
430 NUI(2)=LERR
C SET UP STORAGE BUFFER
C CALL INIBFR(BUF,NBUF)
C
C READ DATA CARD, SEE IF VALID COMMAND
500 WRITE(LO,501)
501 FORMAT(IH1)
502 IGO=INTURP(DICT,NDICT,LI,LC)
C
C IF (IGO)510,510,530
C NOT VALID
510 WRITE (LO,520)
520 FORMAT(IH+ 90X,7HCOMMENT)
GO TO 502

```

,1

,2
,3
,4

,5 ,6 ,7

,8

,9

,10

,11 ,12 ,13

,14

,15

,16 ,17

CLOMD		10/04/85
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
C	330 GO TO (800,800,1000,1000,1600,2000,1700,1700, X 2100),160	,18
C	C	
C	800 BODY	,19
C	800 CALL BODY1(DAT,LI,LO,BUF,LSTA,NSTA,LBPL,NBPL,LTHETA 1,BAXIS,BTITLE,LGDEF,NU)	,20
C	810 GO TO 500	
C	C	
C	1000 WING	,21
C	1000 CALL WINGA(BUF,LI,LO,DAT,LGDEF,LOK,LWPF,WTITLE,NU)	,22
C	1010 CONTINUE	,23
C	GO TO 500	
C	C	
C	DEFEND	,24
C	1600 GO TO 2050	
C	C	
C	NOTAPE	,25
C	1700 LGTAPE=.FALSE.	,26
C	GO TO 500	
C	C	
C	WBX	,27
C	2000 INTWB=-1	
C	C	,28
C	2050 CALL DEFEND(BUF,LOK,LO,LTAPE,LGDEF,LGTAPE,INTWB)	,29
C	IF(INTWB)2060,2080,2080	
C	C	,30
C	2060 INTWB=1	,31
C	CALL WBXUL(BUF,LI,LO,DAT,LGDEF,LOK,BTITLE,WTITLE,BAXIS,NU)	,32
C	2070 GO TO 500	
C	C	,33
C	2080 IF(.NOT. LTUMP) GO TO 9000	,35
C	CALL TDUMP(LO,LTAPE,LGDEF)	,34
C	GO TO 9000	,37
C	C	
C	TDUMP	,38
C	2100 LTUMP=.TRUE.	,39
C	GO TO 500	
C	C	,40
C	9000 CALL CLEAR(BUF)	,41
C	RETURN	,42
C	END	,43

09/08/67

GPIDS - EFN SOURCE STATEMENT - IFNIS)

```

SUBROUTINE GRIDS
COMMON /GRIDA/ MODE,DX,DY,DZ,IX,IY,IZ,XO,YO,ZO,XA,YA,ZA,LIT
COMMON DUM(4),N8,DM(3),N5,N6
COMMON /INTGA/GP(3,500),VLS(4,500)
DATA 8X/1HX/.8Y/1HY/.8Z/1HZ/
DATA NMAX/500/
INTEGER 8X,8Y,8Z
1000 FORMAT(1H0,3F15.6,5X,3F15.7,5X,F15.7)
1001 FORMAT(1H0,24HY-Z CUT, FOR THIS CUT X=F10.5)
1002 FORMAT(1H0,7X,1HX,14X,1MY,14X,1HZ,16X,1HU,14X,1HV,14X,1HW,16X,1HCP
    S)
1003 FORMAT(1H0,24HX-Z CUT, FOR THIS CUT Y=F10.5)
1004 FORMAT(1H0,24HX-Y CUT, FOR THIS CUT Z=F10.5)
1005 FORMAT(1H-,35OPTION REQUESTED---RECTANGULAR GRID)
1006 FORMAT(1H-,28OPTION REQUESTED---SKEW GRID)
1007 FORMAT(1H1)
IF(BLUNDR(IX,IY,IZ,MODE,NMAX).NE.0.) RETURN
IF(MODE.EQ.4) GO TO 101
WRITE(N6,1005)
GO TO (1,21,40),MODE
1 DO 20 I=1,IX
    IC=0
    DO 5 K=1,IZ
        DO 5 J=1,IY
            IC=IC+1
            GP(1,IC)=XO+FLOAT(I-1)*DX
            GP(2,IC)=YO+FLOAT(J-1)*DY
            GP(3,IC)=ZO+FLOAT(K-1)*DZ
            CALL COMP(GP,VLS,IC)
            WRITE(N6,1007)
            WRITE(N6,1001) GP(1,1)
            WRITE(N6,1002)
            WRITE(N6,1000) (GP(1,J),GP(2,J),GP(3,J),VLS(1,J),VLS(2,J),VLS(3,J),
    S,VLS(4,J)),J=1,IC)
            CALL FLOUT(IC)
20 CONTINUE
GO TO 500
21 CONTINUE
DO 30 J=1,IY
    IC=0
    DO 22 K=1,IZ
        DO 22 I=1,IX
            IC=IC+1
            GP(1,IC)=XO+FLOAT(I-1)*DX
            GP(2,IC)=YO+FLOAT(J-1)*DY
            GP(3,IC)=ZO+FLOAT(K-1)*DZ
            CALL COMP(GP,VLS,IC)
            WRITE(N6,1007)
            WRITE(N6,1003) GP(2,1)
            WRITE(N6,1002)
            WRITE(N6,1000) (GP(1,L),GP(2,L),GP(3,L),VLS(1,L),VLS(2,L),VLS(3,L),
    S,VLS(4,L)),L=1,IC)
            CALL FLOUT(IC)

```

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08/08/67

GRIDS - EFN SOURCE STATEMENT - IFN(S) -

```

30 CONTINUE
GO TO 500
40 CONTINUE
DO 50 K=1,12
IC=0
DO 42 I=1,IX
DO 42 J=1,IY
IC=IC+1
GP(1,IC)=XO*FLOAT(I-1)*DX
GP(2,IC)=YO*FLOAT(J-1)*DY
42 GP(3,IC)=ZO*FLOAT(K-1)*DZ
CALL CCMP(GP,VLS,IC)
WRITE(N6,1004) GP(3,1)
WRITE(N6,1002)
WRITE(N6,1000) (GP(1,J),GP(2,J),GP(3,J),VLS(1,J),VLS(2,J),VLS(3,J)
$ ,VLS(4,J),J=1,IC)
CALL FLOUT(IC)
50 CONTINUE
GO TO 500
101 CONTINUE
WRITE(N6,1007)
WRITE(N6,1006)
S=SQRT((XO-XA)**2+(YO-YA)**2+(ZC-ZA)**2)
XAS=S/(XA-XC)
YAS=S/(YA-YC)
ZAS=S/(ZA-ZC)
IF(LIT.EQ.9Y) GO TO 120
IF(LIT.EQ.9Z) GO TO 130
IF(DY.EQ.0.) GO TO 108
DS=DY*YAS
IS=IY
GO TO 110
108 DS=DZ*ZAS
IS=IZ
110 IC=0
DO 112 I=1,IX
DO 112 J=1,IY
IC=IC+1
GP(1,IC)=XO*FLOAT(J-1)*DS/XAS+FLOAT(I-1)*DX
GP(2,IC)=YO*FLOAT(J-1)*DS/YAS
112 GP(3,IC)=ZO*FLOAT(J-1)*DS/ZAS
CALL CCMP(GP,VLS,IC)
WRITE(N6,1002)
WRITE(N6,1000) (GP(1,J),GP(2,J),GP(3,J),VLS(1,J),VLS(2,J),VLS(3,J)
$ ,VLS(4,J),J=1,IC)
CALL FLOUT(IC)
GO TO 500
120 CONTINUE
IF(DX.EQ.0.) GO TO 124
DS=DX*XAS
IS=IX
GO TO 125
124 DS=DZ*ZAS
IS=IZ

```

c7
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08/08/67

GRIDS - EFM SOURCE STATEMENT - IFN(S) -

```

125 IC=0
DO 127 I=1,1Y
DO 127 J=1,1S
  IC=IC+1
  GP(1,IC)=XO+FLOAT(J-1)*DS/XAS
  GP(2,IC)=YO+FLOAT(J-1)*DS/YAS+FLOAT(I-1)*DY
127 GP(3,IC)=ZO+FLOAT(J-1)*DS/ZAS
  CALL COMP(GP,VLS,IC)
  WRITE(N6,1002)
  $,VLS(4,J),J=1,IC)
  CALL FLCOUT(IC)
  GO TO 500
130 CONTINUE
  IF(IX.EQ.0.) GO TO 133
  DS=DX*XAS
  IS=IX
  GO TO 134
133 DS=DY*YAS
  IS=1Y
134 CONTINUE
  IC=0
  DO 135 I=1,1Z
  DO 135 J=1,1S
    IC=IC+1
    GP(1,IC)=XO+FLOAT(J-1)*DS/XAS
    GP(2,IC)=YO+FLOAT(J-1)*DS/YAS
135 GP(3,IC)=ZO+FLOAT(J-1)*DS/ZAS+FLOAT(I-1)*DZ
    CALL COMP(GP,VLS,IC)
    WRITE(N6,1002)
    $,VLS(4,J),J=1,IC)
    CALL FLCOUT(IC)
  500 CONTINUE
  RETURN
  END

```

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```

CIADARY      MICHAEL SYNGE      6-9247      COMPILED 21 AUG 64
FUNCTION IADARY(APRAY,IN,PR,NARAY)
DIMENSION ARRAY(1),BFR(1)

C TO ADD AN ARRAY TO A BUFFER
C
C      I - THE LENGTH OF THE CURRENT ARRAY
C      M - FIRST WORD OF CURRENT ARRAY
C      MM - THE TOTAL LENGTH OF THE BUFFER
C      N - THE LENGTH OF THE ARRAY TO BE ADDED
C
C      SEARCH FOR A FREE ARRAY WHICH IS BIG ENOUGH
C
      N=IABS(IN)
      K=0
      IF(ICODE(BFR)-4)95,1,95
      1 MM=-IBFR(BFR(3))
      2 M=4
      3 I=LENG(BFR(M-1))
      4 IF(ICODE(BFR(M-2)))5,4,5
      5 M=M+I+2
      IF(M-MM)3,6,6

C      PACK THE BUFFER IF NECESSARY
C
      IF(K)90,7,90
      7 K=1
      IF(IPACK(BFR))85,85,2

C      FREE ARRAY FOUND
C      SET UP CODE WORDS
C
      10 IADARY=M
      IF(IN)25,25,15
      15 DO 20 K=1,N
      BFR(M)=APRAY(K)
      20 M=M+1
      25 BFR(IADARY-1)=ARSEC(I,NARAY)
      BFR(IADARY-2)=ARFUL(IADARY)
      30 NARAY=IADARY
      CALL IRLAS(BFR(IADARY),N)
      80 RETURN
C
C      ERRORS
C
      85 IADARY=-1
      GO TO 80
      90 IADARY=-2
      GO TO 80
      95 IADARY=-3
      GO TO 80
      END

```

IADA0030
 IADA0040
 IADA0060
 IADA0070
 IADA0090
 IADA0100
 IADA0110
 IADA0120
 IADA0130
 IADA0140
 IADA0150
 IADA0160
 IADA0170
 IADA0180
 IADA0190
 IADA0200
 IADA0210
 IADA0220
 IADA0230
 IADA0240
 IADA0250
 IADA0260
 IADA0270
 IADA0280
 IADA0290
 IADA0300
 IADA0310
 IADA0320
 IADA0330
 IADA0340
 IADA0350
 IADA0360
 IADA0370
 IADA0380
 IADA0390
 IADA0400
 IADA0410
 IADA0420
 IADA0430
 IADA0440
 IADA0450
 IADA0460
 IADA0470
 IADA0480
 IADA0490
 IADA0500
 IADA0510
 IADA0520
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 IADA0550
 IADA0560

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IBFR
7094 RELMOD ASSEMBLY.

\$IBLDQ IBFR
ASSEMBLED TEXT.

\$TEXT IBFR

07/31/65

IBFR0000

IBFR0001

ASSEMBLED 21 AUG 64

MICHAEL SYNGE

6-9247

*IBFR

* TO LOCATE THE FIRST CELL OF A BUFFER
* RELATIVE TO THE FIRST CELL OF AN ARRAY

CALLING SEQUENCE

M=IBFR (ARRAY)

NOTE - M IS ALWAYS NEGATIVE
UNLESS THE GIVEN ARGUMENT IS
NOT THE FIRST WORD OF AN ARRAY.

ENTRY IBFR

BINARY CARD (NOT PUNCHED)

00000	0500 00 4 30003	10300	IBFR	CLA	3,4
00001	0402 00 0 00017	10001		SUR	=2
00002	0021 00 0 00003	10001	A	STA	A
00003	4500 00 0 00009	10000		CAL	**
00004	0621 00 0 00016	10001		STA	R
00005	4320 00 0 00020	10001		ANA	=077777700000
00006	4340 00 0 00021	10001		LAS	=0700000
00007	0020 00 0 00011	10001		TRA	FRPOR
00010	0020 00 0 00013	10001		TRA	SUCCESS
00011	0500 00 0 00022	10001	ERRDP	CLA	=1
00012	0020 00 0 00015	10001		TRA	EXIT
00013	0500 00 0 00016	10001	SUCCESS	CLA	9
00014	4760 00 0 00003	10000		SSM	
00015	0020 00 4 00001	10000	EXIT	TRA	1,4
00016	0 0000 0 00000	10000	*		
00017	0000 00000002	10000		*LORG	
00020	077777700000	10000			
00021	000007000000	10000			
00022	000000000001	10000			

BINARY CARD (NOT PUNCHED)

00000	01111
-------	-------

END

07/31/65

IBFR
CONTROL DICTIONARY

IBFR0302

\$CDICT IBFR

BINARY CARD (NOT PUNCHED)
000023000000
000004000005
312226516060
000023000000
312226516060
000000000000

PREFACE
DECK
REAL

IBFR
IBFR

START=0,LENGTH=19,TYPE=7094,CAPLX=5
LOC=0,LENGTH=19
LOC=0,LENGTH=0

IBFR0303

\$DKEND IBFR

NO MESSAGES FOR THIS ASSEMBLY
SYMBOL REFERENCE DATA

REFERENCES TO DEFINED SYMBOLS.

CLASS	SYMBOL	VALUE	REFERENCES
A		00003	2
9		00016	4,13
ERROR		00011	7
EXIT		00015	12
IBFR		00000	
LCTR	RLCTR		
QUAL	UNOS		
LCTR	//		
	SUCES	00013	10

ICODE
7C94 RELMOD ASSEMBLY.

07/31/65

\$IBLOR ICODE
ASSEMBLED TEXT.

ICOD00000

\$TEXT ICODE

ICOD00001

ASSEMBLED 21 AUG 64

MICHAEL SYNGE 6-9247
TO VERIFY THAT THE GIVEN WORD
IS INDEED THE FIRST CODE OF AN
ARRAY AND TO CONVERT ITS PREFIX
INTO AN ADDRESS INTEGER. THE
RESULT IS -1 IF THE WORD IS
NOT THE EXPECTED CODE.

CALLING SEQUENCE

I=ICODE(A)

ENTRY ICODE

BINARY	CARD (NOT PUNCHED)	ICOD00000	ICOD00001	LDQ*	ENTRY	ICOD00000	ICOD00001
00000	0560 60 4 00003	10000	10000	3+4			
00001	0754 00 0 00000	10000	10000	0+0			
00002	4763 00 0 00003	10000	10000	3			
00003	0600 00 0 00016	10001	10001	STZ			
00004	0621 00 0 00016	10001	10001	STA			
00005	4130 00 0 00000	10000	10000	XCL			
00006	4320 00 0 00017	10001	10001	ANA			
00007	4340 00 0 00020	10001	10001	LAS			
00010	0020 00 0 01002	10011	10011	TRA			
00011	0020 00 0 00014	10001	10001	TRA			
00012	0500 00 0 00021	10001	10001	CLA			
00013	0020 00 0 00015	10001	10001	TRA			
00014	0500 00 0 00015	10001	10001	CLA			
00015	0020 00 4 00001	10000	10000	EXIT			
00016	0 00000 0 00000	10000	10000	TEMP			
00017	77777C00000	10000	10000	*LORG			
00020	000007000000	10000	10000				
00021	400030000001	00000	01111	END			

ICODE
CONTROL DICTIONARY

07/31/65

\$COICT ICODE

IC0000002

BINARY CARD (NOT PUNCHED)

000022000000
000004000005
312346242560
000022000000
312346242560
000000000000

PREFACE

START=0,LENGTH=18,TYPE=7094,CPLX=5

ICODE DECK

LOC=0,LENGTH=18

ICODE REAL

LOC=0,LENGTH=0

\$DKEND ICODE

IC0000003

NO MESSAGES FOR THIS ASSEMBLY
SYMBOL REFERENCE DATA

REFERENCES TO DEFINED SYMBOLS.

CLASS	SYMBOL	VALUE	REFERENCES
EXIT		00015	13
ICODE		00000	
OK		00014	11
LCIP	BLCTR		
QUAL	UNQS		
LCIP	//		
TEMP		00016	3,4,14

IDLE
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

07/31/65

CIDLE	MICHAEL SYNGE	6-9247	COMPILED 21 AUG 64	
C	TO DELETE AN ARRAY FROM A BUFFER			IDLE0030
C				IDLE0050
C	FUNCTION IDLETE (ARRAY)			IDLE0060
C				IDLE0070
C	DIMENSION ARRAY(1)			IDLE0080
				IDLE0100
	M=-18FR (ARRAY)			IDLE0110
	IF (4) 90, 90, 10			IDLE0120
	10 I=32767			IDLE0130
	ARRAY(1)=ARFRE(M)			IDLE0140
	IDLETE=0			IDLE0150
	GO TO 100			IDLE0160
	90 IDLETE=1			IDLE0170
	100 RETURN			IDLE0180
C				IDLE0190
C				IDLE0200
	END			IDLE0210

07/31/65

INIBITION

TOCBOINI

#INIBFR MICHAEL SYNGE 6-9247 ASSEMBLED 21 SEP 64

TO INITIALIZE ANY NUMBER OF STORAGE BUFFERS

CALLING SEQUENCE -

CALL INIBR(BUFA,NBUFA,BUF9,NBUF8,.....)

ENTRY INIBFR

BINARY CARD (NOT PUNCHED)

Case	Not Purchased	Purchased
1	00000	0634 00 4 00004
2	00001	0500 00 4 00003
3	00002	4320 00 0 00076
4	00003	0100 00 0 00006
5	00004	0774 00 4 00000
6	00005	0020 00 4 00001

INIBFR	SXA	EXIT,4
CLA	3,4	
ANA	=077777700000	
TZE	NEXT	
AXT	0,4	
TRA	1,4	
EXIT		

000006	0500	00	4	00003	10000
000010	0400	00	0	00027	10001
000017	0621	00	0	00017	10001
000011	0400	00	0	00027	10001
000012	0621	00	0	00024	10001
000013	0500	60	4	00004	10000
000014	4501	00	0	00030	10001
000015	0602	60	4	00003	10000
000016	0500	00	0	00031	10001
000017	0601	00	0	00000	10000
000020	0500	60	4	00004	10000
000021	0402	00	0	00032	10001
000022	0767	00	0	00022	10000

NEXT	CLA	3,4
	ADD	= 1
	STA	ARR1
ODD	ADD	= 1
	STA	ARR2
	CLA*	4,4
	ORA	= 0x0
LENG	SLW*	3,4
	CLA	= 070
ARR1	STO	**
	CLA*	4,4
	SUB	= 3
	ALS	18

PUFFER LENGTH

FIRST CODE WORD OF BUFFER

BINARY CARD (NOT PUNCHED)

CARD (NET PUNCHED)	
00023	0600 60 0 00024
00024	0622 00 0 00009
00025	1 77776 4 02001
00026	00000 00000 00000
00027	00000 00000 00000
00028	00000 00000 00000
00029	00000 00000 00000
00030	00000 00000 00000
00031	00000 00000 00000
00032	00000 00000 00000
00033	00000 00000 00000
00034	00000 00000 00000
00035	00000 00000 00000
00036	00000 00000 00000
00037	00000 00000 00000
00038	00000 00000 00000
00039	00000 00000 00000
00040	00000 00000 00000
00041	00000 00000 00000
00042	00000 00000 00000
00043	00000 00000 00000
00044	00000 00000 00000
00045	00000 00000 00000
00046	00000 00000 00000
00047	00000 00000 00000
00048	00000 00000 00000
00049	00000 00000 00000
00050	00000 00000 00000
00051	00000 00000 00000
00052	00000 00000 00000
00053	00000 00000 00000
00054	00000 00000 00000
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00056	00000 00000 00000
00057	00000 00000 00000
00058	00000 00000 00000
00059	00000 00000 00000
00060	00000 00000 00000
00061	00000 00000 00000
00062	00000 00000 00000
00063	00000 00000 00000
00064	00000 00000 00000
00065	00000 00000 00000
00066	00000 00000 00000
00067	00000 00000 00000
00068	00000 00000 00000
00069	00000 00000 00000
00070	00000 00000 00000
00071	00000 00000 00000
00072	00000 00000 00000
00073	00000 00000 00000
00074	00000 00000 00000
00075	00000 00000 00000
00076	00000 00000 00000
00077	00000 00000 00000
00078	00000 00000 00000
00079	00000 00000 00000
00080	00000 00000 00000
00081	00000 00000 00000
00082	00000 00000 00000
00083	00000 00000 00000
00084	00000 00000 00000
00085	00000 00000 00000
00086	00000 00000 00000
00087	00000 00000 00000
00088	00000 00000 00000
00089	00000 00000 00000
00090	00000 00000 00000
00091	00000 00000 00000
00092	00000 00000 00000
00093	00000 00000 00000
00094	00000 00000 00000
00095	00000 00000 00000
00096	00000 00000 00000
00097	00000 00000 00000
00098	00000 00000 00000
00099	00000 00000 00000
00100	00000 00000 00000

STZ* ARR2

NAME
**
SECOND CODE WORD OF FIRST ARRAY
INIBFR+1,4,-2

#LJRG

00026	777777700000	10000
00027	000000000001	10000
00030	400000700000	10000
00031	000000700004	10000
00032	000000000003	10000
	90000	01111

INIBFR
CONTROL DICTIONARY

07/31/65

\$CDICT INIBFR

INIB00002

RTNARY CARD (NOT PUNCHED)

00003300C000
00000040000005
314531222651
000033000000
314531222651
000000000000

PREFACE

START=0,LENGTH=27,TYPE=7094,CPLX=5

INIBFR DECK

LOC=0,LENGTH=27

INIBFR REAL

LOC=0,LENGTH=0

\$DKEND INIBFR

INIB00003

NO MESSAGES FOR THIS ASSEMBLY

SYMBOL REFERENCE DATA

REFERENCES TO DEFINED SYMBOLS.

CLASS	SYMBOL	VALUE	REFERENCES
	ARR1	00017	10
	ARR2	00024	12,23
	EXIT	00004	0
	INIBFR	00000	25
	LENG	00015	
	NEXT	00006	3
	ODD	00011	
LCTR	BLCTR		
QUAL	UNOS		
LCTR	//		

05/22/87

INOUT - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE INOUT(NTAPEO,KASE,CPCALC,POLAR,THICK,VCUT,XMACH,SEMI,
 1XP,ZP,CBAR,RFAREA,SYM)

C PRINTS OUT ALL INPUT AERODYNAMIC DATA

```

WRITE (NTAPEO,6010)
IF (SYM) 110,100,110
100 WRITE (NTAPEO,6015)
GO TO 120
110 WRITE (NTAPEO,6020)
120 CONTINUE

GO TO (130,140,150),KASE
130 WRITE (NTAPEO,6025)
GO TO 160
140 WRITE (NTAPEO,6030)
GO TO 160
150 WRITE (NTAPEO,6035)
160 CONTINUE

IF (CPCALC-1.) 170,180,185
170 WRITE (NTAPEO,6040)
GO TO 190
180 WRITE (NTAPEO,6045)
GO TO 190
185 WRITE (NTAPEO,6047)
190 CONTINUE

IF (POLAR) 210,200,210
200 WRITE (NTAPEO,6050)
GO TO 220
210 WRITE (NTAPEO,6055)
220 CONTINUE

IF (THICK) 240,230,240
230 WRITE (NTAPEO,6060)
GO TO 250
240 WRITE (NTAPEO,6065)
250 CONTINUE

IF (VCUT) 270,260,270
260 WRITE (NTAPEO,6070)
GO TO 280
270 WRITE (NTAPEO,6075)
280 CONTINUE

WRITE (NTAPEO,6095) XMACH
WRITE (NTAPEO,6090) XP,ZP,CBAR
WRITE (NTAPEO,6085) RFAREA
WRITE (NTAPEO,6080) SEMI

```

6010 FORMAT(1H0//30H DESCRIPTION OF CASE REQUESTED)

```

6015 FORMAT(1H0,85H UNSYMMETRICAL CONFIGURATION - PANELS LOCATED ONLY 0
      IN ONE SIDE OF X-Z PLANE(SYM = 0.))
6020 FORMAT(1H0,80H SYMMETRICAL CONFIGURATION - PANELS LOCATED ON BOTH
      SIDES OF X-Z PLANE(SYM = 1.))
6025 FORMAT(1H0,9HCASE = 1.,10X,35HCALCULATE WING SHAPE, GIVEN WING CL)
6030 FORMAT(1H0,9HCASE = 2.,10X,25HCALCULATE CL, GIVEN SHAPE)
6035 FORMAT(1H0,9HCASE = 3.,10X,19HOPTIMIZE WING SHAPE)
6040 FORMAT(1H0,11HPCALC = 0.,9X,9HLINEAR CP)
6045 FORMAT(1H0,11HPCALC = 1.,8X,13HNON-LINEAR CP)
6047 FORMAT(1H0,11HPCALC = 2.,8X,8HEXACT CP)
6050 FORMAT(1H0,10HPOLAR = 0.,9X,20HPOLARS NOT REQUESTED)
6055 FORMAT(1H0,10HPOLAR = 1.,9X,16HPOLARS REQUESTED)
6060 FORMAT(1H0,10HTHICK = 0.,9X,40HWING THICKNESS PRESSURES NOT TO BE
      1 ADDED)
6065 FORMAT(1H0,10HTHICK = 1.,9X,36HWING THICKNESS PRESSURES TO BE ADDE
      1 D)
6070 FORMAT(1H0,9HVOUT = 0.,10X,37HVELOCITY COMPONENTS NOT TO BE PRINTED)
      1 D)
6075 FORMAT(1H0,9HVOUT = 1.,10X,33HVELOCITY COMPONENTS TO BE PRINTED)
6080 FORMAT(1H0,17HWING SEMI-SPAN = ,F10.4)
6085 FORMAT(1H0,21HWING REFERENCE AREA =,F10.4)
6090 FORMAT(1H0,48HPOINT ABOUT WHICH THE MOMENTS ARE TO BE COMPUTED/16H
      1 X-COORDINATE =,F10.4/16H Z-COORDINATE =,F10.4//
      225H REFERENCE CHORD LENGTH =,F10.4)
6095 FORMAT(1H0,13HMACH NUMBER =,F10.4)

```

RTTI0N

09/14/65
 INPUTB
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

SUBROUTINE INPUTB
 COMMON DATE(2),NTAPE1,ND1,NTAPE2,ND2(3),NREAD,
 INWRITE,NBODY,NWING,XMACH,SYM,KACE
 COMMON /COM1/ KODEB,KODEM,KODEU,KODEI,KODEC,XPER,YPER,KOPTB,KOPTW
 1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPERI
 2,NPLANE,NPLN1
 COMMON /COM2/ NPLNB,NPLNW,JLEAD,JTRAIL,IMID,NPTS(16),XI(16,90),YI(16
 1,90),ZI(16,90),XCEPT(21),XCEPTB(21),XCEPTW(16),ZCEPTW(16
 2),CODEBW(16),KPADEL(15,20),XCOR(16,21),YCOR(16,21),ZCOR(16,21),XIN
 3(15,20,21),YINT(15,20,21),ZINT(15,20,21),XCEN(15,20),YCEN(15,20),ZCE
 4N(15,20),XCON(15,20),YCON(15,20),ZCON(15,20),AREA(15,20),ARAT(15,2
 50),THETA(15,20),ALPHA(15,20),CHORD(15,20)
 DIMENSION REC(500),LREC(10)

C SUBROUTINE TO INPUT DATA FOR BODY PANELING

C SUBROUTINES
 ND4=ND2(1)

C READ CARD INPUT - PLANB,PLANW ARE CODES FOR PLANES
 C THAT INTERSECT BODY PLANB IS NUMBER OF CUTTING
 C PLANES TO INTERSECT FORE AND AFT OF BODY-WING
 C INTERSECTION REGION PLANW IS NUMBER OF CUTTING
 C PLANES TO INTERSECT IN THE BODY-WING INTERSECTION
 C REGION PLANE IS TOTAL NUMBER OF PLANES
 C TO INTERSECT BODY AND DEFINE PANEL LEADING AND
 C TRAILING EDGES TOLB IS TOLERANCE USED
 C IN PROGRAM CHECK FOR SMALL SUBPANELS IF SLOPE
 C OF SUBPANEL EDGE FROM STREAMWISE IS LESS THAN
 C TOLERANCE, SUBPANEL IS OMITTED FROM OUTPUT
 C 10 READ (NREAD,900) PLANB,PLANW,TOLB
 WRITE INWRITE,950)

C DEFINE CONSTANTS

NPLNB=PLANB
 IF (NPLNB .LT. 0 .OR. NPLNB .GT. 21) GO TO 298
 NPLNW=PLANW
 IF (NPLNW .LT. 0 .OR. NPLNW .GT. 16) GO TO 298
 NPLANE=NPLNB+NPLNW
 IF (NPLANE .LT. 2 .OR. NPLANE .GT. 21) GO TO 298
 NPLN1=NPLANE-1
 KOPTB=0

SYN=TOLB
 IF (KOPTB) 300,15,200
 IF (NPLANE) 300,300,20
 15 IF (NPLNB) 300,35,25
 20 IF (NPLNB) 300,35,25

C READ CARD INPUT - X-AXIS INTERCEPT VALUES OF
 C BODY CUTTING PLANES TO INTERSECT FORE AND AFT OF
 C BODY-WING INTERSECTION REGION
 25 READ (NREAD,900) (XCEPTB(I),I=1,NPLNB)
 READ (ND1) (REC(I),I=1,6)
 A=REC(5)
 B=REC(6)

,1	,3	,4	
,2			
,5	,6		
,7	,9	,10	
,11			
,12	,13	,14	
,15			
,16	,17	,18	
,19			
,20			
,21			
,22			
,23			
,24	,26	,27	,28 ,29
,25	,31	,32	,33 ,34
,30			
,35			

INPUTB

EXTERNAL FORMULA NUMBER - SOURCE STATEMENT

C	CHANGE X-AXIS INTERCEPT VALUES TO ALLOW FOR	
C	BODY CAMBER	,36
	DO 30 I=1,NPLNB	,37
30	XCEPTB(I)=A*XCEPTB(I)+B	,38
	CALL CHECK (XCEPTB,NPLNB,2,L,NWRITE)	,39
	IF (L) 298,35,29F	,40
C	READ TAPE INPUT - BODY-WING INTERSECTION	
35	NREC=4	,41
	KCHK=NREC+1	,42
	CALL FSR (NREC,ND4,LERROR)	,43
	READ (ND4) (LREC(J),J=1,10)	,44
	KREC=LREC(1)	,45
	IF (KREC-KCHK) 253,40,293	,46
40	KCODE=LREC(3)	,47
		,48
		,49
C	DEFINE KINT IF KINT = 0, BODY-WING INTER-	
C	SECTION HAS NOT BE REQUESTED OR CALCULATED	
C	IF KINT = 1, OTHERWISE	
43	IF (KCODE) 293,44,43	,52
	KINT=0	,53
	GO TO 115	,54
44	KINT=1	,55
	NWORD=LREC(2)	,56
45	IF (NWORD-5000) 45,45,294	,57
	NPER=LREC(4)	,58
	IF (NPER-16) 46,46,294	,59
C	READ X-, Y- AND Z-COORDINATES OF	
C	BODY-WING INTERSECTION	
46	READ (ND4) (REC(J),J=1,NWORD)	,60
	DO 47 J=1,NPER	,61
	XI(J)=REC(3*J-2)	,62
	YI(J)=REC(3*J-1)	,63
47	ZI(J)=REC(3*J)	,64
50	IF (NPLNW) 300,115,53	,65
		,66
		,67
		,68
		,69
C	READ CARD INPUT - CODES INDICATING WING PERCENT	
C	LINE THAT ARE TO DEFINE BODY-CUTTING PLANES TO	
C	INTERSECT IN BODY-WING INTERSECTION REGION	
C	DEFINE CONSTANT NLOOP TO BE NUMBER OF CARDS	
C	TO BE READ	
53	NLOOP=((NPLNW-1)/6)+1	,71
	DO 57 J=1,NLOOP	,72
	JSTART=1+(J-1)*6	,73
	JEND=6*(J-1)*6	,74
	READ (NREAD,900) (CODEBW(K),K=JSTART,JEND)	,75
	IF (J-1) 300,55,57	,76
		,77
		,78
		,79
		,80
C	CHECK FOR CONSTANT OF -1 IN FIRST FIELD OF	
C	FIRST CARD	
55	IF (CODEBW(1)) 65,300,57	,81
		,82

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INPUTB	EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
57		CONTINUE	
C		DEFINE X-AXIS INTERCEPTS OF BODY CUTTING PLANES	
C		THAT INTERSECT IN BODY-WING INTERSECTION REGION	
60		DO 63 J=1,NPLNW	,83
		K=CODEBW(J)+.001	,85
		XCEPTW(J)=XI(K)	,86
		YCEPTW(J)=YI(K)	,87
		ZCEPTW(J)=ZI(K)	,88
63		GO TO 70	,89
		DO 67 J=1,NPLNW	,90
65		XCEPTW(J)=XI(J)	,91
		YCEPTW(J)=YI(J)	,92
		ZCEPTW(J)=ZI(J)	,93
67			,94
C		REDEFINE BODY-CUTTING PLANES	
70		IF (NPLNB) 300,105,75	,95
75		IF (NPLNW) 300,115,80	,96
80		JLEAD=0	,97
		DO 100 J=1,NPLANE	,98
		IF (XI(1)-XCEPT8(J)) 90,297,85	,99
85		XCEPT(J)=XCEPT8(J)	,100
		JLEAD=J	,101
		GO TO 100	,102
90		DO 93 K=1,NPLNW	,103
		L=JLEAD+K	,104
93		XCEPT(L)=XCEPTW(K)	,105
		IF (XI(NPER)-XCEPT8(JLEAD+1)) 95,297,297	,106
95		JTRAIL=JLEAD+NPLNW	,107
		JLEFT=NPLANE-JTRAIL	,108
		DO 97 K=1,JLEFT	,109
		L=JTRAIL+K	,110
		M=JLEAD+K	,111
97		XCEPT(L)=XCEPT8(M)	,112
		GO TO 130	,113
100		CONTINUE	,114
		GO TO 130	,115
105		IF (NPLANE-NPLNW) 300,107,300	,116
107		DO 110 J=1,NPLNW	,117
110		XCEPT(J)=XCEPTW(J)	,118
		GO TO 130	,119
115		IF (NPLANE-NPLNB) 300,117,300	,120
117		DO 120 J=1,NPLNB	,121
120		XCEPT(J)=XCEPT8(J)	,122
130		REWIND ND4	,123
			,124
			,125
			,126
			,127
			,128
			,129
C		WRITE TAPE OUTPUT - X-PRIME INTERCEPTS OF	
C		BODY CUTTING PLANES	
		WRITE (NWRITE,960) NPLANE,(XCEPT(J),J=1,NPLANE)	,130
C		READ TAPE INPUT - NPER IS NUMBER	
C		OF DEFINING BODY PERCENT LINES	
C		READ X-, Y- AND Z-COORDINATES OF POINTS ON	

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INPUTB	EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
C		BODY MERIDIAN LINES	
160	READ (ND4) (LREC(I),I=1,10)		,131 ,132 ,133 ,134 ,135 ,136
	KREC=LREC(I)		,137
	IF (KREC-1) 290,163,290		,142 ,143
163	KCODE=LREC(3)		,144
	IF (KCODE) 290,164,290		,145
164	NWORD=LREC(2)		,146
	IF (NWORD-5000) 167,167,294		,147
167	NPER=LREC(4)		,148
	IF (NPER-16) 168,168,294		,149
168	NPER1=NPER-1		
C	READ TAPE INPUT - NPTS IS NUMBER OF POINTS		
C	ON BODY PERCENT LINES		
	READ (ND4) (REC(I),I=1,NWORD)		,150 ,152 ,153 ,154 ,155
	X=-2		,156
	DO 170 I=1,NPER		,157
	K=K+3		,158
170	NPTS(I)=REC(K+1)		,159 ,160
	DO 175 I=1,NPER		,161
	IF (NPTS(I)-90) 175,175,294		,162 ,164
175	CONTINUE		,165
	DO 180 I=1,NPER		,166
	NSTOP=NPTS(I)		,167
	DO 180 J=1,NSTOP		,168
	K=K+3		,169
	X(I,J)=REC(K)		,170
	Y(I,J)=REC(K+1)		,171 ,172 ,173
180	Z(I,J)=REC(K+2)		,174
	REWIND ND4		
	GO TO 300		
C	READ CARD INPUT - X-, Y- AND Z-COORDINATES OF		
C	BODY PANEL CORNER POINTS		
200	NPER=COLB*1.		,175
	NPER1=NPER-1		,176
	DO 210 I=1,NPER1		,177
	DO 210 J=1,NPLN1		,178 ,179
210	READ (NREAD,900) XCOR(I,J),XCOR(I+1,J),XCOR(I,J+1),		
	1XCOR(I+1,J+1),YCOR(I,J),YCOR(I+1,J),YCOR(I,J+1),YCOR(I+1,J+1),		
	ZCOR(I,J),ZCOR(I+1,J),ZCOR(I,J+1),ZCOR(I+1,J+1)		,180 ,181 ,182 ,183 ,184
	WRITE (NWRITE,940)		,185 ,186
	GO TO 300		
C	ERROR MESSAGES		
290	KODEB=1		,187
	GO TO 300		,188
293	KODE1=1		,189
	GO TO 300		,190
294	WRITE (NWRITE,970)		,191
	GO TO 290		,192 ,193
297	WRITE (NWRITE,990)		,194
	GO TO 290		,195 ,196
			,197

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INPUTB	EXTERNAL FORMULA NUMBER	- SOURCE STATEMENT	- INTERNAL FORMULA NUMBER(S)
298	WRITE (NWRITE,980)		,198 ,199
	GO TO 290		,200
300	RETURN		,201
900	FORMAT (6F10.0)		
940	FORMAT (1H1.9X,43HBODY PANELS HAVE BEEN DEFINED ON CARD INPUT)		
950	FORMAT (1H1.9X,16HBODY PANEL ROUTINE)		
960	FORMAT (1H0.9X,10H THERE ARE ,I3,51H TRANSVERSE VERTICAL PLANES THA		
	IT INTERSECT THE BODY/10X,42HTO DEFINE PANEL LEADING AND TRAILING E		
	20GES//10X,12HX-INTERCEPTS/(IF20.5))		
965	FORMAT (1H0.9X,43HBODY PANELS HAVE BEEN DEFINED ON CARD INPUT)		
970	FORMAT (1H1.9X,33HERROR MESSAGE - SUBROUTINE INPUTB/10X,		
	151HIMPROPER BODY DEFINITION OR INTERSECTION DEFINITION/10X,		
	250HDIMENSION EXCEEDED FOR NPTS, X, Y, Z OR REC ARRAYS)		
980	FORMAT (1H1.9X,33HERROR MESSAGE - SUBROUTINE INPUTB/10X,		
	121HINPUT CARD DATA ERROR)		
990	FORMAT (1H1.9X,33HERROR MESSAGE - SUBROUTINE INPUTB/10X		
	121HINPUT CARD DATA ERROR/10X		
	1104HCUTTING PLANE THAT IS DEFINED BY X-AXIS INTERCEPT VALUE INTERS		
	ECTS BODY IN BODY-WING INTERSECTION REGION)		
	END		,202

09/14/65
 INPUTW
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

SUBROUTINE INPUTW
COMMON DATE(2),NTAPE1,ND1,NTAPE2,ND2(3),NREAD,
1NWRITE,NBODY,NWING,XMACH,SYM,KACE
COMMON /COM1/ KODEB,KODEW,KODEL,KODEC,XPER,YPER,KOPTB,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPERI
2,NPLANE,NPLN1
COMMON /COM2/IJ,NPTS(16),X(90,16),Y(90,16),Z(90,16),KPNT,VALUE(5),
1YCEPT(16),SLOPE,KPANEL(2,15),XCOR(16,16),YCOR(16,16),ZCOR(16,16),X
2INT(2,15),YINT(2,15),ZINT(2,15),XCEN(15,15),YCEN(15,15),ZCEN(15,15)
3,XCON(15,15),YCON(15,15),ZCON(15,15),AREAL(15,15),ARAT(15,15),THET
4A(15,15),ALPHA(15,15),CHORD(15,15),XFOL(16,25,2),ZFOL(16,25,2),X
5NUM(16,2),XTAB(25),ZTAB(25),XTAB2(25),ZTAB2(25)
DIMENSION REC(5000),LREC(10)

```

C SUBROUTINE TO INPUT DATA FOR WING PANELING
 C SUBROUTINES

10 ND4=ND2(1)
 REWIND ND4
 IF (IJ-1) 20,190,300

,1
 ,2

```

C READ CARD INPUT - PLANE IS NUMBER OF PLANES
C TO INTERSECT WING AND DEFINE WING PANEL
C INBOARD AND OUTBOARD EDGES OPTF IS CODE FOR CARD
C INPUT OPTION IF OPTF = 1, UPPER AND LOWER
C SURFACE AIRFOIL COORDINATES ARE READ FROM
C ADDITIONAL INPUT CARDS IF OPTF = 0, OTHERWISE
C SNUM IS NUMBER OF AIRFOIL SECTION COORDINATE
C TABLES TO BE READ TOLW IS TOLERANCE USED IN
C PROGRAM CHECK FOR SMALL SUBPANELS IF SLOPE
C OF SUBPANEL EDGE FROM STREAMWISE IS LESS THAN
C TOLERANCE, SUBPANEL IS OMITTED FROM OUTPUT
C NOTE THAT ALL PANELS OF MAIN WING REGION
C ARE ONE PART PANELS AND NO CHECK IS NECESSARY
C HOWEVER, FOR PANELS ON INBOARD EDGE OF WING
C IN BODY-WING CASE WITH NON-STREAMWISE INTER-
C SECTION LINE AND FOR PANELS ON NON-STREAM-
C WISE OUTBOARD EDGE SUBPANEL IS CHECKED AGAINST
C TOLERANCE

```

20 READ (NREAD,900) PLANE,OPTF,SNUM,TOLW

,3
 ,4 ,5 ,6
 ,7 ,8 ,9 ,10
 ,11
 ,12
 ,13
 ,14
 ,15
 ,16
 ,17
 ,18

```

C DEFINE CONSTANTS
NPLANE=PLANE
IF (NPLANE .LT. 1 .OR. NPLANE .GT. 16) GO TO 295
NPLN1=NPLANE-1
KOPTW=0
KOPTF=OPTF
NUMS=SNUM
KACE=0
SYM=TOLW
IF (KOPTW) 300,25,250
IF (NPLANE) 300,300,30
30 NREC=2

```

25 IF (KOPTW) 300,25,250
 IF (NPLANE) 300,300,30

```

C READ CARD INPUT - Y-AXIS INTERCEPT VALUES FOR
C PLANES THAT INTERSECT WING NOTE THAT ALL BUT
C LAST (FOR OUTBOARD) CUTTING PLANE MUST BE
C STREAMWISE AND Y-AXIS INTERCEPTS ARE SAME
C AS Y-COORDINATES OF CUTTING PLANE AND LEADING
C EDGE INTERSECTION LAST CUTTING PLANE HAS, IN
C GENERAL, AN ARBITRARY SLOPE AND IS DEFINED
C BY CODE AND ARRAY OF VALUES CPNT IS CODE
C IF CPNT = 0, X- AND Y-COORDINATES OF LEADING
C AND TRAILING EDGE INTERSECTIONS WITH CUTTING
C PLANE ARE GIVEN IF CPNT = 1, LEADING EDGE
C INTERCEPTS AND SLOPE ARE GIVEN IF CPNT =
C 2, TRAILING INTERCEPTS AND SLOPE ARE GIVEN
70 READ (NREAD,900) (YCEPT(I),I=1,NPLN1)
READ (NREAD,900) CPNT,(VALUE(I),I=1,5)

CALL CHECK (YCEPT,NPLN1,2,L,NWRITE)
IF (L) 295,75,295
75 KPNT=CPNT

C CALCULATE OUTBOARD CUTTING PLANE SLOPE IF
C NOT GIVEN AS INPUT
80 IF (KPNT-1) 80,90,90
83 SLOPE=0.
GO TO 100
87 SLOPE=(VALUE(3)-VALUE(1))/(VALUE(4)-VALUE(2))
GO TO 100
90 SLOPE=VALUE(5)

C WRITE TAPE OUTPUT - INPUT CARD DATA
100 WRITE (NWRITE,910)
WRITE (NWRITE,920) NPLANE
WRITE (NWRITE,930) (YCEPT(I),I=1,NPLN1)
115 IF (KPNT-1) 115,115,120
WRITE (NWRITE,935) VALUE(1),VALUE(2),SLOPE
GO TO 125
120 WRITE (NWRITE,940) VALUE(3),VALUE(4),SLOPE
GO TO 125
125 WRITE (NWRITE,950)

C READ TAPE INPUT - NPTS IN NUMBER OF POINTS
C ON ARBITRARY PERCENT LINE
150 CALL FSR (NREC,NC4,LEERRR)
KCHECK=NREC+1
READ (ND4) (LREC(I),I=1,10)
KREC=LREC(1)
IF (KREC-KCHECK) 280,160,280
160 KCODE=LREC(3)
IF (KCODE) 280,163,280
163 NWORO=LREC(2)
IF (NWORO-5000) 165,165,287
165 NPER=LREC(4)

```

19 21 22 23 24
 20 26 27 28 29 30
 25
 31 32
 33 34 35 36 37 38 39
 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59
 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75

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INTERNAL FORMULA NUMBER(S)

```

INPUTW
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

167 IF (NPER-16) 167,167,287 ,76
    NPER1=NPER-1

C READ X-, Y- AND Z-COORDINATES OF POINTS ON
C WING PERCENT CHORD LINES
    READ (ND4) (REC(I),I=1,NWORD)
    K=-2
175 DO 180 J=1,NPER
    K=K+3
180 NPTS(J)=REC(K+1)
    DO 183 J=1,NPER
    IF (NPTS(J)-90) 183,183,287
183 CONTINUE
    DO 185 J=1,NPER
    NSTOP=NPTS(J)
    DO 185 I=1,NSSTOP
    K=K+3
    X(I,J)=REC(K)
    Y(I,J)=REC(K+1)
    Z(I,J)=REC(K+2)
185 REMIND ND4
    GO TO 300

C READ CARD INPUT - UPPER AND LOWER SURFACE
C AIRFOIL COORDINATES
190 IF (KOPTF) 300,290,195
195 KACE=1
200 IF (NUMS-1) 300,200,205
    ISTOP=1
    GO TO 210
205 ISTOP=NPLN1+KSTART-1
210 DO 220 I=1,ISTOP
    DO 220 N=1,2
    READ (NREAD,900) XNUM(I,N)
    NUM=XNUM(I,N)
220 READ (NREAD,900) (XFOIL(I,J,N),ZFOIL(I,J,N),J=1,NUM)

C CONVERT AIRFOIL(S) TO UNIT AIRFOIL(S)
225 DO 240 I=1,ISTOP
    DO 240 N=1,2
    NUM=XNUM(I,N)
    IF (XFOIL(I,NUM,N)-1.) 230,240,230
230 DO 235 J=1,NUM
    ZFOIL(I,J,N)=ZFOIL(I,J,N)/XFOIL(I,NUM,N)
235 XFOIL(I,J,N)=XFOIL(I,J,N)/XFOIL(I,NUM,N)
240 CONTINUE
    GO TO 300

C READ CARD INPUT - X-, Y- AND Z-COORDINATES OF
C WING PANEL CORNER POINTS
250 NPER=ROW+1.
    NPER1=NPER-1
    NPLANE=NPLANE+1

```

,77 ,78 ,79 ,80 ,81 ,82
,83
,84
,85
,86 ,87
,88
,89
,90 ,91
,92
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,96
,97
,98 ,99 ,100
,101

,102
,103
,104
,105
,106
,107
,108
,109
,110
,111 ,112 ,113
,114

,115 ,116 ,117 ,118 ,119 ,120
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,122
,123
,124
,125
,126
,127
,128 ,129
,130 ,131 ,132

,133
,134
,135
,136

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INPUT	EXTERNAL FORMULA NUMBER	- SOURCE STATEMENT	- INTERNAL FORMULA NUMBER(S)
	NPLN1=NPLANE-1		,137
	DO 260 I=1,NPLN1		,138
	DO 260 J=1,NPER1		,139
260	READ (NREAD,900) XCOR(I+1,J),XCOR(I+1,J),XCOR(I+1,J),XCOR(I+1,J+1),		
	YCOR(I+1,J+1),YCOR(I+1,J),YCOR(I+1,J),YCOR(I+1,J+1),YCOR(I+1,J+1),		
	ZCOR(I+1,J),ZCOR(I+1,J),ZCOR(I+1,J),ZCOR(I+1,J+1),ZCOR(I+1,J+1)		,140 ,141 ,142 ,143 ,144
	GO TO 300		
C	ERROR MESSAGES		
280	IJ1=IJ+1		,145
	GO TO (283,285),IJ1		,146
283	KODEW=1		,147
	GO TO 300		,148
285	KODEWU=1		,149
	GO TO 300		,150
287	WRITE (NWRITE,980)		,151
	GO TO 283		,152 ,153
290	WRITE (NWRITE,970)		,154
	GO TO 283		,155 ,156
295	WRITE (NWRITE,990)		,157
	GO TO 283		,158 ,159
300	RETURN		,160
900	FORMAT (6F10.0)		,161
910	FORMAT (1H1,15X,18H WING PANEL ROUTINE)		
920	FORMAT (1H0,9X,10H THERE ARE ,13,67H VERTICAL PLANES THAT INTERSECT		
	1 THE WING TO DEFINE PANEL SIDE EDGES)		
930	FORMAT (1H0,9X,12H LEADING-EDGE/10X,		
	11HY-INTERCEPT/(F20.5))		
935	FORMAT (1H0,19X,22H OUTBOARD CUTTING PLANE/17X,		
	112H LEADING-EDGE/10X,11HX-INTERCEPT,5X,11HY-INTERCEPT,8X,		
	25HSLOPE/(F19.5,F16.5,F18.5))		
940	FORMAT (1H0,19X,22H OUTBOARD CUTTING PLANE/17X,		
	113H TRAILING-EDGE/10X,11HX-INTERCEPT,5X,11HY-INTERCEPT,8X,		
	25HSLOPE/(F19.5,F16.5,F18.5))		
950	FORMAT (1H0,9X,45H ZERO-SLOPE INDICATES STREAMWISE CUTTING PLANE)		
960	FORMAT (1H0,9X,43H WING PANELS HAVE BEEN DEFINED ON CARD INPUT)		
970	FORMAT (1H1,9X,63H UPPER AND LOWER SURFACE AIRFOIL COORDINATES NOT		
	1 READ FROM CARDS)		
980	FORMAT (1H1,9X,33H ERROR MESSAGE - SUBROUTINE INPUTW/10X,		
	151H IMPROPER WING DEFINITION OR INTERSECTION DEFINITION/10X,		
	250H DIMENSION EXCEEDED FOR NPTS, X, Y, Z OR REC ARRAYS)		
990	FORMAT (1H1,9X,33H ERROR MESSAGE - SUBROUTINE INPUTW/10X,		
	121H INPUT CARD DATA ERROR)		
	END		,162

```

INTAPE - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE INTAPE
  C READS IN GEOMETRICAL DATA FROM PANELING AND DEFINITION LINKS
  COMMON DATE(2),NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI
  1,NTAPEJ,NBODY,NWING,XMACH,SYM,KACE
  COMMON /BLOCK/ALPHAS(210),AREA(210),A(210),ALPHAC(110),ALPHAT(110)
  C,CHORD(210)
  I,ISYM
  N,NPART(210),NPANEL,NROW(2)
  T,THETA(210),TAIL
  U,U(210)
  V,V(210),VPM(210),VV(210),VPMH(210)
  W,W(210),WPH(210),WH(210),WPMH(210)
  X,X(210,3,4),XBAR(210),XC(210)
  Y,Y(210,3,4),YBAR(210),YC(210)
  Z,Z(210,3,4),ZBAR(210),ZC(210)
  DIMENSION JSAVE(2),NSAVE(2),XB(51),R(51),ZDELTA(51)
  DIMENSION ARRAY(3,10),THETAB(10)
  DIMENSION XYZ(3)

  C READ IN MACH NUMBER, CONFIGURATION SYMMETRY CONDITION
  C BOUNDARY CONDITION TYPE AND TAIL OPTION CODE
  READ (NTAPEI,5000) XMACH,SYM
  BCOND=0
  KCND=BCOND
  IF (SYM) 50,45,50
  ISYM=1
  GO TO 55
  ISYM=2
  55 CONTINUE

  C CODE TO INDICATE IF THE CASE INCLUDES A THICK WING
  THKW=KACE

  C TEST FOR TYPE OF CONFIGURATION
  IF (NBODY) 120,110,120

  C WING ONLY CASE
  110 KACE=1
  JSAVE(1)=0
  NSAVE(1)=NWING
  NPANEL=NWING
  NBODYS=0
  ARG=1
  S=1.
  T=0.
  GO TO 160

  120 CONTINUE

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05/22/67

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INTAPE - EFN SOURCE STATEMENT - IFN(S) -

C READ NUMBER OF BODY SOURCE SEGMENTS AND THE INDEX OF THE X -
C COORDINATE AT LEADING EDGE OF THE WING
  READ (NTAPEB) (XYZ(1),I=1,3),ZA,S,T
  ALPHA=XYZ(3)/XYZ(1)
  READ (NTAPEB) NBODYS,NXLE
15
C READ BODY X-COORDINATES, BODY RADIUS, AND INCREMENT OF BODY CAMBER
  READ (NTAPEB) (XB(1),R(1),ZDELTA(1),I=1,NBODYS)
  REMIND NTAPEB
22
25
34
  IF (NBODY) 130,999,140

C BODY ONLY CASE
  KACE=2
  NPANEL=0
  NMING=0
  WRITE (NTAPEB) NBODY,NMING,XMACH,SYN,KACE
  GO TO 325
39

C WING AND BODY CASE
  KACE=3
  JSAVE(1)=0
  NSAVE(1)=NBODY
  JSAVE(2)=NBODY
  NSAVE(2)=NMING
  NPANEL=NMING+NBODY
  NRG=2
  CONTINUE
160

DC 210 L=1,NRG
J=JSAVE(L)
M=NSAVE(L)

DC 190 I=1,N
J=J+1

C READS IN PANEL COORDINATES
  READ (NTAPEB) NPN,NPART(J),(X(J,1,K),Y(J,1,K),Z(J,1,K),K=1,4)
  IF (NPART(J)-1)170,190,170
170 NPT=NPART(J)
  DC 180 M=2,NPT
  READ (NTAPEB) (X(J,M,K),Y(J,M,K),Z(J,M,K),K=1,4)
180 CONTINUE
190 CONTINUE
54
69
  J=JSAVE(L)
  DO 200 I=1,N
  J=J+1

C READS IN COORDINATES OF CENTROIDS, CONTROL POINTS, AREAS, THETAS,
C ALPHAS, AND CHORD LENGTHS
  READ (NTAPEB) NPN,XBAR(J),YBAR(J),ZBAR(J),XC(J),YC(J),ZC(J),AREA(J)

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1),THETA(I),ALPHA(J),CHORD(J)
200 CONTINUE
84

C READS IN THE NUMBER OF PANELS IN A COLUMN AND THE LOCATION OF THE
C CONTROL POINT
C READ (NTAPEC) NROW(L),XCTP
97
210 CONTINUE
REMIND NTAPEC
101

240 CONTINUE
DO 250 J=1,NWING
JJ=J+NBODY

C STORES THICKNESS SLOPES AND CAMBER SLOPES
ALPHA(J)=THETA(JJ)
250 ALPHA(J)=ALPHA(JJ)
NS=NBODY+1
DO 300 J=NS,NPANEL
THETA(J)=0.
ALPHA(J)=0.
300 CONTINUE
WRITE (NTAPEC) NBODY,NWING,XMACH,SYM,KACE

C WRITES COORDINATES OF CENTROIDS, CONTROL POINTS, AREAS, THETAS,
C ALPHAS, CHORD LENGTHS, NUMBER OF REGIONS, NUMBER OF ROWS PER
C COLUMN IN A REGION, AND CONTROL POINT LOCATION
WRITE (NTAPEC) (I,XBAR(I),YBAR(I),ZBAR(I),XC(I),YC(I),ZC(I),AREA(I
1),THETA(I),ALPHA(I),CHORD(I),I=1,NPANEL),NRG,(NROW(I),I=1,NRG),XC
2TP
END FILE NTAPEC
122
123

C WRITE THICKNESS SLOPES
WRITE (NTAPEC) (ALPHA(I),I=1,NWING)
145
END FILE NTAPEC
146

C WRITE CAMBER SLOPES
WRITE (NTAPEC) (ALPHA(I),I=1,NWING)
153
END FILE NTAPEC
154
161

IF (NBODY) 325,510,325
325 CONTINUE

C WRITE SLOPE OF BODY AXIS WITH RESPECT TO THE DEFINING AXIS
WRITE (NTAPEC) ALPHA

C WRITE NUMBER OF BODY SOURCE SEGMENTS, INDEX OF X- COORDINATE AT
C LEADING EDGE OF WING, HEIGHT OF WING PLANE ABOVE BODY AXIS, X
C COORDINATE OF BODY
WRITE (NTAPEC) NBDYS,NMLE,ZA,(XB(I),I=1,NBDYS)
163
IF (NWING) 400,350,400
164
350 CONTINUE

C FOR BODY ONLY CASE, READ NUMBER OF THETAS REPRESENTING BODY

```


INTAPE - EFN SOURCE STATEMENT - IFN(S) -

READ (INTAPE) NDUMMY,NDUMMY,NDUMMY,NTHETA

172
177
187

C READ BODY THETAS

READ (INTAPE) ((ARRAY(I,J),I=1,3),J=1,NTHETA)

REINC (NTAPE)

DO 375 J=1,NTHETA

375 THETAB(J)=ARRAY(1,J)

GC TC 450

C FOR WING-BODY CASE, COMPUTE NUMBER OF THETAS AND THETAS FROM

C PANEL REPRESENTATION OF BODY

400 CONTINUE

NROWB=NROW(1)

NTHETA=NBODY/NROWB

DO 425 J=1,NTHETA

JJ=(J-1)*NROWB+1

425 THETAB(J)=ABS(THETA(JJ))*57.2957795

450 CONTINUE

C WRITE NUMBER OF THETAS, AND THETAS

WRITE (NTAPE) NTHETA,(THETAB(I),I=1,NTHETA)

208
215
222
229

C WRITE RADIUS AND CAMBER INCREMENT OF BODY

WRITE (NTAPE) (R(1),I=1,NBODY)

WRITE (NTAPE) (ZDELTA(1),I=1,NBODY)

WRITE (NTAPE) (ZDELTA(1),I=1,NBODY)

END FILE NTAPEC

IF (NBODY) 500,500,550

500 CONTINUE

END FILE NTAPEC

END FILE NTAPEC

510 CONTINUE

END FILE NTAPEC

236
238
239

C STORE GEOMETRY DATA ON SCRATCH/SAVE TAPE

C FOR USE IN FLOW VISUALIZATION LINK

550 CONTINUE

NWINGS=NWING+NWING/NROW(NRG)

WRITE (NTAPE) KACE,NPANEL,NBODY,NWING,NBODY,NWINGS

S,NROW,XMACH,SYM

END FILE NTAPEC

240

243

245

IF (NPANEL) 600,600,575

575 CONTINUE

WRITE (NTAPE) NPANEL

DC 580 J=1,NPANEL

WRITE (NTAPE) NPART(J)

NPT=NPART(J)

WRITE (NTAPE) ((X(J,M,K),Y(J,M,K),Z(J,M,K),K=1,4),M=1,NPT)

580 CONTINUE

WRITE (NTAPE) (XBAR(J),YBAR(J),ZBAR(J),J=1,NPANEL)

WRITE (NTAPE) (XC(J),YC(J),ZC(J),J=1,NPANEL)

WRITE (NTAPE) (ALPHAS(J),THETA(J),CHORD(J),J=1,NPANEL)

247

250

253

265

274

283

600 CONTINUE
END FILE NTAPEC

999 CONTINUE
5000 FORMAT(7F10.0)
5200 FORMAT(13)
5100 FORMAT(6F10.0)
RETURN
END

292

INPOL
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

SUBROUTINE INTPCL (NM,NROW,RATIOX,RATIOC,CHORD,ALPHAM,ALPHAD)

C INTERPOLATES FOR NORMAL VELOCITY COMPONENT AT A SPECIFIED PERCENT
C OF PANEL CHORD

DIMENSION CHORD(1),ALPHAM(1),ALPHAD(1)

NCCL=NM/NROW

R=RATIOC-RATIOX

RR=-R

J=0

DO 100 K=1,NCCL

J=J+1

ALPHAD(J)=ALPHAM(J)+R*(ALPHAM(J+1)-ALPHAM(J))/(1.+RATIOX

1*(CHORD(J+1)/CHORD(J)-1.))

DO 100 I=2,NROW

J=J+1

CR=CHORD(J)/CHORD(J-1)

ALPHAD(J)=ALPHAM(J)+CR*R*(ALPHAM(J)-ALPHAM(J-1))/(1.+

RATIOX*(CR-1.))

100 CONTINUE

RETURN

END

,1
,2
,3
,4
,5
,6
,7
,8
,9
,10
,11
,12 ,13 ,14
,15
,16

FUNCTION INTURP(IDIC,NDIC,LI,LO)

C READ AND WRITE A COMMAND CARD,SEE IF COMMAND (IN THE
C FIRST WORD) IS IN THE DICTIONARY.

DIMENSION IDIC(1),CCM(14)
EQUIVALENCE (COM,ICOM)

C IDIC (INSTEAD OF DIC) IS USED AS AN ARGUMENT
C SO THAT A FIXED-POINT COMPARISON CAN BE MADE

110	READ (LI,110)COM	,1	,2	,3
	FORMAT(13A6,A2)			
	IF (LG)140,140,115	,4		
115	WRITE (LO,120)COM	,5	,6	,7
120	FORMAT(/1H014A6)			
140	DO 200 INTERP=1,NDIC	,8		
	IF (IDIC(INTERP)-ICOM)200,500,200	,9		
200	CONTINUE	,10	,11	
	INTERP=0	,12		
500	INTURP=INTERP	,13		
	RETURN	,14		
	END	,15		

INV4S
ASSEMBLED TEXT.

08/17/65

\$TEXT INV4S

INV40001

```

*INV4S  SINGLE PRECISION 7094 INVERSION ROUTINE (ADAPTION OF INV40)
*
* CALLING SEQUENCE -
* CALL INV4S,A,N,ERR1,ERR2,SCALE,DET,DETXP
* A = STARTING ADDRESS OF MATRIX
* N = NUMBER OF ROWS (COLUMNS) OF MATRIX
* ERR1 = 0 IF INVERSION SUCCESSFUL
*       = 1 IF OVERFLOW OCCURS
*       = 2 IF MATRIX IS SINGULAR
*       = 3 IF SCALED INVERSE CANNOT BE RE-SCALED
*       = 4 IF ROWS AND COLUMNS CANNOT BE RE-ARRANGED
*       THIS IS BASICALLY A MACHINE ERROR
*       = 10 + I IF ERROR CODE 3 OCCURRED SUBSEQUENT
*           TO ERROR CODE I
*       = 20 + I IF ERROR CODE 4 OCCURRED SUBSEQUENT
*           TO ERROR CODE I
* ERR2 = CURRENT REDUCTION STAGE IF ERR1=1
*       = RANK OF MATRIX IF ERR1 = 2
*       = 0 OTHERWISE
* SCALE = 0 IF ERR1 NOT = 3
*       = SCALING FACTOR IF ERR1=3
* DET = DECIMAL PART OF DETERMINANT IF ERR1.
*       NOT = 2 - A NUMBER GT OR E TO 1. AND LT 10.
*       = 0 IF ERR1=2
* DETXP = EXPONENT PART OF DETERMINANT IF ERR1
*       NOT = 2 - AN ADDRESS INTEGER GIVING
*       POWER OF TEN FOR DETERMINANT
*       DETERMINANT = DET*10.**DETXP
*
* ENTRY  INV4S
*
* SET UP CONSTANTS AND INITIALIZE CELLS

```

BINARY CARD ID.	INV40002	00000	0760	00	0	00016	10000	034
		00001	4760	00	0	00002	10000	035
		00002	0634	00	1	00361	10001	036
		00003	0634	00	2	00362	10001	037
		00004	0634	00	3	00363	10001	038
		00005	0634	00	4	00364	10001	039
		00006	0634	00	5	00365	10001	040
		00007	0634	00	6	00366	10001	041
		00010	0634	00	7	00367	10001	042
		00011	0600	00	0	00000	10000	043
		00012	0600	00	0	00466	10001	044
		00013	0600	00	0	00467	10001	045
		00014	0600	00	0	00470	10001	046
		00015	0600	00	0	00010	10000	047
		00016	0602	00	0	00443	10001	048
		00017	4500	00	0	00444	10001	049
		00020	0602	00	0	00010	10000	050
		00021	0600	60	4	00007	10000	051
		00022	0600	00	0	00451	10001	052

XR1.1	CHRCNG	CLEAR CELL 0 FOR FPT
XR2.2	ERRCD1	CLEAR CELL FOR CHARACTERISTIC SCALING
XR3.3	ERRCD2	CLEAR ERROR CODE CELLS
XR4.4	8	SAVE CELL 8 FOR (FPT)
XR5.5	TEMP8	STORE TRANSFER FOR FPT ANALYSIS.
XR6.6	FPTRA	ZERO SCALING CELL
XR7.7	7.4	ZERO DETERMINANT EXPONENT
0	DETXP	

INV4S
ASSEMBLED TEXT.

BINARY	CARD ID.	INV#0004	ACL	N	ADPRM	ADDRESS OF CURRENT PIVOT ROW + N
00046	0361	00 0 00452	10001			072
00047	0621	00 0 00456	10001			073
00050	0534	00 1 00452	10001	N.1		074
00051	4634	00 1 00652	10001	SXD	REDUC4,1	075
00052	0500	00 0 00734	10001	CLA	=1.	076
00053	0601	60 0 00446	10001	DET	START DET OFF AT 1.	077
00054	0500	00 0 00735	10001	CLA	=10.	078
00055	0601	60 0 00450	10001	STO*	LOAD 10 IN DOUBLE PRECISION CELL	079
00056	0534	00 7 00452	10001	LXA	N.7	080
00057	4634	00 7 00204	10001	SXD	ROLDED,7	081
00060	4634	00 7 00067	10001	SXD	STOINT,7	082
00061	0754	00 0 00000	10000	PXA	0.0	083
00062	0774	00 1 00001	10000	AXT	1,1	084
00063	0754	00 1 00000	10000	PXA	0.1	085
00064	0601	60 0 00463	10001	ADCNT	ADCNT HAS A TAG OF 1	086
00065	0601	60 0 00462	10001	ADINT	ADINT HAS A TAG OF 1	087
00066	1 00001	1 01001	10011	TXI	**1,1,1	088
00067	7 00000	1 41004	10011	STOINT TXL	**4,1,**	089
			*		N IN DECREMENT	090
			*		START OF REDUCTION LOOP	091
			*		REDUCTION STAGE IS KEPT IN XRI	092
			*		AT THE END OF THIS LOOP ALL INVERSION	093
			*		ARITHMETIC IS DONE	094
			*			095
00070	0774	00 1 00001	10000	AXT	1.1	INITIALIZE REDUCTION STAGE

BINARY	CARD ID.	INV#0005	RDLPST	TSX	FINDLE,4	FIND LARGEST ELEMENT IN N-XRI+1 SUB MATRIX	O97
00071	0074	00 4	00546	10001	TEMPXR,1		O98
00072	0634	00 1	00473	10001			O99
00073	0754	00 1	00000	10000	0,1	DO WE INTERCHANGE ROWS	O99
00074	0340	00 0	00464	10001	LGSTWR	YES	100
00075	0020	00 0	01002	10011	4+2		101

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INV4S
ASSEMBLED TEXT.

00076	0020 00 0 00115	10001	TRA	EXCHCL	NO	102
00077	0500 60 0 00466	10001	CLA*	DET	YES,ADJUST DET. SIGN	103
00100	0760 00 0 00002	10000	CHS			104
00101	0601 60 0 00466	10001	STO*	DET		105
00102	0074 00 4 00476	10001	TSX	INRCHR,4	EXCHANGE ROWS TO GET LGST NO ON PIV POS.	106
00103	0074 00 0 00473	10001	TSX	TEMPXR		107
00104	0074 00 0 00464	10001	TSX	LGSTRW	EXCHANGE ROW INTEGERS	108
00105	0500 00 0 00462	10001	CLA	ADPRINT		109
00106	0402 00 0 00464	10001	SUR	LGSTRW		110
00107	0621 00 0 01002	10011	STA	**2		111
00110	0621 00 0 01003	10011	STA	**3		112
00111	0500 00 0 00000	10000	CLA	**	LGSTRW INTEGER	113
00112	0560 60 0 00462	10001	LQ*	ADPRINT	ADPRINT HAS TAG OF 1	114
00113	4600 00 0 00000	10000	STQ	**	LGSTRW INTEGER	115

BINARY CARD ID. INV40006

00114	0601 60 0 00462	10001	STO*	ADPRINT		117
00115	0754 00 1 00000	10000	EXCHCL PXA	0,1		118
00116	0340 00 0 00465	10001	CAS	LGSTCL	DO WE INTERCHANGE COLS.	119
00117	0020 00 0 01002	10011	TRA	**2	YES	120
00120	0020 00 0 00137	10001	TRA	STRTSC	NO	121
00121	0500 60 0 00466	10001	CLA*	DET	YES, ADJUST DET. SIGN	122
00122	0760 00 0 00002	10000	CHS	DET		123
00123	0601 60 0 00466	10001	STO*	INRCHR,4	INTERCHANGE COLUMNS FOR LGST NO.	124
00124	0074 00 4 00521	10001	TSX	TEMPXR		125
00125	0074 00 0 00473	10001	TSX	LGSTCL	INTERCHANGE COLUMN INTEGERS	126
00126	0074 00 0 00465	10001	TSX			127
00127	0500 00 0 00463	10001	CLA	ADPRINT		128
00130	0402 00 0 00465	10001	SUR	LGSTCL		129
00131	0621 00 0 01002	10011	STA	**2		130
00132	0621 00 0 01003	10011	STA	**3		131
00133	0500 00 0 00000	10000	CLA	**		132
00134	0560 60 0 00463	10001	LQ*	ADPRINT	ADPRINT HAS A TAG OF 1	133
00135	4600 00 0 00000	10000	STQ	**		134
00136	0601 60 0 00463	10001	STO*	ADPRINT		135
00137	3 00001 1 00162	10001	STRTSC TXH		START OF CHARACTERISTIC SCALING ROUTINE	136
00140	4500 60 0 00455	10001	CAL*	APVEL	THE LARGEST MAGNITUDE IN THE MATRIX WILL	137
00141	4320 00 0 00736	10001	ANA		BE FORCED TO HAVE A CHARACTERISTIC OF 177	138
00142	0402 00 0 00737	10001	SUR		AND ALL OTHERS WILL BE ADJUSTED ACCORDINGLY	139
00143	0760 00 0 00002	10000	CHS			140
00144	0601 00 0 00466	10001	STO	CHRCNG	SAVE CHARACTERISTIC SCALING	141
00145	0100 00 0 00162	10001	TZE	SCLOPP+1	AV-PASS SCALING IF NOT NEEDED	142
00146	0534 00 7 00453	10001	LXA	NSO,7		143
00147	4570 60 0 00461	10001	FSTSC LNT*	APLNSC	APLNSO HAS A TAG OF 7	144

BINARY CARD ID. INV40007

00137	3 00001 1 00162	10001	STRTSC TXH		SCLOPP+1,1,1	143
00140	4500 60 0 00455	10001	CAL*	APVEL	LARGEST ELEMENT = PIVOT ELEMENT	144
00141	4320 00 0 00736	10001	ANA		MASK PUT ALL BUT CHARACTERISTIC	145
00142	0402 00 0 00737	10001	SUR		=01770000000000 FIND DIFFERENCE FROM 177	146
00143	0760 00 0 00002	10000	CHS			147
00144	0601 00 0 00466	10001	STO	CHRCNG	SAVE CHARACTERISTIC SCALING	148
00145	0100 00 0 00162	10001	TZE	SCLOPP+1	AV-PASS SCALING IF NOT NEEDED	149
00146	0534 00 7 00453	10001	LXA	NSO,7		150
00147	4570 60 0 00461	10001	FSTSC LNT*	APLNSC	APLNSO HAS A TAG OF 7	151

INV4S
ASSEMBLED TEXT.

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00150	0070	00	0	00161	10001	TRA	SCLOOP	152
00151	0500	00	0	00466	10001	CLA	CHRCNG	153
00152	0401	60	0	00461	10001	ADM*	APLNSO	154
00153	0120	00	0	01003	10011	TPL	++3	155
00154	0600	60	0	00461	10001	STZ*	APLNSO	156
00155	0020	00	0	00161	10001	TRA	SCLOOP	157
00156	0560	60	0	00461	10001	LQR*	APLNSQ	158
00157	0763	00	0	00000	10000	LLS	0	159
00160	0601	60	0	00461	10001	STO*	APLNSQ	160
00161	2	00001	7	00147	10001	TIX	FSTSCL,7,1	161

BINARY CARD ID. INV40008

00162	0074	00	4	00612	10001	TSX	REDUCE,4	162
00163	0500	60	0	00455	10001	CLA*	ADPVEL	163
00164	0074	00	4	00654	10001	TSX	SCALE,6	164
00165	0131	00	0	00000	10000	XCA	SCALE PIVOT ELEMENT	165
00166	0260	60	0	00446	10001	FMP*	DET	166
00167	0074	00	4	00654	10001	TSX	SCALE,4	167
00170	0601	60	0	00446	10001	STD*	DET	168
00171	0534	00	7	00452	10001	LXA	N,7	169
00172	0500	60	0	00455	10001	CLA*	ADPVEL	170
00173	0601	60	0	00447	10001	MULTPL	MULTPL	171
00174	0500	60	0	00456	10001	CLA*	ADPVRW	172
00175	0241	60	0	00447	10001	FDP*	MULTPL	173
00176	4600	60	0	00456	10001	STO*	ADPVRW	174
00177	2	00001	7	00174	10001	TIX	ADPVRW	175
00200	0500	00	0	00734	10001	CLA	ADJUST,7,1	176
00201	0241	60	0	00447	10001	FDP*	=1.	177
00202	4600	60	0	00455	10001	STO*	MULTPL	178
00203	1	00001	1	01001	10011	TIX	ADPVEL	179
00204	3	00000	1	00215	10001	ROLPED TXH	**1,1,1	180

BINARY CARD ID. INV40009

00205	0500	00	0	00455	10001	CLA	ADPVEL	181
00206	0400	00	0	00733	10001	ADD	=1	182
00207	0400	00	0	00452	10001	STA	N	183
00210	0621	00	0	00455	10001	CLA	ADPVEL	184
00211	0500	00	0	00456	10001	ADD	ADPVRW	185
00212	0400	00	0	00452	10001	STA	N	186
00213	0621	00	0	00456	10001	TRA	ADPVRW	187
00214	0020	00	0	00071	10001	ROLPED	ROLPED	188

*
*
*
*
*

00215	0534	00	7	00452	10001	REDVR LXA	N,7	189
00216	0600	00	0	00471	10001	STZ	TEMP1	190
00217	0754	00	7	00000	10000	PXA	0,7	191
00220	0734	00	1	00000	10000	PAX	0,1	192
00221	0754	00	7	00000	10000	PXA	0,7	193
00222	0402	60	0	00462	10001	SUB*	ADPVRW	194
00223	0100	00	0	00226	10001	TZE	FOUND	195

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INV45
ASSEMBLED TEXT.

00224	2	00001	1	00221	10001	TIX	RMSRCH,1,1		202
00225	0020	00	0	00431	10001	TRA	ERR4	CANNOT FIND ROW	203
00226	0754	00	7	00000	10000	FOUNDR PXA	0,7		204
00227	0634	00	1	00471	10001	SXA	TEMP1,1		205

BINARY CARD ID.	INV40010									
00230	0402	00	0	00471	10001	SUB	TEMP1	COLUMN IS IN CORRECT PLACE	206	
00231	0100	00	0	00246	10001	TZE	RWLPED		207	
00232	0634	00	7	00473	10001	SXA	TEMPXR,7		208	
00233	0074	00	4	00521	10001	TSX	INRCHC,4		209	
00234	0074	00	0	00473	10001	TSX	TEMPXR	ROW INTEGER FOUND	210	
00235	0074	00	0	00471	10001	TSX	TEMP1	LOCATION OF ROW INTEGER	211	
								INTERCHANGE ROW INTEGERS.	212	
00236	0534	00	7	00473	10001	LXA	TEMPXR,7		213	
00237	0500	00	0	00462	10001	CLA	ADRINT		214	
00240	0402	00	0	00473	10001	SUA	TEMPXR		215	
00241	0621	00	0	01001	10011	STA	**+1		216	
00242	0500	00	0	00000	10000	CLA	**		217	
00243	0601	60	0	00462	10001	STO*	ADRINT	ADRINT HAS A TAG OF 1	218	
00244	0500	00	0	00473	10001	CLA	TEMPXR		219	
00245	0601	60	0	41003	10011	STO*	**+3		220	
00246	2	00001	7	00217	10001	RWLPED TIX	RMSRCH-2,7,1	LOOP FOR N ROWS.	221	
								NOW INTERCHANGE ROWS ACCORDING TO COLUMN TABLE	222	
									223	
00247	0534	00	7	00452	10001	LXA	N,7		224	
00250	0754	00	7	00000	10000	PXA	0,7		225	
00251	0734	00	1	00000	10000	PAX	0,1		226	
00252	0754	00	7	00000	10000	CLSRCH PXA	0,7		227	

BINARY CARD ID.	INV40011									
00253	0402	60	0	00463	10001	SUB*	ADCINT	ADCINT HAS A TAG OF 1	229	
00254	0100	00	0	00257	10001	TZE	FOUNDJC		230	
00255	2	00001	1	00252	10001	TIX	CLSRCH,1,1		231	
00256	0020	00	0	00431	10001	TRA	ERR4	CANNOT FIND COLUMN	232	
00257	0754	00	7	00000	10000	FOUNDC PXA	0,7		233	
00260	0634	00	1	00471	10001	SXA	TEMP1,1		234	
00261	0402	00	0	00471	10001	SUB	TEMP1	ROW IS IN CORRECT PLACE	235	
00262	0100	00	0	00277	10001	TZE	CLLPED		236	
00263	0634	00	7	00473	10001	SXA	TEMPXR,7		237	
00264	0074	00	4	00476	10001	TSX	INRCHC,4		238	
00265	0074	00	0	00473	10001	TSX	TEMPXR		239	
00266	0074	00	0	00471	10001	TSX	TEMP1		240	
								INTERCHANGE COLUMN INTEGERS	241	
00267	0534	00	7	00473	10001	LXA	TEMPXR,7		242	
00270	0500	00	0	00463	10001	CLA	ADCINT		243	
00271	0402	00	0	00473	10001	SUB	TEMPXR		244	
00272	0621	00	0	01001	10011	STA	**+1		245	
00273	0500	00	0	00000	10000	CLA	**		246	
00274	0601	60	0	00463	10001	STO*	ADCINT	ADCINT HAS A TAG OF 1	247	
00275	0500	00	0	00473	10001	CLA	TEMPXR		248	
BINARY CARD ID.	INV40012									249
00276	0601	60	0	41003	10011	STO*	**+3			

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00277	2	00001	7	00250	10001	CLLPPD TIX	CLSRCH-2,7,1	LOOP FOR N COLUMNS	
*									
*									
*									
*									
00300	0500	00	0	00466	10001	CLA	CHRCNG		
00301	0100	00	0	00361	10001	TZE	OSLPED+1		
00302	4120	00	0	00315	10001	THI	RESCAL		
00303	0774	00	1	00001	10000	AXT	1,1		
00304	0500	00	0	00454	10001	CLA	ADA		
00305	0400	00	0	00452	10001	ADD	N		
00306	0621	00	0	00456	10001	STA	ADPVRW		
00307	0074	00	4	00546	10001	TSX	FINDLE,4		
00310	0500	00	0	00466	10001	CLA	CHRCNG		
00311	0401	00	0	00471	10001	ADM	TEMP1		
00312	4760	00	0	00001	10000	PBT			
00313	0020	00	0	01002	10011	TRA	**2		
00314	0020	00	0	00431	10001	TRA	ERR4		
00315	0534	00	7	00453	10001	LXA	NSQ,7		
00316	0500	00	0	00466	10001	CLA	CHRCNG		
00317	0401	60	0	00461	10001	ADM*	APLNSQ		
00320	0120	00	0	01003	10011	TPL	**3		

BINARY CARD	IN. ID.	INVT	STZ*	APLNSQ	UNDERFLOW, STORE ZERO	272
00321	0600	60	0	00461		273
00322	0020	00	0	00326		274
00323	0560	60	0	00461		275
00324	0763	00	0	00000		276
00325	0601	60	0	00461		277
00326	2	00001	7	00316		278
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						300

2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	2100	2101	2102	2103	2104	2105	2106	2107	2108	2109	2110	2111	2112	2113	2114	2115	2116	2117	2118	2119	2120	2121	2122	2123	2124	2125	2126	2127	2128	2129	2130	2131	2132	2133	2134	2135	2136	2137	2138	2139	2140	2141	2142	2143	2144	2145	2146	2147	2148	2149	2150	2151	2152	2153	2154	2155	2156	2157	2158	2159	2160	2161	2162	2163	2164	2165	2166	2167	2168	2169	2170	2171	2172	2173	2174	2175	2176	2177	2178	2179	2180	2181	2182	2183	2184	2185	2186	2187	2188	2189	2190	2191	2192	2193	2194	2195	2196	2197	2198	2199	2200	2201	2202	2203	2204	2205	2206	2207	2208	2209	2210	2211	2212	2213	2214	2215	2216	2217	2218	2219	2220	2221	2222	2223	2224	2225	2226	2227	2228	2229	2230	2231	2232	2233	2234	2235	2236	2237	2238	2239	2240	2241	2242	2243	2244	2245	2246	2247	2248	2249	2250	2251	2252	2253	2254	2255	2256	2257	2258	2259	2260	2261	2262	2263	2264	2265	2266	2267	2268	2269	2270	2271	2272	2273	2274	2275	2276	2277	2278	2279	2280	2281	2282	2283	2284	2285	2286	2287	2288	2289	2290	2291	2292	2293	2294	2295	2296	2297	2298	2299	2300	2301	2302	2303	2304	2305	2306	2307	2308	2309	2310	2311	2312	2313	2314	2315	2316	2317	2318	2319	2320	2321	2322	2323	2324	2325	2326	2327	2328	2329	2330	2331	2332	2333	2334	2335	2336	2337	2338	2339	2340	2341	2342	2343	2344	2345	2346	2347	2348	2349	2350	2351	2352	2353	2354	2355	2356	2357	2358	2359	2360	2361	2362	2363	2364	2365	2366	2367	2368	2369	2370	2371	2372	2373	2374	2375	2376	2377	2378	2379	2380	2381	2382	2383	2384	2385	2386	2387	2388	2389	2390	2391	2392	2393	2394	2395	2396	2397	2398	2399	2400	2401	2402	2403	2404	2405	2406	2407	2408	24
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BINARY	CAPD	ID.	INV40014	LLS	SCALE,4	
00344	0763	00	0	00000	10000	294
00345	0074	00	4	00654	10001	295
00346	0601	60	0	00446	10001	296
00347	0020	00	0	00360	10001	297
00350	0500	60	0	00446	10001	298
00351	0241	60	0	00450	10001	299

INV4S
ASSEMBLED TEXT.

BINARY	CARD	ID.	INV40015	XRT	AXT	**7	RESTORE	CELL	0
00357	0774	00	7	00000	10000				310.
00370	4500	00	0	00443	10001	TEMP8			317
00371	0602	00	0	00010	10000	9			318
00372	0500	60	0	00446	10001	DET			319
00373	0601	60	4	00010	10000	8,4			320
00374	0500	00	0	00451	10001	DETYP			321
00375	0601	60	4	00011	10000	9,4			322
00376	0500	00	0	00467	10001	ERRCD1			323
00377	0601	60	4	00005	10000	5,4			324
00400	0500	00	0	00470	10001	ERRCD2			325
00401	0601	60	4	00006	10000	6,4			326
00402	0020	00	4	00001	10000	1,4			327
					TRA				

[illegible]

INV45
ASSEMBLED TEXT.

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00424	0500	00	0	00734	10001	CLA	=1.	CHRCNG	-0201400000000	350
00425	0400	00	0	00466	10001	ADD	X94.4			351
00426	0534	00	4	00364	10001	LXA				352
00427	0601	60	4	00007	10000	STO*	7.4	STORE SCALING FACTOR		353
00430	0020	00	0	00327	10001	TRA	RSCLED+1	GO BACK AND SCALE DETERMINANT		354
00431	0500	00	0	00467	10001	ERR4 CLA	ERRCD1	CANNOT RE-ARRANGE ROWS,COLUMNS -MACH. ERROR		355
00432	4100	00	0	00441	10001	TNZ	ERR4PL			356
00433	0500	00	0	00742	10001	CLA	=4			357
00434	0601	00	0	00467	10001	STO	ERRCD1	CANNOT RE-ORDER ROWS AND COLUMNS		358
BINARY CARD ID. INV40017										
00435	0600	00	0	00470	10001	STZ	ERRCD2	FPT GIVES STORAGE TRAP		359
00436	0020	00	0	00361	10001	TRA	OSLPED+1	RETURN IMMEDIATELY		360
00437	0400	00	0	00743	10001	ERR3PL ADD	=10			361
00440	0020	00	0	00422	10001	TRA	ERR3+3			362
00441	0400	00	0	00744	10001	ERR4PL ADD	=20			363
00442	0020	00	0	00434	10001	TRA	ERR4+3			364
* STORAGE FOR PROGRAM CONSTANTS										365
* STORAGE FOR CORE LOCATION B (DEC)										366
00443	0	00000	0	00000	10000	TEMP8 PZE	0			367
00444	0020	00	0	00707	10001	FPTRA TRA	FLPSPL			368
00445	0	00000	0	00000	10000	CELLO PZE	0	STORAGE FOR FLPSPL CODE		369
00446	0	00000	0	00000	10000	DET PZE	0	ADDRESS OF DETERMINANT		370
00447	0	00000	0	00000	10000	MULTPL PZE	0	ADDRESS OF REDUCTION FACTOR		371
00450	0	00000	0	00000	10000	TEN PZE	0	ADDRESS OF FLOATING POINT 10.		372
00451	0	00000	0	00000	10000	DETXP PZE	0	CELL FOR DETERMINANT EXPONENT		373
00452	0	00000	0	00000	10000	N PZE	0			374
00453	0	00000	0	00000	10000	NSQ PZE	0	N*2		375
00454	0	00000	0	00000	10000	ADA PZE	0	ADDRESS OF MATRIX		376
00455	0	00000	0	00000	10000	ADPVEL PZE	0	ADDRESS OF CURRENT PIVOT ELEMENT		377
00456	0	00000	7	00000	10000	ADPVRW PZE	0.7	ADDRESS OF CURRENT PIVOT ROW +2N		378
00457	0	00000	6	00000	10000	ADDPPEL PZE	0.6	ADDRESS OF ELEMENT BEING REDUCED		379
BINARY CARD ID. INV40018										380
00460	0	00000	7	00000	10000	ADDPWR PZE	0.7	ROW OF ADPEL		381
00461	0	00000	7	00000	10000	APLNSQ PZE	0.7	ADDRESS OF FIRST CELL BEYOND MATRIX		382
00462	0	00000	1	00000	10000	ADPINT PZE	0.1	ADDRESS OF ROW INTEGERS + N		383
00463	0	00000	1	00000	10000	ADCTNT PZE	0.1	ADDRESS OF COLUMN INTEGERS + N		384
00464	0	00000	0	00000	10000	LGSTRW PZE	0	ROW INDEX OF LARGEST ELEMENT IN SUB-MATRIX		385
00465	0	00000	0	00000	10000	LGSTCL PZE	0	COLUMN INDEX OF LARGEST ELEM. IN SUB-MATRIX		386
00466	0	00000	0	00000	10000	CHRCNG PZE	0	CHARACTERISTIC SCALF FACTOR		387
00467	0	00000	0	00000	10000	ERRCD1 PZE	0	ERROR CODE 1		388
00470	0	00000	0	00000	10000	ERRCD2 PZE	0	ERROR CODE 2		389
00471	0	00000	0	00000	10000	TEMP1 PZE	0			390
00472	0	00000	0	00000	10000	TEMP2 PZE	0	TEMPORARY FOR ADDRESS ONLY		391
00473	0	00000	0	00000	10000	TEMPXR PZE	0	TEMPORARY STORAGE FOR FLPSPL		392
00474	0	00000	0	00000	10000	TEMPAC PZE	0	TEMP AS ABOVE		393
00475	0	00000	0	00000	10000	TEMPHQ PZE	0	CLOSED SUBROUTINE TO INTERCHANGE ROWS		394
* TWO ARGUMENTS -I,J=ROWS TO BE MOVED										395
* INPCHR L00*										396
00476	0560	60	4	00001	10000	INPCHR L00*	1.4			397
* INPCHR L00*										398
* INPCHR L00*										399

INV4S
ASSEMBLED TEXT.

BINARY	CARD	IN. ID.	INV40024	STO*	ADOPRM	REDUC2,7,1	PUT REDUCTION FACTOR WHERE ZERO WAS PRODUCED	GO TO NEXT ROW	519
00642	0601	60	0	00460	10001				520
00643	2	00001	7	00637	10001				521
00644	0500	60	0	00447	10001	MULTPL			522
00645	0601	60	0	00457	10001	ADOPPL			523
00646	0500	00	0	00450	10001	ADOPRM			524
00647	0400	00	0	00452	10001	N			525
00650	0621	00	0	00460	10001	ADOPRM			526
00651	1	00001	5	01001	10011	**1,5,1			527
00652	2	00000	4	00625	10001	REDUC1,6,**			528
00653	0020	00	4	00001	10000	1,4			529
							DONE		530
								X85 = ROW ABOUT TO BE REDUCED	
								N IN DECREMENT	

LINE	ADDRESS	OPERATION	DATA	COMMENT
529	00654	SCALE	STO	TEMPAC
530	00655	SSP	00000	
531	00656	SCALE	CAS	TEN
532	00657	TRA	00001	DIVIDE
533	00658	TRA	00001	DIVIDE
534	00659	TSTONE	CAS	=1.
535	00660	TRA	00001	CHKSGN
536	00661	TRA	00001	CHKSGN
537	00662	TRA	00001	CHKSGN
538	00663	TRA	00001	CHKSGN

BINARY CARD ID.	INV400ZS
FMP#	TEN
SFO*	MULTPL
CLA	OETXP
SUB	=1
TEMPORARY STORAGE	
545	10001
546	00450
547	00447
548	10001
	00451
	00733
	10001

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INV4S
ASSEMBLED TEXT.

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00671 0601 00 0 00451 10001
00672 0500 60 0 00447 10001
00673 0020 00 0 00661 10001
00674 0241 60 0 00450 10001
00675 4600 60 0 00447 10001
00676 0500 00 0 00451 10001
00677 0400 00 0 00733 10001
00700 0601 00 0 00451 10001
00701 0500 60 0 00447 10001
00702 0020 00 0 00656 10001
00703 0560 00 0 00474 10001
00704 0763 00 0 00000 10000
00705 0560 00 0 00745 10001
00706 0020 00 4 00001 10000

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STD
CLA*
TRA
DIVIDE
FDP*
STQ*
CLA
ADD
STD
CLA*
TRA
CHKSGN LDQ
LLS
LDQ
TRA

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FLOATING POINT SPILL ROUTINE TO ANALYZE
OVER/UNDER FLOW DURING DOUBLE PRECISION
OPERATIONS

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FLPSPL STD
TEMPAC

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BINARY CARD ID. INV40026
00710 0500 00 0 00000 10000
00711 0622 00 0 00445 10001
00712 0500 00 0 00445 10001
00713 0340 00 0 00746 10001
00714 0020 00 0 00723 10001
00715 0020 00 0 00721 10001
00716 0500 00 0 00474 10001
00717 0560 00 0 00745 10001
00720 0020 60 0 00000 10000
00721 0754 00 0 00000 10000
00722 0020 00 0 41003 10011
00723 0340 00 0 00747 10001
00724 0020 00 0 01003 10011
00725 0020 60 0 00000 10000
00726 0020 00 0 00403 10001
00727 0340 00 0 00750 10001
00730 0020 00 0 00403 10001
00731 0020 00 0 00721 10001
00732 0020 00 0 00721 10001

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CLA
STD
Cello
Cello
CAS
GRT3
TRA
ALLUND
CLA
LDQ
TRA*
ALLUND PXA
TRA
GRT3 CAS
TRA*
TRA
ERR1
CAS
FRR1
TRA
ALLUND
TRA

```

```

BINARY CARD ID. INV40027
00733 000000000001 10000
00734 201400000000 10000
00735 204500000000 10000
00736 377000000000 10000
00737 177000000000 10000
00740 000000000002 10000
00741 000000000003 10000
00742 000000000004 10000

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*LORG

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INV4S
ASSEMBLED TEXT.

00743 00000000012 10000
00744 00000000024 10000
00745 00000000000 10000
00746 00003000000 10000
00747 00001100000 10000
00750 00001300000 10000
00000 01111

END

591

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INV4S
CONTROL DICTIONARY

\$CDICT INV4S

INV40028

BINARY CARD ID. INV40029

000751000000
000004000005
314565046260
000751000000
314565046260
000000000000

PREFACE START=0,LENGTH=489,TYPE=7094,CMPLEX=5

DECK LOC=0,LENGTH=489

REAL LOC=0,LENGTH=0

INV4S

INV4S

\$DKEND INV4S

INV40030

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INV88 - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE INV88

C FOR WING BODY CASE, PREPARES AERODYNAMIC INFLUENCE MATRIX FOR
C MATRIX REDUCTION
C MAXIMUM SIZE MATRIX INVERSION =110
COMMON DATE(2),NTAPEA,NTAPES,NTAPEEC,NTAPED,NTAPEE,NTAPEF,NTAPEI
1,NTAPEO,NBODY,NWING,XMACH,SYM,KACE
DIMENSION ABB(115,115),AWB(110)

MCEMEN=115

C READ AERODYNAMIC INFLUENCE MATRIX (INFLUENCE ON BODY DUE TO BODY
C AND INFLUENCE ON WING DUE TO BODY) INTO CORE

CALL FSF(1,NTAPEA,IRR)
DO 100 J=1,NBODY
READ (NTAPEA) (ABB(I,J),I=1,NBODY),(AWB(I),I=1,NWING)

WRITE (NTAPED) (AWB(I),I=1,NWING)

100 CONTINUE

END FILE NTAPED

C INVERT AERODYNAMIC INFLUENCE MATRIX (INFLUENCE ON BODY DUE TO BODY)

CALL SINVRT(ABB,MCEMEN,NBODY,IRR1,IRR2,SCALE,DET,NDETXP)

IF (IRR1) 150,200,150

150 CONTINUE

WRITE (NTAPED,6000) IRR1,IRR2,SCALE

REWIND NTAPEA

STOP

200 CONTINUE

DO 300 J=1,NBODY

WRITE (NTAPED) (ABB(I,J),I=1,NBODY)

300 CONTINUE

END FILE NTAPED

REWIND NTAPED

6000 FORMAT(1H1,33HERROR IN INVERSION OF BODY MATRIX,5X,
16HIRR1 =,I3,5X,6HIRR2 =,I3,5X,7HSCALE =,E12.6)

RETURN
END

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INVRM - EFN SOURCE STATEMENT - IFMIS) -

SUBROUTINE INVRM

C INVERT REDUCED MATRIX
C MAXIMUM SIZE MATRIX INVERSION =110

COMMON DATE(2),NTAPFA,NTAPEB,NTAPFC,NTAPED,NTAPEE,NTAPEF
1,NTAPEI,NTAPEO,NBODY,NWING,XMACH,SYM,KACE

DIMENSION ARW(115,115)

MDMEM=115

DC 700 J=1,NWING

READ (NTAPEE) (ARW(I,J),I=1,NWING)

700 CONTINUE

END FILE NTAPEE

C MATRIX INVERSION

CALL SINVRT(ARW,MDMEM,NWING,IRR1,IRR2,SCALE,DET,NDETXP)
IF (IRR1) 750,800,750

750 CONTINUE

WRITE (NTAPEO,6010) IRR1,IRR2,SCALE

REWIND NTAPEE

STOP

800 CONTINUE

DC 850 J=1,NWING

WRITE (NTAPEE) (ARW(I,J),I=1,NWING)

850 CONTINUE

END FILE NTAPEE

REWIND NTAPEE

6010 FORMAT(1H1,36HERROR IN INVERSION OF REDUCED MATRIX,5X,
16HIRR1 -,13,5X,6HIRR2 -,13,5X,7HSCALE =,E12.6)

RETURN

END

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05/22/67

INW - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE INW

C FOR WING ONLY CASE, STORES MATRIX (A) AND (A) INVERSE ON TAPE
C MAXIMUM SIZE MATRIX INVERSION =110

COMMON DATE(2),NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI
1,NTAPEJ,NBODY,NWING,XWACH,SYM,KACE

DIMENSION AMW(115,115)

MCMEM=115

C READ (A) MATRIX INTO CORE, WRITE ON TAPE

CALL FSF(1,NTAPEA,IRR4

DO 100 J=1,NWING

READ (NTAPEA) (AMW(1,J),I=1,NWING)

WRITE (NTAPEE) (AMW(1,J),I=1,NWING)

100 CONTINUE

END FILE NTAPEE

REWIND NTAPEA

C INVERT MATRIX (A)

CALL SINVRT(AMW,MDEPEN,NWING,IRR1,IRR2,SCALE,DET,NOETXP)

IF (IRR1) 150,200,150

150 WRITE (NTAPED,6000) IRR1,IRR2,SCALE

REWIND NTAPEE

STOP

200 CONTINUE

DO 250 J=1,NWING

WRITE (NTAPEE) (AMW(1,J),I=1,NWING)

250 CONTINUE

END FILE NTAPEE

REWIND NTAPEE

6000 FORMAT(1H1,30HERROR IN INVERSION OF WING ONLY MATRIX
1,5X,6HIRR1 =,13,5X,6HIRR2 =,13,5X,7HSCALE =,E12.6)

RETURN

END

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CIPACK MICHAEL SYNGE 6-9247 COMPILED 3 SEP 64
C TO PACK A BUFFER BY MOVING ALL FULL ARRAYS TO THE BEGINNING
C AND CONDENSING ALL THE EMPTY ARRAYS INTO ONE AT THE END.
C
C FUNCTION IPACK(RUF)
C DIMENSION RUF(1)
C
C N - TOTAL LENGTH OF BUFFER
C M - FIRST CELL OF CURRENT ARRAY
C J - TOTAL NUMBER OF FREE CELLS
C
C IF (ICODE(RUF)-4)90,2,90
C 2 N=-I(RUF(3))
C IF (N)80,80,3
C 3 M=4
C J=0
C 5 L=LENG(RUF(M-1))
C IF (ICODE(RUF(M-2)))10,40,10
C 10 IF (J)50,50,20
C
C MOVE UP FULL ARRAY
C
C 20 I1=N-2-J
C I2=I1+L+1
C K=M-2
C DO 30 I=I1,I2
C RUF(I)=RUF(K)
C 30 K=K+1
C RUF(I1)=RUF(I1+2)
C CALL UPDATE(RUF(I1+1))
C GO TO 50
C 40 J=J+L+2
C 50 IF (N-L-M)100,100,70
C 70 M=M+L+2
C GO TO 5
C 100 IF (J)1000,1000,110
C
C SET UP FINAL (EMPTY) ARRAY
C
C 110 I1=N-J+1
C IPACK=J-2
C RUF(I1)=ARFREQ(I1+2)
C RUF(I1+1)=ARSEC(IPACK,IPACK)
C GO TO 1000
C
C ERRORS
C
C 80 IPACK=-2
C GO TO 1000
C 90 IPACK=-1
C 1000 RETURN
C
C END

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IRLEAS
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
07/31/65

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CIRLEAS      MICHAEL SYNGE      6-9247      COMPILED 21 SEP 64
C            TO RELEASE ALL EXCEPT THE
C            FIRST K WORDS OF AN ARRAY
C
C            FUNCTION IRLEAS(IRRAY,K)
C            DIMENSION IRRAY(1)
C
C            M      - INITIAL LENGTH OF THE ARRAY
C            K      - THE NUMBER OF WORDS TO BE RETAINED
C
C            N=K+2
C            IF(N-2)70,70,5
C            5 I=32767
C            IF (ICODE(IRRAY(1)))90,50,10
C            10 M=LENG(IRRAY(1+1))
C            IF (M-N)50,20,20
C            20 IRRAY(1+1)=IRRAY(1+1)-262144*(M-N+2)
C            IRRAY(N-1)=IRFEIN-IRFR(IRRAY)
C            IRRAY(N)=IRSEC(M-N,IRLEAS)
C            50 IRLEAS=0
C            GO TO 100
C            70 IRLEAS=IDLETE(IRRAY)
C            GO TO 100
C            90 IRLEAS=-1
C            100 RETURN
C
C            END

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IRLE0030
IRLE0040
IRLE0060
IRLE0070
IRLE0080
IRLE0100
IRLE0110
IRLE0120
IRLE0130
IRLE0140
IRLE0150
IRLE0160
IRLE0170
IRLE0180
IRLE0190
IRLE0210
IRLE0230
IRLE0240
IRLE0250
IRLE0260
IRLE0270
IRLE0280
IRLE0290
IRLE0300
IRLE0310

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IRSERV
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
07/31/65

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CIRSERV  MICHAEL SYNGE      6-9247      COMPILED 21 AUG 64
C  TO RESERVE AN ARRAY OF N CELLS IN A BUFFER. THE ARRAY CAN
C  SUBSEQUENTLY BE REFERRED TO AS BUF(NAME) .
C
C  FUNCTION  IRSERV(N,BUF,NAME)
C
C  M=-N
C  IRSERV=IADARY(M,M,BUF,NAME)
C  RETURN
C
C  END

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IRSE0030
IRSE0040
IRSE0050
IRSE0070
IRSE0080
IRSE0090
IRSE0100
IRSE0110
IRSE0120
IRSE0130
IRSE0140

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06/02/67

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KARMOR - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE KARMOR(NBODY,NTHETA,
1,XP,ZP,RFAREA,XB,R,THETAB,ZDELTA,XC,YC,ZC,THETA,U,VV,W,WM,ANI,CPB
2,DBCL,BCD,BCM)
    COMMON DATE(2),NTAPEA,NTAPEB,NTAPEC,NTAPEF,NTAPEE,NTAPEF,NTAPEI
1,NTAPEO,NBODY,NWING,XMACH,SYR,KACE
    DIMENSION XB(1),R(1),THETAB(1),ZDELTA(1),XC(1),YC(1),ZC(1)
1,U(1),VV(1),WM(1),ANI(1),CPB(55),THETA(1)
    DIMENSION ALPHAC(55),OTHEA(10),T(55),TC(55),TX(55),CPB(10,55)
1,UB(55,10),VB(55,10),VTA(55,10),SY(2)
    DIMENSION FDI(55),SD(55),NBS(10),C(10)

C CALCULATION OF VELOCITY COMPONENTS DUE TO BODY THICKNESS
C USING SMOOTH BODY SOLUTION
    ACOSMU=2.*ALOG(SQRT(ABS((U+1.)/2.))+SQRT(ABS((U-1.)/2.)))

    PI=3.1415926
    XMACH2=XMACH*XMACH
    BT2=XMACH2-1.
    BETA=SQRT(BT2)
    NI=NBODY-1
    MACEL=0

    DO 60 J=1,NI
    60 ALPHAC(J)=ARA-(ZDELTA(J+1)-ZDELTA(J))/(XB(J+1)-XB(J))
    DO 65 J=1,NTHETA
    65 THETAB(J)=THETA(J)/57.2957795

C COMPUTE FIRST AND SECOND DERIVATIVES
    CALL DERIVS(XB,R,NBODY,FD,SD)

    TANDEL=FD(1)
    COTDEL=1./FD(1)
    COB=COTDEL/BETA

C CALCULATE SOURCE STRENGTHS
    NB=0
    DO 160 I=1,NI
    160 I=1,NI
    M=I+1
    UBSUM=0.
    VBSUM=0.
    WBSUM=0.
    VDBSUM=0.
    VTDSUM=0.
    UC=0.
    VC=0.
    PHIX=0.
    PHISUM=0.

```

2 3 4

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KARNOR - EFN SOURCE STATEMENT - IFN(S) -

PHID=0.

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RS=ALPHAC(I)
RDRXS=FD(I+1)
TRM=XB(I+1)-XB(I)+BETA*R(I)
TRM2=BETA*R(I+1)
TRM3=TRM2/TRM0
TRM4 = SORT(1.-TRM3+TRM3)
RAB1=BETA+SQRT(1.-TRM3**2)/TRM3
RUB1=-ACOSH(TRM0/TRM2)
RAB0=-.5*B2*(SQRT(1.-TRM3**2)/TRM3**2-RUB1)
RUBD=RAB1
VTD=-.5*B2*(SQRT(1.-TRM3**2)/TRM3**2+RUB1)
RN1=RAB1-FD(I+1)*RUB1
RN1=RABD-FD(I+1)*RUBD
IF(1-NE.1)GO TO 100
IF(1.EQ.1.AND.R(1).NE.0.)GO TO 80

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IF I EQUALS 1, DO TANGENT COME SOLUTION
OR CORNER SOLUTION FOR NOSE
T11= TANDEL/SQRT(COTDEL**2-BT2)+TANDEL*ACOSH(COB))
TC11 = -ALPHAC(I)/RM1
GO TO 85

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80 T11=0.

TC11=0.

85 CONTINUE

DO 87 K=1,NTHETA

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UB(1,K) = -ACOSH(COB)*T11+COS(THETAB(K))*RUBD*TC11
VB(1,K) = SQRT(COTDEL**2-BT2)*T11+COS(THETAB(K))*RABD*TC11
87 VTB(1,K) = SIN(THETAB(K))*VTD*TC11

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100 CONTINUE

DO 155 J=1,I

NL=NB

NCC=0.

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TRM1=XB(I+1)-XB(J)+BETA*R(J)
IF (R(I+1).EQ.0.) GO TO 152

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TRM3=TRM2/TRM1

TRM32=TRM3**2

TRM4=SQRT(1.-TRM32+TRM3)

TRM5=ACOSH(TRM1/TRM2)

RAB2=BETA*TRM1*(TRM4+TRM3-TRM3*TRM5)

RUB2=.2*(TRM1*(TRM5-TRM4)

RN=RAB2+FD(I+1)*RUB2

IF (TRM3.EQ.0.) RN=0.

RABD2=-TRM1**3/R(I+1)**2*(1.-4.*TRM32)/3.*TRM4+TRM32*TRM5)

RUBD2=-TRM1**2/R(I+1)*(TRM4-TRM32*TRM5)

VTD2=-TRM1**3/R(I+1)**2*(1.-2.*TRM32)/3.*TRM4-TRM32*TRM5)

RN=RABD2-FD(I+1)*RUBD2

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IF (J .NE. 1) GO TO 150
130 T(J)=(RDRXS-RN1*T11-RNCC)/RN
TC(J)=-(RS+RN1*TC11)/RN
150 RDRXS=RDRXS-RN*T(J)
IF (J .NE. 1) GO TO 151
UBSUM = RUB1*T11
VBSUM = RAB1*T11
UBDSUM = RUBD*TC11
VBDSUM = RABD*TC11
VTDSUM = VTD*TC11
151 CONTINUE
UBSUM = UBSUM - RUB2*T(J)+UC
VBSUM = VBSUM + RAB2*T(J)+VC
UBDSUM = UBDSUM + RUBD2*TC(J)
VBDSUM = VBDSUM + RABD2*TC(J)
VTDSUM = VTDSUM + VTD2*TC(J)
PHIX=PHIX-RUB2*T(J)
RS=RS+RN*TC(J)
GO TO 155
152 IF(1.EQ.J) GO TO 154
IF (J.NE.1) GO TO 153
PHISUM = TRM0*T11
PHID=TRM0*TC11
153 PHISUM = PHISUM+TRM1*TRM1+T(J)
PHID=PHID+TRM1*TRM1+TC(J)
GO TO 155

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KARNOR - EFN SOURCE STATEMENT - IFN(S) -

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154 T(J) = -PHISUM/TRM1**2
TC(J)=-PHID/TRM1**2
155 CONTINUE
DO 157 K=1,NTHETA
UB(M,K)=UBSUM+UBDSUM*COS(THETAB(K))
VB(M,K)=VBSUM+VBDSUM*COS(THETAB(K))
157 VT(M,K)=VTDSUM*SIN(THETAB(K))
160 CONTINUE

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C CALCULATION OF VELOCITY COMPONENTS IN THE FIELD
IF (NMING) TCO,800,700
700 CONTINUE
IF (NACEL.NE.0) GO TO 703
NS=NRDXY+1
JM=1
SY(1)=0.
GO TO 705
703 NS=1
JM=2
SY(1)=1.
SY(2)=-1.

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705 CONTINUE
NPANEL=NBODY+NMING
II=0
DO 790 I=NS,NPANEL
  II=II+1
  U(II)=0.
  V(II)=0.
  W(II)=0.
  AN(II)=0.
  CO 790 N=1,JM
  THETA=ATN1(YC(II)-SY(N)*YN,ZC(II)-ZN)
  COSTHA=COS(THETA)
  SINHA=SIN(THETA)
  R2=(YC(II)-SY(N)*YN)**2+(ZC(II)-ZN)**2
  R1=SQRT(R2)
  BR2=BT2/R2
  NC=0
  US=0.
  VS=0.
  UD=0.
  VD=0.
  VT=0.
  VTF=0.
  VF=0.
  TRM2=SQRT(BR2)
  DO 780 J=1,N1
    TRM1=(XC(II)-XN)-XB(J)+BETA*R(J)
    TRM3=TRM2/TRM1
    TRM32=TRM3*TRM3
    IF (TRM3.GT.1.-OR.TRM3.LE.0.) GO TO 780

C VELOCITY DUE TO LINEARLY VARIING SINGULARITIES
    TRM4=SQRT(1.-TRM32)
    TRM5=ACOSH(TRM1/TRM2)
    US=-2.*TRM1*(TRM5-TRM4)*T(J)
    VS=BETA*TRM1*(TRM4/TRM3-TRM3*TRM5)*T(J)
    UD=TRM1**2/R1*(TRM4-TRM32*TRM5)*TC(J)
    VD=-TRM1**3/R1**2*((1.-4.*TRM32)/3.*TRM4+TRM32*TRM5)*TC(J)
    VT=-TRM1**3/R2*((1.+2.*TRM32)/3.*TRM4-TRM32*TRM5)*TC(J)

C VELOCITY DUE TO TANGENT CONE
  IF (J.NE.1) GO TO 710
  US=US-ACOSH(TRM1/TRM2)*T11
  VS=VS+BETA*SQRT(1.-TRM32)/TRM3*T11
  UD=UD+BETA*SQRT(1.-TRM32)/TRM3*TC11
  VD=VD-5*BT2*(SQRT(1.-TRM32)/TRM32-BETA*SQRT(1.-TRM32)/TRM3)
  $TC11
  VT=VT-5*BT2*(SQRT(1.-TRM32)/TRM32-ACOSH(TRM1/TRM2))*TC11
710 CONTINUE

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KARMOR - EFN SOURCE STATEMENT - IFN

C SUMMATION OF VELOCITY COMPONENTS

750 CONTINUE

U(I1) = U(I1)+US+COSTHA*UD

VF = VF +VF +VS+COSTHA*VD

VTF = VTF + VT*SINTHA

TRM = (XC(I1)-XN)-XB(NBODY5)+BETA*R(NBODY5)

IF (TRM-LE,TRM2) GO TO 775

XI = XB(NBODY5)-(XB(J)-BETA*R(J))-BETA*R(NBODY5)

TRM6 = SORT(TRM+TRM-BR2)

IF (J,NE-1) GO TO 765

U(I1) = U(I1)+T11*(ACOSH(TRM/TRM2)+XI/TRM6)

VF = VF -T11*(TRM1+TRM-BR2)/(R1+TRM6)

765 CONTINUE

U(I1) = U(I1)-.5*(3.*TRM6*(TRM1+TRM1-2.*TRM1+XI-XI*XI-BR2)/TRM6-

S4.*TRM1*ACOSH(TRM/TRM2))*T(J)

VF = VF +(((TRM1+TRM1+BR2)*XI-TRM1*(TRM1+TRM1-BR2))/(R1+TRM6)

)+BR2/R1*ACOSH(TRM/TRM2))*T(J)

775 CONTINUE

780 CONTINUE

VV(I1) = VF*SINTHA+VTF*COSTHA

WW(I1) = VF*COSTHA-VTF*SINTHA

SYN=2*(JM-N)-1

THETAS=THETAA-SYN*THETA(I)

AN(I1) = VF*COS(THETAS)-VTF*SIN(THETAS)

790 CONTINUE

800 CONTINUE

NT=NT+THETA-1

DTMETHA(1)=(THETAB(2)+THETAB(1))/2.

DTMETHA(NT+1)=PI-(THETAB(NT+1)+THETAB(NT))/2.

DO 310 J=2,NT

310 DTMETHA(J)=(THETAB(J+1)-THETAB(J-1))/2.

C CALCULATION OF PRESSURES, FORCES, AND MOMENTS

BODYL=XB(NBODY5)-XB(1)

DO 360 J=1,NT+1

DO 350 I=1,NBODY5

IF (CPCALC-1.) 320,330,335

C LINEAR CP CALCULATIONS

320 CONTINUE

CPBB(J,I)=-2.*UB(I,J)

GO TO 340

C NON-LINEAR CP CALCULATIONS

330 CONTINUE

XN2=XMACH2-1.

CPBB(J,I)=-2.*UB(I,J)+XM2*UB(I,J)**2-VT8(I,J)**2-V8(I,J)**2

GO TO 340

C EXACT CP CALCULATIONS

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230 231

335	CONTINUE	273
	UBD=COS(ARA)+UB(I,J)	275
	VBD=SIN(ARA)+COS(THETAB(J))+VB(I,J)	276
	VTB=VTB(I,J)-SIN(ARA)*SIN(THETAB(J))	279
	Q2=UBD**2+VBD**2+VTB**2	280
	CPB(J,I)=1.42857/XMACH2*((1.+2.*XMACH2*(1.-Q2))**.5-1.)	283
340	CONTINUE	
350	CONTINUE	
360	CONTINUE	
	BBCL=0.	
	BBCL=0.	
	BBCL=0.	
	CALL SCH(XB,R,FD,THETAB,CPB,1,NBODYS,NTHETA,XP,ZP,CX,IRRO)	291
	CALL SCH(XB,R,FD,THETAB,CPB,1,NBODYS,NTHETA,XP,ZP,CN,IRRO)	293
		06/02/67
	KARMOR - EFN SOURCE STATEMENT - IFN(S) -	
	CALL SCH(XB,R,FD,THETAB,CPB,1,NBODYS,NTHETA,XP,ZP,CX,IRRO)	295
	BBCL = BBCL + (CN*COS(ARA))-CX*SIN(ARA)	297
	BBCL = BBCL + (CN*SIN(ARA))+CX*COS(ARA)	299
	BBCL = BBCL - CN*CX*ZP	300
	NST=1	
	IF (R(1).NE.0.) NST=2	
	NBODYS=NBODYS-NST	
	DC 585 I=NST,N1	
	K=I-NST+1	
	DO 580 J=1,NTHETA	
580	CPB (K,J)=CPB(J,I)	
585	CONTINUE	
590	THETAB(J)=THETAB(J)*57.2957795	

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C      OPTIONAL PRINT OF VELOCITY COMPONENTS
      WRITE (NTAPEO,6005) (XB(I),ZDELTA(I),R(I),FD(I),SD(I),I=1,NBODYS)
      IF (VOUT) 610,999,610
610  CONTINUE
      WRITE (NTAPEO,6010)
      WRITE (NTAPEO,6025)
      WRITE (NTAPEO,6015) (THETAB(J),J=1,NTHETA)
      WRITE (NTAPEO,6020)
      DO 620 I=1,NBODYS
620  WRITE (NTAPEO,6000) XB(I),(UB(I,J),J=1,NTHETA)
      WRITE (NTAPEO,6030)
      WRITE (NTAPEO,6015) (THETAB(J),J=1,NTHETA)
      WRITE (NTAPEO,6020)
      DO 630 I=1,NBODYS
630  WRITE (NTAPEO,6000) XB(I),(VB(I,J),J=1,NTHETA)
      WRITE (NTAPEO,6035)
      WRITE (NTAPEO,6015) (THETAB(J),J=1,NTHETA)
      WRITE (NTAPEO,6020)
      DO 640 I=1,NBODYS
640  WRITE (NTAPEO,6000) XB(I),(VTB(I,J),J=1,NTHETA)

999  CONTINUE
      CALL FSF(9,NTAPEC,IRR)
      IF (NACEL.EQ.1) GO TO 1000
      WRITE (NTAPEC) NBODYS
      WRITE (NTAPEC) (XB(J),R(J),J=1,NBODYS)
      WRITE (NTAPEC) (T(J),TC(J),J=1,NBODYS)
      WRITE (NTAPEC) TII,TCII
1000 CONTINUE
      END FILE NTAPEC
      REWIND NTAPEC
      RETURN

6000 FORMAT(1H ,F14.4,F15.5,9F10.5/(F29.5,9F10.5))
6005 FORMAT (1H17/14H BODY GEOMETRY/56X,5HFIRST,9X,6HSECEND/9X,9HX-STAT
$ICN,7X,6HCAMBER,9X,6HRADIUS,2X,2(5X,10HDERIVATIVE//11X,5F15.4))
6010 FORMAT(1H17/66H VELOCITY COMPONENTS ON BODY DUE TO BODY LINE SOURC
$ES AND DOUBLET)
6015 FORMAT(1H0,4X,11HTHETA(DEC.),F14.4,9F10.4/(F29.4,9F10.4))
6020 FORMAT(1H ,9X,1HX)
6025 FORMAT(1H0,5X,8HAXIAL(U))
6030 FORMAT(1H0,5X,10HRADIAL(VR))
6035 FORMAT(1H0,5X,14HTANGENTIAL(VT))
      END

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08/09/67

LACKEY - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE LACKEY(ISTR,XB,YB,ZB,U,V,W,CP)
 COMMON /THICK/THK,ARA,CPCALC,CAMN
 COMMON /FLOV1/KACE,NPANEL,NBODY,NWING,NBDYS,NRWINGS,NRCW,XMACH,SYM
 COMMON /FLOV4/COSARA,SINARA,XMACH2,BT2
 COMMON /FLOV5/N1,N2,N3,N4
 U=0.
 V=0.
 W=0.
 UT=0.
 VT=0.
 WT=0.

C SELECTS MODE OF COMPUTATION
 GO TO(5,10,15),KACE

C WING ALONE

5 CONTINUE

7 IF(THK.EQ.0.) GO TO 8
 CALL EVAL1(N1,1.,XB,YB,ZB,UT,VT,WT,NPANEL)
 U=U+UT
 V=V+VT
 W=W+WT

8 CONTINUE
 IF(CAMN.EQ.1.) GO TO 23
 CALL EVAL1(N1,0.,XB,YB,ZB,UT,VT,WT,NPANEL)
 U=U+UT
 V=V+VT
 W=W+WT

IF(ISTR.EQ.0) WRITE(N2) XB,YB,ZB,UT,VT,WT
 IF(KACE.NE.3) GO TO 23
 CALL EVAL1(1,0.,XB,YB,ZB,UT,VT,WT,NBODY)

U=U+UT
 V=V+VT
 W=W+WT

IF(ISTR.EQ.0) WRITE(N3) XB,YB,ZB,UT,VT,WT
 23 CONTINUE

C GO TO (18,18,10),KACE
 COMPUTES FOR BODY ALONE
 10 CALL VEL1(XB,YB,ZB,UT,VT,WT)

U=U+UT
 V=V+VT
 W=W+WT

IF(ISTR.EQ.0) WRITE(N4) XB,YB,ZB,UT,VT,WT
 GO TO(5,18,18),KACE

C BODY AND WING

15 NI=NBODY+1
 GO TO 7

18 CONTINUE
 IF (CPCALC-1.) 320,320,335
 320 CONTINUE

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LACKEY - EFM SOURCE STATEMENT - IFN(S) -

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C      LINEAR CP FORMULA
      CP = -2.*U
      GO TO 340
330 CONTINUE
C      NON-LINEAR CP FORMULA
      CP = -2.*U+8T2*U-U-V*V-b*b
      GO TO 340
C      **EXACT** ISENTROPIC CP FORMULA
335 Q2=(U+COSARA)**2+V*V+(W+SINARA)**2
      CP = 1.42857/XMACH2*(1.+2.*XMACH2*(1.-Q2))**3.5-1.)
340 CONTINUE
      U = U + COSARA
      W = W + SINARA
20 RETURN
      END

```

43

LENG
7094 RELMOD ASSEMBLY.

07/31/65

\$IBLDR LENG
ASSEMBLED TEXT.

LENG0000

\$TEXT LENG

LENG0001

*LENG: MICHAEL SYNGE 6-9247 ASSEMBLED 27 AUG 64
* TO OBTAIN THE CONTENTS OF THE DECREMENT OF A
* CODE WORD AS A FULL WORD INTEGER

* CALLING SEQUENCE

* N=LENG(CODE)

ENTRY LENG

BINARY CARD (NOT PUNCHED)

00000 0500 60 4 00003 10000
00001 4320 00 0 00004 10001
00002 0771 00 0 00022 10000
00003 0020 00 4 00001 10000

LENG CLA* 3,4
ANA =077777000000
ARS 18
TRA 1,4

00004 077777000000 10000
00000 01111

*LORG
END

CONTROL DICTIONARY

\$CDICT LENG

LENG0002

BINARY CARD (NOT PUNCHED)

0000005000000
0000004000005
432545276060
0000050000000
432545276060
0000000000000

PREFACE START=0,LENGTH=5,TYPE=7094,CMPLEX=5

DECK LOC=0,LENGTH=5

REAL LOC=0,LENGTH=0

\$OKEND LENG

LENG0003

NO MESSAGES FOR THIS ASSEMBLY

SYMBOL REFERENCE DATA

REFERENCES TO DEFINED SYMBOLS.

CLASS SYMGL VALUE REFERENCES

LENG 00000

LCR BLCTR

DUAL UNQS

LCR //

LOC
7094 RELMOD ASSEMBLY.
06/02/67
ILOC00000

\$18LOR ILOC

ILOC
ASSEMBLED TEXT.
STEXT ILOC
ILOC00001

ENTRY	LOC
LOC CLA	3,4
ANA	=077777
TRA	1,4
*LORG	
END	

DEBIS294
DEBIS295
DEBIS296

ILOC
CONTROL DICTIONARY
\$CDICT ILOC
ILOC00003

BINARY CARD ID. ILOC0004
000004000000
000004000005
314346236060
000004000000
434623606060
000000000000

PREFACE START=0,LENGTH=4,TYPE=7094,CNPLX=5
DECK LOC=0,LENGTH=4
REAL LOC=0,LENGTH=0

\$DKEND ILOC
ILOC00005

NO MESSAGES FOR THIS ASSEMBLY

05/22/67

MDMATE - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE MDMATE

```

C      FORMATION OF DRAG MINIMIZATION MATRIX
C      MAXIMUM SIZE MATRIX INVERSION =112
C      MUST BE 2 PLUS MAXIMUM NUMBER OF WING PANELS(110)

COMMON DATE(2),NTAPEA,NTAPEB,NTAPEC,NTAPEE,NTAPEF,NTAPEI
1,NTAPEO,NBODY,NWING,XMACH,SYM,KACE

DIMENSION WM(115,115),XBAR(210),AREA(210)

MDMEN=115
READ (NTAPEC) NBODY,NWING,XMACH,SYM,KACE
NPANEL=NBODY+NWING
READ (NTAPEC) (I,XBAR(I),DUMMY1,DUMMY2,DUMMY3,DUMMY4,DUMMYS
1,AREA(I),DUMMY6,DUMMY7,DUMMY8,I=1,NPANEL)
REWIND NTAPEC

DO 100 J=1,NWING
  READ (NTAPEE) (WM(I,J),I=1,NWING)
  CCNTINUE
  REWIND NTAPEE

DO 200 I=1,NWING
  I=1
  II=1+NBODY
  DO 200 J=1,I
    JJ=J+NBODY
    WM(I,J)=-WM(I,J)+AREA(II)-WM(J,I)*AREA(JJ)
    WM(J,I)=WM(I,J)
  CONTINUE

  NN=NWING+1
  NNN=NWING+2
  DO 300 J=1,NWING
    JJ=J+NBODY
    WM(J,NN)=-AREA(JJ)
    WM(NN,J)=-AREA(JJ)
    XA=-XBAR(JJ)*AREA(JJ)
    WM(J,NNN)=XA
    WM(NN,NNN)=XA
  CONTINUE

  WM(NN,NN)=0.0
  WM(NN,NNN)=0.0
  WM(NNN,NN)=0.0
  WM(NNN,NNN)=0.0

  CALL FFF(1,NTAPEA,IRR)
DO 325 J=1,NNN
  WRITE (NTAPEA) (WM(I,J),I=1,NNN)
END FILE NTAPEA

C      INVERT DRAG MINIMIZATION MATRIX CONSTRAINED FOR CL

```

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05/22/67

MDMATE - FFM SOURCE STATEMENT - IFM(S) -

CALL SINVRT (WM,MDMEM,NN,IRR1,IRR2,SCALE,DFT,NDETXP)

IF (IRR1) 350,400,350

350 CONTINUE

WRITE (NTAPE,6000) IRR1,IRR2,SCALE

REWIND NTAPE

STOP

400 CONTINUE

DO 450 J=1,NN

450 WRITE (NTAPE)(WM(I,J),I=1,NN)

END FILE NTAPE

REWIND NTAPE

CALL FSF(1,NTAPE,IRR)

DO 475 J=1,NN

475 READ (NTAPE)(WM(I,J),I=1,NN)

CALL FSF(2,NTAPE,IRR)

C

INVERT DRAG MINIMIZATION MATRIX CONSTRAINED FOR CL AND CM

CALL SINVRT (WM,MDMEM,NN,IRR1,IRR2,SCALE,DET,NDETXP)

IF (IRR1) 350,500,350

500 CONTINUE

DO 550 J=1,NN

550 WRITE (NTAPE)(WM(I,J),I=1,NN)

END FILE NTAPE

REWIND NTAPE

6000 FORMAT(1H1,46HERROR IN INVERSION OF DRAG MINIMIZATION MATRIX

1,6HIRR1 =,13,5X,6HIRR2 =,13,5X,7HSCALE =,E12.6)

RETURN

END

78

81

82

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94

95

100

107

109

116

122

123

SUBROUTINE MEAN (X,Y,N)
DIMENSION X(1),Y(1)

C SUBROUTINE TO SMOOTH DATA

```

10 MC=1
20 M3=N-3
   DO 90 I=1,M3
   I=I
   A=(Y(I+2)-Y(I))/(X(I+2)-X(I))
   C=(Y(I+3)-Y(I+1))/(X(I+3)-X(I+1))
   B=Y(I)-A*X(I)
   D=Y(I+1)-C*X(I+1)
   IF (A-C) 40,30,4C
   IF (B-D) 80,90,80
   XINT=(B-D)/(C-A)
   IF (XINT-X(I)) 8C,50,50
   IF (XINT-X(I+2)) 60,60,80
   IF (XINT-X(I+1)) 80,70,70
   IF (XINT-X(I+3)) 90,90,80
   YF=A*X(I+1)+B
   Y(I+1)=(Y(I+1)+YF)/2.
   Y5=C*X(I+2)+D
   Y(I+2)=(Y(I+2)+Y5)/2.
   CONTINUE
   MC=MC+1
   IF (MC-5) 20,20,100
100 RETURN
   END

```

'1
'2
'3
'4
'5
'8

'6
'9
'7
'10

'11
'12
'13
'14
'15

```

1000      MERR = 0
1010      IF(NU-IJK)100,500,100
1020      LT = NUT(2)
1030      NU(3)=NU(3)-1
1040      IF(LT -LF, 0) -OR. (NU(3) -LE, 0)) GO TO 400
1050      WRITE (LT,200) M,NU(1),SR
1060      FORMAT( 6HERROR 16,6H, CODE 16,15H IN SUBROUTINE A6,
1070      1 28H DURING GEOMETRIC DEFINITION)

```

```

MERR = 0
IF(NU-10K)100,500,100
LT= NU(2)
100
NU(3)=NU(3)-1
IF(LT-.LF, 0) .OR. (IN
WRITE (LT,200) M,NU(1)
200
FORMAT( 6HOERR 16,6H
1 28H DURING GEOMETRIC
MERR=1
GO TO 500
400 MERR=-1
500 RETURN
END

```

```

MERR=1
GO TO 500
400 MERR=-1
500 RETURN
END

```



```

C CONTROL LINK
  DIMENSION DICT(7)
  COMMON DAT(2),LA,LB,LC,LD,LE,LF,LI,LO,
  1 NBODY,NWING,XMACH,SYM,KACE
  2 /LGOMD/LGDEF(3,6)
  LOGICAL LGDEF
  DATA DICT/6HDEFINE,6HDEFINE,5HPANEL,6HAERODY,6HAERODY,
  1 6HEND OF,6HEND OF/

C INITIALIZE
C CALL OPCAM1

C READ COMMAND CARD
C
C 100 IGO=INTURP(DICT,7,LI,LO)
C
C THE FOLLOWING THREE STATEMENTS CAN BE REMOVED IF THE TIME AND DATE
C OPPOSITE EACH COMMAND ARE NOT WANTED OR IF AN APPROPRIATE
C SUBROUTINE CLOK IS NOT AVAILABLE. OR ELSE A DUMMY SUBROUTINE CLOK
C WHICH RETURNS BLANKS FOR TIM AND DAYT CAN BE USED.
C CALL CLOK(TIM,DAYT)
C WRITE(LO,105)TIM,DAYT
C 105 FORMAT(1H+ 101X,4HTIME 2A7)

C IF (IGO)100,100,150
C 150 GO TO (200,200,300,400,400,500,500 ),IGO
C
C WHEN A NEW COMMAND IS NEEDED,
C INCREASE DIMENSION OF DICT BY 1
C ADD COMMAND TO DATA STATEMENT
C INCREASE 2ND ARGUMENT OF INTURP BY 1
C ADD THE NEW STATEMENT NO. TO THE GO TO AT 150
C ADD THE STATEMENT, FOLLOW WITH GO TO 100
C
C A WING AND/OR BODY ARE TO BE DEFINED
C 200 CALL GEOM(DAT,LI,LO,LO,LA)
C GO TO 100
C
C CALL PANEL LINK
C TRANSFORM BODY TO NEW COORD. SYSTEM, FLATTEN WING, INTERSECT BODY
C AND WING. THEN CALL PANEL LINK.
C 300 CALL TFLAT(DAT,LI,LO,LA,LB,LD,NBODY,NU)
C IF(NU)100,310,100
C NBODY WAS SET TO -1 BY TFLAT IF THIS IS A BODY-ONLY CASE.
C THEN WE DO NOT CALL THE PANEL LINK. NBODY = 0 OTHERWISE.
C 310 IF(NBODY+1)320,100,320
C IF TFLAT DETECTS AN ERROR, IT READS DATA CARDS UNTIL IT
C HITS AN END OF DATA CARD OR A DEFINE CARD.
C THEN THE INPUT TAPE IS BACKSPACED 1 RECORD.
C 320 CALL PANEL
C GO TO 100
C

```


OPCAM		08/19/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)	
	CALL AERODYNAMIC LINK		
C 400	CALL AERO		.15
	GO TO 100		.16
C	END OF OR END OF CARD WAS READ		.17
C 500	STOP		.18
	END		.19

```

C INITIALIZATION FOR OPCAM
C
C SUBROUTINE OPCAM I
C
C COMMON DAT(2),LA,LB,LC,LD,LE,LF,LI,LO,
C 1 NBODY,NWING,XMACH,SYM,KACE
C
C DIMENSION ICARD(14),ICODE(2)
C
C DATA ICODE/6HEND OF,6HEND OF/
C
C ASSIGN TAPE NUMBERS. TAPES 1-4 AND 7-9 ARE SCRATCH TAPES.
C LIN IS THE SYSTEM INPUT TAPE. DATA IS TRANSFERRED FROM LIN TO LI,
C AS SHOWN BELOW. LO IS THE SYSTEM OUTPUT TAPE.
C
C LA=1
C LB=2
C LC=3
C LD=4
C LIN=5
C LO=6
C LE=7
C LF=8
C LI=9
C
C CALL DATE(DAT,DAT(2))
C WRITE(LO,100)DAT
100 FORMAT(1H1 56X 2A6/69H PROGRAM FOR ANALYSIS AND DESIGN OF SUPERSON
C .IC WING-BODY COMBINATIONS/
C .28HODATA CARDS ARE LISTED BELOW//)
C
C READ DATA CARDS FROM TAPE LIN, WRITE THEM ON TAPE LO
C (AS PART OF JOB PRINTOUT), AND ALSO WRITE THEM ON TAPE LI
C WHICH WILL BE USED AS THE INPUT TAPE FOR REST OF JOB.
C REWIND LI
C DO 1000 I=1,10000
C READ (LIN,200) ICARD
200 FORMAT(13A6,A2)
C WRITE (LI,200) ICARD
C WRITE (LO,300) ICARD
300 FORMAT(1H 14A6)
C DO 400 J=1,2
C IF(ICARD-ICODE(J)) 400,2000,400
400 CONTINUE
1000 CONTINUE
C 2000 CONTINUE
C END FILE LI
C REWIND LI
C WRITE(LO,5000) I
5000 FORMAT(1H0 5X 10HA TOTAL OF 15,22H DATA CARDS WERE READ/1H1)
C
C RETURN
C END

```

```

C SUBROUTINE OPTIM3(X,Y,ZEE,A,B,K,L,M)
C
C INTERPOLATES BETWEEN GIVEN POINTS, CHOOSING AND INSERTING
C IN EACH INTERVAL THE NECESSARY AND SUFFICIENT NUMBER OF
C INTERMEDIATE POINTS TO MAKE THE MAXIMUM DISTANCE FROM CHORD
C TO ARC NO MORE THAN A GIVEN CONSTANT, Z. THE FUNCTION USED
C HAS A CONTINUOUS FIRST DERIVATIVE.
C
C DIMENSION X(4),Y(4),A(200),B(200),C(3,2),S(3)
C
C EPS=.002
C CALL DVCHK (K000FX)
C GO TO(1,1),K000FX
C 1 IF (ZEE) 2,2,3
C 2 Z=EPS*ABS(X(K+1)-X(K))
C GO TO 4
C 3 Z=ZEE
C 4 KEY=0
C MU=0
C NU=0
C IF (X(1)-X(4)) 12,5,10
C 5 M=0
C GO TO 100
C 10 MU=1
C DO 11 I=1,4
C 11 X(I)=X(1)
C 12 I=1
C J=2
C IF (K-2) 13,15,14
C 13 J=1
C GO TO 19
C 14 I=2
C GO TO 19
C 15 DO 18 N=1,3
C S(N)=(Y(N+1)-Y(N))/(X(N+1)-X(N))
C IF (N-2) 18,16,16
C 16 IF (ABS(S(N)-S(N-1))-EPS) 17,18,18
C 17 I=N-1
C J=N-1
C NU=1
C GO TO 19
C 18 CONTINUE
C 19 DO 20 N=1,J
C J1=N
C J2=N+1
C J3=N+2
C D=(Y(J2)-Y(J1))/(X(J2)-X(J1))
C C(3,N)=(Y(J3)-Y(J1))/(X(J3)-X(J1))-D/(X(J3)-X(J2))
C C(2,N)=D-C(3,N)*X(J2)+X(J1)
C C(1,N)=Y(J1)-X(J1)*C(2,N)-X(J1)**2*C(3,N)
C 20 DX=X(3)-X(2)
C D=0.0

```

OPTI0030
OPTI0040
OPTI0050
OPTI0060
OPTI0070
OPTI0080
OPTI0090
OPTI0100
OPTI0110
OPTI0120
OPTI0140
OPTI0150
OPTI0160
OPTI0170
OPTI0180
OPTI0190
OPTI0200
OPTI0210
OPTI0220
OPTI0230
OPTI0240
OPTI0250
OPTI0260
OPTI0270
OPTI0280
OPTI0290
OPTI0300
OPTI0310
OPTI0320
OPTI0330
OPTI0340
OPTI0350
OPTI0360
OPTI0370
OPTI0380
OPTI0390
OPTI0400
OPTI0410
OPTI0420
OPTI0430
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OPTI0560

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OPTIM3 09/14/65

EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
E=X(K)		OPT10570 .46
DO 85 I=1,200		OPT10580 .47
L=I		OPT10590 .48
E=E+D		OPT10600 .49
IF (E+.01*(X(K+1)-X(K))-X(K+1)) 40,35,35		OPT10610 .50
35 L=L-1		OPT10620 .51
GO TO 90		OPT10630 .52
40 A(L)=E		OPT10640 .53
IF (NU) 45,42,45		OPT10650 .54
42 P=AMIN1(AMAX1((X(3)-E)/DX,0.0),1.0)		OPT10660 .55
GO TO 50		OPT10670 .56
45 P=2-J		OPT10680 .57
50 Q=1.0-P		OPT10690 .58
F=P*(C(1,1)+E*(C(2,1)+E*(C(3,1)))+Q*(C(1,2)+E*(C(2,2)+E*(C(3,2))))		OPT10700 .59
B(L)=F		OPT10710 .60
G=P*(C(1,1)+2.0*E*(C(3,1))+Q*(C(2,2)+2.0*E*(C(3,2))))		OPT10720 .61
T=ATAN(G)		OPT10730 .62
W=Z*COS(T)		OPT10740 .63
H=2.0*(P*(C(3,1)+Q*(C(3,2))))		OPT10750 .64
60 R=ISQRT(1.0+G**2)**3/ABS(H)		OPT10760 .65
CALL DVCHK (K000FX)		OPT10770 .66
GO TO(80,65),K000FX		OPT10780 .67
65 IF (R-W) 70,70,75		OPT10790 .68
70 D=W		OPT10800 .69
GO TO 85		OPT10810 .70
75 V=ACOS(1.0-W/R)		OPT10820 .71
U=T+SIGN(V,H)		OPT10830 .72
D=2.828*CDOS(U)*SQRT(R*W)		OPT10840 .73
GO TO 85		OPT10850 .74
80 IF (KEY) 90,82,9C		OPT10860 .75
82 KEY=1		OPT10870 .76
D=.2*(X(K+1)-X(K))		OPT10880 .77
85 CONTINUE		OPT10890 .78
IF (E+D-X(K+1)) 88,90,90		OPT10900 .80
88 M=2		OPT10910 .81
GO TO 91		OPT10920 .82
90 M=1		OPT10930 .83
91 B(1)=Y(K)		OPT10940 .84
IF (NU) 92,100,92		OPT10950 .85
92 DO 95 I=1,4		OPT10960 .86
95 X(I)=X(I)		OPT10970 .87
DO 98 I=1,L		OPT10980 .89
98 A(I)=A(I)		OPT10990 .90
100 RETURN		OPT11000 .92
END		OPT11010 .93

SUBROUTINE OPTMW (NN,NTAPEX,A,B,CONSNT,CLBAR,XCPBAR,RFAREA,AREA,CL
1)

C OPTIMIZE WING ONLY CASE

DIMENSION A(1),B(1),AREA(1),CL(1)

NN=NN+1

B(NN)=CLBAR*RFAREA

C TEST IF PITCHING MOMENT CONSTRAINT

IF (CONSNT) 100,150,100

CONTINUE

NN=NN+2

B(NN)=XCPBAR*CLBAR*RFAREA

150 CONTINUE

DO 200 J=1,NW

CL(J)=0.

DO 350 J=1,NN

READ (NTAPEX) (A(I),I=1,NN)

IF (J-NW) 350,350,250

CONTINUE

DO 300 I=1,NW

CL(I)=CL(I)+A(I)*B(J)

300 CONTINUE

RETURN

END

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05/22/67

OPTMWB - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE OPTMWB (NM,NR,NTAPEX,NTAPEY,THICK,A,B,ALPHA,ABX,ALPHAX,
1 AREA,CONSNT,CLBAR,XCPBAR,RFAREA,CL)

C OPTIMIZE WING-BODY CASE

DIMENSION A(1),B(1),ALPHA(1),ALPHAX(1),AREA(1),CL(1)
DIMENSION ABX(1)

IF (THICK) 50,25,50

25 CONTINUE

DC 40 I=1,NB

40 B(I)=0.

GO TO 75

50 CONTINUE

DC 60 I=1,NB

60 B(I)=-ABX(I)

75 CONTINUE

DO 100 J=1,NM

100 ALPHA(J)=ALPHAX(J)

DO 150 J=1,NB

READ (NTAPEY) (A(I),I=1,NM)

DC 150 I=1,NM

150 ALPHA(I)=ALPHA(I)-A(I)*B(J)

DO 200 J=1,NM

200 B(J)=AREA(J)*ALPHA(J)

NN=NM+1

B(MN)=CLBAR*RFAREA

C TEST IF PITCHING MOMENT CONSTRAINT

IF (CONSNT) 275,325,275

275 CONTINUE

NN=NM+2

B(MN)=XCPBAR*CLBAR*RFAREA

325 CONTINUE

DO 350 J=1,NM

350 CL(J)=0.

DO 400 J=1,NM

READ (NTAPEX) (A(I),I=1,MN)

DC 400 I=1,NM

400 CL(I)=CL(I)+A(I)*B(J)

RETURN

END

32

72

OUTB 08/14/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

SUBROUTINE OUTB (NTAPEO,NBODY,NTHETA,NROWB,THETA,Z)

C BODY OUTPUT FORMAT

```

DIMENSION Z(1),THETA(1)
WRITE (NTAPEO,6005) (THETA(I),I=1,NTHETA)
WRITE (NTAPEO,6010)
DO 100 J=1,NROWB
  100 WRITE (NTAPEO,6015) (J,(Z(I),I=J,NBODY,NROWB))

6005 FORMAT(1H0,4X,11HTHETA(DEG.),F14.4,9F10.4,(F29.4,9F10.4))
6010 FORMAT(1H0,6X,7HROW NO.)
6015 FORMAT(1H ,110,F19.5,9F10.5,(F29.5,9F10.5))
RETURN
END

```

.1	.2	.3	.4	.5
.6	.7			
.8				
.9	.10	.11	.12	.13
.15				.14
.16				
.17				

08/16/65
INTERNAL FORMULA NUMBER(S)

OUTPTB

EXTERNAL FORMULA NUMBER - SOURCE STATEMENT

```

SUBROUTINE OUTPTB
COMMON DATE(2),NTAPE1,NO1,NTAPE2,ND2(3),NREAD,
1NWRITE,NBODY,NWING,XMACH,SYM,KACE
COMMON /COM1/ CODEB,KODEM,KODEWU,KODE1,KODEC,XPER,YPER,KOPTR,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPERI
2,NPLANE,NPLN1
COMMON /COM2/ NPLNB,NPLNW,JLEAD,JTRAIL,IMID,NPTS(16),X(16,90),Y(16
1,90),Z(16,90),XCEPT(21),XCEPTB(21),XCEPTW(16),YCEPTW(16
2),CODEBW(16),KPANEL(15,20),XCOR(16,21),YCOR(16,21),ZCOR(16,21),XIN
3T(15,20,2),YINT(15,20,2),ZINT(15,20,2),XCEN(15,20),YCE(15,20),ZCE
4N(15,20),XCON(15,20),YCON(15,20),ZCON(15,20),AREA(15,20),ARAT(15,2
50),THETA(15,20),ALPHA(15,20),CHORD(15,20)
DIMENSION C(3,6)
DIMENSION ND3(6108)
EQUIVALENCE (ND3,XCOR)

```

C SUBROUTINE TO OUTPUT BODY PANEL DATA

C DEFINE CONSTANTS

```

NBODY=0
KODEB=0
KODEI=0
NUMBER=0
NPART1=1
NPART2=2
NPART3=3
E=SYM
F=0.00001
REIND NTAPE2

```

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,2
,3
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,6
,7
,8
,9

C DO-LOOP TO SET SMALL NEGATIVE AND POSITIVE

```

C VALUES EQUAL TO ZERO
DO 20 I=1,6108
IF (ABS(ND3(I))-F) 10,10,20
10 ND3(I)=0.
20 CONTINUE

```

,10
,11
,12
,13

C WRITE PRINTOUT HEADINGS

```

WRITE (NWRITE,900)
WRITE (NWRITE,910)

```

,14
,15
,16
,17

C WRITE TAPE OUTPUT - NUMBER IS PANEL NUMBER

```

C NPART1,NPART2 AND NPART3 INDICATE 1-, 2- AND
C 3-PART PANELS XCOR,YCOR,ZCOR
C ARE PANEL CORNER POINT COORDINATES
50 DO 130 I=1,NPER1
DO 130 J=1,NPLN1
KGO=KPANEL(I,J)
GO TO (52,53,52,53),KGO

```

,18
,19
,20
,21
,22

C SETUP OUTPUT ARRAY

```

C(1,1)=XCOR(I,J+1)
C(2,1)=YCOR(I,J+1)

```

,23
,24
,25


```

C(3,1)=ZCOR(I,J+1)
C(1,2)=XCOR(I,J)
C(2,2)=YCOR(I,J)
C(3,2)=ZCOR(I,J)
C(1,3)=XINT(I,J,1)
C(2,3)=YINT(I,J,1)
C(3,3)=ZINT(I,J,1)
GO TO 55
53 C(1,1)=XCOR(I,J)
C(2,1)=YCOR(I,J)
C(3,1)=ZCOR(I,J)
C(1,2)=XINT(I,J,1)
C(2,2)=YINT(I,J,1)
C(3,2)=ZINT(I,J,1)
C(1,3)=XCOR(I,J+1)
C(2,3)=YCOR(I,J+1)
C(3,3)=ZCOR(I,J+1)
GO TO (57,57,58,58),KGO
55 C(1,4)=XCOR(I+1,J)
57 C(2,4)=YCOR(I+1,J)
C(3,4)=ZCOR(I+1,J)
C(1,5)=XINT(I,J,2)
C(2,5)=YINT(I,J,2)
C(3,5)=ZINT(I,J,2)
C(1,6)=XCOR(I+1,J+1)
C(2,6)=YCOR(I+1,J+1)
C(3,6)=ZCOR(I+1,J+1)
GO TO 60
58 C(1,4)=XINT(I,J,2)
C(2,4)=YINT(I,J,2)
C(3,4)=ZINT(I,J,2)
C(1,5)=XCOR(I+1,J+1)
C(2,5)=YCOR(I+1,J+1)
C(3,5)=ZCOR(I+1,J+1)
C(1,6)=XCOR(I+1,J)
C(2,6)=YCOR(I+1,J)
C(3,6)=ZCOR(I+1,J)
CHECK SUBPANELS AGAINST TOLERANCE
60 KTYPE=1
GO TO (63,64,63,64),KGO
63 JTEMP=J+1
GO TO 65
64 JTEMP=J
65 SC=SQRT((YCOR(I,JTEMP)-YINT(I,J,1))*2+(ZCOR(I,JTEMP)-
ZINT(I,J,1))*2)/(XCOR(I,J+1)-XCOR(I,J))
IF (ABS(SC)-E) 67,67,70
67 KTYPE=2
70 GO TO (73,73,74,74),KGO
73 JTEMP=J+1
GO TO 75
74 JTEMP=J
75 SC=SQRT((YCOR(I+1,JTEMP)-YINT(I,J,2))*2+(ZCOR(I+1,JTEMP)-
ZINT(I,J,2))*2)/(XCOR(I+1,J+1)-XCOR(I+1,J))

```

```

77 IF (ABS(SC)-E) 77,77,80
78 KTYPE=KTYPE+2
79 NUMBER=NUMBER+1
90 GO TO (90,100,110,120),KTYPE
WRITE (NWRITE,920) NUMBER,NPART3,
1((C(K,L),K=1,3),L=1,2),((C(K,L),K=1,3),L=1,3,2)

WRITE (NTAPE2) NUMBER,NPART3,
1((C(K,L),K=1,3),L=1,2),((C(K,L),K=1,3),L=1,3,2)

WRITE (NWRITE,930) ((C(K,L),K=1,3),L=2,4,2),
1((C(K,L),K=1,3),L=3,5,2)

WRITE (NTAPE2) ((C(K,L),K=1,3),L=2,4,2),
1((C(K,L),K=1,3),L=3,5,2)

WRITE (NWRITE,930) ((C(K,L),K=1,3),L=4,6,2),
1((C(K,L),K=1,3),L=5,6)

WRITE (NTAPE2) ((C(K,L),K=1,3),L=4,6,2),
1((C(K,L),K=1,3),L=5,6)

GO TO 130
100 WRITE (NWRITE,920) NUMBER,NPART2,
1((C(K,L),K=1,3),L=2,4,2),((C(K,L),K=1,3),L=3,5,2)

WRITE (NTAPE2) NUMBER,NPART2,
1((C(K,L),K=1,3),L=2,4,2),((C(K,L),K=1,3),L=3,5,2)

WRITE (NWRITE,930) ((C(K,L),K=1,3),L=4,6,2),
1((C(K,L),K=1,3),L=5,6)

WRITE (NTAPE2) ((C(K,L),K=1,3),L=4,6,2),
1((C(K,L),K=1,3),L=5,6)

GO TO 130
110 WRITE (NWRITE,920) NUMBER,NPART2,
1((C(K,L),K=1,3),L=1,2),((C(K,L),K=1,3),L=1,3,2)

WRITE (NTAPE2) NUMBER,NPART2,
1((C(K,L),K=1,3),L=1,2),((C(K,L),K=1,3),L=1,3,2)

```

INTERNAL FORMULA NUMBER(S)

256	257	258	259	260	261
262	263	264	265	266	267
268	269				

256 257 258 259 260 261
262 263 264 265 266 267
268 269

200	270	271	272	273	274	275
	276	277	278	279	280	281
	282	283				
	284					

270, 271, 272, 273, 274, 275
276, 277, 278, 279, 280, 281
282, 283, 284

284

205 .286 .287 .288 .289 .290

4674 0678 1674

300, 301, 302, 303, 304, 305

315, 316, 317, 318

319
320 321

322 , 323
324

322 324

327 328 329

626 1 626 1 126 1

330 .331 .332 .333 .334

335

336, 337, 338

339

OUTPTB
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
 08/16/65
 940 FORMAT (1H1,9X,49H8ODY PANEL CENTROID AND CONTROL POINT COORDINATE
 1S)
 950 FORMAT (1H0,5HPANEL,6X,2(1HX,8X,1HY,8X,1HZ,8X),5X,4HAREA,9X,
 16HTHETA-,3X,6HALPHA-/13X,3(1HC,8X),3(2HCP,7X),17X,6HINCLIN,3X,
 25HINCID//)
 960 FORMAT (1H ,1X,13,4X,6F9.5,5X,F9.5,5X,2F9.5)
 END
 , 340

09/14/65
 SUBROUTINE OUTPUTM
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

SUBROUTINE OUTPUTM
COMMON DATE(2),NTAPE1,ND1,NTAPE2,ND2(3),NREAD,
1NWRITE,NBODY,NMING,XMACH,SYM,KACE
COMMON /COM1/ KODEB,KODEW,KODEU,KODEI,KODEC,XPER,YPER,KOPTB,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPERI
2,NPLANE,NPLNI
COMMON /COM2/ IJ,NPTS(16),X(90,16),Y(90,16),Z(90,16),KPNT,VALUE(5),
1YCEPT(16),SLOPE,KPANEL(2,15),XCOR(16,16),YCOR(16,16),ZCOR(16,16),X
2INT(2,15),YINT(2,15),ZINT(2,15),XCEN(15,15),YCEN(15,15),ZCEN(15,15
3),XCEN(15,15),YCON(15,15),ZCON(15,15),AREA(15,15),ARAT(15,15),THEY
4A(15,15),ALPHA(15,15),CHORD(15,15),XFOIL(16,25,2),ZFOIL(16,25,2),X
5NUM(16,2),XTAB1(25),XTAB2(25),ZTAB2(25)
DIMENSION C(3,5)
DIMENSION ND3(3333)
EQUIVALENCE (ND3,XCOR)

```

C SUBROUTINE TO OUTPUT WING PANEL DATA

C DEFINE CONSTANTS

```

NMING=0
KODEW=0
NUMBER=0
NPART1=1
NPART2=2
E=SYM
F=0.00001
ZHT=ZCOR(1,1)

```

,1
 ,2
 ,3
 ,4
 ,5
 ,6
 ,7

C DO-LOOP TO SET SMALL NEGATIVE AND POSITIVE

```

C VALUES EQUAL TO ZERO
DO 20 I=1,3333
IF (ABS(ND3(I))-F) 10,10,20
ND3(I)=0.
20 CONTINUE

```

,8
 ,9
 ,10
 ,11

C WRITE PRINTOUT HEADINGS

```

WRITE (NWRITE,900)
WRITE (NWRITE,910)

```

,12 ,13
 ,14 ,15

```

C WRITE TAPE OUTPUT - NUMBER IS PANEL NUMBER
C NPART1,NPART2 INDICATE 1- AND 2-PART PANELS
C XCOR,YCOR AND ZCOR ARE PANEL CORNER POINT
C COORDINATES

```

C IF KSTART = 2, WRITE OUTPUT DATA FOR

```

C INTERSECTION REGION
C IF (KSTART-1) 150,40,21
21 DO 39 J=1,NPERI
I=1
NUMBER=NUMBER+1
KGO=KPANEL(1,J)
IF (KGO-1) 150,23,24

```

,16 ,17
 ,18
 ,19
 ,20
 ,21
 ,22

```

C
23  SETUP OUTPUT ARRAY
    C(1,1)=XCOR(I,J+1)
    C(2,1)=YCOR(I,J+1)
    C(3,1)=ZCOR(I,J+1)
    C(1,2)=XCOR(I,J)
    C(2,2)=YCOR(I,J)
    C(3,2)=ZCOR(I,J)
    C(1,3)=XINT(I,J)
    C(2,3)=YINT(I,J)
    C(3,3)=ZINT(I,J)
    GO TO 25
24  C(1,1)=XCOR(I,J)
    C(2,1)=YCOR(I,J)
    C(3,1)=ZCOR(I,J)
    C(1,2)=XINT(I,J)
    C(2,2)=YINT(I,J)
    C(3,2)=ZINT(I,J)
    C(1,3)=XCOR(I,J+1)
    C(2,3)=YCOR(I,J+1)
    C(3,3)=ZCOR(I,J+1)
    C(1,4)=XCOR(I+1,J)
    C(2,4)=YCOR(I+1,J)
    C(3,4)=ZCOR(I+1,J)
    C(1,5)=XCOR(I+1,J+1)
    C(2,5)=YCOR(I+1,J+1)
    C(3,5)=ZCOR(I+1,J+1)
    KTYPE=1
    GO TO (27,28),K60
25  C
27  CHECK SUBPANELS AGAINST TOLERANCE
    JTEMP=J+1
    KTEMP=J
    GO TO 30
28  JTEMP=J
    KTEMP=J+1
30  SC=(YCOR(I,JTEMP)-YINT(I,J))/(XCOR(I,J+1)-
    1XCOR(I,J))
    IF (ABS(SC)-E) 31,31,32
31  KTYPE=2
32  IF (YCOR(I+1,KTEMP)-YCOR(I,KTEMP)) 33,33,34
33  KTYPE=KTYPE+2
34  GO TO (36,37,38,140),KTYPE
36  WRITE INWRITE,920) NUMBER,NPART2,((C(K,L),K=1,3),
    1L=1,2),((C(K,L),K=1,3),L=1,3,2)
    WRITE (NTAPE2) NUMBER,NPART2,((C(K,L),K=1,3),
    1L=1,2),((C(K,L),K=1,3),L=1,3,2)
    WRITE (INWRITE,930) ((C(K,L),K=1,3),L=2,4,2),
    1((C(K,L),K=1,3),L=3,5,2)

```

09/14/65

OUTPTW	EXTERNAL FORMULA NUMBER	- SOURCE STATEMENT	- INTERNAL FORMULA NUMBER(S)
	WRITE (NTAPE2) ((C(K,L),K=1,3),L=2,4,2),		,106 ,107 ,108 ,109 ,110 ,111
	1((C(K,L),K=1,3),L=3,5,2)		,112 ,113 ,114 ,115 ,116 ,117
			,118 ,119
			,120
	GO TO 39		
37	WRITE (NWRITE,920) NUMBER,NPART1,((C(K,L),K=1,3),L=2,4,2),		,121 ,122 ,123 ,124 ,125 ,126
	1((C(K,L),K=1,3),L=3,5,2)		,127 ,128 ,129 ,130 ,131 ,132
			,133 ,134 ,135
	WRITE (NTAPE2) NUMBER,NPART1,((C(K,L),K=1,3),L=2,4,2),		,136 ,137 ,138 ,139 ,140 ,141
	1((C(K,L),K=1,3),L=3,5,2)		,142 ,143 ,144 ,145 ,146 ,147
			,148 ,149 ,150
			,151
	GO TO 39		
38	WRITE (NWRITE,920) NUMBER,NPART1,((C(K,L),K=1,3),		,152 ,153 ,154 ,155 ,156 ,157
	1L=1,2),((C(K,L),K=1,3),L=1,3,2)		,158 ,159 ,160 ,161 ,162 ,163
			,164 ,165 ,166
	WRITE (NTAPE2) NUMBER,NPART1,((C(K,L),K=1,3),		,167 ,168 ,169 ,170 ,171 ,172
	1L=1,2),((C(K,L),K=1,3),L=1,3,2)		,173 ,174 ,175 ,176 ,177 ,178
			,179 ,180 ,181
39	CONTINUE		
C	WRITE OUTPUT TAPE FOR MAIN WING REGION		,182 ,183
40	DO 50 I=KSTART,KEND		,184
	DO 50 J=1,NPER1		,185
	NUMBER=NUMBER+1		,186
	WRITE (NWRITE,920) NUMBER,NPART1,XCOR(I,J),YCOR(I,J),		
	1ZCOR(I,J),XCOR(I+1,J),ZCOR(I+1,J),XCOR(I+1,J+1),		
	2YCOR(I+1,J),ZCOR(I+1,J),XCOR(I+1,J+1),YCOR(I+1,J+1),ZCOR(I+1,J+1)		,187 ,188 ,189
50	WRITE (NTAPE2) NUMBER,NPART1,XCOR(I,J),YCOR(I,J),		
	1ZCOR(I,J),XCOR(I+1,J),YCOR(I+1,J),ZCOR(I+1,J),XCOR(I+1,J+1),		
	2YCOR(I+1,J),ZCOR(I+1,J),XCOR(I+1,J+1),YCOR(I+1,J+1),ZCOR(I+1,J+1)		
			,190 ,191 ,192 ,193 ,194
			,195
			,196
			,197
			,198
			,199
	I=NPLN1		
	GO TO 163,64),KGO		
C	IF KEND LESS THAN NPLN1 WRITE OUTPUT DATA		
C	FOR WING-TIP REGION OTHERWISE SKIP THIS		
C	SET OF INSTRUCTIONS		
	IF (KEND-NPLN1) 60,85,150		
60	DO 80 J=1,NPER1		
	NUMBER=NUMBER+1		
	KGO=KPNEL(2,J)		
	I=NPLN1		
	GO TO 163,64),KGO		
C	SETUP OUTPUT ARRAY		
63	C(1,2)=XINT(2,J)		,200
	C(2,2)=YINT(2,J)		,201
	C(3,2)=ZINT(2,J)		,202
	C(1,4)=XCOR(I+1,J+1)		,203
	C(2,4)=YCOR(I+1,J+1)		,204
	C(3,4)=ZCOR(I+1,J+1)		,205
	C(1,5)=XCOR(I+1,J)		,206
	C(2,5)=YCOR(I+1,J)		,207
			,208

OUTPTW 09/14/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

      WRITE (NTAPE2) NUMBER,NPART1,((C(K,L),K=1,3),
      1L=2,5,3),((C(K,L),K=1,3),L=4,5)
      ,317 ,318 ,319
      ,320 ,321 ,322 ,323 ,324 ,325
      ,326 ,327 ,328 ,329 ,330 ,331
      ,332 ,333 ,334
      ,335 ,336
      ,337

80 CONTINUE
85 NMING=NUMBER
   NUMBER=0

C WRITE PRINTOUT HEADINGS
  WRITE (NWRITE,940)
  WRITE (NWRITE,950)

C WRITE TAPE OUTPUT - XCEN AND YCEN ARE
C PANEL CENTROID COORDINATES XCON AND YCON
C ARE PANEL CONTROL POINT COORDINATES AREA
C IS PANEL AREA ZCEN AND ZCON ARE PANEL
C THICKNESS AND CAMBER ORDINATES THETA AND
C ALPHA ARE PANEL THICKNESS AND CAMBER SLOPES

C WRITE OUTPUT TAPE
  DO 100 I=1,NPLN1
  DO 100 J=1,NPERI
    NUMBER=NUMBER+1
    WRITE (NWRITE,960) NUMBER,XCEN(I,J),YCEN(I,J),
    1ZHT,XCON(I,J),YCON(I,J),ZHT,AREA(I,J),ZCEN(I,J),THETA(I,J),
    2ZCON(I,J),ALPHA(I,J)
  100 WRITE (NTAPE2) NUMBER,XCEN(I,J),YCEN(I,J),
    1ZHT,XCON(I,J),YCON(I,J),ZHT,AREA(I,J),THETA(I,J),ALPHA(I,J),
    2CHORD(I,J)
    ,341 ,342
    ,343
    ,344
    ,345
    ,346 ,347 ,348

C WRITE TAPE OUTPUT - NUMBER OF PANELS PER
C COLUMN AND FRACTION OF PANEL STREAMWISE
C CHORD FOR PANEL CONTROL LOCATION
  110 WRITE (NTAPE2) NPERI,XPER
    GO TO 150
  140 WRITE (NWRITE,970)
  150 RETURN
  900 FORMAT (1H1, 9X,35HWHING PANEL CORNER POINT COORDINATES/10X,
    18H1 AND 2 INDICATE WING PANEL LEADING-EDGE POINTS, 3 AND 4 INDICA
    2TE TRAILING-EDGE POINTS)
  910 FORMAT (1H0,5X,5HPANEL, 4(8X,1HX,8X,1HY,8X,1HZ)/
    15X,2HNO,2X,5HPARTS,6X,
    2 3(1H1,8X),3(1H2,8X),3(1H3,8X),3(1H4,8X1//)
  920 FORMAT (1H ,3X,13,3X,11,3X,12F9.5)
  930 FORMAT (1H ,13X,12F9.5)
  940 FORMAT (1H1, 9X,49HWHING PANEL CENTROID AND CONTROL POINT COORDINAT
    1ES)
    950 FORMAT (1H0,1X,5HPANEL,6X,2(1HX,8X,1HY,8X,1HZ,8X),5X,4HAREA,7X,
    11HZ,9X,6HALPHA-,2X,1HZ,10X,6HALPHA-/1X,3(1HC,8X),3(1HCP,7X),
    216X,215HTHICK,4X),2(6HCAMBER,4X)///)
  960 FORMAT (1H ,1X,13,4X,6F9.5,5X,F9.5,5X,4F9.5)
  970 FORMAT (1H1,33HERROR MESSAGE - SUBROUTINE OUTPTB/10X,54HINBOARD (O
    1R OUTBOARD) PANEL COLUMN HAS ZERO-AREA PANEL/10X,45HNON-CONSTANT N

```

349 ,350 ,351 ,352 ,353
354 ,355 ,356
357
358 ,359
360


```

64 C(3,5)=ZCOR(I+1,J)
   GO TO 65
   C(1,2)=XCOR(I+1,J)
   C(2,2)=YCOR(I+1,J)
   C(3,2)=ZCOR(I+1,J)
   C(1,4)=XINT(2,J)
   C(2,4)=YINT(2,J)
   C(3,4)=ZINT(2,J)
   C(1,5)=XCOR(I+1,J+1)
   C(2,5)=YCOR(I+1,J+1)
   C(3,5)=ZCOR(I+1,J+1)
   C(1,1)=XCOR(I,J)
   C(2,1)=YCOR(I,J)
   C(3,1)=ZCOR(I,J)
   C(1,3)=XCOR(I,J+1)
   C(2,3)=YCOR(I,J+1)
   C(3,3)=ZCOR(I,J+1)
   KTYPE=1
   GO TO (67,68),KGC

65 C(1,1)=XCOR(I,J)
   C(2,1)=YCOR(I,J)
   C(3,1)=ZCOR(I,J)
   C(1,3)=XCOR(I,J+1)
   C(2,3)=YCOR(I,J+1)
   C(3,3)=ZCOR(I,J+1)
   KTYPE=1
   GO TO (67,68),KGC

C CHECK SUBPANELS AGAINST TOLERANCE
67 JTEMP=J
   KTEMP=J+1
   GO TO 70
68 JTEMP=J+1
   KTEMP=J
   70 SC=(YCOR(I+1,JTEMP)-YINT(2,J))/(XCOR(I+1,J+1)-
     1*XCOR(I+1,J))
     IF (ABS(SC)-E) 73,73,74
73 KTYPE=2
   74 IF (YCOR(I+1,KTEMP)-YCOR(I,KTEMP)) 75,75,76
   75 KTYPE=KTYPE+2
   76 GO TO (77,78,79,140),KTYPE
   77 WRITE (NWRITE,920) NUMBER,NPART2,((C(K,L),K=1,3),L=1,4)
     WRITE (NTAPE2) NUMBER,NPART2,((C(K,L),K=1,3),L=1,4)
     WRITE (NWRITE,930) ((C(K,L),K=1,3),L=2,5,3),
       1((C(K,L),K=1,3),L=4,5)
     WRITE (NTAPE2) ((C(K,L),K=1,3),L=2,5,3),
       1((C(K,L),K=1,3),L=4,5)

78 GO TO 80
   WRITE (NWRITE,920) NUMBER,NPART1,((C(K,L),K=1,3),L=1,4)
   WRITE (NTAPE2) NUMBER,NPART1,((C(K,L),K=1,3),L=1,4)

   GO TO 80
79 WRITE (NWRITE,920) NUMBER,NPART1,((C(K,L),K=1,3),
   1L=2,5,3),((C(K,L),K=1,3),L=4,5)

```

OUTPUT
 09/14/65
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
 NUMBER OF PANELS FOR THAT COLUMN)
 END
 ,361

OUTW 08/14/65
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

SUBROUTINE OUTW (NTAPEO,NWING,NCOLW,NROWW,Z)

C WING DUPUT FORMAT

```

  DIMENSION Z(1)
  WRITE (NTAPEO,6005) (I,I=1,NCOLW)
  WRITE (NTAPEO,6010)
  DO 100 J=1,NROWW
    100 WRITE (NTAPEO,6015) (J,{Z(I),I=J,NWING,NROWW})

  6005 FORMAT(1H0,2X,16HSPANWISE STATION,18,9I10,(18X,18,9I10))
  6010 FORMAT(1H ,2X,17HCHORDWISE STATION)
  6015 FORMAT(1H ,110,F19.5,9F10.5,(F29.5,9F10.5))
  RETURN
  END

```

.1	.2	.3	.4	.5
.6	.7			
.8				
.9	.10	.11	.12	.13
.15				.14
.16				
.17				

PANEL	EXTERNAL	FORMULA NUMBER	-	SOURCE STATEMENT
1	1	1	-	1
2	2	2	-	2
3	3	3	-	3
4	4	4	-	4
5	5	5	-	5
6	6	6	-	6
7	7	7	-	7
8	8	8	-	8
9	9	9	-	9
10	10	10	-	10
11	11	11	-	11
12	12	12	-	12
13	13	13	-	13
14	14	14	-	14
15	15	15	-	15
16	16	16	-	16
17	17	17	-	17
18	18	18	-	18
19	19	19	-	19
20	20	20	-	20
21	21	21	-	21
22	22	22	-	22
23	23	23	-	23
24	24	24	-	24
25	25	25	-	25
26	26	26	-	26
27	27	27	-	27
28	28	28	-	28
29	29	29	-	29
30	30	30	-	30
31	31	31	-	31
32	32	32	-	32
33	33	33	-	33
34	34	34	-	34
35	35	35	-	35
36	36	36	-	36
37	37	37	-	37
38	38	38	-	38
39	39	39	-	39
40	40	40	-	40
41	41	41	-	41
42	42	42	-	42
43	43	43	-	43
44	44	44	-	44
45	45	45	-	45
46	46	46	-	46
47	47	47	-	47
48	48	48	-	48
49	49	49	-	49
50	50	50	-	50
51	51	51	-	51
52	52	52	-	52
53	53	53	-	53
54	54	54	-	54
55	55	55	-	55
56	56	56	-	56
57	57	57	-	57
58	58	58	-	58
59	59	59	-	59
60	60	60	-	60
61	61	61	-	61
62	62	62	-	62
63	63	63	-	63
64	64	64	-	64
65	65	65	-	65
66	66	66	-	66
67	67	67	-	67
68	68	68	-	68
69	69	69	-	69
70	70	70	-	70
71	71	71	-	71
72	72	72	-	72
73	73	73	-	73
74	74	74	-	74
75	75	75	-	75
76	76	76	-	76
77	77	77	-	77
78	78	78	-	78
79	79	79	-	79
80	80	80	-	80
81	81	81	-	81
82	82	82	-	82
83	83	83	-	83
84	84	84	-	84
85	85	85	-	85
86	86	86	-	86
87	87	87	-	87
88	88	88	-	88
89	89	89	-	89
90	90	90	-	90
91	91			

```

SUBROUTINE PANEL
COMMON DATE(2),NTAPE1,NL1,NTAPE2,ND2(3),NREAD,
NWRITE,NBODY,NWING,XMAC,H,SYM,KACE
COMMON /COM1/ KODEB,KODEW,KODEWU,KODEI,KODEC,XPER,YPER,KOPTB,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,XINT,XI(16),YI(16),ZI(16),NPER,NPER1
2,NPLANE,NPLN1

```

```
COMMON /COM2/ ND3(11000)
DIMENSION TABLE(3)
```

```
COMMON /COM2/ ND3(11000)
DIMENSION TABLE(3)
```

C CONTROL PROGRAM FOR PANELING SUBROUTINES
DATA TABLE /IO4BODY PANEL, IOHWING PANEL, 6-HPANEND/

```

C      DEFINE TAPE UNITS AND CONSTANTS
C      ND1, ND4 ARE INPUT SCRATCH TAPES
C      OUTPUT SCRATCH TAPE
C      ND4=ND2(1)
C      NTAP=2 IS

```

1
2
3
4
5
6

4, 5, 6

C READ CARD INPUT - X- AND Y-PERCENT VALUES FOR
BODY AND WING PANEL CONTROL POINT LOCATION
C READ (NREAD,890) XPER,YPER

7

```

C      DEFINE KODEC      IF KODEC = 0, Y-PRIME FOR
C      CONTROL POINT TO BE SAME AS THAT FOR CENTROID
      KODEC=1
      IF (YPER) 150,5,10
5      KODEC=0
10     N=3
10

```

11
12
13

11
12
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510

```

C      READ CARD INPUT FOR CONTROL CARD
15      KCODE=INTURP(TABLE,N,NREAD,NWRITE)
      IF (KCODE) 15,15,20

```

14
15

```

C      CALL SURROUTINES
20    GO TO (50,100,140),KCODE
50
    CALL BODY
    IF (KODEB) 150,55,150
55    IF (KODEI) 150,15,150
100   CALL WING
    IF (KODEW) 150,15,150
140   WRITE (NWRITE,930)
150   REMIND NTAPEZ
      RETURN
890   FORMAT (6F10.0)
930   FORMAT (1H1)
      END

```

CALL SUB	IF (KODEB)	150,55,150
55	IF (KODEI)	150,15,150

```

100 CALL WING
      IF (KODEW) 150,15,150
140 WRITE (NWRITE,930)

```

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```

890 FORMAT (6F10.0)
930 FORMAT (1H1)
      END

```

27

05/22/67

PARTV - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE PARTV

C PARTITION VELOCITY COMPONENTS MATRIX

COMMON DATE(2),NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI
1,NTAPEO,NBODY,NWING,XHACH,SYM,KACE

DIMENSION U(110),V(110),W(110),UU(110),VV(110),WW(110)

CALL FSF(1,NTAPEA,IRR)
CALL FSF(1,NTAPEB,IPR)
DO 100 J=1,NBODY
READ (NTAPEB) (U(I),V(I),W(I),I=1,NBODY),(UU(I),VV(I),WW(I),I=1,
NWING)

WRITE (NTAPEO) (U(I),V(I),W(I),I=1,NBODY)
WRITE (NTAPEA) (UU(I),VV(I),WW(I),I=1,NWING)

100 CONTINUE
END FILE NTAPED
REWIND NTAPEA

CALL FSF(1,NTAPEA,IRR)
DO 200 J=1,NBODY
READ (NTAPEA) (UU(I),VV(I),WW(I),I=1,NWING)
WRITE (NTAPEO) (UU(I),VV(I),WW(I),I=1,NWING)

200 CONTINUE
END FILE NTAPED
REWIND NTAPEA

CALL FSF(1,NTAPEA,IRR)
DO 300 J=1,NWING
READ (NTAPEB) (U(I),V(I),W(I),I=1,NBODY),(UU(I),VV(I),WW(I),I=1,NW
ING)

WRITE (NTAPEO) (U(I),V(I),W(I),I=1,NBODY)
WRITE (NTAPEA) (UU(I),VV(I),WW(I),I=1,NWING)

300 CONTINUE
REWIND NTAPEA
REWIND NTAPB
END FILE NTAPED

CALL FSF(1,NTAPEA,IRR)
DO 400 J=1,NWING
READ (NTAPEA) (UU(I),VV(I),WW(I),I=1,NWING)
WRITE (NTAPEO) (UU(I),VV(I),WW(I),I=1,NWING)

400 CONTINUE
END FILE NTAPED
REWIND NTAPEA
REWIND NTAPED

RETURN
END

2
4
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POLYN
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
07/31/65

2000 L=-1

C

9000 RETURN

END

,36
,37
,38

CRAT
07/31/65
INTERNAL FORMULA NUMBER(S)

EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

SUBROUTINE QRAT(X,Y,IXY,KODE,XI,YI,C,NU)
  DIMENSION X(1),Y(1),C(3)
  C
  C FIND COEFFICIENTS OF QUADRATIC THRU 3 POINTS.
  C 1ST PT IS IX,Y), 2ND PT IS (X(1XY+1),Y(1XY+1)),
  C 3RD PT IS(X(2*IXY+1),Y(2*IXY+1))
  C IF KODE .GT. 0, EVALUATE AT X=XI
  C
  C USING 32769 INSTEAD OF 1, ALLOWS IXY TO BE NEGATIVE.
  JXY=IXY+32769
  KXY=IXY+JXY
  DX21=X(JXY)-X
  DY21=Y(JXY)-Y
  DX32=X(KXY)-X(JXY)
  DY32=Y(KXY)-Y(JXY)
  DX31=X(KXY)-X
  DY31=Y(KXY)-Y
  SX31=X(KXY)+X
  C
  C 100 IF (DX21*DX32+DX31)*300,200,300
  C 200 NU=1
  C 300 GO TO 1000
  C
  C(3)=(DY32/DX32-DY21/DX21)/DX31
  C(2)=DY31/DX31-C(3)*SX31
  C(1)=Y(JXY)-(C(2)+C(3)*X(JXY))*X(JXY)
  NU=0
  C
  C 400 IF (KODE)1000,1000,500
  C 500 VI=C(1)+(C(2)+C(3)*XI)*XI
  C 1000 RETURN
  C END

```

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05/22/67

READ - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE READ (NTAPEI,NTAPEO,NTAPEC,NM,S)
DIMENSION S(1),DICT(2)

C CONTROLS DATA READ IN OPTION FOR SPECIFYING WING CAMBER AND
C PRESSURE DISTRIBUTION, ALSO BODY CAMBER

DATA DICT/6PCONSTA,5P-GIVEN/

IGO=INTURP(DICT,2,NTAPEI,NTAPEO)

IGO= IGO+1

GO TO (50,60,70),IGO

CONTINUE

50 READ (NTAPEI,5000) (S(I),I=1,NM)

GO TO 999

CONTINUE

60 READ (NTAPEI,5000) SCONST

DC 65 I=1,NM

S(I)=SCONST

GO TO 999

CONTINUE

70 READ (NTAPEC) (S(I),I=1,NM)

5000 FORMAT(7F10.0)

999 CONTINUE

RETURN

END

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05/22/67

REDUCE - EFN SOURCE STATEMENT - IFN(S) -

SURROUTINE REDUCE

C REDUCE AERODYNAMIC INFLUENCE COEFFICIENTS MATRIX AND FORM THE
C (D) AND (E) MATRICES

COMMON DATE(2),NTAPEA,NTAPES,NTAPEE,NTAPEE,NTAPEE,NTAPEE
1,NTAPE1,NTAPE2,NBODY,NWING,XMACH,SYM,KACE
DIMENSION AB(100),ABB(100,100),ABW(100,25),AMB(110,100),AWW(110,25)
1),E(100,25),D(110),NSIZE(5)
EQUIVALENCE (ABB,AWR)

C COMPUTE SIZE OF PARTIONS
MAXP=25
CALL SIZE (NWING,MAXP,NPART,NSIZE)

DC 100 J=1,NBODY
100 READ (NTAPE2) (AWB(I,J),I=1,NWING)
CALL FSF(1,NTAPE2,IRR)

C FORM (D) MATRIX
DO 300 K=1,NBODY
READ (NTAPE2) (AB(I),I=1,NBODY)
DC 250 I=1,NWING
D(I)=0.0
DO 250 J=1,NBODY
D(I)=D(I)+AB(I,J)*AB(J)
250 CONTINUE
WRITE (NTAPE2) (D(I),I=1,NWING)
300 CONTINUE
END FILE NTAPEF

REWIND NTAPE2
CALL FSF(1,NTAPE2,IRR)
DC 325 J=1,NBODY
325 READ (NTAPE2) (ABB(I,J),I=1,NBODY)

C COPY INVERSE BODY MATRIX
DO 350 J=1,NBODY
350 WRITE (NTAPEF) (ABB(I,J),I=1,NBODY)

C MATRIX REDUCTION
DO 600 L=1,NPART
NS=NSIZE(L)
IF (L.EQ. 1) GO TO 370
DC 360 J=1,NBODY
360 READ (NTAPE2) (ABB(I,J),I=1,NBODY)
370 REWIND NTAPE2
DC 380 K=1,NS
380 READ (NTAPEA)(ABW(I,K),I=1,NBODY), (AWW(I,K),I=1,NWING)

C FORM (E) MATRIX
DO 400 K=1,NS
DO 400 M=1,NBODY

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05/22/67

REDUCE - EFN SOURCE STATEMENT - IFN(S) -

```

F(M,K)=0.
DC 400 N=1,NBODY
E(M,K)=E(M,K)-ABB(M,N)*ABW(N,K)
400 CONTINUE
DC 450 J=1,NBODY
450 READ (NTAPE)(AWB(I,J),I=1,NWING)
CALL FSI1,NTAPE,IRR)
DO 500 K=1,NS
DC 500 I=1,NWING
DC 500 M=1,NBODY
AWW(I,K)=AWW(I,K)+AWB(I,M)*E(M,K)
500 CONTINUE
DC 550 K=1,NS
550 WRITE (NTAPEF)(E(I,K),I=1,NBODY)
DO 560 K=1,NS
560 WRITE (NTAPEF)(AWW(I,K),I=1,NWING)
600 CONTINUE
REWIND NTAPEA
REWIND NTAPE
REWIND NTAPEE
END FILE NTAPEF
REWIND NTAPEF
RETURN
END

```

113
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08/16/65

```

SUBROUTINE RICH3A(NP,P,Q,KD,MAX,CHD,NA,A,NU)
DIMENSION P(3),Q(3),A(3),NU(3),T(12),U(3),V(3)
P = ARRAY OF NP POINTS, STORED (X1,Y1,Z1,X2,Y2,Z2,...)
Q = SCRATCH ARRAY OF LENGTH 3*NP. IT MAY BE THE SAME ARRAY
  AS P IF OK TO DESTROY P.

```

```

RICH3A PERFORMS A 3D INTERPOLATION TO PRODUCE ARRAY A
WHICH CONTAINS P WITH INTERSPERSED POINTS.

```

```

NA = NO OF POINTS IN A.
MAX = DIMENSION OF A.
KD = 0 IF ENRICHING IS DONE IN PLANE THRU 1ST PT, LAST PT,
  AND PT FARTHEST FROM LINE THRU END PTS.
KD = 1 OR 2 IF IN PLANE THRU END PTS WHICH IS NORMAL TO
  XY PLANE
KD = 1 IF PROJECTION OF A ON XY PLANE IS TO BE STRAIGHT LINES
  BETWEEN POINTS OF P (WHEN PROJECTED TO XY PLANE).
KD = 2 OTHERWISE.
CHD = CHORD HEIGHT TOLERANCE (SEE ENRYCH)

```

```

INPUTS ARE NP,P,KD,MAX,CHD,NU(2),NU(3)
OUTPUTS ARE Q,NA,A,NU(1),NU(3)

```

```

MU=0
NA=0
NP2=NP+NP
NP3=NP2+NP
MAXR=MAX-NP2

```

```

IF(NP .LE. 3 -OR. CHD .LE. 0.) GO TO 7000
IF(KD)30,30,90
FIND ROTATION MATRIX TO SYSTEM WHICH HAS ORIGIN AT 1ST PT,
  +X AXIS PASSING THRU LAST PT, Z AXIS IN PLANE DESCRIBED FOR KD=0

```

```

FIND THE POINT STARTING IN P(3*JP-2) WHICH IS FARTHEST FROM
  THE LINE THRU END PTS, AND ITS DISTANCE = DIST.

```

```

CALL DMAXL(P,NP,DIST,JP,U,NU)
U IS UNIT VECTOR FROM 1ST PT TO LAST PT.

```

```

IF(NU)9000,40,9000
IF(DIST-CHD)7000,7000,50
D=UVECN(P,P(3*JP-2),V,0,3)
I=1
NU=21

```

```

CALL VCROSS(V,U,T(4),D,I)
IF(I)9000,60,9000
T(4)=V CROSS U IS UNIT VECTOR ALONG NEW Y AXIS
I=1

```

```

CALL VCROSS(U,T(4),T(7),D,I)
CALL TRAV(T,U,3)
ROTATION MATRIX NOW FORMED.
T(12)=P(3)
GO TO 130

```

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 ,3
 ,4

 ,5
 ,6 ,7 ,9

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 ,10
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 ,15
 ,16

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 ,18
 ,19

 ,20
 ,21

EXTERNAL FORMULA NUMBER - SOURCE STATEMENT

```

C
C KD=1 OR 2
C T = TRANSFORMATION MATRIX (SEE TROTPT).
C 90 DO 100 I=1,12
C 100 T(I)=0.
C
C T(1)=P(NP3-2)-P(1)
C T(2)=P(NP3-1)-P(2)
C D=SQRT(T**2+T(2)**2)
C IF (D)110,110,120
C 110 NU=7
C GO TO 9000
C
C 120 T(1)=T(1)/D
C T(2)=T(2)/D
C T(9)=1.
C T(4)=-T(2)
C T(5)=T(1)
C
C 130 T(10)=P(1)
C T(11)=P(2)
C T(12)=T(10),T(11),T(12), NOW FORMED
C
C TRANSLATION MATRIX, IN T(10),T(11),T(12), NOW FORMED
C
C TRANSFORM POINTS IN P TO Q
C JX=-2
C DO 200 I=1,NP
C JX=JX+3
C 200 CALL TROTPT(T,T(10),2,P(JX),Q(JX))
C
C 400 IF (MAXR)400,400,500
C NU=1
C GO TO 9000
C
C 500 IA=MAXR
C IB=IA+NP
C IQ=IA+1
C IYQ=IB+1
C DO 600 I1=3,NP3,3
C IA=IA+1
C IB=IB+1
C A(IA)=Q(I1-2)
C A(IB)=Q(I1)
C
C 600 NO=MAXR
C CALL ENRYCHI(IYQ),A(IYQ),NP,CHD,A,NO,NU)
C IF (NU)800,1000,800
C 800 IF (NU-3)9000,900,9000
C 900 NU=-1
C 1000 NA=NO/2
C IF (MAX-NO-NA)1100,1200,1200
C 1100 NU=6
C GO TO 9000
C
C 1200 IA=NO

```

EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
DO 1300 I=1,NO		,67
I8=IA+IA/2		,68
A(I8)=A(IA)		,69
1300 IA=IA-1		,70 ,71
C		,72
1500 DO 1700 I=1,NA		,73
IA=IA+3		,74
CALL BITURP(Q,Q(2),3,NP,KS,A(IA),A(IA+1),NU)		,75
IF (NU)1600,1700,1600		,76
1600 NU=NU+10		,77
GO TO 9000		,78
1700 CALL TROTPT(T,T(10),1,A(IA),A(IA))		,79 ,80
GO TO 8000		
C		
NO INTERPOLATION BECAUSE NP .LT. 4 OR CHD .LE. 0 OR PTS. COLLINEAR		,81
7000 NA=NP		,82
CALL TRAV(A,P,NP3)		,83
C		
8000 NU=MU		,84
C		
9000 RETURN		,85
END		,86

C GIVEN M ARRAYS OF 3D POINTS, WHERE EACH ARRAY HAS N POINTS, STORED
C IN A SINGLE ARRAY A OF LENGTH MAX.
C USE RICH3A ON EACH ARRAY SO THAT EACH ARRAY WILL CONTAIN MORE
C POINTS. UPON RETURN, THE DENSE ARRAYS WILL BE STORED IN A,
C HEADED BY A TABLE OF CONTENTS. THE ORIGINAL ARRAYS
C ARE DESTROYED.

NA=0	14
MN=MN	15
IA=MIX-MN	16
IAI=IA+1	17
MAXR=IA-M	18
IDA=M+1	19
IF(KOD)100,100,20	10

C	MOVE ARRAY TO BOTTOM OF A.	
C	DO 200 J=1,MN	,11
	IA=I+1	,12
150	DO 200 I=1,3	,13
	A(I,IA)=A(I,J)	,14
200		
C	DO 1000 IR=1,M	,15
300		,16
		,17
		,18

C CHECK FOR POINTS WHICH HAVE X,Y NEARLY SAME AS PREV. POINT AND
C Z DIFFERENT. WRITE COMMENT IF ANY FOUND. THESE POINTS WILL BE
C REMOVED LATER BY NWEED, BUT USER SHOULD KNOW ABOUT IT.

```

      LL=IAI*N-1
      DO 350 L=LF,LL
      DO 320 I=1,2
      IF (ABS(A(I,L)-A(I,L-1))-EPS)320,350,350
320 CONTINUE
      ,23
      ,24
      ,25
      ,26
      ,27
      ,28

```

```

330 IF (ABS(D(3,L)-A(3,L-1))-EPS)350,330
      LM=L-1
      WRITE (LTAPE,340)B,((A(I,J),I=1,3),J=L,M,L)
331
332
      29
      30
      31
      32

```

350 CONTINUE

	REMOVE POINTS TOO CLOSE TO PRECEDING POINT	
360	NS=NS+50(A(I,1A1),N,3,EP)	.40
C	IF (NS-11400,400,500	.42
		.41

RICHNA		07/31/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	-	INTERNAL FORMULA NUMBER(S)
C	ALL POINTS MUST BE COINCIDENT (WITHIN EP)		
400	NU=-1		,43
	GO TO 9000		,44
C			
500	CALL RICH3A(NS,A(1,IAI),A(1,IAI),KOD,3*MAXR,CHD,ND,A(1,IDA),NU)		,45
	IF (NU)9000,600,9000		,46
C	MAKE ENTRIES IN TABLE OF CONTENTS		
600	A(1,IB)=P(IB)		,47
	A(2,IB)=ND		,48
	A(3,IB)=(IDA-1)*3+1		,49
C			
	IAI=IAI+N		,50
	IDA=ICA+ND		,51
	MAXR=MAXR+N-ND		,52
	NA=NA+ND		,53
C			
1000	CONTINUE		,54
C			
9000	RETURN		,55 ,56
	END		,57 ,58

05/22/67

RITE - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE RITE (NFMT,NTAPEO,NP,NROW,NCOL,THETA,U,V,W)

C PRINT OUT VELOCITY COMPONENTS

DIMENSION NFMT(1),U(1),V(1),W(1)

IF (NFMT(1)) 5,999,5

5 CONTINUE

IGC=NFMT(1)

GO TO (10,20,30,40,50,60,70,300,200),IGC

10 WRITE (NTAPEO,6030)

GO TO 200

20 WRITE (NTAPEO,6040)

GO TO 200

30 WRITE (NTAPEO,6045)

GO TO 200

40 WRITE (NTAPEO,6050)

GO TO 300

50 WRITE (NTAPEO,6055)

GO TO 300

60 WRITE (NTAPEO,6060)

GO TO 300

70 WRITE (NTAPEO,6065)

GO TO 300

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C PRINT OUT VELOCITY COMPONENTS AT BODY PANELS

200 CONTINUE

WRITE (NTAPEO,6010)

CALL OUTB (NTAPEO,NP,NCOL,NROW,THETA,U)

WRITE (NTAPEO,6015)

CALL OUTB (NTAPEO,NP,NCOL,NROW,THETA,V)

WRITE (NTAPEO,6020)

CALL OUTB (NTAPEO,NP,NCOL,NROW,THETA,W)

GO TO 999

C PRINT OUT VELOCITY COMPONENTS AT WING PANELS

300 CONTINUE

WRITE (NTAPEO,6010)

CALL OUTW (NTAPEO,NP,NCOL,NROW,U)

WRITE (NTAPEO,6015)

CALL OUTW (NTAPEO,NP,NCOL,NROW,V)

WRITE (NTAPEO,6020)

CALL OUTW (NTAPEO,NP,NCOL,NROW,W)

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```

6000 FORMAT(1P,10F11.5)
6010 FORMAT(1H0,5X,8HAXIAL(U))
6015 FORMAT(1H0,5X,13HTRANSVERSE(V))
6020 FORMAT(1H0,5X,11HVERTICAL(W))
6030 FORMAT(1H1,76H VELOCITY COMPONENTS ON BODY PANELS DUE TO BODY PAN
      1EL PRESSURE SINGULARITIES)
6040 FORMAT(1H1,76H VELOCITY COMPONENTS ON BODY PANELS DUE TO WING PAN
      1EL PRESSURE SINGULARITIES)
6045 FORMAT(1H1,55H VELOCITY COMPONENTS ON BODY PANELS DUE TO WING SOU
      1RCES)
6050 FORMAT(1H1,76H VELOCITY COMPONENTS ON WING PANELS DUE TO WING PAN
      1EL PRESSURE SINGULARITIES)
6055 FORMAT(1H1,55H VELOCITY COMPONENTS ON WING PANELS DUE TO WING SOU
      1RCES)
6060 FORMAT(1H1,76H VELOCITY COMPONENTS ON WING PANELS DUE TO BODY PAN
      1EL PRESSURE SINGULARITIES)
6065 FORMAT(1H1,73H VELOCITY COMPONENTS ON WING PANELS DUE TO BODY LIN
      1E SOURCES AND DOUBLETS)

999 CONTINUE
      RETURN
      END

```

RRAT - EFN SOURCE STATEMENT - IFN(S) -

```

SUBROUTINE RRAT(X,Y,IXY,KODE,XI,YI,C,NU)
DIMENSION X(1),Y(1),C(3)

C
C FIND COEFFICIENTS OF QUADRATIC THRU 3 POINTS.
C 1ST PT IS (X,Y), 2ND PT IS (X(IXY+1),Y(IXY+1)),
C 3RD PT IS (X(2+IXY+1),Y(2+IXY+1))
C IF KODE .GT. 0, EVALUATE AT X=XI
C
C JXY=IXY+32769
C KXY=IXY+JXY
C DX21=X(JXY)-X
C DY21=Y(JXY)-Y
C DX32=X(KXY)-X(JXY)
C DY32=Y(KXY)-Y(JXY)
C DX31=X(KXY)-X
C DY31=Y(KXY)-Y
C SX31=X(KXY)+X

C 100 IF (DX21+DX32+DX31)/300,200,300
C 200 NU=1
C GO TO 1000

C 300 C(3)=(DY32/DX32-DY21/DX21)/DX31
C C(2)=DY31/DX31-C(3)*SX31
C C(1)=Y(JXY)-(C(2)+C(3)*X(JXY))*X(JXY)
C NU=0

C 400 IF (KODE)1000,1000,500
C 500 YI=C(1)+(C(2)+C(3)*XI)*XI
C 1000 RETURN
C END

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05/22/67

SAVTAP - EFN SOURCE STATEMENT - IFN(S) -

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SURROUTINE SAVTAP(IISAVET)
COMMON DATE(2),NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI
1,NTAPEO,NBODY,NWING,XMACH,SYM,KACE
DIMENSION A(210),B(210),C(210)
DIMENSION DUM(10),NROW(2)
IF (IISAVET) 20,20,10
10 READ (NTAPEI,NBODY,NWING,XMACH,SYM,KACE
GO TO ( 50, 20, 50),KACE
20 CALL FSF(6,NTAPEC,IRR)
GO TO 900
50 NPANEL=NBODY+NWING
READ (NTAPEC) (I,(DUM(J),J=1,10),I=1,NPANEL),NRG,
1(NROW(I),I=1,NRG),DUMMY
NCOLM=NWING/NROW(NRG)
CALL FSF( 6,NTAPEC,IRR)
GO TO (100,900,200),KACE
100 CONTINUE
CALL TTAPE (0,NWING,NWING+NCOLM,NTAPEA,NTAPEB,A,B,C)
CALL FSF(1,NTAPEA,IRR)
CALL TTAPE(0,NWING,NWING,NTAPEA,NTAPEB,A,B,C)
CALL FSF(1,NTAPEA,IRR)
CALL TTAPE(0,NWING+1,NWING+1,NTAPEA,NTAPEB,A,B,C)
CALL FSF(1,NTAPEA,IRR)
CALL TTAPE(0,NWING+2,NWING+2,NTAPEA,NTAPEB,A,B,C)
REWIND NTAPEA
CALL TTAPE(1,NWING,NWING+NCOLM,NTAPEB,NTAPEC,A,B,C)
CALL FSF(1,NTAPEB,IRR)
CALL TTAPE(1,NWING,NWING,NTAPEB,NTAPEC,A,B,C)
REWIND NTAPEB
CALL TTAPE(0,NWING,NWING,NTAPEE,NTAPEF,A,B,C)
CALL FSF(1,NTAPEE,IRR)
CALL TTAPE(0,NWING,NWING,NTAPEE,NTAPEF,A,B,C)
REWIND NTAPEE
GO TO 900
200 CONTINUE
CALL TTAPE(0,NPANEL,NWING +NCOLM,NTAPEA,NTAPEB,A,B,C)
CALL FSF(1,NTAPEA,IRR)
CALL TTAPE(0,NWING,NWING,NTAPEA,NTAPEB,A,B,C)
CALL FSF(1,NTAPEA,IRR)
CALL TTAPE(0,NWING+1,NWING+1,NTAPEA,NTAPEB,A,B,C)
CALL FSF(1,NTAPEA,IRR)
CALL TTAPE(0,NWING+2,NWING+2,NTAPEA,NTAPEB,A,B,C)
REWIND NTAPEA
CALL TTAPE(1,NPANEL,NWING +NCOLM,NTAPEB,NTAPEC,A,B,C)
REWIND NTAPEB
CALL TTAPE(1,NBODY,NBODY,NTAPED,NTAPEE,A,B,C)
CALL FSF(1,NTAPED,IRR)
CALL TTAPE(1,NWING,NBODY,NTAPED,NTAPEE,A,B,C)
CALL FSF(1,NTAPED,IRR)
CALL TTAPE(1,NBODY,NWING,NTAPED,NTAPEE,A,B,C)
CALL FSF(1,NTAPED,IRR)
CALL TTAPE(1,NWING,NWING,NTAPED,NTAPEE,A,B,C)
REWIND NTAPEE

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CALL TTAPE(O,NWING,NWING,NTAPE,NTAPE,A,B,C)
CALL FSFI,NTAPE,IRR)
CALL TTAPE(O,NWING,NWING,NTAPE,NTAPE,A,B,C)
REWIND NTAPE
CALL TTAPE(O,NWING,NBODY,NTAPE,NTAPE,A,B,C)
CALL FSFI,NTAPE,IRR)
CALL TTAPE(O,NBODY,NBODY,NTAPE,NTAPE,A,B,C)
CALL TTAPE(O,NBODY,NWING,NTAPE,NTAPE,A,B,C)
REWIND NTAPE
900 CONTINUE
END FILE NTAPE
REWIND NTAPE
RETURN
END

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05/22/67

SCAMP4 - FFN SOURCE STATEMENT - IFN(S) -

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C
C
C      SURROUTINE SCAMP4(X,Y,N,NDA,NDR,DA,DB,C,S,M)
C
C      GIVEN A SET OF N POINTS WHOSE ABSCISSAE FORM A STRICTLY MONOTONE
C      SEQUENCE, AND GIVEN A FIRST OR SECOND DERIVATIVE AT X(1) AND A FIRST
C      OR SECOND DERIVATIVE AT X(N), TO FIND THE SMOOTHEST POSSIBLE CURVE
C      PASSING RIGOROUSLY THROUGH THE GIVEN POINTS, SATISFYING THE
C      SPECIFIED BOUNDARY CONDITIONS, AND POSSESSING CONTINUOUS FIRST AND
C      SECOND DERIVATIVES. THE CRITERION OF SMOOTHNESS IS THE
C      MINIMIZATION OF THE INTEGRAL OF THE SQUARE OF THE SECOND DERIVATIVE,
C      AND THE CURVE FOUND IS ACCORDINGLY A CHAIN OF CUBICS, I.E., A
C      SEPARATE CUBIC ON EACH INTERVAL X(I),X(I+1).
C
C      DIMENSION C(4,1),S(1),X(1),Y(1),Z(4)
C
C      L=1
C      KK=1
C      D1=DA
C      D2=DB
C      IF (N-12) 20,10,20
C      10 KK=2
C      20 IF (NDA+1) 30,40,50
C      30 D1=DERIV2(X,Y,X)
C      GO TO 50
C      40 D1=DERIV(X,Y,1)
C      50 NA=ABS(NDA)
C      IF (NDB+1) 60,70,80
C      60 D2=DERIV2(X(N-3),Y(N-3),X(N))
C      GO TO 80
C      70 D2=DERIV(X(N-2),Y(N-2),3)
C      80 NB=ABS(NDR)
C      100 CALL COMCU(D1,D2,S,X,Y,L,M,N,NA,NB)
C      IF (M) 200,110,200
C      110 K=N-1
C      DO 170 J=1,K
C      CALL CUBIC2(X(J),Y(J),S(J),Z,M)
C      IF (M-1) 120,130,120
C      120 M=100+J+M
C      GO TO 200
C      130 GO TO (140,160),KK
C      140 DO 150 I=1,4
C      150 C(I,J)=Z(I)
C      GO TO 170
C      160 L=7+J
C      C(L-6,1)=X(J)
C      C(L-5,1)=X(J+1)
C      C(L-4,1)=3.0
C      C(L-3,1)=Z(1)
C      C(L-2,1)=Z(2)
C      C(L-1,1)=Z(3)
C      C(L,1)=Z(4)
C      170 CONTINUE
C      M=0
C      200 RETURN
C      END

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SCAM0030
SCAM0020
SCAM0040
SCAM0050
SCAM0060
SCAM0070
SCAM0080
SCAM0090
SCAM0100
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SCAM0120
SCAM0130
SCAM0140
SCAM0150
SCAM0170
SCAM0180
SCAM0190
SCAM0200
SCAM0210
SCAM0220
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SCAM0240
SCAM0250
SCAM0260
SCAM0270
SCAM0280
SCAM0290
SCAM0300
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SCAM0370
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SCAM0390
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SCAM0470
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SCAM0490
SCAM0500
SCAM0510
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SCAM0560
SCAM0570

05/22/67

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SIMUN3 - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE SIMUN3(X,Y,M,A,K)
  DIMENSION X(1),Y(1)
  DIMENSION C(4,55),FD(55),XI(55),YI(55)

C NUMERICAL INTEGRATION ROUTINE USING PARABOLIC (OR SIMPSONS)
C RULE ON DATA FIT WITH CUBIC CHAIN
  K=0
  MS=M
  IF (MS .LE. 2) GO TO 1000

C USE SCAMP4 TO FIT CUBIC CHAIN TO POINTS
  CALL SCAMP4(X,Y,MS,-1,-1,0,0,C,FD,LI)
  IF (L .NE. 0) GO TO 1010

  N=MS-1
  IF (MOD(N,2) .EQ. 1) N=N+1
  D=(X(MS)-X(1))/FLOAT(N)

C DEFINE SET OF M (IF M ODD) OR M+1 (IF M EVEN)
C EQUALLY SPACED POINTS
  XI(1)=X(1)
  YI(1)=Y(1)
  XI(N+1)=X(MS)
  YI(N+1)=Y(MS)
  JF=1
  DO 200 I=2,N
    XI(I)=XI(I-1)+D
    DO 100 J=JF,MS
      IF (XI(I) .GT. X(J)) GO TO 100
      JF=J-1
      YI(I)=C(1,JF)+XI(I)*(C(2,JF)+XI(I)*(C(3,JF)+C(4,JF)*
        IXI(I)))
    GO TO 200
  100 CONTINUE
  GO TO 1020
  200 CONTINUE

C USE PARABOLIC RULE TO DO NUMERICAL INTEGRATION
  A=YI(1)+4.*YI(2)+YI(N+1)
  IF (N .LE. 2) GO TO 500
  NL=(N-2)/2
  DO 300 I=1,NL
    A=A+2.*YI(2*I+1)+4.*YI(2*I+2)
  300 CONTINUE
  500 A=D/3.*A
  RETURN

C SET ERROR CODE
  1000 K=1
  GO TO 500
  1010 K=2
  GO TO 500
  1020 K=3
  GO TO 500
  END

```


SINVRT		08/17/65
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
C	IF ANY OTHER ERROR BUT 3, DO NOT REARRANGE	
C		.18
		.19
125	IF (IR1) 150,150,125	
C	IF (IR1-3) 7500,150,7500	
C	EXPAND STORAGE TO NORMAL	
C		.20
150	IF (N-K) 175,275,275	.21
175	L=N*2	.22
	J=N	.23
180	I=N	.24
190	A(I,J)=A(L,I)	.25
	A(L,I)=0.	.26
	L=L-1	.27
	IF (I-1) 225,225,200	.28
200	I=I-1	.29
	GO TO 190	.30
225	IF (J-2) 275,275,250	.31
250	J=J-1	.32
	GO TO 180	
C	TRANSPDSE RACK TO COLUMN-WISE STORAGE	
C		.33
C		.34
275	DO 300 J=1,NH1	.35
	L=J+1	.36
	DO 300 I=L,N	.37
	TEMP=A(I,J)	.38
	A(I,J)=A(J,I)	.39
300	A(J,I)=TEMP	.40
7500	RETURN	.41
	END	.42
		.43

05/22/67

SIZE - EFN SOURCE STATEMENT - IFN(S) -

SUBROUTINE SIZE(MM,NMAX,NPART,NSIZE)
DIMENSION NSIZE(1)

C MM SIZE OF MATRIX
C NMAX MAXIMUM SIZE OF PARTITIONS
C NPART NUMBER OF PARTITIONS
C NSIZE ARRAY OF THE SIZE OF EACH PARTITION

NPMIN=2
NT=MM
NPART=MAXO (NPMIN,1+(NT-1)/NMAX)
N=NPART
NSIZE(N)=NT/N
NT=NT-NSIZE(N)
N=N-1
IF (N) 20,20,10
RETURN
END

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```

SUBROUTINE SLOPEW
COMMON DATE(2),NTAPE1,NOL,NTAPE2,ND2(3),NREAD,
INWRITE,NBODY,NWING,XMACH,SYM,KACE
COMMON /COM1/ KODEB,KODEW,KODEU,KODEI,KODEC,XPER,YPER,KOPTB,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPERI
2,NPLANE,NPLN1
COMMON /COM2/IJ,NPTS(16),X(90,16),Y(90,16),Z(90,16),KPNT,VALUE(5),
1,YCENT(16),SLOPE,KPANEL(2,15),XCOR(16,16),YCOR(16,16),ZCOR(16,16),X
2,INT(2,15),YINT(2,15),ZINT(2,15),XCEN(15,15),YCEN(15,15),ZCEN(15,15
3),XCON(15,15),YCON(15,15),ZCON(15,15),AREAL(15,15),ARAT(15,15),THET
4,AL(15,15),ALPHA(15,15),CHORD(15,15),XFOIL(16,25,2),ZFOIL(16,25,2),X
5,NUM(16,2),XTAB1(25),XTAB2(25),XTAB2(25),ZTAB2(25)
DIMENSION C(4),P(3,50),R(3,50),Q(3,5),LDC(3)
DIMENSION CLEN(15),NC(3)

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C SUBROUTINE TO CALCULATE WING PANEL THICKNESS
C AND CAMBER SLOPES
C IF (KOPTF) 500,470,10

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C DEFINE CONSTANTS
C M,MAX,E AND C ARE CONSTANTS AND ARRAYS
C USED BY SUBROUTINE PCLXN IX,Y,KXY AND NC ARE
C USED BY SUBROUTINE BITURP

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10 M=3
MAX=1
E=0.001
NPER2=NPER-2
NPERT=NPER+1
CUNST=10000.
IXY=1
KXY=2
ZHT=ZCOR(1,1)
C(1)=0.
C(2)=-1.
C(3)=0.
NC(1)=0
NC(2)=6
NC(3)=500

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C DEFINE ARRAYS FOR WING LEADING AND TRAILING
C EDGES P IS ARRAY FOR LEADING EDGE AND R
C IS ARRAY FOR TRAILING EDGE

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20 N1=NPTS(1)
DO 30 I=1,N1
P(1,I)=X(1,1)
P(2,I)=Y(1,1)
P(3,I)=Z(1,1)
N2=NPTS(NPER)
DO 40 I=1,N2
R(1,I)=X(1,NPER)
R(2,I)=Y(1,NPER)
R(3,I)=Z(1,NPER)
40 IF (KSTART-1) 500,150,50

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C      CALCULATE PANEL SLOPES ON INBOARD COLUMN IF
C      WING AND BODY INTERSECT IN NON-STREAMWISE LINE
50      I=1
60      NUM1=XNUM(1,1)
      .31
      .32

C      DEFINE ARRAYS FOR AIRFOIL COORDINATES      XIAB1,ZIAB1
C      ARE ARRAYS FOR UPPER SURFACE COORDINATES  XIAB2,
C      ZIAB2 ARE ARRAYS FOR LOWER SURFACE COORDINATES
      .33
      .34
      .35
      .36
      .37
      .38
      .39
      .40
      .41
      .42
      .43
      .44
      .45
      .46
      .47
      .48

      DO 65 J=1,NUM1
      XTAB1(J)=XFOIL(I,J,1)
      ZTAB1(J)=ZFOIL(I,J,1)
      CALL CHECK (XTAB1,NUM1,2,L,NWRITE)
      IF (L) 450,70,450
70      NUM2=XNUM(1,2)
      DO 75 J=1,NUM2
      XTAB2(J)=XFOIL(I,J,2)
      ZTAB2(J)=ZFOIL(I,J,2)
      CALL CHECK (XTAB2,NUM2,2,L,NWRITE)
      IF (L) 450,77,450
77      DO 100 J=1,NPER1

C      CALCULATE CHORD LENGTH
C      XLEAD AND XTRAIL ARE WING LEADING- AND TRAILING-
C      EDGE INTERCEPTS OF CHORD THROUGH CONTROL POINT
C      CLENG IS CHORD LENGTH
      C(4)=YCON(1,J)
      CALL POLXN (C,P,M,N1,E,MAX,Q,LOC,NINT)
      IF (NINT-1) 480,80,490
80      XLEAD=Q(1,1)
      CALL POLXN (C,R,M,N2,E,MAX,Q,LOC,NINT)
      IF (NINT-1) 480,50,490
90      XTRAIL=Q(1,1)
      CLENG(J)=XTRAIL-XLEAD

C      CALCULATE CAMBER AND THICKNESS ORDINATES
C      ZCON AND ZCEN ARE Z-CAMBER AND Z-THICKNESS
C      ORDINATES
      FRAC=IXCON(I,J)-XLEAD)/CLENG(J)
      FRAT=IXCON(I,J)-XLEAD)/CLENG(J)
      CALL BITURP (XTAB1,ZTAB1,IXY,NUM1,KXY,FRAC,ZR,NC)
      IF (NC(1)) 460,92,92
92      ZCU=ZR
      CALL BITURP (XTAB2,ZTAB2,IXY,NUM2,KXY,FRAC,ZR,NC)
      IF (NC(1)) 460,93,93
93      ZCL=ZR
      ZCON(1,J)=((ZCU+ZCL)/2.)*CLENG(J)+ZHT
      CALL BITURP (XTAB1,ZTAB1,IXY,NUM1,KXY,FRAT,ZR,NC)
      IF (NC(1)) 460,97,97
97      ZTU=ZR
      CALL BITURP (XTAB2,ZTAB2,IXY,NUM2,KXY,FRAT,ZR,NC)
      IF (NC(1)) 460,98,98
98      ZTL=ZR
      ZCEN(1,J)=((ZTU-ZTL)/2.)*CLENG(J)+ZHT
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100 CONTINUE
C CALCULATE CAMBER AND THICKNESS SLOPES
C ALPHA AND THETA ARE ALPHA-CAMBER AND -THICKNESS
C SLOPES
C NOTE THAT IF SINGLE AIRFOIL IS INPUT ON
C CARDS CONSTANT ARRAY FOR ALPHA-CAMBER AND
C -THICKNESS IS CALCULATED
C IF (NUMS-1) 500,150,103
103 XTAB1(1)=XLEAD
   ZTAB1(1)=ZFOIL(1,1)*CLENG(NPER1)+ZHT
   XTAB2(1)=XLEAD
   ZTAB2(1)=ZHT
   DO 110 J=2,NPER
   XTAB1(J)=XCON(I,J-1)
   ZTAB1(J)=ZCON(I,J-1)
   XTAB2(J)=XCEN(I,J-1)
   ZTAB2(J)=ZCEN(I,J-1)
110 XTAB1(NPER)=XTRAIL
   ZTAB1(NPER)=ZFOIL(1,NUM1,1)*CLENG(NPER1)+ZHT
   XTAB2(NPER)=XTRAIL
   ZTAB2(NPER)=ZHT
120 DO 130 J=2,NPER
   EPS=CLENG(J-1)/CONST
   XR=XTAB1(J)-EPS
   XS=XTAB1(J)+EPS
123 CALL BITURP (XTAB1,ZTAB1,IXY,NPERT,KXY,XR,ZR,NC)
   IF (NC(1)) 460,124,124
124 CALL BITURP (XTAB1,ZTAB1,IXY,NPERT,KXY,XS,ZS,NC)
   IF (NC(1)) 460,125,125
125 ALPHA(I,J-1)=ATAN((ZS-ZR)/(XS-XR))
   XR=XTAB2(J)-EPS
   XS=XTAB2(J)+EPS
127 CALL BITURP (XTAB2,ZTAB2,IXY,NPERT,KXY,XR,ZR,NC)
   IF (NC(1)) 460,128,128
128 CALL BITURP (XTAB2,ZTAB2,IXY,NPERT,KXY,XS,ZS,NC)
   IF (NC(1)) 460,129,129
129 THETA(I,J-1)=ATAN((ZS-ZR)/(XS-XR))
130 CONTINUE

C CALCULATE PANEL SLOPES FOR MAIN WING REGION
150 DO 250 I=KSTART,KEND
C CALCULATE CHORD LENGTH
C XLEAD AND XTRAIL ARE WING LEADING- AND TRAILING-
C EDGE INTERCEPTS OF CHORD THROUGH CONTROL POINT
C CLENG IS CHORD LENGTH
C(4)=YCCN(1,1)
CALL POLXN (C,P,M,N1,E,MAX,0,LOC,NINT)
IF (NINT-1) 480,153,490
153 XLEAD=Q(1,1)
CALL POLXN (C,R,M,N2,E,MAX,0,LOC,NINT)
IF (NINT-1) 480,157,490
157 XTRAIL=Q(1,1)

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C      CLENG(I)=XTRAIL-XLEAD
C      EPS=CLENG(I)/CONST
C      IF (NUMS-1) 500,160,170
160  IR=1
      GO TO 190
170  IR=I+KSTART-1
190  NUM1=XNUM(IR,1)

C      DEFINE ARRAYS FOR AIRFOIL COORDINATES      XTAB1,ZTAB1
C      ARE ARRAYS FOR UPPER SURFACE COORDINATES  XTAB2,
C      ZTAB2 ARE ARRAYS FOR LOWER SURFACE COORDINATES
      DO 195 J=1,NUM1
195  ZTAB1(J)=XFOL(IR,J,1)
      XTAB1(J)=XFOL(IR,J,1)
      CALL CHECK (XTAB1,NUM1,2,L,NWRITE)
      IF (L) 450,200,450
200  NUM2=XNUM(IR,2)
      DO 205 J=1,NUM2
205  ZTAB2(J)=ZFOL(IR,J,2)
      XTAB2(J)=ZFOL(IR,J,2)
      CALL CHECK (XTAB2,NUM2,2,L,NWRITE)
      IF (L) 450,207,450

C      CALCULATE CAMBER AND THICKNESS ORDINATES
C      ZCON AND ZCEN ARE Z-CAMBER AND Z-THICKNESS
C      ORDINATES
207  DO 220 J=1,NPER1
      FRAC=(XCON(I,J)-XLEAD)/CLENG(I)
      FRAT=(XCEN(I,J)-XLEAD)/CLENG(I)
210  CALL BITURP (XTAB1,ZTAB1,IXY,NUM1,KXY,FRAC,ZR,NC)
      IF (NC(I)) 460,211,211
211  ZCU=ZR
      CALL BITURP (XTAB2,ZTAB2,IXY,NUM2,KXY,FRAC,ZR,NC)
      IF (NC(I)) 460,212,212
212  ZCL=ZR
      ZCON(I,J)=((ZCU+ZCL)/2.)*CLENG(I)+ZHT
      CALL BITURP (XTAB1,ZTAB1,IXY,NUM1,KXY,FRAT,ZR,NC)
      IF (NC(I)) 460,217,217
217  ZTU=ZR
      CALL BITURP (XTAB2,ZTAB2,IXY,NUM2,KXY,FRAT,ZR,NC)
      IF (NC(I)) 460,218,218
218  ZTL=ZR
      ZCEN(I,J)=((ZTU-ZTL)/2.)*CLENG(I)+ZHT
220  CONTINUE

C      CALCULATE CAMBER AND THICKNESS SLOPES
C      ALPHA AND THETA ARE ALPHA-CAMBER AND -THICKNESS
C      SLOPES
C      NOTE THAT IF SINGLE AIRFOIL IS INPUT ON
C      CARDS CONSTANT ARRAY FOR ALPHA-CAMBER AND
C      -THICKNESS IS CALCULATED
      IF (I-KSTART) 500,230,223
223  IF (NUMS-1) 500,225,230
225  K=KSTART

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DO 227 J=1,NPER1
  ALPHA(I,J)=ALPHA(K,J)
  227 THETA(I,J)=THETA(K,J)
  GO TO 250
230 XTAB1(I)=XLEAD
  ZTAB1(I)=ZFOIL(IR,1,1)*CLENG(I)+ZHT
  XTAB2(I)=XLEAD
  ZTAB2(I)=ZHT
  DO 231 J=2,NPER
    XTAB1(J)=XCON(I,J-1)
    ZTAB1(J)=ZCON(I,J-1)
    XTAB2(J)=XCEN(I,J-1)
    ZTAB2(J)=ZCEN(I,J-1)
  231 ZTAB1(NPERT)=XTRAIL
  ZTAB1(NPERT)=ZFOIL(IR,NUM1,1)*CLENG(I)+ZHT
  XTAB2(NPERT)=XTRAIL
  ZTAB2(NPERT)=ZHT
  DO 240 J=2,NPER
    XR=XTAB1(J)-EPS
    XS=XTAB1(J)+EPS
  233 CALL BITURP (XTAB1,ZTAB1,IXY,NPERT,KXY,XR,ZR,NC)
  IF (NC(I)) 460,234,234
  234 CALL BITURP (XTAB1,ZTAB1,IXY,NPERT,KXY,XS,ZS,NC)
  IF (NC(I)) 460,235,235
  235 ALPHA(I,J-1)=ATAN1(ZS-ZR)/(XS-XR)
  XR=XTAB2(J)-EPS
  XS=XTAB2(J)+EPS
  237 CALL BITURP (XTAB2,ZTAB2,IXY,NPERT,KXY,XR,ZR,NC)
  IF (NC(I)) 460,238,238
  238 CALL BITURP (XTAB2,ZTAB2,IXY,NPERT,KXY,XS,ZS,NC)
  IF (NC(I)) 460,239,239
  239 THETA(I,J-1)=ATAN1(ZS-ZR)/(XS-XR)
  240 CONTINUE
  250 CONTINUE
  IF (KSTART-1) 500,257,253
  253 IF (NUMS-1) 500,254,257
  254 K=KSTART
  DO 255 J=1,NPER1
    ALPHA(I,J)=ALPHA(K,J)
    255 THETA(I,J)=THETA(K,J)
  C
  C CALCULATE PANEL SLOPES FOR WING TIP REGION
  C
  IF OUTBOARD WING EDGE IS NON-STREAMWISE LINE
  257 IF (KEND-NPLN1) 258,510,500
  258 I=NPLN1
  260 DO 270 J=1,NPER
    JN=NPER+1-J
    R(1,J)=XCOR(I+1,JN)
    R(2,J)=YCOR(I+1,JN)
    R(3,J)=ZCOR(I+1,JN)
  270 GO TO 310
  280 DO 290 J=1,NPER
    P(1,J)=XCOR(I+1,J)

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SLOPEM		08/12/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)	
	P(2,J)=YCUR(I+1,J)	.229	
290	P(3,J)=ZCOR(I+1,J)	.230	.231
310	NUM1=XNUM(NUMS,1)		
C	DEFINE ARRAYS FOR AIRFOIL COORDINATES	.232	
C	ARE ARRAYS FOR UPPER SURFACE COORDINATES	.233	.234
C	ZTAB2 ARE ARRAYS FOR LOWER SURFACE COORDINATES	.235	
	DO 315 J=1,NUM1	.236	.237
	XTAB1(J)=XFIL(NUMS,J,1)	.238	
315	ZTAB2(J)=ZFIL(NUMS,J,1)	.239	
	CALL CHECK (XTAB1,NUM1,2,L,NWRITE)	.240	
	IF (L) 450,320,450	.241	.242
320	NUM2=XNUM(NUMS,2)	.243	
	DO 325 J=1,NUM2	.244	.245
	XTAB2(J)=XFIL(NUMS,J,2)	.246	
325	ZTAB2(J)=ZFIL(NUMS,J,2)	.247	
	CALL CHECK (XTAB2,NUM2,2,L,NWRITE)		
	IF (L) 450,327,450		
327	DO 380 J=1,NPER1		
C	CALCULATE CHORD LENGTH	.248	.249
C	XLEAD AND XTRAIL ARE WING LEADING- AND TRAILING-	.250	
C	EDGE INTERCEPTS OF CHORD THROUGH CONTROL POINT	.251	
C	CLENG IS CHORD LENGTH	.252	
	C(4)=YCGN(1,J)	.253	
	IF (SLOPE) 330,500,340	.254	
330	NL=N1	.255	
	NT=NPER	.256	
	GO TO 350	.257	
340	NL=NPER	.258	
	NT=N2	.259	
350	CALL POLYN (C,P,M,NL,E,MAX,Q,LOC,NINT)	.260	
	IF (NINT-1) 480,360,490	.261	
360	XLEAD=Q(1,1)	.262	
	IF (J-1) 500,363,364	.263	
363	XLS=XLEAD	.264	
364	CALL POLYN (C,R,M,NT,E,MAX,Q,LOC,NINT)	.265	
	IF (NINT-1) 480,367,490	.266	
367	XTRAIL=Q(1,1)	.267	
	IF (J-NPER1) 370,368,500		
368	XTS=XTRAIL		
	CLS=XTS-XLS		
370	CLENG(J)=XTRAIL-XLEAD		
C	CALCULATE CAMBER AND THICKNESS ORDINATES	.268	
C	ZCON AND ZCEN ARE Z-CAMBER AND Z-THICKNESS	.269	
C	ORDINATES	.270	
	FRAC=(XCON(I,J)-XLEAD)/CLENG(J)	.271	
	FRAT=(XCEN(I,J)-XLEAD)/CLENG(J)	.272	
371	CALL BITURP (XTAB1,ZTAB1,IXY,NUM1,KXY,FRAC,ZR,NC)	.273	
	IF (INC(1)) 460,372,372	.274	
372	ZCU=ZR	.275	
	CALL BITURP (XTAB2,ZTAB2,IXY,NUM2,KXY,FRAC,ZR,NC)		
	IF (INC(1)) 460,373,373		


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373 ZCL=ZR
ZCON(I,J)=((ZCU+ZCL)/2.)*CLENG(J)+ZHT
CALL BITURP (XTAB1,ZTAB1,IXY,NUM1,KXY,FRAT,ZR,NC)
IF (NC(I)) 460,377,377
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377 ZTU=ZR
CALL BITURP (XTAB2,ZTAB2,IXY,NUM2,KXY,FRAT,ZR,NC)
IF (NC(I)) 460,378,378
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378 ZTL=ZR
ZCEN(I,J)=((ZTU-ZTL)/2.)*CLENG(J)+ZHT
380 CONTINUE

C CALCULATE CAMBER AND THICKNESS SLOPES
C ALPHA AND THETA ARE ALPHA-CAMBER AND -THICKNESS
C SLOPES
C NOTE THAT IF SINGLE AIRFOIL IS INPUT ON
C CARDS CONSTANT ARRAY FOR ALPHA-CAMBER AND
C -THICKNESS IS CALCULATED
IF (NUMS-1) 500,383,387
383 K=KSTART
L=KEND
DQ 385 J=1,NPER1
ALPHA(L,J)=ALPHA(K,J)
385 THETA(L,J)=THETA(K,J)
GO TO 510

387 XTAB1(I)=XLS
ZTAB1(I)=ZFOIL(NUMS,1,1)*CLS+ZHT
XTAB2(I)=XLS
ZTAB2(I)=ZHT
DO 390 J=2,NPER
XTAB1(J)=XCON(I,J-1)
ZTAB1(J)=ZCON(I,J-1)
XTAB2(J)=XCON(I,J-1)
ZTAB2(J)=ZCON(I,J-1)
390 XTAB1(NPERT)=XIS
ZTAB1(NPERT)=ZFOIL(I,NUM1,1)*CLS+ZHT
XTAB2(NPERT)=XIS
ZTAB2(NPERT)=ZHT
DO 410 J=2,NPER
EPS=CLENG(J-1)/CONST
XR=XTAB1(J)-EPS
XS=XTAB1(J)*EPS
403 CALL BITURP (XTAB1,ZTAB1,IXY,NPERT,KXY,XR,ZR,NC)
IF (NC(I)) 460,404,404
404 CALL BITURP (XTAB1,ZTAB1,IXY,NPERT,KXY,XS,ZS,NC)
IF (NC(I)) 460,405,405
405 ALPHA(I,J-1)=ATAN((ZS-ZR)/(XS-XR))
XR=XTAB2(J)-EPS
XS=XTAB2(J)*EPS
407 CALL BITURP (XTAB2,ZTAB2,IXY,NPERT,KXY,XR,ZR,NC)
IF (NC(I)) 460,408,408
408 CALL BITURP (XTAB2,ZTAB2,IXY,NPERT,KXY,XS,ZS,NC)
IF (NC(I)) 460,409,409
409 THETA(I,J-1)=ATAN((ZS-ZR)/(XS-XR))
410 CONTINUE

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08/12/65
INTERNAL FORMULA NUMBER(S)

SOURCE STATEMENT

EXTERNAL FORMULA NUMBER

SLOPEW

420 GO TO 510

C ERROR MESSAGES

450 WRITE (NWRITE,940)

GO TO 455

460 WRITE (NWRITE,930)

GO TO 495

470 WRITE (NWRITE,900)

GO TO 495

480 WRITE (NWRITE,910)

GO TO 495

490 WRITE (NWRITE,920)

GO TO 495

495 CODEW=1

GO TO 500

500 RETURN

C USE SUBROUTINE MEAN TO SMOOTH CAMBER AND

C THICKNESS SLOPES

510 IF (NUMS-1) 500,520,550

520 K=KSTART

DO 530 J=1,NPER1

XTAB1(J)=XCON(K,J)

ZTAB1(J)=ALPHA(K,J)

XTAB2(J)=XCEN(K,J)

ZTAB2(J)=THETA(K,J)

530 CALL MEAN (XTAB1,ZTAB1,NPER1)

533 CALL MEAN (XTAB2,ZTAB2,NPER1)

DO 540 I=1,NPLN1

DO 540 J=1,NPER1

ALPHA(I,J)=ZTAB1(J)

THETA(I,J)=ZTAB2(J)

GO TO 500

550 DO 580 I=1,NPLN1

DO 560 J=1,NPER1

XTAB1(J)=XCON(I,J)

ZTAB1(J)=ALPHA(I,J)

XTAB2(J)=XCEN(I,J)

ZTAB2(J)=THETA(I,J)

560 CALL MEAN (XTAB1,ZTAB1,NPER1)

563 CALL MEAN (XTAB2,ZTAB2,NPER1)

DO 570 J=1,NPER1

ALPHA(I,J)=ZTAB1(J)

THETA(I,J)=ZTAB2(J)

CONTINUE

GO TO 500

900 FORMAT(1H1,9X,33HERROR MESSAGE - SUBROUTINE SLOPEW/10X,

119HPROGRAM LOGIC ERROR/10X,

234HINCORRECT COMPUTED GO TO STATEMENT)

910 FORMAT(1H1,9X,33HERROR MESSAGE - SUBROUTINE SLOPEW/10X,

124HSUBROUTINE POLYN FAILURE/10X,

255HING CHORD LENGTH NOT CALCULATED NO INTERSECTION FOUND)

920 FORMAT(1H1,9X,33HERROR MESSAGE - SUBROUTINE SLOPEW/10X,

124HSUBROUTINE POLYN FAILURE/10X,

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SLOPEW
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
 08/12/65
 262HWINO CHORD LENGTH NOT CALCULATED MULTIPLE INTERSECTIONS FOUND)
 330 FORMAT(1H1,9X,33HERROR MESSAGE - SUBROUTINE SLOPEW/10X,
 125HSUBROUTINE B11URP FAILURE/10X,
 233HINTERPOLATED VALUE NOT CALCULATED)
 940 FORMAT(1H1,9X,33HERROR MESSAGE - SUBROUTINE SLOPEW/10X,
 121HINPUT CARD DATA ERROR/10X,
 147HX-COORDINATES OF AIRFOIL NOT STRICTLY MONOTONIC/10X,
 219HINCREASING SEQUENCE)
 END

• 388

05/31/67

STRM1 - FFN SOURCE STATEMENT - IFN(S) -

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IF(JCD.EQ.5) GO TO 35
JC=0
79 I=I+1
  XT(I)=TD(36)
  YT(I)=TD(35)
  ZT(I)=TD(34)
  CPT(I)=CP
  IF(JCD.EQ.5) GO TO 15
  IF(1.LY.200.AND.XT(I).LT.XMAX.AND.XT(I).GT.XMIN) GO TO 15
  IF(IND1.EQ.2) GO TO 38
  IS=1/2
  DO 36 J=1,IS
    L=I-J+1
    TA=A(L)
    TB=B(L)
    TC=C(L)
    TD=D(L)
    A(L)=A(J)
    B(L)=B(J)
    C(L)=C(J)
    D(L)=D(J)
    A(J)=TA
    B(J)=TB
    C(J)=TC
    D(J)=TD
36 CONTINUE
  IF(PRINT.NE.0.) GO TO 60
  FIN=ADD(XT(I),XDELT)
  XINI=XT(I)+XDELT-FIN
  IXM=ABS(XT(I)-XINI)/XDELT
  XL=XINI
  NUI(1)=0
  NUI(2)=6
  NUI(3)=0
  CALL BJTURP(XT,YT,1,1,2,XL,YL,NUI)
  CALL BJTURP(XT,ZT,1,1,2,XL,ZL,NUI)
  CALL BJTURP(XT,CPT,1,1,2,XL,CPL,NUI)
  WRITE(N6,1014) XL,YL,ZL,CPL
  GO TO 51
38 CONTINUE
  XL=X-YDELT
  DO 40 J=1,I
    K=I-J+2
    L=K-1
    XT(K)=XT(L)
    YT(K)=YT(L)
    ZT(K)=ZT(L)
    CPT(K)=CPT(L)
40 CONTINUE
  I=I+1
  XT(I)=X
  YT(I)=Y
  ZT(I)=Z
  CPT(I)=CPLT

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IF(PRINT-NE-Q.) GO TO 65	
IXM=ABS(XT(I)-XT(I))/XDELT	
51 CONTINUE	
DO 52 J=1,IXM	
XL=XL+XDELT	109
CALL RJTURP(XT,YT,1,1,2,XL,YL,MU)	111
CALL RJTURP(XT,CPT,1,1,2,XL,CPL,MU)	113
CALL RJTURP(XT,ZT,1,1,2,XL,ZL,MU)	114
WRITE(N6,1015) XL,YL,ZL,CPL	
52 CONTINUE	
53 CONTINUE	
35 JC=JC+1	
IF(JC.LE.3) GO TO 29	
I=I-JC+1	
JC=1	
GO TO 29	
60 CONTINUE	126
WRITE(N6,1016)	
DO 64 J=1,I	133
CALL LACKEY(I,XT(J),YT(J),ZT(J),U,V,W,CP)	134
64 WRITE(N6,1017) XT(J),YT(J),ZT(J),U,V,W,CP	
GO TO 53	
65 CONTINUE	
DO 67 J=1,I	148
CALL LACKEY(I,XT(J),YT(J),ZT(J),U,V,W,CP)	149
67 WRITE(N6,1017) XT(J),YT(J),ZT(J),U,V,W,CP	
GO TO 53	
END	

TDUMP
09/14/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

SUBROUTINE TDUMP (LO, LTAPE, LGDEF)
DIMENSION R(2000), IR(10)
LOGICAL LGDEF(3,6)

USED BY GEOMD TO DUMP CONTENTS OF PERCENT LINE TAPE

DO 10 M=1,6
IF(LGDEF(3,M)) GO TO 50
CONTINUE
GO TO 9000

WRITE(10,100)
FORMAT(10H1TAPE DUMP)
REWIND LTAPE
JR=0

DO 1000 K=1,9

JR=JR+1
READ (LTAPE) IR
WRITE(10,200)JR,IR

FORMAT(7HORECORD 13/1016)

JR=JR+1

L=IR(2)
READ(LTAPE)(R(I),I=1,L)
WRITE(LG ,300)JR,(R(I),I=1,L)

FORMAT(7HORECORD 13/11H 9F13.4)

1000 CONTINUE

9000 RETURN
END

'1	'3	'4
'2	'6	
'5		
'7		
'8	'9	
'10		
'11		
'12		
'13		
'14	'15	'16
'17	'18	'19
'20		
'21		
'22	'23	'24
'27	'28	'29
	'30	'31
		'32
'33	'34	
'35		
'36		

09/14/65
TFLAT
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

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SUBROUTINE TFLAT(DAT,LI,LO,LA,LB,LD,NBODY,IOK)

C   USED BY OPCAM TO TRANSFORM BODY AND WING TO A NEW
C   COORDINATE SYSTEM, FLATTEN THE WING, AND INTERSECT
C   THE TRANSFORMED BODY WITH THE TRANSFORMED AND FLATTENED WING
C

C   DIMENSION DAT(2),STA(51),OLDSTA(51),
C   * 8(4368),RT(3,4),RX(3,51),W(4368),NU(3),BCODE(2),S(1000),
C   * BW(3,100),ALFBET(2),NAME(3),RZ(51,2)
C   * ,IREC(10),JREC(11C),DUM(9)
C   * ,BTIL(12),WTITL(12),BAX(2)
C   LOGICAL LGDEF,BODY,WING
C   COMMON /LGDEF/LGDEF(3,6)
C   DATA IREC,JREC,DUM,NU/10*0,1,9,1,7*0,9*0,.0,6,30/,
C   * ,NAME/6HDEFINE,6HDEFINE,6HEND OF/
C   * ,BAX/0,.0./,BTIL(11)/
C   * ,72HTRANSFORMED BODY (PRIMED-AXIS SYSTEM)
C   * ,/WTITL(11)/
C   * ,72HPOINTS ON FLAT TRANSFORMED WING (PRIMED-AXIS SYSTEM)
C   /

C INPUTS ARE
C   C   DAT = DATE
C   C   LI = INPUT TAPE
C   C   LO = OUTPUT TAPE
C   C   LA = TAPE WRITTEN BY GEOMETRIC DEFINITION LINK, AND
C   C   USED BY TFLAT
C   C   LB = TAPE TO BE WRITTEN FOR AERO LINK
C   C   LD = TAPE TO BE WRITTEN FOR PANEL LINK
C   C   OUTPUT IS
C   C   IOK = 0 IF TFLAT IS SUCCESSFUL
C

100 WRITE(LO,110)DAT
110 FORMAT(1H1 55X 2A6/68H PROGRAM ENTERED LINK TO TRANSFORM BODY AND/
,OR WING BEFORE PANELLING)

C   CLEAR STORAGE (PROGRAM DOES NOT REQUIRE THIS, BUT HELPFUL FOR DUMPS)
DO 120 I=1,4368
  B(I)=-0.
  W(I)=-0.
120 CALL TRAVIRX,B,153)
    CALL TRAVIS,B,1000)
    CALL TRAVIS,B,300)
    CALL TRAVIRZ,B,102)

  NU(2)=LO
  NBODY=0
  REWIND LA
  REWIND LD
  READ(LI,210) XNRX,CHD,BCODE,EPRC
210 FORMAT(6F10.0)
  NRX=XNRX
  KODEBR=BCODE(1)
  KODEBS=BCODE(2)

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09/14/65
TFLAT - INTERNAL FORMULA NUMBER(S)

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C      NRX = NO. OF POINTS DESIRED IN RX ARRAY (RADIUS AND Z VS. X)
C      LINEAR INTERPOLATION, =2 FOR BIQUADRATIC INTERPOLATION.
C      KODEBR IS USED BY BITURP TO GET RX ARRAY
C      KODERS IS USED BY MBXX
C      CHD IS USED BY TFLAT1
C      EPRC IS USED BY TFLAT1. Z-CENTROID AND RADIUS SET =0 IF LESS THAN EPRC.
C
C      MU = 2
C      IF(NRX .GT. 2 .AND. NRX .LT. 50) GO TO 400
C      NRX=50
C      CONTINUE
C
C      TEST FOR ERROR IN PREVIOUS LINK
C      BODY=.FALSE.
C      WING=.FALSE.
C      IF(.NOT. LGDEF(1,3)) GO TO 500
C      BODY WAS REQUESTED. SEE IF PROCESSED.
C      IF(.NOT. LGDEF(3,3)) GO TO 700
C      BODY= .TRUE.
C      CHECK WING
C      IF(.NOT. LGDEF(1,1)) GO TO 600
C      UPPER WING REQUESTED. SEE IF PROCESSED.
C      IF(.NOT. LGDEF(3,1)) GO TO 700
C      WING= .TRUE.
C      CHECK THAT AT LEAST A BODY OR A WING IS DEFINED
C      IF(BODY .OR. WING) GO TO 800
C
C      WRITE(LO,710)
C      FORMAT(23H0ERROR IN PREVIOUS LINK)
C      GO TO 8000
C
C      IF(800Y) GO TO 1000
C      NO BODY, BUT THERE IS A WING. WRITE DUMMY RECORDS FOR BODY
C      MERIDIAN LINES ON TAPE LD.
C      WRITE(LO)JREC
C      WRITE(LO)DUM
C      SKIP RECORDS 1-4 ON TAPE LA
C      CALL FSR(4,LA,10K)
C      GO TO 3000
C
C      READ BODY DEFINITION FROM TAPE LA
C      CONTINUE
C      READ(LA)IREC
C      NSTA=IREC(2)
C      MU = 4
C      IF((NSTA .LT. 2) .OR. (NSTA .GT. 51) .OR. (IREC(1) .NE. 1) .OR.
C      , (IREC(3) .NE. 0)) GO TO 8000
C      READ(LA)(STAT(1),I=1,NSTA)
C      SAVE ORIGINAL BODY STATIONS FOR LATER PRINTOUT
C      CALL TRAV(LO,STA,NSTA)
C      READ(LA)IREC
C      MU = 6
C      IF(IREC(1) .NE. 3 .OR. IREC(3) .NE. 0 .OR. IREC(2) .GT. 4368)
C      , GO TO 8000

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LD 1
LD 2
LA 1-4

LA 1

LA 2

LA 3

09/14/65

TELAT	EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
C	183	NPCT=IREC(4)	183
C	184	NPCT = NO. OF BODY MERIDIAN LINES	184
C	LA 4	NBEL=IREC(2)	
C		READ(LA)(8(1),I=1,NBEL)	
C		FIND TRANSFORMATION RT TO NEW COORD. SYSTEM.	
C		C TRANSFORM AND SHEAR BODY MERIDIAN LINES B	
C		C TRANSFORM BODY STATIONS	
C		C FIND RADIUS AND Z-COORD. OF CENTROID VS. X-PRIME	
C	2000	MU = H	185 ,86 ,87 ,88 ,89
C		CALL TFLAT1(CHD,NSTA,STA,NBPCT,B,S,W,RT,ALFBET,RZ,EPRC,NU)	190
C		IF(NU)8000,2050,8000	191
C	2050	CONTINUE	192
C		WRITE(LO,2100)(RT(I,4),I=1,3),(RT(I,1),I=1,3),	193
C		(1,ULDSTA(1),STA(1),RZ(1,1),RZ(1,2),I=1,NSTA)	194 ,95 ,96 ,97 ,98 ,99
C	2100	FORMAT(51)O THE ORIGIN OF THE NEW BODY COORDINATE SYSTEM IS AT /	100 ,101 ,102 ,103 ,104
C		5X12H(X,Y,Z) = (F10.4,1H,F10.4,1H,F10.4,1H) /	
C		52H0A UNIT VECTOR ALONG THE X-PRIME AXIS HAS COMPONENTS /	
C		5X12H(X,Y,Z) = (F10.4,1H,F10.4,1H,F10.4,1H) /	
C		/1H0 12X 8HORIZONTAL 5X 12HCIRCULARIZED 7X 4HBODY 8X 6HZ-BODY	
C		/6X 3HNU. 2X 12HBODY STATION 3X 12HBODY STATION 6X 6HRAIDUS	
C		6X 8HCENTROID/(1H 17,F13.4,F15.4,2F14.4)	
C		WRITE TRANSFORMED BODY MERIDIAN LINES ON OUTPUT TAPE	
C		CALL TFLATM(8,NBPCT,BAX,BTTL,DAT,LO,STA)	
C		WRITE BODY RECORDS ON TAPE LD	
C		IREC(1)=1	105
C		WRITE(LO)IREC	106
C		WRITE(LO)(8(1),I=1,NBEL)	107 ,108 ,109
C		LD 1	
C		LD 2	
C		BODY DONE. PROCESS WING.	
C		IF(WING) GO TO 3000	110 ,111 ,112 ,113 ,114
C		NO. WING. WRITE DUMMY WING RECORDS ON TAPE LD	115 ,116 ,117
C		JREC(3)=1	118
C		DO 2500 I=3,5,2	119
C		JREC(1)=1	120
C		WRITE(LO)JREC	121 ,122 ,123
C	2500	WRITE(LO)IDJM	124 ,125 ,126 ,127
C		ZAV=0.	128
C		GO TO 5000	
C		WING IS TO BE PROCESSED. READ WING DEFINITION FROM TAPE LA	129
C	3000	CONTINUE	130
C		CALL FSR(2,LA,10K)	131
C		READ(LA)IREC	132 ,133 ,134
C		MU = 10	135
C		IF(IREC(1)) -NE. 7) GO TO 8000	136 ,137 ,138
C		NWPL=IREC(4)	139
C		NWEL=IREC(2)	
C		NWPL = NO. OF WING PERCENT LINES	140

09/14/65

INTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
1	IF(LA)	
2	MU = 12	
3	IF(NWEL .GT. 4368) GO TO 8000	
4	RECORD 3 ON LD IS SAME AS 7 ON LA (EX. WORD 1). WRITE IT.	
5	IFREC(1)=3	
6	WRITE(LD)IREC	
7	READ(LA) (W(1),I=1,NWEL)	
8	WE DO NOT TRANSFORM WING IF THERE IS NO BODY	
9	IF(.NOT. BODY) GO TO 4000	
10	TRANSFORM WING	
11	CALL TRAPT(W,NWPCL,RT)	
12	FIND WING-BODY INTERSECTIONS	
13	MU = 14	
14	CALL WXXX(18,NBPCT,W,NWPCL,1.E-4,KODEBS,S,BW,MU)	
15	IF(NU)8000,3200,8000	
16	INTERSECTION POINTS ARE IN BW. USE AVERAGE OF Z FOR	
17	FIRST AND LAST INTERSECTION POINTS.	
18	ZAV=18W(3,1)+8W(3,NWPCL))*5	
19	CHECK THAT BOTH INTERSECTION POINTS WERE OK. IF ANY WING	
20	PERCENT LINE FAILED TO PIERCE BODY, THEN COORD. OF 1.E+30	
21	WAS INSERTED (BY W8X) FOR X,Y AND Z.	
22	MU = 16	
23	IF(ZAV-1.E+5)4200,8000,8000	
24	THIS IS WING WITHOUT BODY. FOR HEIGHT OF FLAT WING	
25	USE AVERAGE OF Z FOR 1ST POINT OF 1ST PERCENT LINE AND	
26	1ST PT. OF LAST LINE.	
27	CONTINUE	
28	MU = 18	
29	JZAV=W(3)	
30	ZAVZER=W(JZAV+2)	
31	KZAV=W(3,NWPCL)	
32	ZAVHUN=W(KZAV+2)	
33	ZAV=.5*(ZAVZER+ZAVHUN)	
34	THE FLAT WING WILL HAVE Z=ZAV FOR ALL POINTS	
35	CONTINUE	
36	MU = 20	
37	J=3*NWPCL+3	
38	DO 4220 I=J,NWEL,3	
39	W(I)=ZAV	
40	WRITE FLAT, TRANSFORMED WING ON OUTPUT TAPE	
41	CALL TFLAT(W,NWPCL,WITL,DAT,LD)	
42	WRITE FLAT WING PERCENT LINES ON LD	
43	WRITE(LD) (W(1),I=1,NWEL)	
44	IF(BODY) GO TO 4500	
45	WING ALONE. WRITE DUMMY RECORDS ON LD FOR WING-BODY	
46	INTERSECTION POINTS.	

TFLAT
09/14/65

EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
MU = 22		,186
JREC(11)=5		,187
WRITE(LD)JREC		,188
WRITE(LD)JUM	LD 5	,189 ,190
IOK=0	LD 6	,191 ,192 ,193
GO TO 5000		,194
C		
C	FIND INTERSECTIONS OF FLAT WING WITH BODY	,195
4500	CONTINUE	,196
MU = 24		,197
CALL WBXX(8,NBPC,T,M,NWPCL,1,E-4,KODEBS,S,BM,NU)		,198
IF(NU)8000,4700,8000		
C		
C	WRITE WING-BODY INTERSECTION POINTS ON OUTPUT TAPE	,199
4700	CALL TFLATX(LO,DAT,NWPCL,M,BM,NU)	,200
MU = 26		,201
IF(NU)8000,4800,8000		
C		
C	WRITE INTERSECTION POINTS ON LD	,202
4800	MU = 28	,203
JREC(11)=5		,204
JREC(2)=3*NWPCL		,205
JREC(3)=0		,206
WRITE(LD)JREC	LD 5	,207 ,208 ,209
WRITE(LD) ((BM(I,J),I=1,3),J=1,NWPCL)	LD 6	,210 ,211 ,212 ,213 ,214
C		,216 ,217
		,218
		,219
		,220
5000	CONTINUE	
END FILE LD		
REWIND LD		
6000	IF(.NOT. BODY)GO TO 9000	,221 ,222 ,223
C		
C	WRITE TAPE LB FOR AERO AND PANEL LINKS.	
C	REWIND LB	
C	RECORD 1 = XYZ COMPONENTS OF UNIT VECTOR ALONG X-PRIME AXIS,	
C	FOLLOWED BY ZAV = Z-COORD. OF FLAT WING,	
C	FOLLOWED BY TRANSFORMATION CONSTANTS TO CONVERT OLD	
C	STATIONS TO NEW STATIONS -	
C	NEW X=ALFBET(1)*(OLD X)+ALFBET(2)	
C		
C	WRITE(LB)(RT(I,1),I=1,3),ZAV,ALFBET	,224
C		
C	PREPARE TO FIND POINTS ON CURVE OF BODY RADIUS VS. X,	
C	AND CURVE OF Z-COORD. OF CENTROID VS. X.	
C	THERE ARE NX POINTS. IF THERE IS NO WING, THEN	
C	THE PTS. ARE EQUALLY SPACED IN X. IF THERE IS A WING	
C	THEN THE POINTS WILL BE EQUALLY SPACED FROM NOSE TO	
C	INTERSECTION OF LEADING EDGE WITH BODY, AND EQUALLY	
C	SPACED FROM THERE ON AFT. THESE TWO SPACINGS	
C	WILL BE APPROX. EQUAL.	
C		
		,225 ,226 ,227 ,228 ,229
		,231

```

HLFNG=STAINSTA)
IF(WINGJUD TJ 61C0
C
XNRX=NRX-1
DO 6050 I=1,NRX
XIM=I-1
RX(I,1)=(XIM/XNRX)*BLENG
INDEX=NRX
GO TO 6150
C
BLN=BW(1,1)
HLR=BLENG-BLN
NRXN=(HLN/BLENG)*FLOA'NRX-1)+1.5
NRXN=NRXN-1
DO 6110 I=1,NRXN
XIM=I-1
RX(I,1)=(XIM/XNRX)*BLN
XNRX=NRXN-1
DO 6120 I=2,NRXR
XIM=I-1
J=NRXN+I-1
RX(I,J)=BLN+(XIM/XNRX)*BLR
INDEX=NRXN
C
6150 CONTINUE
C
THE X VALUES ARE NOW IN THE RX ARRAY.
C
THE RADIUS FOR EACH GIVEN STATION STARTS IN RZ(1,1).
C
THE Z-COORD. OF CENTROID FOR EACH STA STARTS IN RZ(1,2)
C
INTERPOLATE TO GET R,Z CORRESPONDING TO X-VALUES IN RX.
C
MU = 32
DO 6300 I=1,NRX
C
DO 6250 J=1,2
CALL BITURP(STA,RZ(1,J),1,NSTA,KDEBR,RX(1,1),RX(J*1,1),NU)
IF(NU)A000,6250,6200
6200 IF(NU-2)6250,6250C,8000
6250 CONTINUE
C
6300 CONTINUE
C
WRITE RECORDS 2,2
WRITE(LB)NRX,INDEX
WRITE(LB) (RX(I,J),I=1,3),J=1,NRX)
C
END FILE LB
REWIND LB
C
WRITE(LO,6400) DAT,(J,(RX(I,J),I=1,3),J=1,NRX)
6400 FORMAT(1H1 53X 2A6/38H BODY RADIUS AND Z-COORDINATE OF BODY
,23HCENTROID VERSUS X-PRIME/5HO NO. 1OX 7HX-PRIME 18X
,6HRAIDUS 13X 7HZ-PRIME /1H 13,F18.4,F24.4,F20.4))

```

```

C
C      IOK=0
      IF(BODY .AND. .NET. WING) NBODY=-1
      GO TO 9000
      ,293
      ,294
      ,295
      ,296

C      ERROR. SKIP OVER DATA CARDS TO NEXT CASE, OR
C      UNTIL END OF DATA CARD IS FOUND
      8000 CONTINUE
      IOK=MU
      ,297
      ,298
      ,299
      ,300
      ,301
      ,302
      ,303
      ,304
      ,305
      ,306

      8005 WRITE(LO,8010)MU,NU(1),(IREC(1),I=1,4)
      ,307
      ,308
      ,309
      ,310
      ,311

      8010 FORMAT(/12H0TFLAT ERKOR I3,7H, CODE I3,
      1 /7H IREC = 4110)
      IF(MU .LT. 14 .OR. MU .GT. 18) GO TO 8100
      WRITE(LO,8020)
      8020 FORMAT(45H0TRANSFORMED WING (BEFORE FLATTENING) FOLLOWS )
      CALL TFLATW(NWPCL,WTITL,DAT,LO)
      ,312
      ,313
      ,314
      ,315

C      8100 READ(11,8110)KIND
      8110 FORMAT(A6)
      ,316
      ,317
      ,318
      ,319
      ,320

      DO 8200 I=1,3
      IF(KIND-NAME(I))8200,8300,8200
      8200 CONTINUE
      GO TO 8100

C      8300 BACKSPACE LI
C
      9000 CONTINUE
      DO 9100 J=1,6
      DO 9100 I=1,3
      9100 LGDEF(I,J) = .FALSE.
      ,321
      ,322
      ,323
      ,324
      ,325
      ,326
      ,327
      ,328
      ,329

      END

```

```

C SURROUTINE TFLAT1(CHO,NSTA,STA,NBPCT,B,S,E,RT,ALFBET,RZ,EPRC,NU)
C
C DIMENSION RZ(51,2),STA(51),B(2448),RT(3,4),ALFBET(2),NU(3),S(100,2
C ,),E(2000),EP(5),SENO(3,2),AREA(2),PAD(2),UNITZ(3)
C
C USED BY TFLAT TO TRANSFORM BODY MERIDIAN LINES TO A
C NEW COORDINATE SYSTEM WITH ORIGIN AT THE CENTROID OF
C THE FIRST BODY SECTION. THE NEW +X AXIS PASSES THRU
C THE CENTROID OF THE LAST BODY SECTION.
C IT IS ASSUMED THAT BODY MERIDIAN LINES ARE GIVEN FOR A HALF-BODY
C AND THAT THE BODY IS SYMMETRICAL ABOUT A PLANE PARALLEL TO THE
C XZ PLANE.
C TRANSFORMED BODY MERIDIAN LINES ARE SCALED (INDIVIDUALLY) SO
C THAT 1ST PT IN EACH LINE HAS X=0 AND EACH LINE HAS SAME
C X-LENGTH (LENGTH BETWEEN END CENTROIDS).
C
C INPUTS ARE
C CHO = CHORD-HEIGHT TOLERANCE. TO FIND THE CENTROID
C OF A BODY SECTION, WE CUT EACH MERIDIAN LINE WITH THE
C X-VALUE OF THE SECTION. THIS GIVES US A POLYGON OF THE
C SECTION IN 2-DIMENSIONS (Y,Z). IF CHO.GT.0, WE THEN
C INTERPOLATE ADDITIONAL POINTS ON THE POLYGON TO BETTER
C APPROXIMATE A SMOOTH BODY. CHO IS USED BY S/R ENRYCH.
C
C NSTA = NO. OF STATIONS
C NBPCT = NO. OF BODY MERIDIAN LINES
C
C INPUT-OUTPUTS ARE
C STA = ARRAY OF BODY STATIONS. ON OUTPUT, SCALED TO AGREE
C WITH TRANSFORMED BODY.
C B = ARRAY OF BODY MERIDIAN LINES (WITH HEADER).
C EPRC IS USED BY BODCR TO SET Z-CENTROID AND RADIUS =0 IF .LE. EPRC.
C
C OUTPUTS ARE
C RT = ROTATION, TRANSLATION MATRIX OF THE TRANSFORMATION
C FROM ORIGINAL SYSTEM TO NEW SYSTEM.
C COL. 1 IS UNIT VECTOR ALONG NEW +X AXIS
C COL. 2 IS UNIT VECTOR ALONG NEW +Y AXIS
C COL. 3 IS UNIT VECTOR ALONG NEW +Z AXIS
C COL. 4 IS ORIGIN OF NEW XYZ SYSTEM
C
C ALL WITH RESPECT TO ORIGINAL XYZ SYSTEM
C ALFBET = PAIR OF CONSTANTS USED TO RELATE OLD STATION
C VALUES TO NEW.
C NEW X = ALFBET(1)*(OLD X)+ ALFBET(2)
C RZ = ARRAYS OF BODY RADIUS AND Z-COORD. OF CENTROID AT
C EACH BODY STATION
C
C SCRATCH ARRAYS ARE S, E
C
C DATA EP/5=.005/
C EP(5)=ARSTEPCT)
C
C SENO (BODY ENDS) ARRAY WILL BE COORD. OF CENTROIDS
C OF THE END SECTIONS OF THE BODY
C
C 100 SENO(1,1)=STA(1)
C SENO(1,2)=STA(NSTA)
C
C FIND EQUIV. RADIUS AND CENTROID OF BODY END SECTIONS

```

,1
 ,2
 ,3

IFLATT
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S) 07/31/65

```

200 DO 200 I=1,2
C MU=1
C CALL BODCR(9,NBPT,BEND(1,1),EP,CHD,2000,S(1,1),E,NE,
C ,BEND(2,1),BEND(3,1),AREA(1),RAD(1),NU)
C IF(NU)8000,200,8000
C 200 CONTINUE
C
C FIND TRANSFORMATION MATRICES TO NEW SYSTEM
C BLEN=UVECN(BEND,BEND(1,2),RT,0,3)
C DATA UNITZ/0.,0.,1./
C IZXP=1
C CALL VCPDS(UNITZ,RT,RT(1,2),NZXP,IZXP)
C IXPDP=1
C CALL VCPDS(RT,RT(1,2),RT(1,3),DXPYP,IXPYP)
C MU=3
C IF(PLENG.EQ.0..OR..IZXP.NE.0..OR..IXPYP.NE.0) GO TO 8000
C CALL TRAVRT(1,4),BEND,3)
C RT = TRANSFORMATION ARRAY IS COMPLETE.
C BLEN = LENGTH OF BODY ALONG NEW X AXIS
C
C TRANSFORM BODY MERIDIAN LINES TO NEW SYSTEM
C 500 CALL TRAPCT(8,NBPT,RT)
C
C NOW SCALE SO ALL MERIDIAN LINES WILL START AT
C X=0, END AT X=BLENG.
C MU=4
C CALL BSCALE(8,NBPT,BLENG,NU)
C I=(NU)8000,1000,8000
C
C SCALE BODY STA ARRAY TO CORRESPOND TO NEW COORD. SYSTEM
C 1000 MU=5
C O=STAINSTA)-STA(1)
C IF(D)1200,8000,1200
C 1200 ALFBET(1)=BLENG/D
C ALFBET(2)=-ALFBET*STA(1)
C DO 1250 I=1,NSTA
C 1250 STA(I)=ALFBET*STA(1)+ALFBET(2)
C
C FIND RADIUS AND Z-COORD. OF CENTROID AT EACH STATION.
C 2000 MU=6
C DO 2100 I=1,NSTA
C CALL BODCR(8,NBPT,STA(1),EP,CHD,2000,S,E,NE,
C ,Y,RZ(1,2),A,RZ(1,1),NU)
C IF(NU)8000,2100,8000
C 2100 CONTINUE
C
C NU=0
C GO TO 9000
C
C ERROR
C 9000 CONTINUE
C LTAP=NU(2)
C IF(LTAP.LE.0)GO TO 8500
C WRITE(LTAP,8100)MU,NU(1)

```


INTERNAL FORMULA NUMBER		SOURCE STATEMENT		INTERNAL FORMULA NUMBER(S)	
IFLATT					
3100	FORMAT(13H)FLATT	FOR	13,7H, CODE 13,5X		
1	4SPRALLURE	IN	TRANSFORMING BODY MERIDIAN LINES, ETC.)		
15	(U,NF, 6100 TO 8500				
3200	WRITE(LTAP, P200)STA(1)			148, 149, 150	
8500	FORMAT(18H) STATION F10.4)			151, 152, 153	
C	9000	RETURN		154, 155, 156	
		END			

TFLATM

EXTERNAL FORMULA NUMBER - SOURCE STATEMENT -

C SAME AS BODYIM EXCEPT DOES NOT IDENTIFY POINTS WHICH LIE
C IN A BODY DEFINING SECTION.

C USED BY TFLAT TO PRINT BODY MERIDIAN LINES.
C ALSO COMPUTES RHO, THETA FOR EACH POINT.
C THE RHO, THETA ORIGIN IS ON BODY AXIS.

C SUBROUTINE TFLATM(B,NB,AXIS,TITLE,DAYT,LO,STA)

C DIMENSION B(1),AXIS(2),TITLE(12),DAYT(2),STA(1),XYZ(3)
C LOGICAL NEWPCT,TITLE
C DATA MAXLIN,DEGRAD/45,0206712273406/

C B IS ARRAY OF NB MERIDIAN LINES, HEADED BY INDEX.
C STA IS ARRAY OF BODY STATIONS (NOT USED BY TFLATM)
C MAXLIN = MAX NO. OF LINES PER PAGE
C MAXEL IS MAX NO. OF XYZ ELEMENTS THAT WILL GO ON A PAGE,
C ASSUMING NO HEADINGS. WE ALLOW FOR HEADINGS LATER.

C MAXEL=3*(MAXLIN-2)
C NELREM=0

C DO 4000 K=1,NB
C WORKING ON KTH MERIDIAN LINE
C JK=3*K
C NPTS=B(JK-1)
C LOCST=B(JK)

C LOCEND=LOCST+3*NPTS-1
C THE X OF THE FIRST POINT IN THE MERIDIAN LINE IS
C IN B(LOCST).
C THE Z OF THE LAST POINT IS IN B(LOCEND).
C FOR PAGE CONTROL WE WRITE A BLOCK OF POINTS FROM
C B(1A) TO B(1B).

C LA=LOCST
C NEWPCT=.TRUE.
C ISTA=1

C WE KEEP COMING BACK TO HERE UNTIL ALL POINTS ARE WRITTEN

C 200 NELREM=NELREM-9
C THIS ALLOWS FOR LEADING
C IF(NELREM-6)300,400,400

C NOT ENOUGH ROOM FOR 2 POINTS, SO WILL START NEW PAGE
C 300 WTITLE=.TRUE.

C NELREM=MAXEL-6
C GO TO 500

C 400 WTITLE=.FALSE.

C 500 LB=MINO (LOCEND,LA+NELREM-1)
C NL=(LB-LA+1)/3
C IF(.NOT. WTITLE) GO TO 600
C WRITE(10,550)TITLE,DAYT

550 FORMAT(11H1 12A6/54X 2A6)

600 IF(NEWPCT) GO TO 700

,1
,2
,3
,4
,5
,6

,7
,8
,9

,10
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,23
,24

TFLATM		09/14/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	-	INTERNAL FORMULA NUMBER(S)
C	WRITE HEADING		
	WRITE(LO,650)K		.25 .26 .27
650	FORMAT(19H0BODY PERIDIAN LINE 14,14H (CONTINUED))		.28 .29 .30
	GO TO 800		
700	WRITE(LO,750)K		.31
750	FORMAT(19H0BODY PERIDIAN LINE 14)		.32 .33 .34
	NUM=0		
800	WRITE(LO,850)		.35
850	FORMAT(14X1HX10X1HY10X1HZ12X3HR07X5HTheta)		.36 .37
C			
C	READY TO WRITE PCINTS, COMPUTING RHO-THETA AS WE GO		
	DO 2000 L=1,NL		.38
	NUM=NUM+1		.39
	CALL TRAV(XYZ,B(LA),3)		.40
	DY=XYZ(2)-AXIS(1)		.41
	DZ=XYZ(3)-AXIS(2)		.42
	RHO=SQRT(DY*DY+DZ*DZ)		.43
	IF(RHO)1100,1100,1200		.44
1100	THETA=0.		.45
	GO TO 1300		.46
1200	THETA = ATN1(ABS(DY),DZ)*DEGRAD		.47
C			
1300	CONTINUE		
C			
1500	WRITE(LO,1550)NUM,XYZ,RHO,THETA		.48 .49 .50 .51
1550	FORMAT(14,4X,3F11.4,3X,2F11.4)		.52
	LA=LA+3		
2000	CONTINUE		.53 .54
C			
	NELREM=NELREM-3*NL		.55
	IF (ILB-LOCEND)3000,4000,4000		.56
3000	NEWPC=.FALSE.		.57
	LA=LB+1		.58
	GO TO 200		.59
C			
4000	CONTINUE		.60 .61
C			
	RETURN		.62
	END		.63

IFLAW		09/14/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	-	INTERNAL FORMULA NUMBER(S)
700	WRITE(LO,750) K,PCT		,33 ,34 ,35
750	FORMAT(24,ROWING PERCENT CHORD LINE 13,1H,F9.4)		
	NUM=0		,36
800	WRITE(LO,850)		,37 ,38
850	FORMAT(14X 1HX 1CX 1HY 10X 1HZ)		
C			
C	READY TO WRITE PCINTS		
	GO 2000 L=L.NL		,39
	NUM=NUM+1		,40
	CALL TRAV(XYZ,8(LA),3)		
C			,41
	WRITE(LO,1550)NUM,XYZ		,42 ,43 ,44
1550	FORMAT(1H 13,4X,2F11.4)		
	LA=LA+3		,45
C			
2000	CONTINUE		,46
C			,47
	NELREM=NELREM-3*AL		,48
	IF(L8-LOCEND)3000,4000,4000		,49
3000	NEPCT=-.FALSE.		,50
	LA=L8+1		,51
	GO TO 200		,52
C			
4000	CONTINUE		,53
C			,54
	RETURN		,55
	END		,56

TFLATX
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
09/14/65

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SUBROUTINE TFLATX(LO,DAT,NW,W,WB,NU)
C
C USED BY TFLAT TO PRINT WING-BODY INTERSECTIONS.
C ADAPTED FROM PART OF WBXUL
C W = ARRAY OF WING PERCENT LINES (WITH HEADER)
C WB = ARRAY OF WING-BODY INTERSECTION POINTS
C NW = NO OF WING PERCENT LINES
C
C DIMENSION DAT(2),W(1),WB(1),PT(3),BAXIS(2)
C
C DATA BAXIS/0.,0./,DEGRAD/0206712273406/
C
C NU=0
C WRITE(LO,100)DAT,BAXIS
100 FORMAT(1H1 53X 2A6/23H INTERSECTIONS OF FLAT
C , 42H WING PERCENT CHORD LINES WITH BODY SURFACE /
C , 41H RHO-THETA ORIGIN IS LOCATED AT (Y,Z) = ( F9.4,1H,F9.4,1H)/
C , 21H (PRIMED-AXIS SYSTEM)/
C , 13H CND. PERCENT 6X 1HX 9X 1HY 9X 1HZ 10X 3HRHO 6X 5H THETA//)
C
C IPCT=1
C IWBX=1
C
C DO 1000 J=1,NW
C   PCT=W(IPCT)
C   IPCT=IPCT+3
C   CALL TRAV(PT,WB(IWBX),3)
C   IWBX=IWBX+3
C   IF(PT.GT. 1.E+25) GO TO 900
C   DY=PT(2)
C   DZ=PT(3)
C   RHO=SQRT(DY*DY+DZ*DZ)
C   IF(RHO)820,820,830
C   THETA=0.
C   GO TO 850
C   THETA=ATN1(ABS(DY),DZ)*DEGRAD
C   WRITE(LO,860)J,PCT,PT,RHO,THETA
C   860 FORMAT(1H 12,F10.4,1X 3F10.4,2X 2F10.4)
C   GO TO 1000
C   900 WRITE(LO,910)J,PCT
C   910 FORMAT(1H 12,F10.4,6X 15HND INTERSECTION)
C   NU=1
C   1000 CONTINUE
C
C RETURN
C END

```

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17	18	19	20
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```

SUBROUTINE THETAB
COMMON DATE(2),NTAPE1,ND1,NTAPE2,ND2(3),NREAD,
1,NWRITE,NBODY,NWING,XMACH,SYM,KACE
COMMON /COM1/ KOBEB,KODEW,KODEWU,KODEI,KODEC,XPER,YPER,KOPTB,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER,NPERI
2,NPLANE,NPLN1
COMMON /COM2/ NPLNB,NPLNW,JLEAD,JTRAIL,IMID,NPTS(16),X(16,90),Y(16
1,90),Z(16,90),XCEPT(21),XCEPTW(16),YCEPTW(16),ZCEPTW(16
2),CODEBW(16),KPAEL(15,20),XCOR(16,21),YCOR(16,21),ZCOR(16,21),XIN
3(15,20,2),YINT(15,20,2),ZINT(15,20,2),XCEN(15,20),YCEN(15,20),ZCE
4N(15,20),XCON(15,20),YCON(15,20),ZCON(15,20),AREA(15,20),ARAT(15,2
50),THETA(15,20),ALPHA(15,20),CHORD(15,20)
DIMENSION C(4),P(3,5),Q(3,5),LOC(3)

```

C SUBROUTINE TO CALCULATE BODY PANEL
C THETA ANGLES

C DEFINE FUNCTIONS TO BE USED IN CALCULATIONS
C DETR CALCULATES MATRIX DETERMINANT
C ANGL CALCULATES THETA-INCLINATION ANGLE USING
C ARCCOSINE FUNCTION ROUTINE
C DETR(A1,A2,A3,B1,B2,B3)=A1*(B2-B3)-A2*(B1-B3)+
1A3*(B1-B2)
C ANGL(C1,C2)=ACOS(C1/SQRT(C1*C1+C2*C2))

C DEFINE CONSTANTS
E=0.001
F=0.000001

C CALCULATE PANEL THETA ANGLES
50 DO 70 I=1,NPERI
70 65 J=1,NPLN1
55 IF (ABS(ZCOR(I+1,J+1)-ZCOR(I,J+1))-F) 55,55,60
60 THETA(I,J)=0.
GO TO 65
C1= DETR(XCOR(I,J),XCOR(I,J+1),XCOR(I+1,J+1),
1YCOR(I,J),YCOR(I,J+1),YCOR(I+1,J+1))
C2=-DETR(XCOR(I,J),XCOR(I,J+1),XCOR(I+1,J+1),
1ZCOR(I,J),ZCOR(I,J+1),ZCOR(I+1,J+1))
THETA(I,J)=(ZCOR(I+1,J+1)-ZCOR(I,J+1))/
1ABS(ZCOR(I+1,J+1)-ZCOR(I,J+1))*ANGL(C1,C2)
65 CONTINUE
70 CONTINUE
100 RETURN
END

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TRAPCT 07/31/65
 INTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

SUBROUTINE TRAPCT(R,N,RT)
  DIMENSION R(3,1),RT(3,4)
  C
  C GIVEN AN ARRAY R OF N BODY MERIDIAN LINES OR WING PERCENT LINES,
  C (WITH A HEADER WHICH DESCRIBES EACH PERCENT LINE), APPLY THE
  C TRANSFORMATION RT TO EACH POINT.
  C
  C 1ST POINT (X,Y,Z) STARTS IN R(1,N+1).
  J=N+1
  C
  C NPT = TOTAL NO. OF POINTS IN R.
  NPT=0
  DO 100 I=1,N
    NP=R(2,I)
    NPT=NPT+NP
  100 CONTINUE
  C TRANSFORM TO NEW COORD. SYSTEM
  DO 200 I=1,NPT
    CALL TRAPCT(RT,PT(1,4),2,B(1,J),B(1,J))
    J=J+1
  200 CONTINUE
  C
  RETURN
  END
  1 2 3 4 5 6 7 8 9 10 11 12

```


TRAV		07/31/65
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
	SUBROUTINE TRAV(A,B,N)	
	DIMENSION A(1),R(1)	
C	DO 100 I=1,N	1
	A(I)=R(I)	2
100		3
C	RETURN	4
	END	5

TROPT
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

```

SUBROUTINE TROPT(R,T,N,P,Q)
  DIMENSION R(3,3),T(3),P(3),Q(3),A(3)
  TRANSLATION AND ROTATION OF A POINT
  P IS A POINT (X,Y,Z) IN FIRST SYSTEM, Q IN 2ND
  N = 1 IF Q GIVEN, P WANTED. N = 2 IF P GIVEN, Q WANTED
  R AND T ARE ROTATION, TRANSL. MATRICES TO MAP Q INTO P
  P = R Q + T
  IF (N-1)/20, 1,20
    1 DO 5 I=1,3
    5 A(I)=Q(I)
    10 DO 15 I=1,3
    15 U=0.
    DO 12 J=1,3
    12 U=U+R(I,J)*A(J)
    15 P(I)=U+T(I)
    GO TO 50
    20 DO 25 I=1,3
    25 A(I)=P(I)-T(I)
    DO 40 I=1,3
    40 U=0.
    DO 30 J=1,3
    30 U=U+R(J,I)*A(J)
    40 Q(I)=U
    50 RETURN
  END
  
```

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05/22/67

TTAPE - EFN SOURCE STATEMENT - IFM(S) -

```

SUBROUTINE YTAPE(KIND,IN,JN,NTIN,NTOUT,A,B,C)
  DIMENSION A(1),B(1),C(1)
  IF(KIND)50,50,150
50 CONTINUE
  DO 100 J=1,JN
    READ(NTIN)(A(I),I=1,IN)
    100 WRITE(NTOUT)(A(I),I=1,IN)
    GO TO 250
150 CONTINUE
  DO 200 J=1,JN
    READ(NTIN)(A(I),B(I),C(I),I=1,IN)
    200 WRITE(NTOUT)(A(I),B(I),C(I),I=1,IN)
  250 CONTINUE
  RETURN
  END

```

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05/22/67

TVEL - EFN SOURCE STATEMENT - IFN(S) -

```

SUBROUTINE TVEL(A,B,C,D,ALPHAT,UBWT,VBWT,WBWT,UMWT,VWMT,WVMT,AM,
$CHORD,THICK,NROW)

```

```

C COMPUTE VELOCITY COMPONENTS INDUCED BY WING SOURCES

```

```

COMMON DATE(2),NTAPEA,NTAPEB,NTAPEC,NTAPEE,NTAPEF,NTAPEI
1,NTAPEO,NBODY,NWING,NMACH,SYM,KACE

```

```

DIMENSION A(1),B(1),C(1),D(1),ALPHAT(1),UBWT(1),VBWT(1),WBWT(1),
1UMWT(1),VWMT(1),WVMT(1),AM(1),NROW(1),CHORD(1)
DIMENSION ATLE(20),TSL(2)
DATA TSL/SHGIVEN,SHGIVEN/

```

```

NS=NBODY+1
NPANEL=NBODY+NWING

```

```

IF (NBODY .EQ. 0) GO TO 95
DO 90 J=1,NBODY
  UMWT(J)=0.
  VWMT(J)=0.
  WBWT(J)=0.
  ANIJ)=0.

```

```

90 CONTINUE
95 DO 100 J=1,NWING
  UMWT(J)=0.
  VWMT(J)=0.
  WBWT(J)=0.
100 CONTINUE

```

```

GO TO (110,500,120),KACE
110 NC=NWING/NROW(1)
NR=NROW(1)
GO TO 130
120 NC=NWING/NROW(2)
NR=NROW(2)
130 N=0
NWING=NWING+NC

```

```

IGD=INTURP(TSL,2,NTAPEI,NTAPEO)
IGD=IGD+1
GO TO (132,136,136),IGD

```

```

C INPUT THICKNESS SLOPES
132 READ (NTAPEI,6000) (A(I),I=1,NWING)
IJ=0
NRI=NR+1
DO 134 J=1,NC
  J1=(J-1)*(NR+1)
  ATLE(J)=A( J1+1)
  DO 133 I=2,NRI
    IJ=IJ+1
    TJI=I+J1
    ALPHAT(IJ)=A(IJ1)

```

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05/22/67

TYEL - EFN SOURCE STATEMENT - IFM(S) -

133 CONTINUE
134 CONTINUE
GO TO 140

C USE PREVIOUSLY CALCULATED PANEL SLOPES
C AND COMPUTE LEADING EDGE SLOPES

136 CALL FSF(1,NTAPEC,IPR)
READ (NTAPEC) (ALPHAT(I),I=1,NWING)

REWIND NTAPEC

NR1=NR-1

DO 138 J=1,NC

J1=(J-1)*NR

JN=NR*DY+J1

AT=-ALPHAT(J1+1)

DO 137 I=1,NR1

IJ=J1+I

IJN=NR*DY+IJ

AT=AT-(ALPHAT(IJ)+ALPHAT(IJ+1))*CHORD(IJN+1)/

-CHORD(IJN+1)

137 CONTINUE

ATLE(IJ)=AT

138 CONTINUE

140 CONTINUE

CALL FSF(8,NTAPEC,IPR)

WRITE (NTAPEC) NWING

DC 200J=1,NWING

READ (NTAPEC) (D(I),I=1,NPANEL)

READ (NTAPEC) (A(I),B(I),C(I),I=1,NPANEL)

JT=J-N*(NR+1)

IF (JT) 160,160,150

150 N=N+1

WT=ATLE(N)

GO TO 170

160 JN=J-N

WT=ALPHAT(JN)

170 CONTINUE

WRITE (NTAPEC) WT

DO 180 I=1,NPANEL

IF (I-CT-NBODY) GO TO 180

UBWT(I)=UBWT(I)+A(I)*WT

VBWT(I)=VBWT(I)+B(I)*WT

WBWT(I)=WBWT(I)+C(I)*WT

AN(I)=AN(I)+D(I)*WT

GO TO 190

180 IN=I-NBODY

UWWT(IN)=UWWT(IN)+A(I)*WT

VWWT(IN)=VWWT(IN)+B(I)*WT

MWWT(IN)=MWWT(IN)+C(I)*WT

190 CONTINUE

200 CONTINUE

500 CONTINUE

END FILE NTAPEC

REWIND NTAPEC

RETURN

6000 FORMAT (7F10.0)

END

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UF00L
 7094 RELMOD ASSEMBLY.
 07/31/65
 \$IRLOR UF00L
 ASSEMBLED TEXT.
 \$TEXT UF00L
 UF000000
 UF000001
 ASSEMBLED 26 JAN 65

BINARY CARD (NOT PUNCHED)
 000000 0020 00 4 00001 10000 F00L TRA 1,4
 *
 00000 01111
 CONTROL DICTIONARY
 \$C0ICT UF00L
 UF000002

BINARY CARD (NOT PUNCHED)
 000001000000
 0000004000005
 642646464360
 000001000000
 264646436060
 000000000000
 312646464360
 000000000000
 PREFACE START=0,LENGTH=1,TYPE=7094,CNPLX=5
 UF00L DECK LOC=0,LENGTH=1
 F00L REAL LOC=0,LENGTH=0
 IF00L REAL LOC=0,LENGTH=0

\$OKEND UF00L
 UF000003

NO MESSAGES FOR THIS ASSEMBLY
 SYMBOL REFERENCE DATA

REFERENCES TO DEFINED SYMBOLS.

CLASS	SYMBOL	VALUE	REFERENCES
F00L	00000		
LOC	31264		
REAL	UNDS		
LOC	//		

UN07
7094 REL400 ASSEMBLY.

07/31/65

\$13L08 UN07

\$FILE UN07

IUNIT07I,C(1),READY,NOLIST,INOUT,RLK=256,HIGH,8 IN

UN070300

UN070301

UN08	07/31/65	
7094 RELMD ASSEMBLY.		
\$IRLDR UN08		UN080000
\$FILE UN08	UNIT081,C(2),READY,NGLIST,INDUT,BLK=256,HIGH,BIN	UN080001

UN09
7094 RELMOD ASSEMBLY.

08/16/65

\$19LDR UN09

UN090000

\$FILE UN09

IUNIT09I,A(1),READY,NOLIST,INOUT,9LK=14,HIGH,BCD

UN090001

UPDATE
70094 RELMOD ASSEMBLY.

07/31/65

\$136DR UPDATE
ASSEMBLED TEXT.

UPDA0300

TEXT UPDATE

UP7A0301

```
#UPDATE      MICHAEL SYNGE      6-9247      ASSEMBLED  21 SEP 64
#           TO UPDATE THE CONTENTS OF AN ARRAY NAME WHEN THE
#           ARRAY IS MOVED (E.G. BY PACKING).
```

CALLING SEQUENCE

CALL UPDATE(RUF(M-1))

WHERE M IS THE FIRST WORD OF THE ARRAY
(AFTER MOVING) IN THE BUFFER BUF .

ENTRY UPDATE

✱

BINARY	CARD	(NOT PUNCHED)	UPDATE	CLA*	3,4 NAME
0000	0500	50 4 00003	10000	STA	3,4
00001	0621	00 0 00007	10001	CLA	3,4
00002	0500	00 4 00003	10000	SUB	=1
00003	0402	00 0 00011	10001	STA	**1
00004	0621	00 C 01001	10011	CLA	**
00005	0500	00 0 00000	10000	ANA	=077777
00006	4320	00 0 00012	10001	STA	**
00007	0621	00 0 00000	10000	TRA	1,4
00010	0020	00 4 00001	10000	*	
00011	000000000001		10000	*LORG	
00012	000000077777		10000	END	
	00000		0111		

```

BINARY CARD {NOT PUNCHED}
0000013000000
00000000000005
644724216325
000013000000
000013000000
644724216325
0000000000000
0000000000000

PREFACE
UPDATE DECK
UPDATE REAL

START=0,LENGTH=11,TYPE=7094,CMLPX=5
LOC=0,LENGTH=11
LOC=0,LENGTH=0

```

\$DKEND UPDATE

NO MESSAGES FOR THIS ASSEMBLY

07/31/65

UPDATE
SYMBOL REFERENCE DATA

REFERENCES TO DEFINED SYMBOLS.

CLASS	SYMBOL	VALUE	REFERENCES
LCIR	NAME	00007	1
QUAL	SLCTR		
LCIR	UNOS		
	//		
	UPDATE	00000	

05/22/67

USETAP - EFN SOURCE STATEMENT - IFN(S) -

```

SURROUTINE USETAP
COMMON DATE(2),NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI
1,NTAPEQ,NBODY,NWING,XMACH,SYM,KACE
DIMENSION A(210),B(210),C(210)
DIMENSION DUM(10),NROW(2)
READ(NTAPEC,NBODY,NWING,XMACH,SYM,KACE
GO TO ( 50,900, 50),KACE
50 NPAPEL=NBODY+NWING
READ (NTAPEC) (1,(DUM(J),J=1,10),I=1,NPAPEL),NRG,
1(NROW(I),I=1,NRG),DUMMY
NCOLW=NWING/NROW(NRG)
CALL PSFT 6,NTAPEC,IRR)
GO TO (100,900,200),KACE
100 CONTINUE
CALL TTAPE(0,NWING,NWING+NCOLW,NTAPEC,NTAPEA,A,B,C)
END FILE NTAPEA
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEA,A,B,C)
END FILE NTAPEA
CALL TTAPE(0,NWING+1,NWING+1,NTAPEC,NTAPEA,A,B,C)
END FILE NTAPEA
CALL TTAPE(0,NWING+2,NWING+2,NTAPEC,NTAPEA,A,B,C)
END FILE NTAPEA
REWIND NTAPEA
CALL TTAPE(1,NWING,NWING+NCOLW,NTAPEC,NTAPEB,A,B,C)
END FILE NTAPEB
CALL TTAPE(1,NWING,NWING,NTAPEC,NTAPEB,A,B,C)
END FILE NTAPEB
REWIND NTAPEB
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEE,A,B,C)
END FILE NTAPEE
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEE,A,B,C)
END FILE NTAPEE
REWIND NTAPEE
GO TO 900
200 CONTINUE
CALL TTAPE(0,NPAPEL,NWING +NCOLW,NTAPEC,NTAPEA,A,B,C)
END FILE NTAPEA
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEA,A,B,C)
END FILE NTAPEA
CALL TTAPE(0,NWING+1,NWING+1,NTAPEC,NTAPEA,A,B,C)
END FILE NTAPEA
CALL TTAPE(0,NWING+2,NWING+2,NTAPEC,NTAPEA,A,B,C)
END FILE NTAPEA
REWIND NTAPEA
CALL TTAPE(1,NPAPEL,NWING +NCOLW,NTAPEC,NTAPEB,A,B,C)
END FILE NTAPEB
REWIND NTAPEB
CALL TTAPE(1,NBODY,NBODY,NTAPEC,NTAPED,A,B,C)
END FILE NTAPED
CALL TTAPE(1,NWING,NBODY,NTAPEC,NTAPED,A,B,C)
END FILE NTAPED
CALL TTAPE(1,NBODY,NWING,NTAPEC,NTAPED,A,B,C)
END FILE NTAPED
  
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CALL TTAPE(1,NWING,NWING,NTAPEC,NTAPE,A,B,C)
END FILE NTAPED
REWIND NTAPED
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEE,A,B,C)
END FILE NTAPEE
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEE,A,B,C)
END FILE NTAPEE
REWIND NTAPEE
CALL TTAPE(0,NWING,NBODY,NTAPEC,NTAPEF,A,B,C)
END FILE NTAPEF
CALL TTAPE(0,NBODY,NBODY,NTAPEC,NTAPEF,A,B,C)
CALL TTAPE(0,NBODY,NWING,NTAPEC,NTAPEF,A,B,C)
END FILE NTAPEF
REWIND NTAPEF
900 CONTINUE
REWIND NTAPEC
RETURN
END

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UVECN 07/31/65 INTERNAL FORMULA NUMBER(S)

```

C      FUNCTION UVECN(A,B,V,K,N)
C      DIMENSION A(1),B(1),V(1)
C      GIVEN VECTORS A,B
C      FIND DISTANCE (= UVECN) FROM A TO B.
C      IF DISTANCE NOT ZERO AND K=0, FIND V, A UNIT
C      VECTOR FROM A TOWARD B.
C      OTHERWISE, V=B-A.
C
C      D=0.
C      DO 100 I=1,N
C      V(I)=B(I)-A(I)
C      D=D+V(I)**2
C      100
C      IF (D)500,500,200
C      D=SQR(D)
C      IF (K)500,300,500
C      DO 400 I=1,N
C      V(I)=V(I)/D
C      400 UVECN=D
C      RETURN
C      END

```

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SUBROUTINE VCROSS(A,B,C,D,K)
DIMENSION A(3),B(3),C(3),X(3),Y(3),Z(3)
FINDS THE CROSS PRODUCT, VECTOR C, OF VECTORS A AND B.
C = A X B. IF K NOT 0 THEN C IS NORMALIZED. =0, NOT.
D = MAGNITUDE OF C BEFORE NORMALIZED.
ON OUTPUT, K=0 IF SUCCESS, =1 IF NORM. REQUESTED BUT 0=0.
C MAY BE STORED IN A OR B IF DESIRED.

```

DO 10 I=1,3
  X(I)=A(I)
  Y(I)=B(I)
  Z(I)=X(2)*Y(3)-X(3)*Y(2)
  Z(2)=X(3)*Y(1)-X(1)*Y(3)
  Z(3)=X(1)*Y(2)-X(2)*Y(1)
  D=E=SQRT (VDOTP(Z,Z))
  IF (K)20,50,20
  20 IF (E)40,30,40
  30 K=1
  40 K=0
  50 E=1.
  100 DO 110 I=1,3
  110 C(I)=Z(I)/E
  RETURN
END

```

VDOTN
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
 07/31/65

```

C      FUNCTION VDOTN(A,B,N)
        DIMENSION A(N),B(N)
        DOT PRODUCT OF TWO VECTORS IN N-SPACE
        VDOTN=0.
        DO 100 I=1,N
          VDOTN=VDOTN+A(I)*B(I)
        RETURN
      END
    100
  
```

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VDOTP
 EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

07/31/65

FUNCTION VDOTP(P,Q)

DIMENSION P(3),Q(3)

FINDS THE DOT PRODUCT OF VECTORS P AND Q

VDOTP=P*Q+P(2)*Q(2)+P(3)*Q(3)

RETURN

END

+1
 +2
 +3

06/02/67

VEL1 - EFM SOURCE STATEMENT - IFM(S) -

```

SUBROUTINE VEL1(XC,YC,ZC,U,VV,MW)
  ACOSH(U)=2.*ALOG(SQRT(ABS((U+1.)/2.))+SQRT(ABS((U-1.)/2.)))
  COMMON /FLOV1/KACE,NPANEL,NBODY,NHING,NBODYS,NWINGS,NROW,XMACH,SYM
  COMMON /FLOV2/A,B,C,NPART,ALPHAS,THETA,XB,R,WT,T,TC,SST,CHORD
  COMMON /FLOV3/T11,TC11
  DIMENSION A(210,3,4),B(210,3,4),C(210,3,4),NROW(2),NPART(210)
  DIMENSION ALPHAS(210),THETA(210)
  DIMENSION XB(50),RI(50),WT(120)
  DIMENSION T(50),TC(50),SST(210),CHORD(210)
  DIMENSION XC(1),YC(1),ZC(1),U(1),V(1),W(1),MW(1)
  COMMON /THICK/THK,M,ARA
  BT2 = XMACH*XMACH - 1.
  BETA = SQRT(BT2)
  PI=3.1415926
  N1 = NBODYS-1
  I = 1
  THETA=ATN1(YC(1),ZC(1))
  COSTHA=COS(THETA)
  SINTHA=SIN(THETA)
  R2=YC(1)**2+ZC(1)**2
  R1=SQRT(R2)
  R2=BT2+R2
  RI=1
  U(1) = 0.
  VS=0.
  VS=0.
  UD=0.
  VD=0.
  VT=0.
  VTF = 0.
  VF = 0.
  DUM = 0.
  US1 = 0.
  UD1 = 0.
  VS1 = 0.
  VD1 = 0.
  VED1 = 0.
  USS = 0.
  UDS = 0.
  VSS = 0.
  VDS = 0.
  VTS = 0.
  TRM2 = SQRT(R2)
  DO 780 J=1,N1
    TRM1 = XC(1)-XB(J)*BETA+R(J)
    TRM = XC(1)-[XB(NBODYS)]-BETA+R(NBODYS)
    XI = XB(NBODYS)-[XB(J)]-BETA+R(J)-BETA+R(NBODYS)
    IF (R2.EQ.0.) GO TO 770
    TRM3 = TRM2/TRM1
    TRM32=TRM3*TRM3
    IF (TRM3-GT.1.-OR.TRM3.LE.0.) GO TO 775
    C SINGULARITY IS INSIDE FORWARD FACING MACH CONE
    C VELOCITY DUE TO QUADRATICALLY VARYING SINGULARITIES
  
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06/02/67

VELL - EFN SOURCE STATEMENT - IFN(S) -

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TRM4=SQRT(1.-TRM32)
TRM5=ACOSH(TRM1/TRM2)
US=-2.*TRM1*(TRM5-TRM4)*T(J)
VS= BETA*TRM1*(TRM4-TRM3-TRM3*TRM5)*T(J)
UD= TRM1*(2/R1*(TRM4-TRM32+TRM5)*TC(J)
VD= -TRM1*(3/R1*(1.-4.*TRM32)/3.*TRM4+TRM32+TRM5)*TC(J)
VT= TRM1*(3/R2*(1.-2.*TRM32)/3.*TRM4-TRM32+TRM5)*TC(J)
VELOCITY DUE TO TANGENT CONE
IF (J-NE-1) GO TO 710
USS = US
VSS = VS

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C

51

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US = US-ACOSH(TRM1/TRM2)*T11
VS = VS+BETA*SQRT(1.-TRM32)/TRM3*T11

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USA = US - VSS
VSA = VS - VSS
UD = UD+BETA*SQRT(1.-TRM32)/TRM3*TC11
VD = VD-.5*BT2*(SQRT(1.-TRM32)/TRM32+TRM5)*TC11
VT = VT-.5*BT2*(SQRT(1.-TRM32)/TRM32-ACOSH(TRM1/TRM2))*TC11

```

710 CONTINUE

750 CONTINUE

C SUMMATION OF VELOCITY COMPONENTS

```

U(1) = U(1)+US+COSTHA*UD
VF = VF +VF +VS+COSTHA*VD
VTF = VTF + VTF + VT+SINETHA
USAVE = U(1)-USA
VSARE = VF-VSA
VSARE = VF - VTF

```

C FIELD POINT IS INSIDE MACH CONE FROM END OF BODY

63

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IF (TAN-LE-TRM2) GO TO 775
TRM6 = SQRT(TRM-TRM-BR2)
IF (J-NE-1) GO TO 765
US1 = T11*(ACOSH(TRM/TRM2)+X1/TRM6)
UD1 = -COSTHA*TC11*((TRM1*TRM-BR2)/TRM6)/R1
VS1 = -T11/R1*(TRM6-X1+TRM/TRM6)
VD1 = DUM
VCOSTHA*TC11/R2*(BR2*X1/TRM6+BR2/2.*ACOSH(TRM/TRM2)*(TRM1+X1)/2.
+TRM6)
VTD1 = -SINTHA*TC11/R2*(BR2*.5*ACOSH(TRM/TRM2)-(TRM1+X1)/2.*
+TRM6)
765 CONTINUE
USS = USS+T(J)*(2.*TRM1*ACOSH(TRM/TRM2)-2.*TRM6*X1+X1/TRM6)
VSS = USS+COSTHA*TC(J)/R1*(BR2*ACOSH(TRM/TRM2)-(2.*TRM1+X1)/3.*
+TRM6*(X1+X1+2.*BR2)-TRM1*(TRM1*TRM-BR2))/3.*TRM6)
VSS = VSS+T(J)/R1*(BR2*ACOSH(TRM/TRM2)-(TRM1+X1)*TRM6-X1+X1
+TRM/TRM6)
VDS = VDS+COSTHA*TC(J)/R2*((TRM1*TRM1+TRM1*X1+X1-2.*BR2)/3.
+TRM6*TRM1+BR2*ACOSH(TRM/TRM2)+BR2*(4.*TRM1+X1-2.*TRM1*TRM1
+X1+X1+2.*BR2)/3.*TRM6)
VTS = VTS-SINTHA*(TRM1*BR2*ACOSH(TRM/TRM2)-(TRM1*TRM1+TRM1*X1
+X1+X1+2.*BR2)*TRM6/3.
+TC(J)/R2

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```

GO TO 775
770 CONTINUE
775 CONTINUE
780 CONTINUE
  U (1) = U(1)+USS+UDS+US1+UD1
  VF = VF + VSS+VDS+VS1+VD1
  VTF = VTF+VTS +VTD1
  SYN=2*(JM-J)-1
  VV(1)=VF *SINTHA+VTF *COSTHA
  MM(1)=VF *COSTHA-VTF *SINTHA
790 CONTINUE
800 CONTINUE
  RETURN
  END

```

```

C
SUBROUTINE WBX(B,NB,W,NW,EPS,KODE,S,BW,NU)
  DIMENSION B(1),W(1),S(2,1),BW(3,1),NU(3)
  1 Q(3,2),R(10),DUM(3)
  2 WPTS(3,2),UVEC(3),WP(3,2)
  3,PTCNWG(3)
  LOGICAL INTD
  USED BY WBXUL TO FIND THE INTERSECTIONS OF THE UPPER OR LOWER
  WING PERCENT LINES WITH THE BODY.
  B IS THE ARRAY OF NB BODY PERCENT LINES.
  W IS THE ARRAY OF NW WING PERCENT LINES.
  A PERCENT LINE OF N POINTS HAS 3*N ELEMENTS
  X1,Y1,Z1, X2,Y2,Z2, ..... , XN,YN,ZN
  THE FIRST 3*J CELLS OF AN ARRAY B OF J PERCENT LINES FORMS A TABLE OF
  CONTENTS TO THE REST OF THE ARRAY. ELEMENTS 1,4,7,... OF B ARE LABELS
  FOR PERCENT LINES 1,2,3,... ELEMENTS 2,5,8,... ARE THE NUMBER OF
  3-DIMENSIONAL POINTS IN PERCENT LINES 1,2,3,... ELEMENTS 3,6,9,... ARE
  THE STARTING LOCATIONS IN B OF PERCENT LINES 1,2,3,...
  FOR EXAMPLE, IF B(7) = 30., B(8) = 12. AND B(9) = 49., THEN THE PERCENT
  LINE WITH THE LABEL 30. CONTAINS 12 POINTS AND STARTS IN B(49).
  EPS IS THE TOLERANCE IN LOCATING INTERSECTION POINTS.
  A WARNING MESSAGE IS WRITTEN IF THE ERROR IS GREATER THAN EPS.
  KODE = 1 IF THE BODY IS POLYGONAL IN CROSS SECTION, = 2 IF SMOOTH.
  S IS A SCRATCH ARRAY AT LEAST 2*NB CELLS LONG. USED FOR 2-DIMENSIONAL
  CROSS SECTIONS THRU THE BODY.
  BW IS AN OUTPUT ARRAY OF BODY-WING INTERSECTION POINTS. IF THE JTH
  WING PERCENT LINE DOES NOT INTERSECT THE BODY, THEN
  BW(1,J) = BW(2,J) = BW(3,J) = 1.E+30.
  NU IS AN ERROR ARRAY WHICH IS PASSED DOWN TO LOWER LEVEL SUBROUTINES.
  NU(1), AN OUTPUT, IS ZERO FOR SUCCESS, NON-ZERO FOR FAILURE.
  NU(2), AN INPUT, MAY BE INTERPRETED AS A TAPE NUMBER ON WHICH TO
  WRITE AN ERROR MESSAGE, IF GREATER THAN ZERO.
  NU(3), BOTH AN INPUT AND AN OUTPUT, IS AN ERROR COUNTER AND ERROR MESSAGE
  LIMITER. SOME LOWER LEVEL SUBROUTINES MAY SUBTRACT 1 FROM NU(3) IF AN
  ERROR OCCURS AND THEN WRITE AN ERROR MESSAGE IF NU(3) AND NU(2) ARE BOTH
  GREATER THAN ZERO.
  INPUTS ARE B,NB,W,NW,EPS,KODE,NU(2),NU(3). OUTPUTS BW,S,BW,NU(1),NU(3)
  DATA SR,DUM/3HWBX,3*1.E+30/
  R(10)=1.E-7
  CUT THE BODY WITH A STATION PLANE THRU EACH WING PERCENT POINT IN TURN
  UNTIL THE INTERSECTION POINT IS ISOLATED BETWEEN 2 ADJACENT WING POINTS.
  THEN ITERATE UNTIL THE X-VALUE OF THE INTERSECTION IS FOUND (WITHIN EPS).
  DO 6000 IW=1,NW
  FOR EACH WING PERCENT LINE IN W.
  100

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WBX
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
08/19/65

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C      INTD=.FALSE.
C      L=IW*3
C      NWP IS NO. OF PTS. IN THE IW PERCENT LINE AND LWP IS THE LOCATION OF THE
C      FIRST POINT IN W. LWP IS UPDATED IN THE LOOP BELOW.
C      NWP=W(L-1)
C      LWP=W(L)
C
C      DO 1200 K=1,NWP
C      FOR EACH POINT W(LWP) IN THE PERCENT LINE.
C
C      FIND THE HORIZONTAL DISTANCE D FROM POINT W(LWP) TO THE BODY AND THE
C      CORRESPONDING POINT Q ON THE BODY.
C      EPC=AMAX1(ABS(W(LWP)),1.)*1.E-6
C      CALL WBXC(B,NB,EPC,W(LWP),KODE,S,D,Q,NU)
C      IF(NU)250,500,300
C
C      250 MU=6
C      NU = -5 MEANS BODY IS NOT DEFINED AT STATION X
C      IF(NU+5)9000,400,9000
C
C      300 MU=7
C      NU = 1 OR 2 MEANS WING POINT IS ABOVE OR BELOW THE BODY
C      IF(NU-2)310,310,9000
C
C      310 MU=8
C      IF(D)510,9000,510
C      SEE IF PREVIOUS POINT WAS OK.
C      400 IF(INTD) GO TO 1250
C      GO TO 1000
C
C      500 IF(D.EQ.0.1) GO TO 1500
C      510 IF(INTD) GO TO 600
C      INTD=.TRUE.
C      GO TO 700
C
C      SEE IF THIS POINT AND PREVIOUS POINT ARE ON OPPOSITE SIDES OF BODY SURFACE
C      600 IF(D*DP)1650,700,700
C      OPPOSITE SIDES
C      THE INTERSECTION PT. IS BETWEEN W(LWPP) AND W(LWP)
C      650 R(4)=D
C      GO TO 1600
C
C      SAME SIDE OR ELSE FIRST TIME WBXC SUCCEEDED.
C      700 DP=D
C
C      1000 LWPP=LWP
C      LWP=LWP+3
C
C      1200 CONTINUE
C
C      GO TO 1300
C
C      THE X-VALUE (=W(LWP)) OF THIS WING PERCENT POINT IS OUTSIDE
C      THE RANGE OF BODY X-VALUES. HOWEVER, THE PREVIOUS WING
C      PERCENT POINT WAS OK. ONLY 1 OF THE BODY END POINTS CAN
C      LIE BETWEEN W(LWPP) AND W(LWP). FIND THIS POINT, INTERSECT
C      THE WING PERCENT LINE SEGMENT WITH THE CORRESPONDING

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C BODY STATION PLANE TO GET A POINT ON THE WING P.C. LINE.
C CALL THIS POINT PTONWG.
C THE DISTANCE FROM THIS PT. TO THE BODY SURFACE WILL BE IN
C R(2)=R(4). THE X-VALUE WILL BE IN R(1)=R(3).
C
1250 CALL WBXD(R,B,NB,KODE,PTONWG,Q,S,W(LWPP),NU)
    MU=5
    IF(NU)9000,1260,9000
1260 D=R(2)
    IF(D*DP)1600,1600,1300
C
C NO INTERSECTION. LEAVE PERCENT LINE UNCHANGED. STORE X,Y,Z = 1.E+30
C AS INTERSECTION POINT.
1300 KOUT=0
    CALL TRAV(BW(1,IW),DUM,3)
    GO TO 5000
C
C WING POINT W(LWP) LIES ON THE BODY SURFACE.
1500 KOUT=K
    GO TO 4500
C
1600 CONTINUE
    CALL TRAV(WGPTS,W(LWPP),6)
    IF(MU.NE.5) GO TO 1650
    CALL TRAV(WGPTS(1,2),PTONWG,3)
C WGPTS CONTAINS THE COORD. OF 2 CONSECUTIVE POINTS ON THE
C WING PERCENT LINE WHICH LIE ON OPPOSITE SIDES OF THE BODY SURFACE.
C FIND THE INTERSECTION OF THE LINE SEGMENT WGPTS WITH THE BODY
C SURFACE AS FOLLOWS. CHOOSE A POINT (IN WP) WHICH IS SOME
C DISTANCE ALONG WGPTS FROM ITS 1ST END POINT. (A UNIT VECTOR
C ALONG WGPTS WILL BE UVEC). USE WBXC TO FIND THE HORIZONTAL
C DISTANCE (IN Y-DIRECTION) FROM WP TO THE BODY SURFACE.
C ITERATE ON DISTANCE ALONG WGPTS UNTIL WP LIES ON BODY SURFACE.
C
C USE FROOTA TO TAKE CARE OF THE BOOK-KEEPING FOR THE ITERATION
C AND TO PREDICT DISTANCES ALONG WGPTS TO USE FOR NEXT ITERATION.
C FROOTA WILL SET JR = 0 WHEN INTERSECTION IS FOUND.
C
1650 CONTINUE
    R(1)=0.
    R(2)=DP
    R(3)=UVEC(WGPTS,WGPTS(1,2),UVEC,0,3)
    R(3) = LENGTH OF THE LINE SEGMENT WGPTS
    R(4) WAS SET TO D PREVIOUSLY
    R(9)=0.
    MU=9
    IF(R(3))9000,9000,1700
1700 MU=10
C
DO 3000 KR=1,100
    CALL FROOTA(R,JR)
C R(1) AND R(3) ARE NEW TRIAL VALUES OF DISTANCE ALONG WGPTS
DO 1900 I=1,2

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08/19/65

WDX	EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
	11=I+1		,65
	00 1800 J=1,3		,66
	1800 WP(J,1)=WGPTS(J,1)+R(I1-1)*UVEC(J)		,67
	CALL W3XC(8,NB,EPC,WP(1,1),MODE,S,R(11),Q(1,1),NU)		,68
	P(2) AND P(4) ARE CORRESPONDING Y-DISTANCES OF WP FROM BODY SURFACE		,69
	IF(NU .LT. 0 .OR. NU .GT. 2) GO TO 9000		,70
	1900 CONTINUE		,71
	2000 MU=11		,72
	GO TO 9000		,73
	3000 CONTINUE		,74
	3100 IF(ARS(R(2))-EPS) 4000,4000,3110		,75
	3110 LTAPE=NU(2)		,76
	NU(3)=NU(3)-1		,77
	IF(LTAPF .LE. 0 .OR. NU(3) .LE. 0) GO TO 4000		,78
	WRITE(LTAPE,3120)IW,EPS,(WP(1,1),I=1,3)		,79
	3120 FORMAT/420*** INTERSECTION OF WING PERCENT LINE NO.		,80
	1 13,40H WITH BODY NOT WITHIN GIVEN TOLERANCE OF		,81
	2 F10.6/27H POINT ON WING HAS COORD. (3F10.4,1H)		,82
	C THE INTERSECTION (IN Q) HAS BEEN FOUND AND LIES BETWEEN		,83
	C POINTS K-1 AND K.		,84
	4000 KOUT=K-1		,85
	C THE FIRST KOUT POINTS ARE INSIDE THE BODY AND ARE TO		,86
	C BE REMOVED.		,87
	C STORE THE INTERSECTION POINT.		,88
	4500 CALL TRAV(RW(1,IW),Q,3)		,89
	C ADJUST THE W ARRAY TO REFLECT ONLY THAT PART OF WING		,90
	C OUTSIDE BODY.		,91
	5000 CALL W3XA(W,IW,KOUT,RW(1,IW),NU)		,92
	MU=4		,93
	IF (NU)9000,6000,9000		,94
	6000 CONTINUE		,95
	MU=0		,96
	GO TO 9900		,97
	7000 WRITE ERROR MESSAGE.		,98
	9000 LT=NU(2)		,99
	NU(3)=NU(3)-1		,100
	IF(LT .LE. 0 .OR. NU(3) .LE. 0) GO TO 9900		,101
	WRITE(LT,9100)MU,NU(1),SR,IW,K		,102
	9100 FORMAT(6H0FERROR 16,6H, CODE 16,15H IN SUBROUTINE A6/		,103
	18H WING PERCENT LINE 15,7H, POINT 15)		,104
	9900 NU=MU		,105
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WHX
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
08/19/65
RETURN
END
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SUBROUTINE WBXA(B,I,K,P,NU)
  DIMENSION B(1),P(3)
  C USED BY WBX TO ADJUST THE B ARRAY OF WING PERCENT LINES
  C TO REMOVE THAT PART OF THE I-TH PERCENT LINE INSIDE BODY.
  C INPUTS ARE B,I,K,P. OUTPUTS ARE B,NU.
  C
  L=3*I
  C KB IS NO. OF POINTS IN I-TH PERCENT LINE.
  KB=B(I)-1
  C KC IS STARTING LOCATION OF I-TH PERCENT LINE.
  KC=B(L)
  KD=KC+3*K-1
  IF (K .GE. KB .OR. K .LT. 0) GO TO 5000
  IF (I .EQ. 1) GO TO 1000
  JB IS NO. OF PTS. IN (I-1)TH PERCENT LINE
  JB=B(L-4)
  C JC IS STARTING LOCATION.
  JC=B(L-3)
  C KN = STARTING LOCATION OF NEW PERCENT LINE
  KN=JC+3*JB
  B(L)=KN
  GO TO 2000
  C
  1000 KN=KC
  2000 NN=KB-K
  IF (K)2100,2100,2200
  2100 NN=NN-1
  C NN+1 = NO. OF PTS. IN NEW PERCENT LINE.
  2200 B(L-1)=NN+1
  KN=KN-1
  C
  IF (K)3000,4000,3000
  C INSERT P AS FIRST PT. IN NEW PERCENT LINE.
  3000 DO 3100 J=1,3
  KN=KN+1
  3100 B(KN)=P(J)
  C
  C MOVE LAST PART OF OLD PERCENT LINE UP TO NEW POSITION.
  4000 NN=3*NN
  DO 4100 J=1,NN
  KN=KN+1
  KD=KD+1
  4100 B(KN)=B(KD)
  C
  NU=0
  GO TO 9000
  C
  5000 NU=1
  9000 RETURN
  END

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C SURROUTINE WBXC(9,NB,EP,P,KODE,S,D,O,MU)
C DIMENSION B(1),P(3),S(1),Q(3),MU(3)
C DATA MU(2)/0/
C
C USED BY WBX AND WBXD. GIVEN A POINT P, CUT THE BODY WITH THE
C PLANE X = P(1) AND GET BODY SECTION S (POINTS Y,Z).
C FIND THE HORIZONTAL DISTANCE D FROM P TO S AND THE
C CORRESP. POINT Q ON S (Q(1)=P(1) AND Q(3)=P(3)).
C INPUTS- R,NB,EP,P,KODE. OUTPUTS- S,D,Q,MU
C
C X=P(1)
C Z=P(3)
C CUT BODY WITH STATION PLANE
C CALL RCUTX(B,NB,X,EP,NS,S)
C NU=-5
C IF (NS .LT. 2) GO TO 9000
C INTERPOLATE WITH Z AS INDEPENDENT VARIABLE TO GET
C CORRESPONDING Y.
C CALL RITURP(S(2),S,2,NS,KODE,Z,Y,MU)
C Q(1)=X
C MU=MU
C IF(MU)9000,5000,4000
C 4000 IF(MU-2)6000,7000,9000
C 5000 Q(2)=Y
C Q(3)=Z
C GO TO 8000
C 6000 Q(2)=S(2)
C Q(3)=S(1)
C GO TO 8000
C 7000 L=NS+NS
C Q(2)=S(L)
C Q(3)=S(L-1)
C 8000 D=P(2)-Q(2)
C 9000 RETURN
C END

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SUBROUTINE WBOXD(R,B,NB,KODE,P,O,S,W,M,NU)
 DIMENSION R(4),B(1),P(3),O(3),S(2,1),W(3,2),NU(3),C(4),LP(2)

USED BY WBX IF NECESSARY TO PROCESS A WING PERCENT POINT
 WITH X-VALUE OUTSIDE THE RANGE OF BODY PERCENT LINE X-VALUES

W(1,1) IS A WING PERCENT POINT WHICH WAS PROCESSED OK BY WBX.
 W(1,2) IS NEXT POINT, WHICH IS OUTSIDE BODY RANGE.

OTHER ARGUMENTS EXPLAINED IN WBX

RECALL THAT B IS HEADED BY TABLE OF CONTENTS.

S IS SCRATCH ARRAY FOR WBOXC.

INPUTS ARE B,NB,KODE,W,NU(2),NU(3)

OUTPUTS ARE P,Q,S,NU(1),NU(3)

DATA SR,C/4HBOXD,-1.,3*0./

NU=0

IF=B(3)

ISEC=B(6)

BXF=B(1F)

BXL=B(1SEC-3)

BXF AND BXL ARE EXTREME X-VALUES OF BODY PERCENT LINE 1

WXL=W(1,1)

WXL=W(1,2)

TEST TO SEE IF BXL IN RANGE OF WING POINTS

IF((BXL-WXL)*(BXL-WXL))100,100,200

BXL WITHIN RANGE

R(1)=BXL

GO TO 300

BXL NOT IN RANGE. ASSUME BXL IS.

R(1)=BXL

R(3)=R(1)

C(4)=R(1)

C IS A STATION PLANE

CALL POLYN(C,W,3,2,0.,1,P,LP,L)

P IS INTERSECTION OF PLANE AND LINE SEGMENT W.

MU=1

IF (L .NE. 1) GO TO 8000

FIND HORIZONTAL DISTANCE FROM P TO BODY AND

CORRESPONDING POINT Q ON BODY.

CALL WBOXC(B,NB,O.,P,KODE,S,R(2),O,NU)

MU=2

IF(NU)8000,1000,500

NU = 1 OR 2 MEANS WING POINT IS ABOVE OR BELOW THE BODY

500 IF(NU-2)600,600,8000

600 IF(R(2)) 1000,8000,1000

1000 CONTINUE

MU=0

R(4)=R(2)

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WBXD		08/19/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	-	INTERNAL FORMULA NUMRFR(S)
	GO TO 9000		
C	WRITE ERROR MESSAGE.		
C	LT=NU(2)		*27
	NU(3)=NU(3)-1		*28
	IF(LT .LE. 0 .OR. NU(3) .LE. 0) GO TO 9000		*29
	WRITE(LT,8100)MU,NU(1),SR		*30
	8100 FORMAT(6HOERROR I6,6H, CODE I6,15H IN SUBROUTINE A6)		*31
C	9000 CONTINUE		*32
	NU=MU		*33
	RETURN		*34
	END		*35
			*36
			*37
			*38
			*39

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SUBROUTINE WBXUL(B,LI,LO,DAT,LGDEF,LOK,BTITLE,WTITLE,BAXIS,NU)
C
C DIMENSION B(1),DAT(2),LOK(3,9),NU(3),UPLO(2),PT(3),
C ,BTITLE(12),WTITLE(12),BAXIS(2)
C
C LOGICAL LGDEF(3,6)
C DATA SP,UPLO(1)/5HWRXUL,12H UPPER LOWER/,DEGRAD/D206712273406/
C ,EP/1.E-5/
C
C USED BY GEOMD TO FIND THE INTERSECTIONS OF THE UPPER AND/OR
C LOWER WING PERCENT LINES WITH THE BODY SURFACE, AND TO
C TRUNCATE THE WING PERCENT LINES SO THAT THEY REPRESENT ONLY
C THAT PART OF THE WING OUTSIDE THE BODY.
C
C INPUTS ARE B,LI,LO,DAT,LGDEF,LOK,BTITLE,WTITLE,BAXIS,NU
C OUTPUTS ARE B,LGDEF,LOK,NU
C
C RECORD THAT THE WING-BODY INTERSECTION HAS BEEN REQUESTED
C LGDEF(1,5)=LGDEF(1,1)
C LGDEF(1,6)=LGDEF(1,2)
C
C NU=0
C SEE IF BODY AND AT LEAST 1 SURFACE OF WING ARE DEFINED.
C IF ((LGDEF(2,1).OR. LGDEF(2,2)).AND. LGDEF(2,3)) GO TO 300
C WRITE (LG,210)
C FORMAT(47H WING-BODY INTERSECTION CANNOT BE FOUND BECAUSE
C 1/44H EITHER THE BODY OR THE WING IS NOT DEFINED.)
C NU=1
C GO TO 9000
C
C 300 READ(LI,310)WRKCODE,EPS
C 310 FORMAT(6F10.0)
C IF(ABS(EPS)-EP) 320,330,330
C 320 EPS=EP
C 330 CONTINUE
C
C CODE=WRKCODE
C CODE = 1 IF BODY IS POLYGONAL IN SHAPE, =2 IF SMOOTH.
C
C 340 WRITE(LO,340)CODE,EPS
C FORMAT(71H OF THE INTERSECTION OF EACH WING PERCENT LINE WITH T
C THE BODY SURFACE. // 1H0 10X 6H CODE = 13/1H0 10X 11H TOLERANCE =F7.4/
C 2/48H01F P BE A POINT WHICH LIES ON THE BODY SURFACE /
C 356H AND Q A POINT ON A LINE SEGMENT CONNECTING TWO ADJACENT /
C 472H WING PERCENT LINE POINTS, SUCH THAT P AND Q HAVE THE SAME X-CO
C ORDINATE. /
C 649H0THE PROGRAM ITERATES UNTIL P AND Q HAVE THE SAME /
C 742H (OR NEARLY THE SAME) Y AND Z COORDINATES. /
C 834H THEN P IS THE INTERSECTION POINT. /
C 952H0IF P AND Q DIFFER BY MORE THAN THE GIVEN TOLERANCE, /
C A30H A WARNING MESSAGE IS WRITTEN. /
C 969H0THE SHAPE OF THE BODY SURFACE BETWEEN MERIDIAN LINES (IN ANY S
C ECTION /
C 059H PARALLEL TO THE YZ PLANE) IS DETERMINED BY THE GIVEN CODE. /

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07/31/65
INTERNAL FORMULA NUMBER(S)

EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
820	CALL TRAPIVT,B(IWAX),3)	,51
	IWBX=IWBX+3	,52
	IF (PI .GT. 1.E+29) GO TO 900	,53
	OY=PI(2)-BAXIS(1)	,54 ,55
	OZ=PI(3)-BAXIS(2)	,56
	RHO=SQRT(OY*OY+OZ*OZ)	,57
	IF (RHO)R2C,820,830	,58
	THETA=0.	,59
	GO TO 850	,60
930	THETA=ATN1(ABS(OY),OZ)*DEGRAD	,61
850	WRITE(LQ,R60)J,PCT,PT,RHO,THETA	,62
860	FORMAT(1H 12,F10.4,1X 3F10.4,2X 2F10.4)	,63 ,64 ,65
	GO TO 1000	,66
900	WRITE(LQ,910)J,PCT	,67
910	FORMAT(1H 12,F10.4,6X 15HND INTERSECTION)	,68 ,69
1000	CONTINUE	
C	RECORD THAT THE INTERSECTIONS HAVE BEEN FOUND	,70 ,71
C	2000 LGDEF(2,K+4)=.TRUE.	,72
C		,73
C	ON 2100 J=1,2	
C	2100 LOK(J,K+2)=LOK(J,K)	,74 ,75
	NLAST=B(IPCT-2)	,76
	LLAST=B(IPCT-1)	,77
C	LOK(3,K+2)=LLAST+3*NLAST-1	
C		,78
C	4000 CONTINUE	,79 ,80
C	MU=0	,81
C	GO TO 8500	
C	WRITE ERROR MESSAGE	,82
C	8000 KE=MERR(NU,NU+1,MU,SR)	,83
C		
C	8500 NU=MU	,84
C	9000 RETURN	,85
	END	,86


```

C
C SUBROUTINE WBXX(B,NB,W,NW,EPS,KODE,S,BW,NU)
C
C SAME AS WBX, EXCEPT DOES NOT STORE TRUNCATED LINES IN B.
C
C DIMENSION B(1),W(1),S(2,1),BW(3,1),NU(3),
C 1 Q(3,2),R(10),DUM(3)
C 2,WP(3,2),UVEC(3),WP(3,2)
C 3,PICNWG(3)
C LOGICAL INTO
C
C USED BY TFLAT TO FIND THE INTERSECTIONS OF WING PERCENT
C LINES WITH THE BODY SURFACE.
C
C B IS THE ARRAY OF NB BODY PERCENT LINES.
C W IS THE ARRAY OF NW WING PERCENT LINES.
C
C A PERCENT LINE OF N POINTS HAS 3*N ELEMENTS
C X1,Y1,Z1, X2,Y2,Z2, ..... XN,YN,ZN
C THE FIRST 3*J CELLS OF AN ARRAY B OF J PERCENT LINES FORMS A TABLE OF
C CONTENTS TO THE REST OF THE ARRAY. ELEMENTS 1,4,7,... OF B ARE LABELS
C FOR PERCENT LINES 1,2,3,... ELEMENTS 2,5,8,... ARE THE NUMBER OF
C 3-DIMENSIONAL POINTS IN PERCENT LINES 1,2,3,... ELEMENTS 3,6,9,... ARE
C THE STARTING LOCATIONS IN B OF PERCENT LINES 1,2,3,...
C FOR EXAMPLE, IF B(7) = 30., B(8) = 12. AND B(9) = 49., THEN THE PERCENT
C LINE WITH THE LABEL 30. CONTAINS 12 POINTS AND STARTS IN B(49).
C
C EPS IS THE TOLERANCE IN LOCATING INTERSECTION POINTS.
C A WARNING MESSAGE IS WRITTEN IF THE ERROR IS GREATER THAN EPS.
C KODE = 1 IF THE BODY IS POLYGONAL IN CROSS SECTION, = 2 IF SMOOTH.
C S IS A SCRATCH ARRAY AT LEAST 2*NW CELLS LONG. USED FOR 2-DIMENSIONAL
C CROSS SECTIONS THRU THE BODY.
C BW IS AN OUTPUT ARRAY OF BODY-WING INTERSECTION POINTS. IF THE JTH
C WING PERCENT LINE DOES NOT INTERSECT THE BODY, THEN
C BW(1,J) = BW(2,J) = BW(3,J) = 1.E+30.
C
C NU IS AN ERROR ARRAY WHICH IS PASSED DOWN TO LOWER LEVEL SUBROUTINES.
C NU(1), AN OUTPUT, IS ZERC FOR SUCCESS, NON-ZERO FOR FAILURE.
C NU(2), AN INPUT, MAY BE INTERPRETED AS A TAPE NUMBER ON WHICH TO
C WRITE AN ERROR MESSAGE, IF GREATER THAN ZERO.
C NU(3), BOTH AN INPUT AND AN OUTPUT, IS AN ERROR COUNTER AND ERROR MESSAGE
C LIMITER. SOME LOWER LEVEL SUBROUTINES MAY SUBTRACT 1 FROM NU(3) IF AN
C ERROR OCCURS AND THEN WRITE AN ERROR MESSAGE IF NU(3) AND NU(2) ARE BOTH
C GREATER THAN ZERO.
C
C INPUTS ARE B,NB,W,NW,EPS,KODE,NU(2),NU(3). OUTPUTS BW,S,BW,NU(1),NU(3)
C
C DATA SR,DUM/3HNBX,3*1.E+30/
C
C R(10)=1.E-7
C
C CUT THE BODY WITH A STATION PLANE THRU EACH WING PERCENT POINT IN TURN
C UNTIL THE INTERSECTION POINT IS ISOLATED BETWEEN 2 ADJACENT WING POINTS.
C THEN ITERATE UNTIL THE X-VALUE OF THE INTERSECTION IS FOUND (WITHIN EPS).

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WXXX 08/19/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

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C 100 DO 6000 IW=1,NW
C FOR EACH WING PERCENT LINE IN W.
C
C INTD=.FALSE.
C L=1W*3
C NWP IS NO. OF PTS. IN THE IW PERCENT LINE AND LWP IS THE LOCATION OF THE
C FIRST POINT IN W. LWP IS UPDATED IN THE LOOP BELOW.
C NWP=W(L-1)
C LWP=W(L)
C
C DO 1200 K=1,NWP
C FOR EACH POINT W(LWP) IN THE PERCENT LINE.
C
C FIND THE HORIZONTAL DISTANCE D FROM POINT W(LWP) TO THE BODY AND THE
C CORRESPONDING POINT Q ON THE BODY.
C EPC=AMAX1(ABS(W(LWP)),1.)*1.E-6
C CALL WBXC18,NB,EPC,W(LWP),KODE,S,D,Q,NU)
C IF(NU)250,500,300
C MU=6
C NU = -5 MEANS BODY IS NOT DEFINED AT STATION X
C IF(NU+5)9000,400,9000
C MU=7
C NU = 1 OR 2 MEANS WING POINT IS ABOVE OR BELOW THE BODY
C IF(NU-2)310,310,9000
C MU=8
C IF(D)510,9000,510
C SEE IF PREVIOUS POINT WAS OK.
C IF(INTD) GO TO 1250
C GO TO 1000
C
C 500 IF(1.EQ.0.) GO TO 1500
C 510 IF(INTD) GO TO 600
C INTD=.TRUE.
C GO TO 700
C
C SEE IF THIS POINT AND PREVIOUS POINT ARE ON OPPOSITE SIDES OF BODY SURFACE
C 600 IF(D*DP)650,700,700
C OPPOSITE SIDES
C THE INTERSECTION PT. IS BETWEEN W(LWPP) AND W(LWP)
C 650 R(4)=D
C GO TO 1600
C
C SAME SIDE OR ELSE FIRST TIME WRXC SUCCEEDED.
C 700 DP=D
C
C 1000 LWPP=LWP
C LWPP=LWP*3
C
C 1200 CONTINUE
C GO TO 1300
C
C THE X-VALUE (=W(LWP)) OF THIS WING PERCENT POINT IS OUTSIDE
C THE RANGE OF BODY X-VALUES. HOWEVER, THE PREVIOUS WING

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C PERCENT POINT WAS OK. ONLY 1 OF THE BODY END POINTS CAN
C LIE BETWEEN WLWPP) AND WLWP). FIND THIS POINT. INTERSECT
C THE WING PERCENT LINE SEGMENT WITH THE CORRESPONDING
C BODY STATION PLANE TO GET A POINT ON THE WING P.C. LINE.
C CALL THIS POINT PTONGW.
C THE DISTANCE FROM THIS PT. TO THE BODY SURFACE WILL BE IN
C R(2)=R(4). THE X-VALUE WILL BE IN R(1)=R(3).
C
C 1250 CALL WBOXDIR,8,NB,KODE,PTONGW,Q,S,W(LWPP),NU)
      MU=5
      IF (NU) 9000,1260,9000
C 1260 D=R(2)
      IF (D*OP) 1600,1600,1300
C
C NO INTERSECTION. LEAVE PERCENT LINE UNCHANGED. STORE X,Y,Z = 1.E+30
C AS INTERSECTION POINT.
C 1300 KOUT=0
      CALL TRAV(BW(1,1W),DUM,3)
      GO TO 5000
C
C WING POINT W(LWP) LIES ON THE BODY SURFACE.
C 1500 KOUT=K
      GO TO 4500
C
C 1600 CONTINUE
      CALL TRAV(WGPTS,W(LWPP),6)
      IF (MU .NE. 5) GO TO 1650
      CALL TRAV(WGPTS(1,2),PTONGW,3)
C
C WGPTS CONTAINS THE COORD. OF 2 CONSECUTIVE POINTS ON THE
C WING PERCENT LINE WHICH LIE ON OPPOSITE SIDES OF THE BODY SURFACE.
C FIND THE INTERSECTION OF THE LINE SEGMENT WGPTS WITH THE BODY
C SURFACE AS FOLLOWS, CHOOSE A POINT (IN WP) WHICH IS SOME
C DISTANCE ALONG WGPTS FROM ITS 1ST END POINT. (A UNIT VECTOR
C ALONG WGPTS WILL BE UVEC). USE WBOXC TO FIND THE HORIZONTAL
C DISTANCE (IN Y-DIRECTION) FROM WP TO THE BODY SURFACE.
C ITERATE ON DISTANCE ALONG WGPTS UNTIL WP LIES ON BODY SURFACE.
C
C USE FROOTA TO TAKE CARE OF THE BOOK-KEEPING FOR THE ITERATION
C AND TO PREDICT DISTANCES ALONG WGPTS TO USE FOR NEXT ITERATION.
C FROOTA WILL SET JR = 0 WHEN INTERSECTION IS FOUND.
C
C 1650 CONTINUE
      R(1)=0.
      R(2)=DP
      R(3)=UVEC(WGPTS,WGPTS(1,2),UVEC,0,3)
      R(3) = LENGTH OF THE LINE SEGMENT WGPTS
      R(4) WAS SET TO D PREVIOUSLY
      R(9)=0.
      MU=9
      IF (R(3)) 9000,9000,1700
C 1700 MU=10
      DO 3000 KR=1,100
      CALL FROOTA(R,JR)

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WRXX

EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

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C R(1) AND R(3) ARE NEW TRIAL VALUES OF DISTANCE ALONG WPTS
      DO 1900 I=1,2
      II=I+1
      DO 1800 J=1,3
      1800 WP(J,I)=WGPTS(J,I)+R(II-I)*UVEC(J)
      CALL WRXC(B,NB,EPC,WP(1,I),CODE,S,R(1),Q(1,I),NU)
      R(2) AND R(4) ARE CORRESPONDING Y-DISTANCES OF WP FROM BODY SURFACE
      IF(NU .LT. 0 .OR. NU .GT. 2) GO TO 9000
      1900 CONTINUE
C
      IF(JR) 2000, 3100, 3000
      2000 MU=11
      GO TO 9000
C
      3000 CONTINUE
C
      DIC NOT CONVERGE
      MU=12
      GO TO 9000
C
      3100 IF(ABS(R(2))-EPS) 4000,4000,3110
      3110 LTAPE=NU(2)
      NU(3)=NU(3)-1
      IF(LTAPE .LT. 0 .OR. NU(3) .LE. 0) GO TO 4000
      WRITE(LTAPE,3120)IW,EPS,(WP(1,I),I=1,3)
      3120 FORMAT(42H0** INTERSECTION OF WING PERCENT LINE NO.
      1 13,40H WITH BODY NOT WITHIN GIVEN TOLERANCE OF
      2 F10.6/27H POINT ON WING HAS COORD. ( 3F10.4,1H )
C
      THE INTERSECTION (IN Q) HAS BEEN FOUND AND LIES BETWEEN
      C POINTS K-1 AND K.
      4000 KOUT=K-1
      C THE FIRST KOUT POINTS ARE INSIDE THE BODY AND ARE TO
      C BE REMOVED.
      C STORE THE INTERSECTION POINT.
      4500 CALL TRAV(BW(1,IW),Q,3)
C
      5000 CONTINUE
C
      6000 CONTINUE
      MU=0
      GO TO 9900
C
      WRITE ERROR MESSAGE.
      9000 LT=NU(2)
      NU(3)=NU(3)-1
      IF(LT .LT. 0 .OR. NU(3) .LE. 0) GO TO 9900
      WRITE(LT,9100)MU,NU(1),SR,IW,K
      9100 FORMAT(6H0ERROR 16,6H, CODE 16,15H IN SUBROUTINE A6/
      , 18H WING PERCENT LINE 15,7H, POINT 15)
      9900 NU=MU
      RETURN

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WBXX
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - 08/19/65 INTERNAL FORMULA NUMBER(S)
END ,111

WING
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)
08/16/65

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SUBROUTINE WING
COMMON DATF(2),NTAPE1,NOL,NTAPE2,ND2(3),NPEAD,
1NWRITE,NBODY,NWING,XMACH,SYM,KAGE
COMMON /COMMON/ KODEW,KODEW,KODEW,KODE1,KODEC,XPER,YPER,KOPT3,KOPTW
1,KOPTF,NUMS,KTYPE,KSTART,KEND,KINT,XI(16),YI(16),ZI(16),NPER3,NPER1
2,NPLANE,NPLN1
COMMON /COMMON/ X(190,15),Y(190,15),Z(190,15),KXNT,VALUE(5),
1YCEP(16),SLOPE,KPANEL(2,15),XCOR(16,15),YCOR(16,15),ZCOR(16,15),Y
2INT(2,15),YINT(2,15),ZINT(2,15),XCEN(15,15),YCEN(15,15),ZCFN(15,15)
3,XCON(15,15),YCON(15,15),ZCON(15,15),AREA(15,15),APAT(15,15),THET
4A(15,15),ALPHA(15,15),CHORD(15,15),XCIL(16,25,2),ZFOIL(16,25,2),X
5NUM(16,2),XTAB1(25),XTAB2(25),XTAB2(25)
DIMENSION ND3(9455)
EQUIVALENCE (ND3(1),NPTS(1))

```

C CONTROL PROGRAM FOR WING PANELING SUBROUTINES
DATA NAME/6H-DEFINE/

```

C DEFINE CONSTANTS
C NING IS NUMBER OF WING PANELS KODEW.
C KODEW ARE INPUT ERROR CODES
C IF KODEW SET = 1 IN INPUTW THEN TAPE ERROR
C ENCOUNTERED ON SCRATCH TAPE IF KODEWU
C SET = 1, ERROR ENCOUNTERED ON INPUT CARDS
C FOR THICK WING (OR CAMBERED SURFACE)
C
10 NHING=0
KODEW=0
KODEWU=0
1J=0

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C INITIALIZE COMMON ARRAYS
DO 20 I=1,9455
20 ND3(I)=0

```

C CALL SUBROUTINES
30 CALL INPUTW
IF (KODEW) 200,40,110
40 CALL CRNRW
IF (KODEW) 200,45,100
45 CALL AREA(XCOR,YCOR,ZCOR,AREA,ARAT,NPLN1,NPER1)
CALL CENED(XCOR,YCOR,ZCOR,ARAT,XCEN,YCEN,ZCFN,
1NPLN1,NPER1)
CALL CNTRW
CALL CHORDW
IF (KODEW) 200,50,100
50 1J=1J+1
CALL INPUTW
IF (KODEW) 200,105,60
60 IF (KODEWU) 200,80,120
80 CALL SLOPEW
IF (KODEW) 200,105,100
100 WRITE (NWRITE,920)
105 CALL OUTPUTW

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WING		06/16/65
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
110	IF (KODEW) 150,150,200	26
	WRITE (NWRITE,900)	27, 28
	GO TO 200	29
120	WRITE (NWRITE,910)	30, 31
	GO TO 200	32
150	RETURN	33
200	READ (NREAD,890) KARD	34, 35, 36
	IF (KARD=NAME) 200,210,200	37
210	BACKSPACE NREAD	38
	KODEW=-1	39
	GO TO 150	40
890	FORMAT (A6)	
900	FORMAT (1H1,9X,31HERROR MESSAGE - SUBROUTINE WING/10X,	
	131HIMPROPER PLANAR WING DEFINITION)	
910	FORMAT (1H1,9X,31HERROR MESSAGE - SUBROUTINE WING/10X,	
	152HIMPROPER THICK WING (OR CAMBERED SURFACE) DEFINITION)	
920	FORMAT (1H1,9X,13HERROR MESSAGE/10X,	
	149HPANELLING DATA NOT COMPLETED DUE TO PROGRAM ERROR/10X,	
	238HINCOMPLETE PANELLING DATA TO BE OUTPUT)	
	END	41

WING1 09/14/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMMR(S)

SUBROUTINE WING1(B,LI,LO,DAT,LLETE,LOGUL,NAF,NPL,LAFN,LPC,T,KOD,
1 CHD,EPS,TITLE,NU)
1 DIMENSION B(1),DAT(2),KOD(2),NU(3),NLTEP(4),LPLF(2),HLETE(2,2),
1 TITLE(12)

LOGICAL LOGUL(2)

WING1 IS USED BY GEOMD. IT READS DATA CARDS WHICH DEFINE
A WING, CHECKS THE DATA, PUTS IT IN STANDARD FORM FOR
LATER USE BY WING2 AND GEOMD.

B IS BUFFER IN WHICH DATA IS STORED

LOGUL(1) = TRUE IF UPPER WING IS DEFINED

LOGUL(2) = TRUE IF LOWER WING IS DEFINED

NAF = NO. OF AIRFOILS

NPL = NO. OF PERCENT LINES DESIRED

LAFN. A TABLE IS STORED IN B(LAFN) WHICH HAS THE

LOCATIONS IN B WHERE AIRFOILS ARE STORED, AND

NO. OF POINTS IN EACH AIRFOIL.

LLETE. THE LEADING AND TRAILING EDGE POINTS OF EACH

AIRFOIL ARE STORED IN B(LLETE).

LPC,T. THE PERCENTS AT WHICH PERCENT LINE ARE TO BE

GENERATED ARE STORED IN B(LPCT).

NU IS ERROR INDICATOR.

DATA HLETE(1,1),HLETE(1,2),WING/THLEADING,8HTRAILING,5HWING1/,
HGIVEN,HUSED/6HGIVEN),6HUSED) /,MAX/150/

LOGUL(1)=.TRUE.

LOGUL(2)=.TRUE.

NU=0

READ AND WRITE TITLE CARD (CARD 1)

READ (LI,310)TITLE

FORMAT(13A6,A2)

WRITE (LO,320)DAT,TITLE

FORMAT(16H1WING DEFINITION 38X,2A6/1H014A6)

READ CARDS 2,3

READ (LI,400)PNLE,PNT,E,AFN,PLN,WUL,CHD,PCODE,ACODE,EPS

FORMAT(6F10.0)

NLTEP(1)=PNLE

NLTEP(2)=PNT,E

NAF=AFN

NPL=PLN

NLTEP(3)=NAF

NLTEP(4)=NPL

WRITE (LO,410)NLTEP

FORMAT(/17H0THE PLANFORM HAS 13,28H POINTS ON THE LEADING EDGE,
/120,29H POINTS ON THE TRAILING EDGE.

/14,20H AIRFOILS ARE GIVEN.

14,35H PERCENT LINES ARE TO BE GENERATED.)

KOD(1)=ACODE

KOD(2)=PCODE

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IF(EPS)411,411,412
411 EPS=.01
412 WRITE(LO,413)PCODE,ACODE,EPS,CHU
413 FORMAT( 8HOPCODE = F3.0, 9H, ACODE = F3.0, 7H, EPS = F10.6,
X 7H, CHD = F7.4)
      ,24
      ,25
      ,26
      ,27
      ,28

420 IF (MUL*(MUL-2.))440,450,430
C MUL NOT 0.,1., OR 2.
430 MU=1
GO TO 9000
      ,29
      ,30
C UPPER WING
440 LOGUL(2)=.FALSE.
WRITE(LO,441)
      ,31
      ,32
      ,33
      ,34
441 FORMAT(30H UPPER WING SURFACE IS DEFINED)
GO TO 480
      ,35
C MUL = 0. OR 2.
450 IF (MUL)470,470,460
C LOWER WING
460 LOGUL(1)=.FALSE.
WRITE(LO,461)
      ,36
      ,37
      ,38
      ,39
461 FORMAT(30H LOWER WING SURFACE IS DEFINED)
GO TO 480
C UPPER AND LOWER WING
470 WRITE(LO,471)
      ,40
      ,41
      ,42
471 FORMAT(42H UPPER AND LOWER WING SURFACES ARE DEFINED)
C
480 CONTINUE
      ,43
      ,44
      ,45
C CHECK FOR REASONABLE VALUES
DO 520 I=1,4
I1=NLTEP(I)-1
IF (I1*(I1-MAX))520,510,510
WRITE ERROR MESSAGE NO. 2 AND GO ON
510 IERR=MERR(0,1,2,WING)
520 CONTINUE
      ,46
      ,47
C PACK BUFFER (B) SO STORAGE FOR AIRFOIL NAMES WILL
NOT LATER BE DISTURBED
LEFT=IPACK(B)
C RESERVE STORAGE FOR NAMES OF AIRFOILS
LAFN=IRSERV(4*NAF,B,LAFN)
IF (LAFN)550,550,560
550 MU=3
GO TO 9000
      ,48
      ,49
C RESERVE STORAGE FOR INTERSECTION OF LE AND TE WITH AIRFOILS
LLETE=INSERV(4*NAF,B,LLETE)
IF (LLETE)570,57C,600
570 MU=4
GO TO 9000
      ,50
      ,51
      ,52
      ,53
C RESERVE STORAGE FOR PLANFORM POINTS, READ THEM.
DO 600 I2=1,2
I5=2*NLTEP(I2)
      ,54
      ,55
      ,56
      ,57
      ,58
      ,59
      ,60

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WING1 09/14/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

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610 IF (IRSERV(15,8,LPLF(12)))610,610,620 ,61
    GO TO 9000 ,62
620 I3=LPLF(12) ,63
    I4=I3+I5-1 ,64
    READ (LI,400)(8(I),I=I3,I4) ,65
    LE,TE POINTS START IN B(LPLF(11)),B(LPLF(21))
640 WRITE (LO,650)HLETE(1,I2),HLETE(2,I2),HGVEN,(8(I),I=I3,I4) ,66
    ,71
650 FORMAT( /10HOPLANFORM A6,A3,I3HEDGE POINTS ( A6,I2H ARE (X,Y) =/ ,77
    , (1H 3(2F10.4,4X)))
C
C READ AIRFOILS AND THEIR LOCATION ON PLANFORM.
C FIND INTERSECTION OF AIRFOILS WITH LE AND TE.
C SCALE AIRFOILS TO FIT ON PLANFORM
700 CALL WINGIA(8,8(LAFN),LPLF,NLTP,LOGUL,B(LLETE),LI,LO,
    ,TITLE,DAT,NU) ,78
    IF (NU)710,800,71C ,79
710 MU=7 ,80
    GO TO 9000
C
C WRITE PLANFORM DETERMINED BY AF INTERSECTIONS WITH LE, TE
800 LL=LLETE ,81
    WRITE (LO,320) DAT,TITLE ,82
    DO 810 I2=1,2 ,83
    L1=LL ,84
    L2=L1+4*NAF-4 ,85
    WRITE (LO,650)HLETE(1,I2),HLETE(2,I2),HUSED,
    , (8(I),8(I+1),I=L1,L2,4) ,86
    ,87
    ,88
    ,89
    ,90
    ,91
    ,92
    ,93
    ,94
810 LL=LL+2
C
C RELEASE STORAGE
    DO 910 I=1,2 ,95
    I3=LPLF(1) ,96
    IF (I)DELETE(8(I3))920,910,920 ,97
910 CONTINUE ,98
    GO TO 1000 ,99
920 MU=8 ,100
    GO TO 9000 ,101
    ,102
    ,103
C
C READ PERCENTS FOR WHICH PERCENT LINES ARE TO BE GENERATED.
C CHECK BETWEEN 0, 100. CONVERT TO PER-UNIT VALUES.
C STORE IN B(LPCT).
1000 LPCT=IRSERV(NPL,B,LPCT) ,104
    IF (LPCT)1010,1010,1050 ,105
1010 MU=9 ,106
    GO TO 9000 ,107
C
C READ CARD 5
1050 I3=LPCT+NPL-1 ,108
    READ (LI,400)(8(I),I=LPCT,I3) ,109
    WRITE (LO,1060)(8(I),I=LPCT,I3) ,110
1060 FORMAT(/56H0THE FOLLOWING PERCENT CHORD LINES ARE TO BE CONSTRUCTE ,111
    ,112
    ,113
    ,114
    ,115
    ,116
    ,117
    ,118
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WING1		09/14/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)	
C	.D/(1H 6F10.4))		
	DO 1200 I=LPCT,I3		,120
	P=B(I)		,121
	IF (P*(P-100.))1200,1200,1150		,122
1150	MU=10		,123
	GO TO 9000		,124
1200	CONTINUE		,125
	GO TO 9100		,126
C	ERROR		,127
C	9000 IERR=MERR(NU,NU+1,MU,WING)		,128
	NU=MU		,129
C	9100 RETURN		,130
	END		,131

```

SUBROUTINE WING1A(B,NAME,LPLF,NLTP,LOGUL,PT,LI,LO,TITLE,DAT,MU)
C
C   USED BY WING1 TO READ AIRFOILS AND SCALE THEM TO FIT ON PLANFORM
C   DIMENSION B(1),NAME(2,2,1),NLTP(3),PT(2,2,1),RUB(2,2),LQ(2),
C   YL(TE(2)),NAFUL(2),CLINE(3),MX(2),HUL(2),LPLF(2),
C   ,TITLE(12),DAT(2)
C   LOGICAL LOGUL(2)
C
C   THE POINTS FOR THE JTH AIRFOIL WILL BE STORED IN B(NAME(1,I,J))
C   WHERE I=1 FOR UPPER, I=2 FOR LOWER AIRFOIL.
C   THE CORRESPONDING NO. OF ELEMENTS (TWICE NO. OF POINTS) IS IN
C   NAME(2,I,J).
C   LE POINTS STORED IN B(LPLF(1)), TE IN B(LPLF(2)).
C   NLTP(1) = NO PTS IN LE, NLTP(2) = NO PT IN TE.
C   NLTP(3) = NO AIRFOILS.
C   LOGUL(1) = .TRUE. IF UPPER AIRFOIL DEFINED.
C   LOGUL(2) = .TRUE. IF LOWER AIRFOIL DEFINED.
C
C   DATA HUL(1)/12H UPPER LOWER/
C
C   MU=0
C   NAF=NLTP(3)
C   CLEAR NAME ARRAY
C   DO 100 I=1,NAF
C   DO 100 J=1,2
C   DO 100 K=1,2
C   NAME(K,J,I)=0
C
C   DO 8000 IA=1,NAF
C
C   WRITE(LO,110) DAT,TITLE
C   FORMAT(16H WING DEFINITION 38X 2A6/1H0 12A6//)
C   READ (LI,200)AFK,BETA,YL,TE,AFNU,AFNL
C   FORMAT(6F10.0)
C   WRITE (LO,210)IA,AFK,BETA,YL,TE,AFNU,AFNL
C   210 FORMAT( /12H0AIRFOIL NO. 13/6H AFK = F4.0,12H, AFANG = F9.4,
C   X9H, YL = F10.4,9H, YT = F10.4/7H AFNU = F3.0,12H, AFNL =
C   X F3.0)
C   NAFUL(1)=AFNU
C   NAFUL(2)=AFNL
C   IC=AFK
C   IF (IC*(IC-4))320,310,310
C   MU=5
C   GO TO 9000
C
C   FIND LE AND TE X VALUES CORRESPONDING TO YL,TE.
C   (ONLY 1 NEEDED IF IC=1 OR 2)
C   320 CLINE(1)=0.
C   CLINE(2)=-1.
C   DO 350 I=1,2
C   CLINE(3)=YL(TE(I))
C   ID=LPLF(1)
C   350 CALL POLYN(CLINE,B(ID),2,NLTP(1),1.E-4,1,RUB(1,I),LQ,MX(1))

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C
400 IF (IC-2)400,400,500
    BETA=BETA* .01745329252
    SN=SIN(BETA)
    LC=COS(BETA)
    CLINE(1)=SN
    CLINE(2)=CS
    IF (MX(1C))420,420,430
    MU=6
    GO TO 9000
430 CLINE(3)=-SN*RUB(1,IC)-CS*RUB(2,IC)
    GO TO 700
C
500 DO 530 I=1,2
    IF (MX(1))520,520,530
    MU=7
    GO TO 9000
530 CONTINUE
C
    CLINE(1)=RUB(2,1)-RUB(2,2)
    CLINE(2)=RUB(1,2)-RUB
    CLINE(3)=RUB*RUB(2,2)-RUB(2,1)*RUB(1,2)
    IF (CLINE(1) .NE. 0. .OR. CLINE(2) .NE. 0.) GO TO 700
C
    AIRFOIL IS A POINT
    DO 610 J=1,2
    DO 610 I=1,2
    PT(I,J,IA)=RUB(I,1)
    CHDL=0.
    GO TO 820
C
    CLINE CONTAINS COEFF. OF LINE (IN XY PLANE) WHICH
    IS THE TRACE OF THE AIRFOIL.
    FIND INTERSECTION WITH LE,TE AND CHORD LENGTH.
    DO 800 I=1,2
    ID=LPLF(I)
    CALL POLYN(CLINE,B(ID),2,NLTP(I),I-E-4,1,PT(I,I,IA),LQ,MX(I))
    IF (MX(I)-1) 750,800,750
    MU=8
    GO TO 9000
    CONTINUE
C
    CHDL=DISPTA(PT(1,1,IA),PT(1,2,IA),2)
C
820 WRITE (LD,850)((PT(I,J,IA),I=1,2),J=1,2),CHDL
850 FORMAT(43H LEADING AND TRAILING EDGE POINTS (X,Y) ARE/
    .2(10X,2F10.4)/15H CHORD LENGTH =F10.4)
C
    READY TO READ, SCALE, AND STORE AIRFOILS
    DO 2000 IB=1,2
C
1000 IF (.NOT. LOGUL(IB)) GO TO 2000
    N=NAFUL(IB)
    IF (N)1040,1040,1100

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07/31/65

WINGIA	EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
	1040 IF (IA-1)1060,1060,1080		,87
	1060 MU=9		,88
	GO TO 9000		,89
	1080 NB=NAME(2,IB,IA-1)		,90
	GO TO 1120		,91
	1100 NB=N+N		,92
C			
	1120 NAME(2,IB,IA)=NB		,93
C	RESERVE STORAGE FOR AIRFOIL POINTS		,94
	IF (IRSERV(NB,9,NAME(1,IB,IA)))1140,1140,1200		,95
	1140 MU=10		
	GO TO 9000		,96
C			,97
	1200 LA=NAME(1,IB,IA)		,98
	LB=NAME(1,IB,IA-1)		
	NA=N+N		,99
C			,100
	CALL WINGIB(11,10,HUL(1B),CHDL,NB,B(1B),NA,B(LA),IU)		,101
	1250 IF (IU)1280,2000,1260		,102
	1260 MU=11		
	GO TO 9000		,103
C	AIRFOIL IS A POINT		,104
	1280 NAME(2,IB,IA)=2		
	IF (CHDL)1300,2000,1300		,105
C	SET TE POINT TO LE PCINT		,106
	1300 ON 1310 I=1,2		
	1310 PT(1,2,IA)=PT(1,1,IA)		,107 ,108
C			
	2000 CONTINUE		,109 ,110
C			,111 ,112
	8000 CONTINUE		,113
	9000 RETURN		,114
	END		

```

SUBROUTINE WING13(LI,LC,UL,CHORD,NB,R,NA,A,NU)
  DIMENSION B(1),A(1)
  USED BY WING1A TO READ,WRITE,SCALE AIRFOILS

  C
  C
  IF (NA-1)400,400,200
  200 READ (LI,210)(A(I),I=1,NA)
  210 FORMAT(6F10.0)
  N=NA/2
  WRITE (LC,220)N,UL
  220 FORMAT(10H0THE GIVEN I4,A6,19H AIRFOIL POINTS ARE/
  ,5X 5HWRING 17X 5HWRING)
  WRITE (LC,230)(A(I),I=1,NA)
  230 FORMAT(1H F11.4,F22.4)
  GO TO 600

  C
  400 IF (N3-3)410,410,420
  410 NU=1
  GO TO 9000
  C
  USE PREVIOUS AIRFOIL
  420 NA=N3
  DO 430 I=1,NA
  430 A(I)=R(I)
  WRITE (LC,440) UL
  440 FORMAT(10H0THE GIVEN A6,37H AIRFOIL IS THE SAME AS PRECEDING ONE)

  C
  600 IF (NA-3)1000,1000,700
  C
  FIND CHORD LENGTH OF AIRFOIL
  700 CHDA=ABS(A(NA-1)-A)
  IF (CHDA)900,900,800
  900 IF (CHORD)900,900,1100
  900 NA=2
  C
  AIRFOIL IS A SINGLE POINT
  1000 NU=-1
  WRITE (LC,1010)
  1010 FORMAT(23H0THE AIRFOIL IS A POINT)
  GO TO 9000

  C
  1100 T=CHORD/CHDA
  C
  DO 1130 I=3,NA,2
  IF (A(I)-A(I-2))1110,1110,1130
  1110 WRITE (LC,1120)
  1120 FORMAT(//49H0POINTS NOT INCREASING IN X. JOB MAY BLOW LATER. 60X.
  1 7HWARNING///)
  GO TO 1200
  1130 CONTINUE

  C
  C
  SCALE A
  1200 DO 1210 I=1,NA
  1210 A(I)=T*A(I)
  NU=0

  C

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WINGIR		07/31/65	
EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	-	INTERNAL FORMULA NUMBER(S)
2000	WRITE (LO,2010)		
2010	FORMAT(52H0AIRFOIL POINTS AFTER SCALING TO FIT ON PLANFORM ARE/		
	,5X 14HXWING (SCALED) 10X 1H7)		
	WRITE (LO,2301)(A(I),I=1,NA)		
C	9000 RETURN		
	END		

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INTERNAL FORMULA NUMBER(S)

WING2
EXTERNAL FORMULA NUMBER SOURCE STATEMENT

SUBROUTINE WING2(B,LC,LGDEF,LOK,LCGUL,NAF,NPL,LAFN,KOD,PLT,
1 NAME,PCT,CHO,EP,ITITLE,DAYT,NU)
DIMENSION NAME(2,2,1),PLT(2,2,1),PCT(1),LOK(3,2),B(1),KOD(2),NU(3)
1,MPL(2),UL(2),ITITLE(12),DAYT(2)
LOGICAL LGDEF(3,6),LCGUL(2)
DATA UL(1)/12H UPPER LOWER/
DATA WING/5HWING2/

USED BY WINGA TO COMPUTE A 3D POINT ON EACH PERCENT LINE
AT EACH AIRFOIL AND THEN ENRICH EACH PERCENT LINE.

C	10	NAF=3*NAF*NPL	,1
C		NU=0	,2
C	50	DO 5000 KA=1,2	,3
C		IF (.NOT. LOGUL(KA)) GO TO 5000	,4
		LEFT=IPACK(B)	,5
C		RFSERVE SPACE FOR PERCENT LINE ARRAY	,6
		IF(IIRSERV(NAP,B,LOK(1,KA)))100,100,200	,7
		MU=1	,8
	100	GO TO 9000	,9
C		IA=LOK(1,KA)-3	,10
C	200	DO 4000 KB=1,NPL	,11
C	300	P=PCT(KB)/100.	,12
		Q=1.-P	,13
C	500	DO 3000 KD=1,NAF	,14
C		IA=IA+3	,15
		LAFP=NAME(1,KA,KD)	,16
		NAFP=NAME(2,KA,KD)/2	,17
		MAFP=LAFP+2*NAFP-2	,18
C		IF (NAFP-1)600,700,800	,19
C	600	MU=2	,20
		GO TO 9000	,21
C	700	B(IA)=PLT(1,1,KD)	,22
		B(IA+1)=PLT(2,1,KD)	,23
		B(IA+2)=B(LAFP+1)	,24
		GO TO 3000	,25
C	800	B(IA)=Q*PLT(1,1,KD)+P*PLT(1,2,KD)	,26
		B(IA+1)=Q*PLT(2,1,KD)+P*PLT(2,2,KD)	,27
		U=0*B(LAFP)+P*B(MAFP)	,28
		CALL BITURP(B(LAFP),B(LAFP+1),2,NAFP,KOD,U,B(IA+2),NU)	,29
		MU=3	,30
C			,31

WING2
08/19/65
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

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C      IF(NU)9000,3000,9000
C      3000 CONTINUE
C      4000 CONTINUE
C      LEFT=IPACK(B)
      KDEL=LCK(1,KA)
      IF(DELETE(B(KDEL)))4910,4920,4910
      4910 MU=5
      GO TO 9000
C      4920 IF(IRSERV(LEFT+NAP,B,LOK(1,KA)))4930,4930,4940
      4930 MU=6
      GO TO 9000
C      4940 IA=LCK(1,KA)
      CALL WING2P(LO,B(IA),NPL,NAF,TITLE,UL(KA),DAYT,PCT)
      CALL RICHNA(B(IA),LEFT/3,NPL,NAF,PCT,EP,CHD,KOD(2),IPL,NU)
      MPL(KA)=3*(IPL+NPL)
C      IF(NU)4550,4960,4950
      4950 MU=7
      GO TO 9000
      4960 KDEL=LCK(1,KA)
      IF(IRLEAS(B(KDEL),MPL(KA)))4970,4980,4970
      4970 MU=8
      GO TO 9000
      4980 LOK(2,KA)=NPL
      LOK(3,KA)=MPL(KA)
      LGDEF12,KA)=.TRUE.
C      5000 CONTINUE
C      RELEASE STORAGE IN B WHICH CONTAINS THE AIRFOIL POINTS AND NAMES
      DO 8100 JA=1,NAF
      DO 8100 JC=1,2
      JB=NAME(1,JC,JA)
      JD=DELETE(B(JB))
      JD=DELETE(B(LAFN))
      GO TO 9900
C      9000 I=MERR(NU,NU+1,MU,WING)
      NU=MU
      9900 RETURN
      END

```

WING2P
EXTERNAL FORMULA NUMBER - SOURCE STATEMENT - INTERNAL FORMULA NUMBER(S)

SUBROUTINE WING2P(LO,W,NPCT,NPT,TITLE,UPLO,DAYT,PCT)
DIMENSION W(3,NPT,NPCT),TITLE(12),DAYT(2),PCT(NPCT)

USED BY WING2 TO WRITE PERCENT LINES (BEFORE ENRICHING)
W = ARRAY OF NPCT PERCENT LINES. EACH LINE CONTAINS
NPT POINTS (X,Y,Z)
UPLO = 6H UPPER OR 6H LOWER
PCT = PERCENT VALUES ASSOC. WITH EACH PERCENT LINE

DATA LINPAG/45/

C LINREM=0

DO 2000 K=1,NPCT
NAF=0
NP=NPT

IF(LINREM .GT. 4) GO TO 200

100 WRITE(LO,110) TITLE,UPLO,DAYT
110 FORMAT(1H1 12A6/10H POINTS ON A6,
,33H WING SURFACE PERCENT CHORD LINES 5X 2A6)
LINREN=LINPAG-6

200 WRITE(LO,210) K,PCT(K)
210 FORMAT(/24H WING PERCENT CHORD LINE 13,1H, F9.4,8H PERCENT
,77H AF NO. 7X 1HX 10X 1HY 10X 1HZ)
N=MIN0(NP,LINREM)
LINREN=LINREN-N-4

DO 300 J=1,N
NAF=NAF+1

300 WRITE(LO,310)NAF,(W(I,NAF,K),I=1,3)

310 FORMAT(1H 13,4X 3F11.4)

C

NP=NP-N
IF(NP)2000,2000,100

2000 CONTINUE

9000 RETURN

END

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WLDN      - EFN      SOURCE STATEMENT - IFN(S) -

SUBROUTINE WLDN (NM,NROW,XP,ZP,RFAREA,AREA,XBAR,ZBAR,ALPHAM
1,THETAM,CPM,SCL,SCD,CL,CD,CM)

C      COMPUTES COEFFICIENT OF LIFT, DRAG, AND MOMENT ON WING
C      SPANWISE DISTRIBUTION OF LIFT AND DRAG COEFFICIENTS

      DIMENSION AREA(1),XBAR(1),ZBAR(1),ALPHAM(1),THETAM(1),CPM(1)
1,SCL(1),SCD(1)

      NCOL=NM/NROW
      WDRAG=0.
      WLIFT=0.
      WMOM=0.
      J=0

      DO 200 K=1,NCOL
      DRAG=0.
      XLIFT=0.

      DO 100 I=1,NROW
      J=J+1
      F=CPM(J)*AREA(J)
      XL=-F*COS(THETAM(J))
      XD=F*ALPHAM(J)
      WMOM=WMOM-XL*(XBAR(J)-XP)+XD*(ZBAR(J)-ZP)
      XLIFT=XLIFT+XL
      DRAG=DRAG+XD
100 CONTINUE

      SCD(K)=DRAG/RFAREA
      SCL(K)=XLIFT/RFAREA
      WDRAG=WDRAG+DRAG
      WLIFT=WLIFT+XLIFT
200 CONTINUE

      CL=WLIFT/RFAREA
      CD=WDRAG/RFAREA
      CM=WMOM/RFAREA

      RETURN
      END

```

6. REFERENCES

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